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## CORONA J

## PERFORMANCE EVALUATION REPORT

MISSION 1030-1 and 1030-2

FTV 1622, J-29

17 MAY 1967

Approved

Advanced Projects

Declassified and Released by the N R O

In Accordance with E. O. 12815

on NOV 26 1997

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## FOREWORD

This report details the performance of the payload system during the operational phase of the [REDACTED] Flight Test Vehicle 1622.

Lockheed Missiles and Space Company has the responsibility for evaluating payload performance under the Level of Effort and "J" System contracts.

This document is the final payload test and performance evaluation report for Missions 1030-1 and 1030-2 which was launched on 9 March 1966.

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## INTRODUCTION

This report presents the final performance evaluation of Missions 1030-1 and 1030-2 of the Corona Program. The purpose of this report is to define the performance characteristics of the J-29 payload system, to identify the source of in-flight anomalies.

The performance evaluation was jointly conducted by representatives of Lockheed Missiles and Space Company (LMSC) and ITEK at the facilities of NPIC and AFSPPF. The off-line evaluation using Corona engineering photography acquired over the United States was performed at the individual contractors plants.

The quantitative data used for this report is obtained from government organizations. The diffuse density data, and MTF/AIM resolution are produced by AFSPPF. The vehicle attitude error values, frame correlation times are made at NPIC who also supply the Processing Summary and MTF/AIM resolution reports published by [REDACTED]

[REDACTED]  
Computer programs developed by A/P are utilized to calculate and plot the frequency distribution of the various contributors to image smear to permit analysis and correlation of the conditions of photography to the information content and quality of the acquired pictures. Computer analysis of the exposure, processing and illumination data provides the necessary data to analyze the exposure criteria selected for the mission.

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## SECTION 1

### SYSTEM PERFORMANCE

#### A. MISSION OBJECTIVES

The payload section of Mission 1030, placed into orbit by Flight Test Vehicle #1622 and LV-2A booster #452, consisted of two panoramic cameras, two Stellar-Index cameras, two Mark 5A recovery capsules and a space structure to enclose the cameras and provide mounting surfaces for all equipments. Figure 1-1 presents an inboard profile of the J-29 payload system. This Corona "J" system is designed to acquire search and reconnaissance photography of selected areas of the earth from orbital altitudes. The planned mission was a 5 day Phase I and a 4 day Phase 2 with no deactivate.

#### B. MISSION DESCRIPTION

The payload was launched from Vandenberg Air Force Base (VAFB) at 2202:03 Z (1402:03 PST) on 9 March 1966. Ascent and injection were normal and the achieved orbit was within nominal tolerances. Tracking and command support was effected by the Air Force Satellite Control Facility consisting of tracking and command stations at [REDACTED]

[REDACTED] under central control of the Satellite Test Center at Sunnyvale, California. The actual mission consisted of 2 five day photo operations.

The comparison of the planned and actual orbit parameters is tabulated as follows:

#### ORBIT PARAMETERS

<u>Parameter</u>	<u>Orbit 1 Predicted</u>	<u>Orbit 42 Actuals</u>	<u>Orbit 120 Actuals</u>
Period (Min.)	90.7	90.6	90.5
Perigee (N. M.)	99.6	97.6	98.8
Apogee (N. M.)	235.5	234.6	230.0
Inclination (Deg.)	75.0	75.0	75.0
Perigee Latitude (Deg.N.)	19.2	24.25	37.5
Eccentricity	0.0188	0.01899	0.01821

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### C. PANORAMIC CAMERAS

The Master and Slave panoramic cameras operated throughout both missions with no significant problems. The cloud cover observed in the photography averaged 35% for the mission. The photographic quality was lower than the best missions due to atmospheric conditions.

### D. STELLAR-INDEX CAMERAS

Stellar-Index cameras operated satisfactorily during both missions. Photography was of acceptable quality.

### E. OTHER SUB-SYSTEMS

The clock, instrumentation and the PMU systems performance was satisfactory.

The command system performed satisfactorily except for the V/h delay stepper switch which occasionally failed to home in Position 1.

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SCHEMATIC INBOARD PROFILE - CORONA J SYSTEM

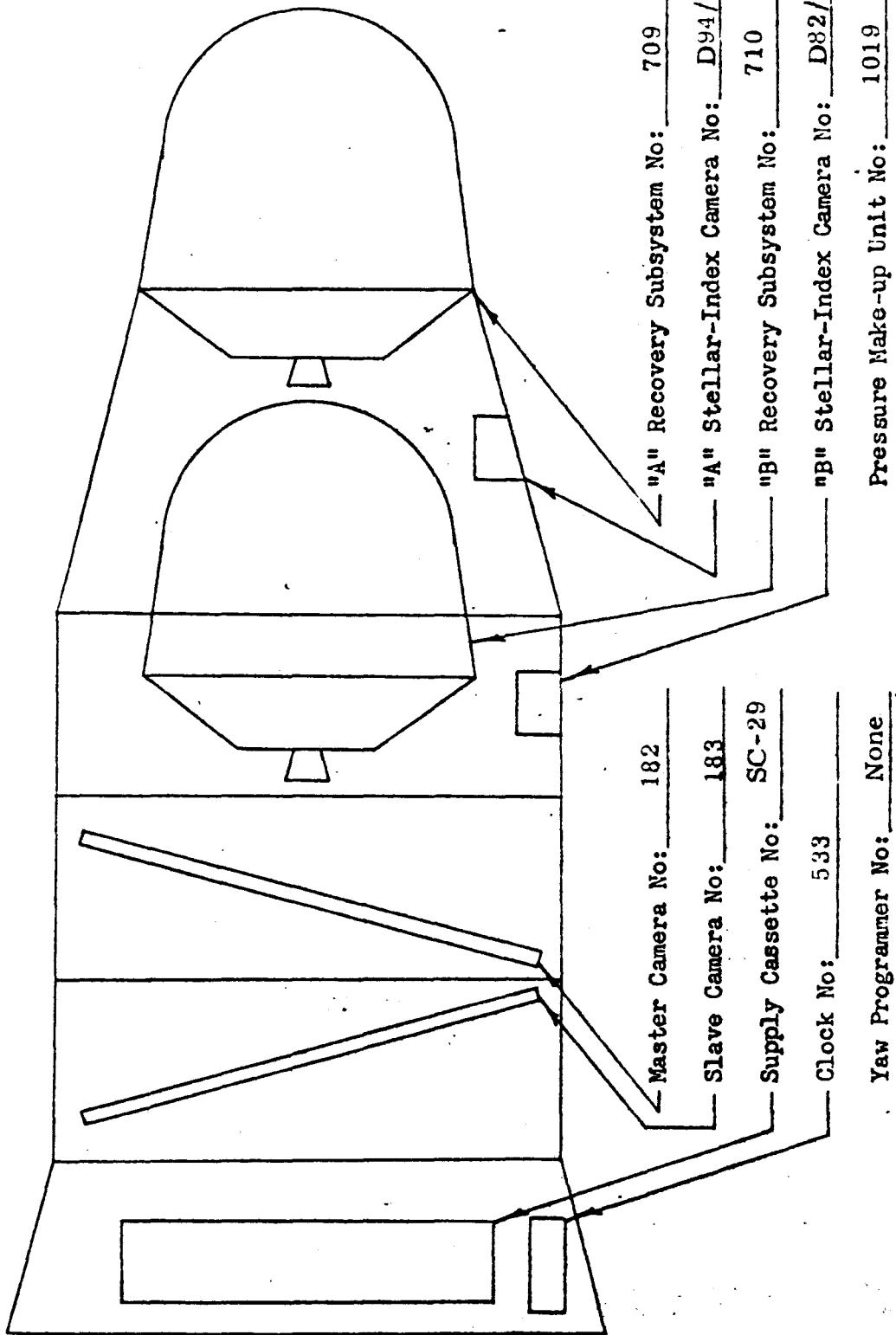


FIGURE 1-1

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SECTION 2

PRE-FLIGHT SYSTEMS TEST

A. ENVIRONMENTAL TESTING

1. Test Objective

As a standard procedure, the J payload systems are subjected to thermal/altitude environmental testing which simulates orbital environment. One of the purposes of this test is to demonstrate the system susceptibility to corona discharge. Such discharge fogs the film thus degrading the operational photography.

2. Test Summary

Performance of the J-29 payload system was generally satisfactory during the environmental test in the TASC Chamber. The test ran from 2-7 October 1965.

Both instruments ran fast throughout the test; the average cycle period was 1.5% fast for both instruments. The instruments ran within  $\pm$  1% of each other with instrument #2 being generally faster. Excessive coasting was observed for both units during some of the operations at the faster rates. In one instance both units coasted into the scan portion of the cycle. Cycle periods are listed in Table 2-1. Approximately 2800 cycles per instrument per mission were made.

The -1 S/I monitor indicated payload movement during several platen command times. The -2 S/I operated satisfactorily.

The clock performance was satisfactory. Results are listed in Table 2-2.

The pressure make-up system operated normally. The average gas consumption rate of 7.4 psi/min is consistent with previous PMU systems.

The lowest internal payload pressure was 0.8 microns. The corona on the payload was very minor.

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Except for several noisy TLM idlers, the instrumentation was normal.

The command system functioned properly for both missions. The RTC switch units stepped to the positions programmed in each case.

The -1 and -2 recovery sequences and vehicle deactivate sequence were satisfactorily performed.

#### B. RESOLUTION TEST

The dynamic resolution test of the J-29 payload system was performed at the A/P facility on 14 October 1965. Each panoramic camera photographed low contrast resolution targets. The resulting through focus resolution data is shown in Figure 2-1 for the Master camera and in Figure 2-2 for the Slave camera. The resolution performance meets the system requirement specifications.

#### C. LIGHT LEAK TEST

The examination of the 3401 Type film threaded in the J-29 system during the light leak test determined that the light tight integrity of the system was acceptable for flight.

#### D. FLIGHT LOADING AND CERTIFICATION

Pan instrument payload exhibits from the flight readiness test were processed and examined on 1 March 1966. Both instruments were acceptable except for excessive amounts of scraped emulsion which caused ragged rail edges and clogged shrinkage markers. On the master instrument, the scraped emulsion also obscured one fiducial mark and caused minus density streaks in the pan format from deposits on the filter. It was therefore necessary to clean both instruments and rerun the test. The second readiness test, also completed on 1 March 1966, showed the system to be in acceptable condition for flight loading.

Loading of the supply cassette and final assembly of the system was performed on 2 March 1966. These operations were completed in a routine manner.

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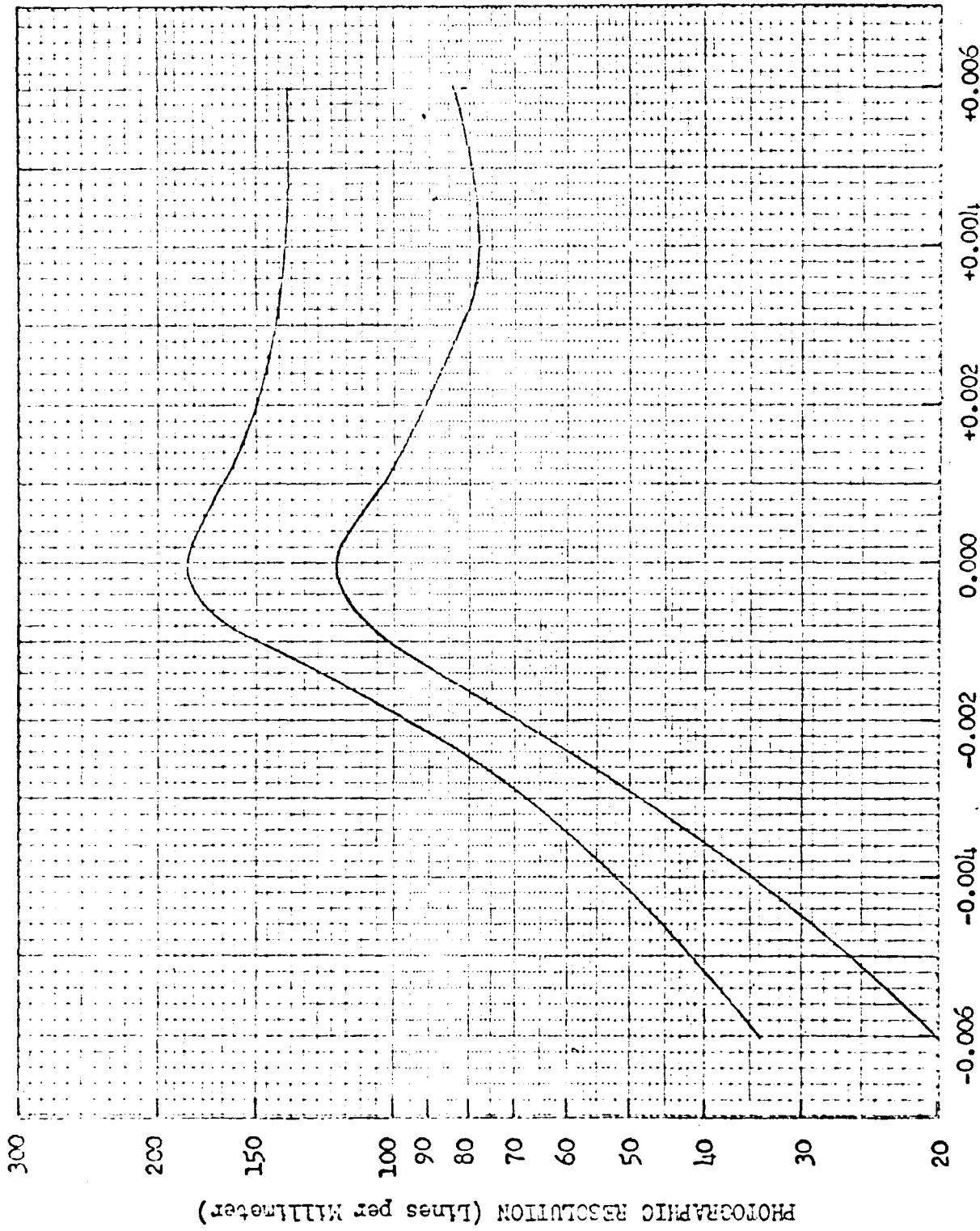
The final light leak check showed no leaks except for one at the take-up side of the master instrument drum. The magnitude of this leak was less than similar leaks on several recent flight systems.

The J-29 system performance was considered acceptable and was certified for flight.

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PRE-LAUNCH DYNAMIC RESOLUTION



THROUGH FOCUS INCREMENTS (Inches)

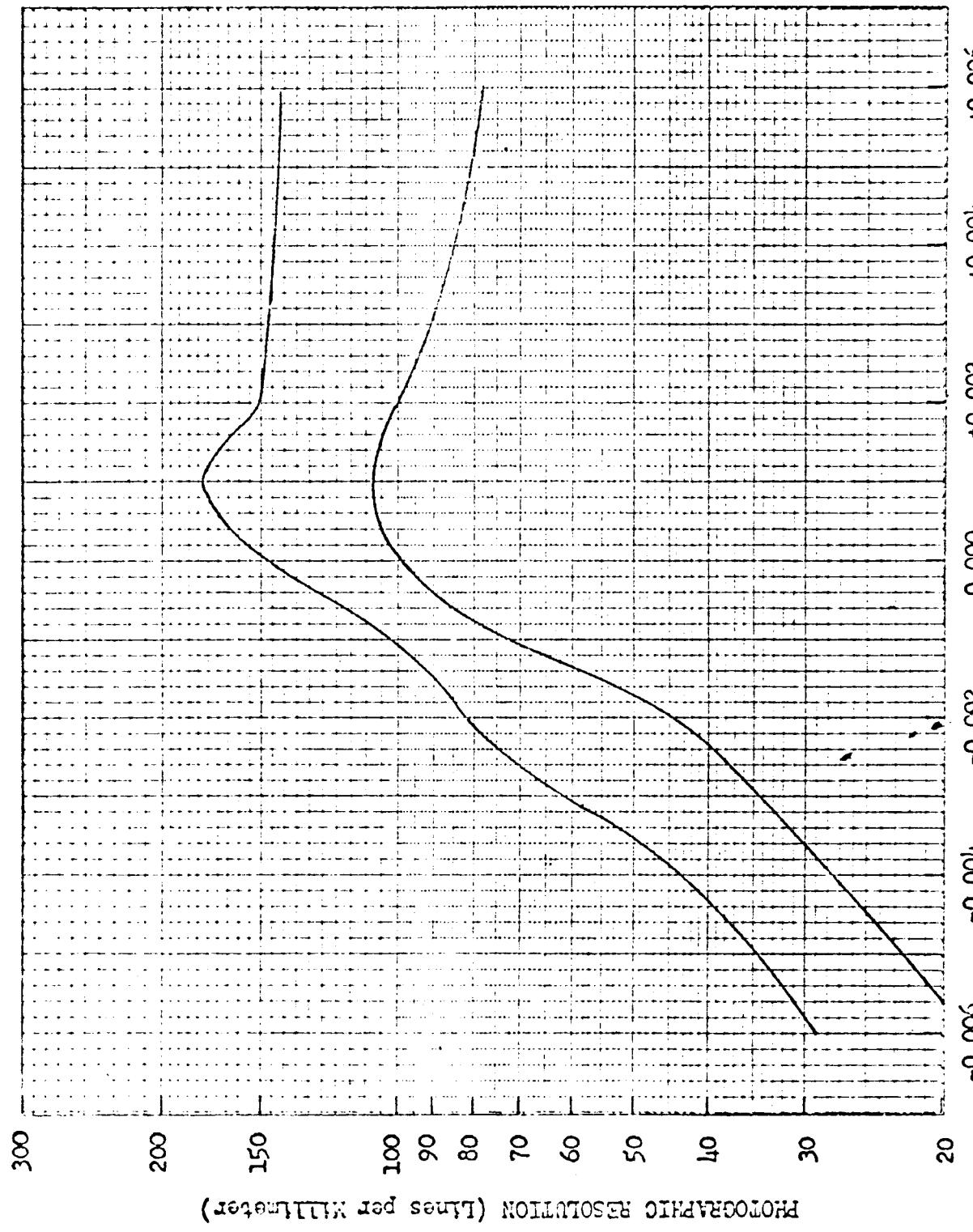
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Figure 2-1

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PRE-FLIGHT DYNAMIC RESOLUTION



THROUGH FOCUS INCREMENTS (Inches)

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Figure 2-2

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## J-29 182/183 ENVIRONMENTAL TEST

REV/MODE	RAMP	T.U.R.		INST 182 ACT. CAL. DEV.	INST 183 ACT. CAL. DEV.	182/183 DIFF.
0 A	7 7	0		3.655 3.649 0.16S	3.645 3.642 0.08S	-0.27
0 A	7 7	0		3.650 3.649 0.02S	3.650 3.642 0.21S	-0.00
1 A	7 7	390		3.500 3.513 0.37F	3.500 3.507 0.19F	-0.00
1 A	7 7	2215		2.550 2.555 0.20F	2.550 2.555 0.18F	-0.00
2 A	4 1	2030		2.155 2.187 1.45F	2.150 2.186 1.66F	-0.23
2 A	5 8	825		2.814 2.822 0.27F	2.820 2.819 0.02S	0.21
3 A	5 8	1645		2.390 2.408 0.73F	2.395 2.408 0.55F	0.21
4 A	7 7	2280		2.550 2.587 1.44F	2.555 2.587 1.23F	0.20
4 A	8 2	240		5.280 5.333 0.99F	5.270 5.320 0.94F	-0.19
5 A	11 1	1360		2.760 2.789 1.05F	2.760 2.787 0.98F	-0.00
5 A	11 1	1460		2.570 2.601 1.18F	2.565 2.600 1.34F	-0.19
6 A	11 1	1940		2.235 2.268 1.46F	2.230 2.270 1.75F	-0.22
6 A	5 8	1090		2.660 2.675 0.54F	2.665 2.673 0.31F	0.19
6 A	5 8	1445		2.455 2.476 0.86F	2.455 2.476 0.87F	-0.00
7 A	7 7	1180		2.820 2.847 0.95F	2.830 2.845 0.52F	0.35
7 A	7 7	1590		2.520 2.553 1.20F	2.520 2.552 1.27F	-0.00
8 A	7 7	2430		2.665 2.684 0.71F	2.655 2.683 1.04F	-0.38
8 A	4 1	1015		2.650 2.675 0.93F	2.640 2.674 1.26F	-0.38
9 A	4 1	3210		3.460 3.521 1.72F	3.465 3.514 1.41F	0.14

Table 2-1

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REV/MODE	RAMP	T.U.R.	INST 182			INST 183			182/183 DIFF.		
			ACT.	CAL.	DEV.	ACT.	CAL.	DEV.			
9	A	11	1	891	4.300	4.362	1.43F	4.315	4.352	0.85F	0.35
9	A	11	1	1880	2.233	2.266	1.46F	2.225	2.268	1.89F	-0.36
10	A	11	1	3140	5.404	5.546	2.55F	5.432	5.532	1.81F	0.52
10	A	7	7	40	3.580	3.647	1.83F	3.590	3.640	1.37F	0.28
11	A	7	7	1910	2.455	2.484	1.15F	2.445	2.484	1.56F	-0.41
11	A	7	7	2286	2.568	2.591	0.87F	2.568	2.590	0.85F	-0.00
12	A	8	2	1155	2.900	2.916	0.53F	2.895	2.913	0.61F	-0.17
12	A	8	2	845	3.620	3.648	0.76F	3.628	3.641	0.35F	0.22
13	A	4	1	2630	2.365	2.398	1.40F	2.358	2.399	1.72F	-0.30
13	A	11	1	1975	2.253	2.275	0.95F	2.243	2.276	1.46F	-0.44
14	A	11	1	3080	5.120	5.203	1.59F	5.138	5.190	1.00F	0.35
15	A	5	8	0	3.050	3.113	2.02F	3.060	3.109	1.57F	0.33
0	B	6	6	1945	2.270	2.275	0.21F	2.265	2.276	0.50F	-0.22
1	B	7	7	390	3.450	3.513	1.79F	3.455	3.507	1.48F	0.14
1	B	7	7	2450	2.670	2.699	1.08F	2.665	2.698	1.22F	-0.19
1	B	4	1	0	4.300	4.394	2.13F	4.300	4.383	1.90F	-0.00
2	B	4	1	1430	2.170	2.206	1.64F	2.150	2.206	2.53F	-0.92
2	B	4	1	1610	2.160	2.192	1.47F	2.140	2.192	2.36F	-0.93
2	B	4	1	2130	2.155	2.190	1.58F	2.140	2.189	2.24F	-0.70
2	B	5	8	730	2.843	2.873	1.06F	2.835	2.871	1.25F	-0.28
3	B	5	8	1550	2.403	2.436	1.34F	2.408	2.436	1.15F	0.21
3	B	5	8	0	3.068	3.113	1.44F	3.073	3.109	1.15F	0.16

Table 2-1

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REV/MODE	RAMP	T.U.R.	INST 182			INST 183			182/183	
			ACT.	CAL.	DEV.	ACT.	CAL.	DEV.	DIFF.	
4	8	7 7	2280	2.573	2.587	0.55F	2.573	2.587	0.53F	-0.00
4	8	8 2	440	4.768	4.822	1.12F	4.758	4.810	1.09F	-0.21
5	8	11 1	1460	2.590	2.601	0.41F	2.580	2.600	0.77F	-0.39
5	8	11 1	1940	2.260	2.268	0.36F	2.250	2.270	0.87F	-0.44
6	8	5 8	1090	2.675	2.675	0.02S	2.680	2.673	0.25S	0.19
6	8	5 8	1645	2.388	2.408	0.81F	2.388	2.408	0.84F	-0.00
7	8	7 7	1230	2.783	2.800	0.61F	2.783	2.798	0.54F	-0.00
7	8	7 7	1590	2.538	2.553	0.58F	2.548	2.552	0.17F	0.39
8	8	7 7	2430	2.675	2.684	0.34F	2.680	2.683	0.10F	0.19
8	8	4 1	1015	2.665	2.675	0.37F	2.670	2.674	0.14F	0.19
9	8	4 1	3310	3.755	3.737	0.48S	3.743	3.730	0.36S	-0.32
9	8	11 1	990	3.958	3.965	0.18F	3.973	3.957	0.41S	0.38
10	8	11 1	2080	2.325	2.318	0.29S	2.318	2.320	0.07F	-0.30
10	8	11 1	3170	5.730	5.726	0.07S	5.725	5.712	0.22S	-0.09
10	8	11 1	0	9.070	9.056	0.15S	9.060	9.049	0.12S	-0.11
10	8	7 7	0	3.650	3.649	0.02S	3.640	3.642	0.06F	-0.27

DEV. AND DIFF. ARE IN PERCENT

THE (-) SIGN INDICATES THAT INST 1 IS SLOWER THAN INST 2  
F=FAST AND S=SLOW

Table 2-1

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J=29. CLKCK/IKG TIME CHECK

IRIG REV_UAY-HR-MIN-SEC	IRIG SEGUNDOS	CLOCK SEGUNDOS	DELTA IRIG	DELTA CLOCK	ERROR
0 275 7 51 57.780	23788317.780	5276.306	---	---	---
1 275 8 30 33.785	23790633.785	7592.324	2316.005	2316.023	0.018
2 275 11 8 14.740	23800094.740	17053.284	9460.955	9460.955	0.000
3 275 12 44 9.880	23805849.880	22806.413	5755.140	5755.129	-0.011
4 275 14 15 0.210	23811300.210	28258.750	5450.330	5450.337	0.007
5 275 15 29 10.050	23815750.050	32708.592	4449.840	4449.842	0.002
6 276 8 1 46.120	23875306.120	92264.655	59556.070	59556.063	-0.007
7 276 9 27 36.475	23880456.475	97415.004	5150.355	5150.349	-0.006
8 276 11 0 6.350	23886006.350	102964.886	5549.875	5549.882	0.007
9 276 13 28 33.375	23894913.375	111871.919	8907.025	8907.033	0.008
10 276 15 11 4.140	23901064.140	118022.668	6150.765	6150.749	-0.016
11 277 8 13 45.220	23962425.220	179383.742	61361.080	61361.074	-0.006
12 277 9 31 15.323	23967075.323	184033.839	4650.103	4650.097	-0.006
13 277 10 57 5.345	23972225.345	189183.887	5150.022	5150.048	0.026
14 277 12 35 25.359	23978125.359	195083.872	5900.014	5899.985	-0.029
1 279 10 1 6.390	24141660.390	358624.881	163541.028	163541.006	-0.021
2 279 12 38 36.405	24151110.405	368074.906	9450.015	9450.025	0.010
3 279 14 14 31.545	24156871.545	373830.039	5755.140	5755.133	-0.007
4 279 15 45 21.425	24162321.425	379279.913	5449.880	5449.874	-0.006
5 279 16 59 31.632	24166771.632	383730.126	4450.207	4450.213	0.006

4 9 7 33.851-DELTA TIME

TOTAL ACCUM. ERROR -0.031

## **POWER DOWN**

6	280	8	59	52.960	24224392.960	9464.737	---	---	---
7	280	10	42	23.355	24230543.355	15615.131	6150.395	6150.394	-0.001
8	280	12	59	2.145	24238742.145	23813.924	8198.790	8198.793	0.003
9	280	14	33	12.260	24244392.260	29464.039	5650.115	5650.115	0.000
10	280	16	15	42.775	24250542.775	35614.551	6150.515	6150.512	-0.003

9 7 15 49.815=DELTA TIME

TOTAL ACCUM. ERROR = 0.001

Table 2-2

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### SECTION 3

#### FLIGHT OPERATIONS

##### A. SUMMARY

All launch, ascent, and injection events occurred as programmed. All Thor and Agena events were normal which resulted in achieving the desired orbit.

Both panoramic instruments operated satisfactorily throughout the flight. Average cycle rates on both units deviated from the pre-flight calibrated values by less than 1.0%.

The -1 and -2 Stellar/Index cameras operated normally throughout the flight.

The clock, instrumentation, and the PMU systems functioned properly throughout the flight.

The command system performed satisfactorily except for the V/h delay stepper switch which failed to home in position one on numerous occasions throughout the flight.

Both the -1 and -2 recovery systems were successfully recovered by air catch on orbits 81 and 159, respectively.

##### B. PANORAMIC CAMERA PERFORMANCE

Camera system dynamics were normal throughout the -1 and -2 missions. The film transport of both camera systems was normal. Cycle rate data (Table 3-1) indicates that the camera systems were generally less than 0.75% from the calibrated systems value. The master and slave instruments were generally less than 1.0% apart throughout most of the flight. The 99/101 average clutch ratio was 6/6 for both instruments. Camera film depletion occurred prior to the engineering operation on Rev. 151.

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Panoramic film consumption

These data are bascd on cycle counter readings and nominal film supply.

	<u>Predicted</u>		<u>Actual</u>	
	<u>Master</u>	<u>Slave</u>	<u>Master</u>	<u>Slave</u>
Pre-Launch	110	110	102	110
-1 Mission	3000	3000	2956	2945
-2 Mission	2935	2935	2991	2995
Total Frames	6045	6045	6049	6050

FMC Match

The RTC command setup (R8-A3-D7) provided a good match between the calibrated rates and the orbit rate requirements throughout the mission. Normal operations occurred well within acceptable tolerance, especially during -1 phase of the mission. However, the malfunctioning of the V/h delay start selector switch caused occasional FMC errors as high as 20%. An error of this magnitude could produce noticeable smear on the photography.

The V/h programmer usually started at the desired delay step or one step later. Therefore, the RTC command setup was changed (R7-A3-D6) to insure the most favorable ramp match. However, when the V/h delay failed to start in either of these positions, excessive FMC errors were produced.

C. INSTRUMENTATION AND COMMAND SYSTEM PERFORMANCE

Instrumentation System Performance

The instrumentation system performed satisfactorily throughout both missions except for points 1 (cal 1/2) and 2 (RTC 6 tens position) on channel 13. These two points on the commutator indicated the same voltage value beginning on Rev 87 of the -2 mission. This condition was present until sometime between the engineering passes on Rev 103 and

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110. Both these points indicated the proper voltage levels on the engineering pass on Rev 110 and throughout the remainder of the mission. The cause of this anomaly remains unresolved.

#### Command System Performance

The payload system responded to all stored and real time commands except for the erratic homing of the V/h delay stepper switch. This anomaly was first encountered on the "Post-Mate Confidence" prior to launch. A special confidence re-run was conducted to insure satisfactory performance of the V/h delay stepper switch. The V/h delay stepper switch was given a homing command five different times. The stepper switch failed to home properly on the first two attempts stopping in position 11. On these two attempts the unregulated voltage was set at 28 volts and 26 volts respectively. The unregulated voltage was then set at 24 volts and the V/h delay stepper switch homed properly to position 1 on the next three attempts.

The vehicle unregulated voltage was predicted to drop to approximately 24 volts after the second day of the mission. It was, therefore, decided to proceed with the launch and if necessary, adjust the ramp, amplitude, and V/h delay start position to compensate for erratic homing.

Refer to Table 3-2 for the orbits in which the V/h delay switch failed to home in the proper position.

The problem of the erratic homing of the V/h stepper switch has been attributed to the installation of two spark suppression diodes in this circuit. A decision was, therefore, made to remove these two diodes from all subsequent systems.

#### D. CLOCK SYSTEM PERFORMANCE

The payload clock system performed satisfactorily during both phases of the mission. The clock/system time correlation data obtained from the acquisitions are included in Table 3-3.

#### E. PRESSURE MAKE-UP SYSTEM PERFORMANCE

The pressure make-up system operated normally throughout the flight. The average gas consumption was 7.7 psi/min. for a total instrument operate time of 249 minutes. The supply pressure dropped from 2350 psig at launch to 420 psig at the end of the -2 mission.

The average gas consumption rate was 7.5 psi/min. for the -1 mission and 8.0 psi/min. for the -2 mission.

#### F. THERMAL ENVIRONMENT

The temperature data obtained from the [REDACTED] acquisitions are contained in Table 3-4. Average panoramic camera temperatures for the master camera varied from 39°F to 72°F and the slave camera temperatures varied from 83°F to 64°F during the mission. The actual system temperatures versus the predicted system temperatures for the major components are compared in Figures 3-1 to 3-3.

#### G. STELLAR/INDEX CAMERA PERFORMANCE

The -1 stellar/index camera operation was normal throughout the mission with telemetry indicating proper metering and shutter operation.

The -2 stellar/index camera operation was also normal throughout the mission with no abnormalities noted in telemetry.

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NO.

J-29 182/183 FLIGHT CYCLE RATES

				INST. 182-----		INST. 183-----						
REV.	CP	RAMP	TUR	SYSTEM	ACTUAL	UNIT	SYSTEM	ACTUAL	UNIT	SYSTEM	182/183	
PULSE		R	A	SECS	CALIB.		LEV.	DEV.		DEV.	DEV.	DIFF.
09	A	8	3	120	5.132	5.055	1.62F	1.50F	5.045	1.58F	1.70F	-0.20
16	A	8	3	1685	2.263	2.280	0.79S	0.75S	2.260	0.17F	0.14F	-0.88
31	A	7	3	1864	2.216	2.215	0.04F	0.03F	2.220	0.21S	0.20S	0.23
47	A	7	3	1642	2.224	2.242	0.80S	0.81S	2.223	0.04F	0.05F	-0.85
63	A	7	3	1700	2.221	2.228	0.32S	0.33S	2.232	0.53S	0.51S	0.18
79	A	7	3	1660	2.223	2.230	0.31S	0.32S				
88	S	7	3	249	4.609	4.603	0.21F	0.09F	4.590	0.24F	0.41F	-0.33
94	S	7	3	1823	2.216	2.251	1.56S	1.57S	2.231	0.68S	0.66S	-0.89
103	S	7	3	340	4.459	4.553	1.99S	2.11S	4.574	2.70S	2.58S	0.40
110	S	7	3	1903	2.216	2.232	0.73S	0.74S	2.217	0.08S	0.07S	-0.67
126	S	7	3	1911	2.216	2.233	0.78S	0.79S	2.224	0.39S	0.38S	-0.40

DEV. AND DIFF. ARE IN PERCENT

THE (-) SIGN INDICATES THAT INST 1. IS SLOWER THAN INST 2

F=FAST AND S=SLOW

Table 3-1

~~TOP SECRET C~~

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NO.

ARMORAL V/H DELAY HOME POSITION

<u>Rev.</u>	<u>Station</u>	<u>Stepper Switch Home Position</u>	<u>V/H Start Position Error</u>
29		11	60 Seconds Late
42		11	60 Seconds Late
44		11	60 Seconds Late
71		11	60 Seconds Late
74		11	60 Seconds Late
80		11	60 Seconds Late
87		11	60 Seconds Late
89		11	60 Seconds Late
91		11	60 Seconds Late
95		11	60 Seconds Late
101		11	60 Seconds Late
104		11	60 Seconds Late
106		11	60 Seconds Late
108		8	240 Seconds Late
111		10	120 Seconds Late
115		7	300 Seconds Late
117		6	300 Seconds Early
119		11	60 Seconds Late
121		7	300 Seconds Late
123		11	60 Seconds Late
126		11	60 Seconds Late
131		11	60 Seconds Late
133		11	60 Seconds Late
135		11	60 Seconds Late
136		7	300 Seconds Late
139		11	60 Seconds Late
142		4	180 Seconds Early
150		11	60 Seconds Late
152		4	180 Seconds Early
153		11	60 Seconds Late
155		7	300 Seconds Late
158		11	60 Seconds Late
159		11	60 Seconds Late

Table 3-2

~~TOP SECRET C~~

~~TOP SECRET~~ C [REDACTED]

NO.

ORDER FIT 1

SYN TIME 1/T	CC TIME 1/T	COMP SYS TM	DELTA ST	REV	STA
0.400201430 05	0.1428123100 05	0.4002614430 05	-0.0018	9	[REDACTED]
0.400201430 05	0.1428494020 05	0.40026284160 05	0.0016	16	[REDACTED]
0.400201430 05	0.2243690510 05	0.3577286120 05	-0.0012	24	[REDACTED]
0.704062100 05	0.2040344750 05	0.7544424560 05	-0.0038	31	[REDACTED]
0.364021700 05	0.3113664640 05	0.3663217260 05	0.0034	40	[REDACTED]
0.701117300 05	0.3560979830 05	0.7601173750 05	-0.0023	47	[REDACTED]
0.371038500 05	0.3483699820 05	0.3760595610 05	-0.0001	56	[REDACTED]
0.704062100 05	0.4370856320 05	0.7659456470 05	-0.0047	63	[REDACTED]
0.474364600 05	0.4853167770 05	0.3753048250 05	0.0035	72	[REDACTED]
0.771766600 05	0.5245622510 05	0.7717666110 05	0.0089	79	[REDACTED]
0.361199710 05	0.3593535740 05	0.3811997290 05	-0.0019	88	[REDACTED]
0.721761200 05	0.6949154560 05	0.7217611660 05	0.0044	94	[REDACTED]
0.431366040 05	0.1108841050 05	0.3313366140 05	0.0026	103	[REDACTED]
0.720760300 05	0.1560403910 05	0.7268844300 05	-0.0040	110	[REDACTED]
0.350222030 05	0.2037336370 05	0.3362289390 05	0.0041	119	[REDACTED]
0.7315524350 05	0.24327360930 05	0.7315524350 05	-0.0105	126	[REDACTED]
0.360760770 05	0.2905914660 05	0.3487597330 05	0.0037	135	[REDACTED]
0.345007700 05	0.3774163160 05	0.3450077760 05	-0.0018	151	[REDACTED]

A0E=0.1021611643 06 A1E=0.9999996370750 00

SIGMA=0.00424 NO. POINTS= 1e

RATIO OF CLOCK TIME TO SYS TIME= 0.1000000302930 01

ORDER FIT 2

SYN TIME 1/T	CC TIME 1/T	COMP SYS TM	DELTA ST	REV	STA
0.400201430 05	0.1428123100 05	0.4002614300 05	0.0000	9	[REDACTED]
0.400201430 05	0.1424494020 05	0.40026284020 05	0.0028	16	[REDACTED]
0.400201430 05	0.2243690510 05	0.3577286050 05	-0.0005	24	[REDACTED]
0.704062100 05	0.2040344750 05	0.7544424560 05	-0.0036	31	[REDACTED]
0.364021700 05	0.3113664640 05	0.3663217260 05	0.0031	40	[REDACTED]
0.701117300 05	0.3560979830 05	0.7601173750 05	-0.0028	47	[REDACTED]
0.371038500 05	0.3483699820 05	0.3760595610 05	-0.0009	56	[REDACTED]
0.704062100 05	0.4370856320 05	0.7659456560 05	-0.0056	63	[REDACTED]
0.474364600 05	0.4853167770 05	0.3753048360 05	0.0024	72	[REDACTED]
0.771766600 05	0.5245622510 05	0.7717666020 05	0.0078	79	[REDACTED]
0.361199710 05	0.3543536700 05	0.3811997400 05	-0.0030	88	[REDACTED]
0.721761200 05	0.6949154560 05	0.7217611950 05	0.0035	94	[REDACTED]
0.431366040 05	0.1108841050 05	0.3313366210 05	0.0019	103	[REDACTED]
0.720760300 05	0.1560403910 05	0.7268844340 05	-0.0044	110	[REDACTED]
0.350222030 05	0.2037336370 05	0.3362289390 05	0.0041	119	[REDACTED]
0.7315524350 05	0.24327360930 05	0.7315526310 05	-0.0101	126	[REDACTED]
0.360760770 05	0.2905914660 05	0.3487597230 05	0.0047	135	[REDACTED]
0.345007700 05	0.3774163160 05	0.3450077560 05	0.0005	151	[REDACTED]

A0E=0.1021611220 06 A1E=0.9999996567620 00

A2E=0.21095698357500-13

SIGMA=0.00413 NO. POINTS= 1e

Table 3-3

~~TOP SECRET~~ C [REDACTED]

~~TOP SECRET~~

NO.

TABLE 3-4

J-29 TEMPERATURE SUMMARY

SENSE

ORBITS ACQUIRED

Master Camera	<u>A</u>   <u>B</u>																		
	0	2	16	24	31	40	47	56	63	72	79	88	94	103	110C	119	126	135	151
3	60	61	79	82	80	80	78	80	76	78	73	74	68	70	65	69	65	69	70
4	58	84	81	84	81	83	79	82	77	80	73	76	69	72	67	71	66	70	70
5	58	90	86	89	86	87	84	87	82	84	80	80	75	77	73	75	70	74	73
6	57	90+	93	95	92	93	89	91	87	89	84	84	78	79	77	75	73	74	74
7	54	90	87	89	88	87	85	86	83	84	81	79	75	75	73	73	70	71	71
8	61	90	87	90	86	88	84	88	82	86	80	81	75	78	74	77	71	75	75
9	59	90	92	96	92	93	88	92	86	90	84	85	79	82	76	80	73	78	78
10	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--
11	65	94	93	95	93	93	89	90	85	88	83	80	74	78	72	75	70	71	70
12	62	82	79	82	80	81	77	81	75	80	73	76	68	73	66	72	65	70	72
13	54	90	87	89	86	85	84	85	81	83	79	76	70	72	66	69	68	68	68
AVG	59	89	86	89	87	87	84	86	81	84	78	78	73	76	72	74	69	72	72

Slave  
Camera

3	57	89	87	88	87	87	84	85	81	82	77	77	71	72	69	70	65	67	66
4	54	83	78	83	79	81	77	81	76	78	72	74	67	70	65	68	62	65	64
5	52	83	80	84	81	82	79	82	77	79	74	75	70	71	68	66	64	68	67
6	56	83	81	83	82	82	80	81	79	80	76	75	70	71	69	69	66	69	70
7	52	85	82	85	83	83	81	81	80	81	78	76	69	72	69	70	67	68	68
8	55	85	82	84	82	83	80	83	79	82	76	78	71	74	69	72	67	71	71
9	56	82	79	81	80	80	78	80	77	80	75	76	69	72	68	71	66	70	71
10	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--
11	58	72	70	71	72	70	69	71	68	69	66	65	62	61	60	60	56	58	59
12	56	86	80	86	81	85	78	82	76	79	73	76	68	73	66	69	63	66	66
13	53	80	80	81	82	79	78	79	76	77	74	71	67	67	64	65	64	64	64
AVG	57	83	80	83	82	81	78	80	77	79	74	74	68	70	67	68	64	66	67

Supply  
Spec

1	55	64	65	67	67	67	69	67	63	64	64	60	58	59	56	57	58	
2	59	73	71	76	74	75	72	76	71	74	69	69	63	65	63	59	62	61

Note: All data corrected for self-heating, except injection.

~~TOP SECRET~~

TABLE 3-4

J-29 TEMPERATURE SUMMARY

SENSOR													OBSERVATIONS ACQUIRED												
													A	B											
Fair ("A")																									
Barrel #1 ("B")	Q	2	16	24	31	40	47	56	63	72	79	86	94	103	110	119	126	135	151						
1	ORH	36	49	39	49	29	42	33	42	26	39	18	34	18	34	15	28	15	15						
2	OBH	3	-4	7	-4	3	-4	3	-4	3	-8	55	45	55	51	55	48	55	58						
3	ORH	-7	-4	-7	4	-11	0	-11	4	-11	-4	71	109	67	106	71	106	67	67						
4	208	54	51	54	54	45	48	48	48	41	38	41	80	38	71	35	61	28	28						
5	227	64	60	64	67	54	64	57	54	47	41	39	52	35	48	32	42	25	25						
6	OBH	60	93	63	90	50	79	53	69	44	60	--	--	--	--	--	--	--	--						
Barrel No. 2																									
1	125	52	77	52	68	39	63	45	58	35	45	32	42	29	35	22	29	22	19						
2	0127	59	103	50	97	40	91	44	85	37	76	37	73	34	66	30	53	27	24						
3	206	64	103	67	106	61	103	64	103	61	103	64	100	64	103	64	97	61	61						
4	227	51	44	54	48	43	48	51	48	51	44	51	44	51	48	51	48	51	57						
5	200	49	59	56	62	49	62	52	62	46	52	39	46	36	46	36	42	32	36						
Conic Adaption																									
1	137	55	68	55	65	49	58	43	52	39	42	33	33	29	26	26	19	19	19						
Clock																									
1	79	69	67	73	69	67	67	69	67	65	61	59	53	57	53	55	51	53	53						
2	83	71	69	73	71	69	67	69	67	67	61	61	55	57	53	57	53	53	53						
Thrust Cone "A" to "B" SRV																									
1	70	46	41	45	41	42	40	42	38	40	35	63	59	60	58	58	57	58	58						
2	64	70	63	66	60	63	58	60	56	58	51	72	67	69	65	65	63	64	64						
Stellar Index "A" & "B"																									
1	--	--	--	--	--	--	--	--	--	--	--	43	78	39	72	36	62	33	26						
2	--	--	--	--	--	--	--	--	--	--	--	34	47	31	41	28	34	21	21						
Recovery Battery "B" SRV																									
1	61	70	72	72	75	66	72	70	70	67	66	79	83	86	81	87	86	86	86						
Master Cassette "A" SRV																									
2	92	70	67	69	68	71	67	68	67	65	65	--	--	--	--	--	--	--	--						

TOP SECRET C  
NO.

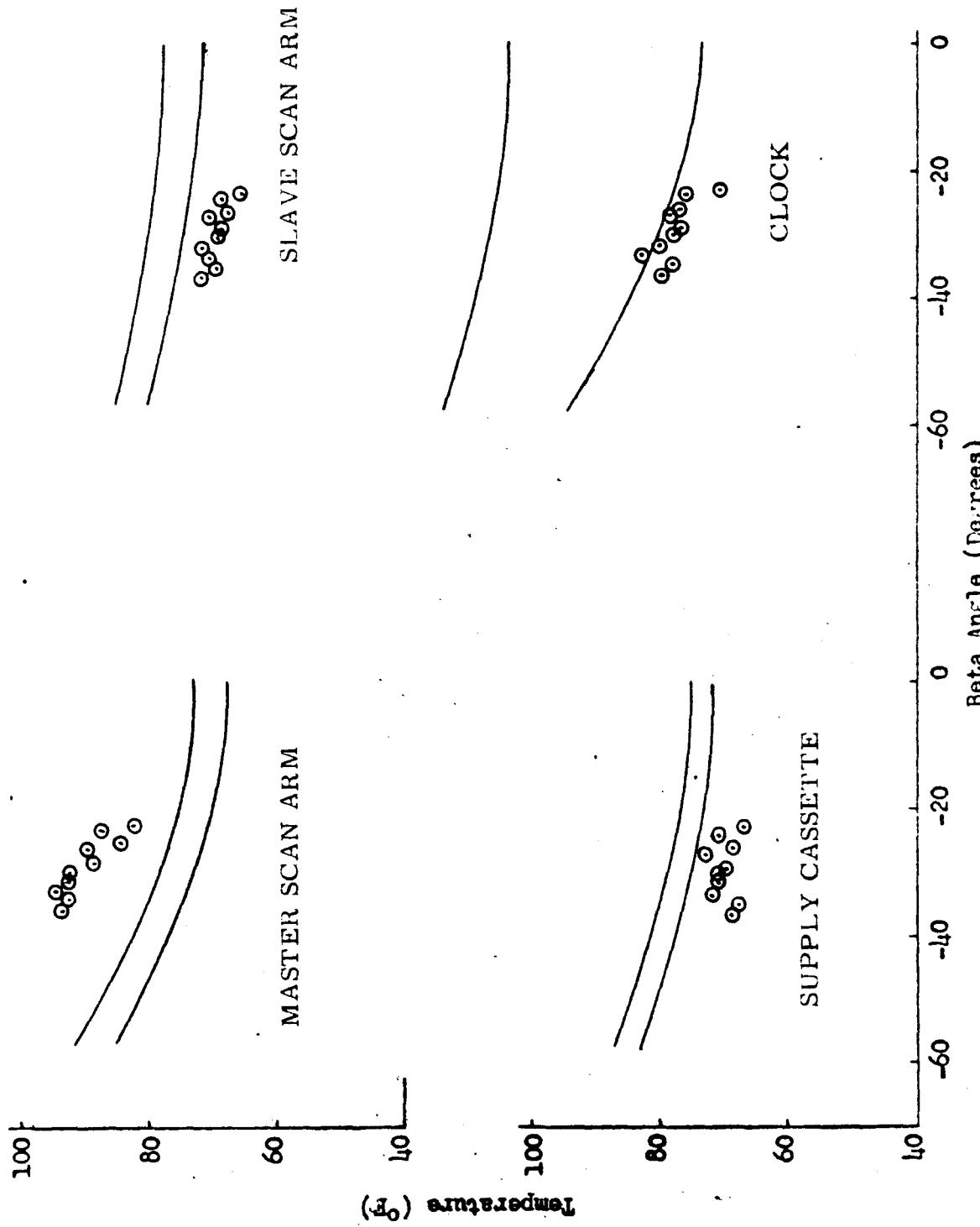


Figure 3-1

Top Graph  
Beta Angle (Degrees)

S/I - 2

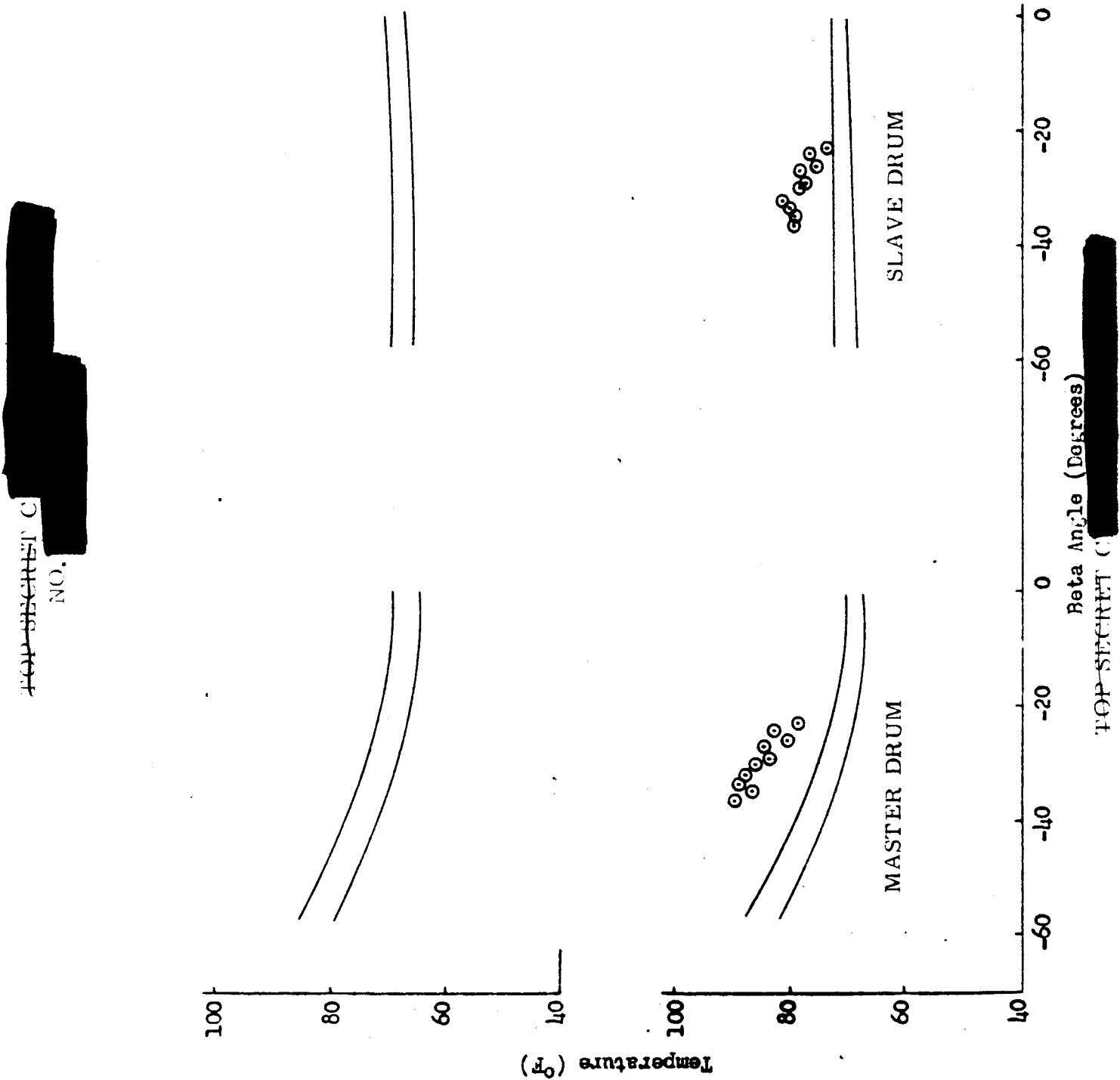
S/I - 1

S/I - 2

Temperature ( $^{\circ}$ F)

24

Figure 3-3



~~TOP SECRET C~~

NO.

#### SECTION 4

##### MISSION 1030-1 RECOVERY SYSTEM

SRV #709 was received at A/P on 16 July 1965. The receiving weight was 149.5 pounds. After modification and incorporation of outstanding E.O.'s, the SRV was delivered to Systems Test for mating to the J-29 system. The capsule was delivered to VAFB on 24 January 1966.

###### -1 Mission

The -1 recovery system was successfully recovered by air catch on orbit 31, March 14, 1966.

###### Impact Point

###### Predicted

$23^{\circ} 33' N$      $168^{\circ} 55' W$

###### Actual

$23^{\circ} 26' N$      $168^{\circ} 37' W$

The sequence of re-entry events is contained in Table 4-1.

~~TOP SECRET C~~

~~TOP SECRET C~~

NO.

## MISSION 1030-1

## RECOVERY SEQUENCE OF EVENTS

<u>Event</u>		<u>Delta Time (Seconds)</u>	
	<u>Actual</u>	<u>Nominal</u>	<u>Events +</u> $\Delta T$
*Arm	76.73	77	$\pm 1.0$
*Transfer	2.0	2.0	$\pm 0.25$
Electrical Disconnect	0.86	0.900	$+ 0.430$ $- 0.400$
**Spin	3.42	3.4	$\pm 0.30$
Retro	7.52	7.55	$\pm 0.45$
Despin	10.55	10.75	$\pm 0.59$
T/C Separation	1.51	1.5	$\pm 0.15$
***"G" Switch Open	486.39	491.8 to 502.6	
Parachute Cover Off	33.98	34.0	$\pm 1.5$
Drogue Chute Deployed	0.66	0.63	$\pm 0.08$
Main Chute Bag Separate	9.97	10.14	$+ .48$ $- .40$
Main Chute Deployed	0.43	0.52	$\pm .13$
Main Chute Disreef	4.63	4.46	$+ .49$ $- .29$

\* From Separation

\*\* From Electrical

\*\*\* From Retro

Spin Rate: 64 RPM

Despin Rate: N/A

Retro Velocities: 1075.8 Ft/Sec.

TABLE 4-1

~~TOP SECRET C~~

~~TOP SECRET C~~

NO.

## SECTION 5

### MISSION 1030-2 RECOVERY SYSTEM

SRV #710 was received at A/P on 16 July 1965. The receiving weight was 149.6 pounds. After modification and incorporation of outstanding E.O.'s the SRV was delivered to Systems Test for mating to the J-29 system. The capsule was delivered to VAFB on 24 January 1966.

#### -2 Mission

The -2 recovery system was successfully recovered by air catch on orbit 159, March 19, 1966.

<u>Predicted</u>	<u>Impact Point</u>	<u>Actual</u>
$22^{\circ} 35' N$	$148^{\circ} 22' W$	$22^{\circ} 42' N$

All recovery events occurred within tolerances. The detailed recovery event times are contained in Table 5-1.

~~TOP SECRET C~~

~~TOP SECRET C~~

NO.

MISSION 1030-2

RECOVERY SEQUENCE OF EVENTS

<u>Event</u>	<u>Actual</u>	Delta Time (Seconds) Nominal <u>Events + △ T</u>
*Arm	76.96	77 <u>±</u> 1.0
*Transfer	2.0	2.0 <u>±</u> 0.25
Electrical Disconnect	0.97	0.900 <sup>+ 0.430</sup> <sub>- 0.400</sub>
Separation	--	--
**Spin	3.37	3.4 <u>±</u> 0.30
Retro	7.55	7.55 <u>±</u> 0.45
Despin	10.72	10.75 <u>±</u> 0.59
T/C Separation	1.55	1.5 <u>±</u> 0.15
***"G" Switch Open	500.23	491.8 to 502.6
Parachute Cover Off	33.43	34.0 <u>±</u> 1.5
Drogue Chute Deployed	0.75	0.63 <u>±</u> .08
Main Chute Bag Separate	9.50	10.14 <sup>+ .48</sup> <sub>.40</sub>
Main Chute Deployed	0.43	0.52 <u>±</u> .13
Main Chute Disreef	4.49	4.46 <sup>+ .49</sup> <sub>.29</sub>

\* From Separation

\*\* From Electrical Disconnect

\*\*\* From Retro

Spin Rate: 64 RPM

Despin Rate: 9.5 RPM

Retro Velocity: 966.4 Ft/Sec.

TABLE 5-1

~~TOP SECRET C~~

SECTION 6

MASTER PANORAMIC CAMERA

A. COMPONENT ASSIGNMENT

<u>Component</u>	<u>Serial Number</u>
Main Camera	182
Main Camera Lens	1902435
Supply Horizon Camera	281-G4
Supply Horizon Camera Lens	E12864
Take-up Horizon Camera	284-G3
Take-up Horizon Camera Lens	E12876
Supply Cassette	SC-29

B. CAMERA DATA AND FLIGHT SETTINGS

Main Camera:

Lens	24" f/3.5
Slit Width	0.275"
Filter Type	Wratten 25
Film Type	Eastman Type 3404

Supply (Port) Horizon Camera:

Lens	55 mm f/6.3
Aperture Setting	f/6.3
Exposure Time	1/100 second
Filter Type	Wratten 25

Take-up (Starboard) Horizon Camera:

Lens	55 mm f/6.3
Aperture Setting	f/8.0
Exposure Time	1/100
Filter Type	Wratten 25

~~TOP SECRET C~~

NO.

### C. POST FLIGHT PERFORMANCE EVALUATION

The overall photographic quality of this mission was low due to severe haze layers over many targets. This caused the contrast to be drastically reduced. The segments of the mission in clear weather displayed excellent image quality.

The measured minimum densities were higher than on previous Corona missions. The correlation between these densities and mission performance will not be fully understood until a research analysis is undertaken. It is noted that this mission received a comparatively low percentage of full processing.

The starboard looking horizon cameras produced poor, but useable imagery early in the mission. As the flight progressed the imagery degraded to a useless condition. They started to clear on pass D-98 and after pass D-132 they were normal. There is no assignable cause at this time for this condition.

The end of pass marker was missing on the film from the master instrument. The pre-flight material indicated that it was operational prior to lift-off so it is surmised that ascent vibration caused the anomaly.

The following characteristic anomalies were normal; format and rail scratches, ragged format edges, edge static and light leaks. These items warrant attention to prevent increased degradation.

~~TOP SECRET C~~

~~TOP SECRET C~~  
NO.

SECTION 7

SLAVE PANORAMIC CAMERA

A. COMPONENT ASSIGNMENT

<u>Component</u>	<u>Serial Number</u>
Main Camera	183
Main Camera Lens	1882435
Supply Horizon Camera	301-G6
Supply Horizon Camera Lens	E12845
Take-up Horizon Camera	301-G5
Take-up Horizon Camera Lens	E12844
Supply Cassette	SC-29

B. CAMERA DATA AND FLIGHT SETTINGS

Main Camera:

Lens	24" f/3.5
Slit Width	0.175
Filter Type	Wratten 21
Film Type	Eastman Type 3404

Supply (Starboard) Horizon Camera:

Lens	55 mm f/6.3
Aperture Setting	f/8.0
Exposure Time	1/100 second
Filter Type	Wratten 25

Take-up (Port) Horizon Camera:

Lens	55 mm f/6.3
Aperture Setting	f/6.3
Exposure Time	1/100 second
Filter Type	Wratten 25

~~TOP SECRET C~~

NO.

### SECTION 3

#### PANORAMIC CAMERA EXPOSURE

The Master camera contained a 0.275 inch slit with a Wratten 25 filter while the Slave camera used a 0.175 inch slit with a Wratten 21 filter. The nominal exposure times for the Master and Slave instruments are shown as a function of latitude for passes 8, 56, 103 and 151 in Figures 3-5 to 3-12. The frequency distributions of the solar elevations and solar azimuths encountered during photographic operations are shown in Figures 8-1 to 8-4.

The predicted level of processing for the original negative is based on the in-flight performance estimate and is tabulated below with the processing levels reported by [REDACTED]

<u>Mission/Camera</u>		<u>Primary</u>	<u>Intermediate</u>	<u>Full</u>
1030-1/FWD	Predicted	0%	58%	42%
	Actual	3%	31.7%	65.3%
1030-1/AFT	Predicted	0%	53%	47%
	Actual	0.2%	45.6%	54.2%
1030-2/FWD	Predicted	1%	42%	57%
	Actual	0.1%	52.5%	47.4%
1030-2/AFT	Predicted	1%	23%	76%
	Actual	0.2%	28.3%	71.5%

~~TOP SECRET C~~

~~TOP SECRET//TTS~~  
SOLAR ELEVATION FREQUENCY DISTRIBUTION

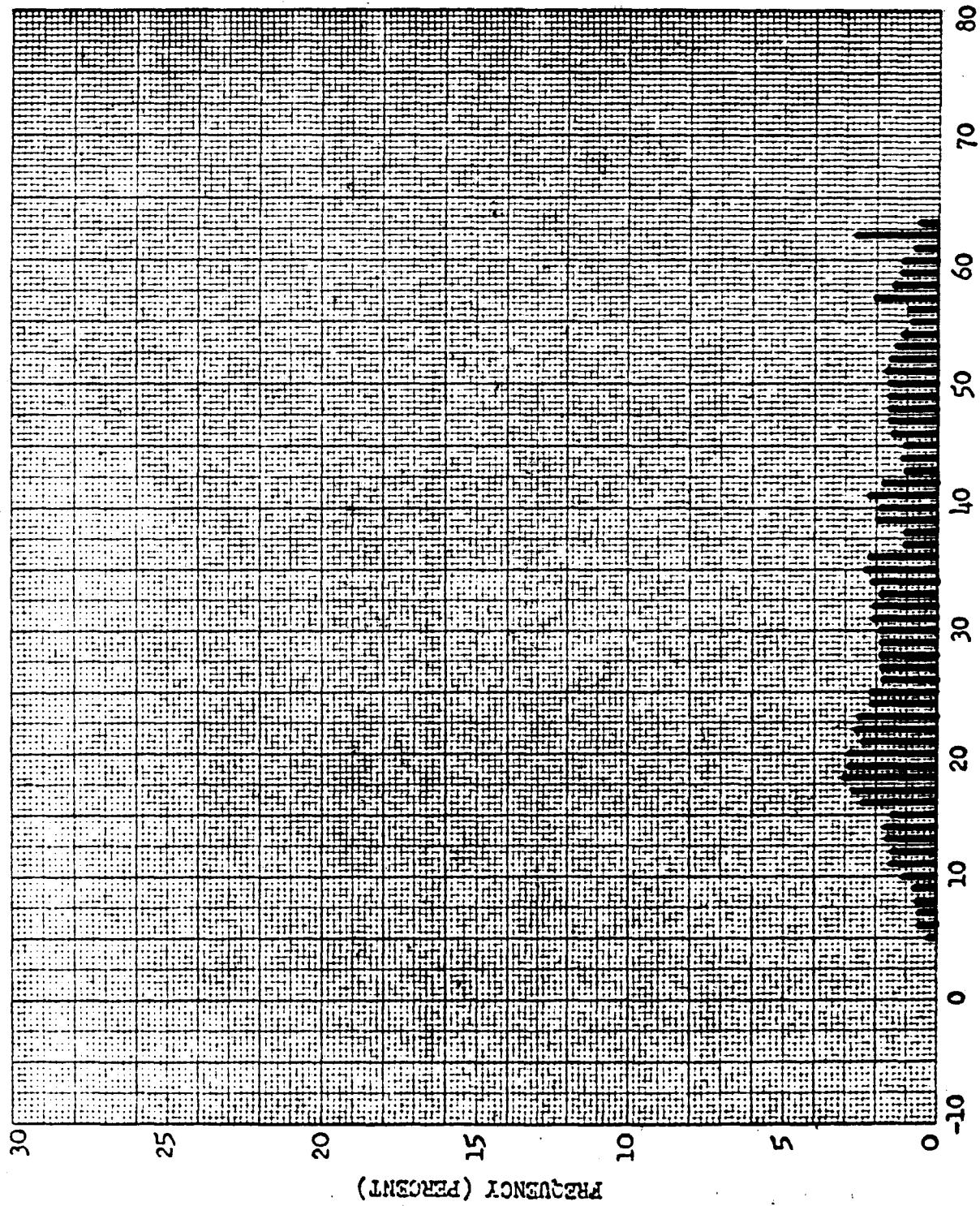
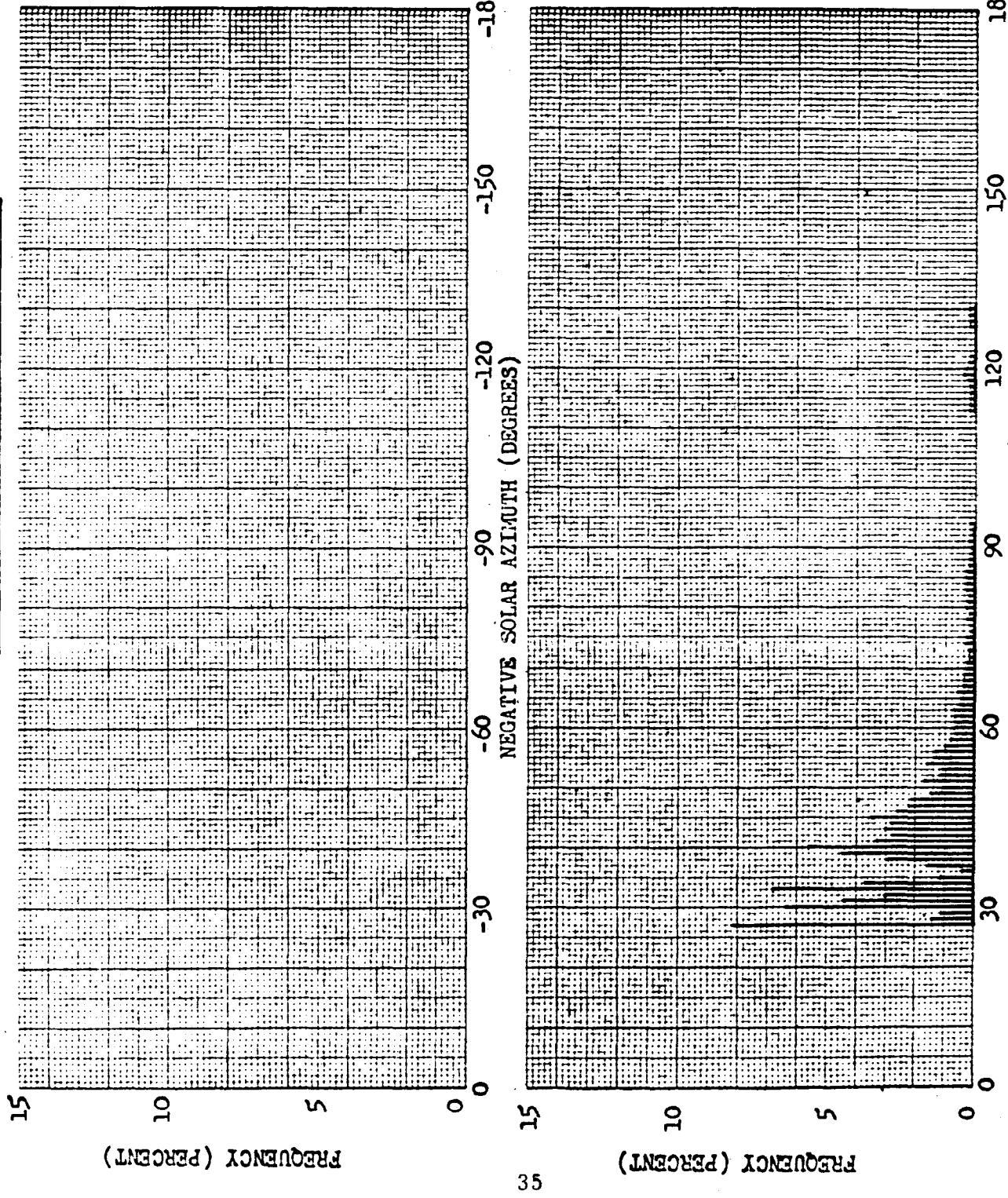


Figure 8-1

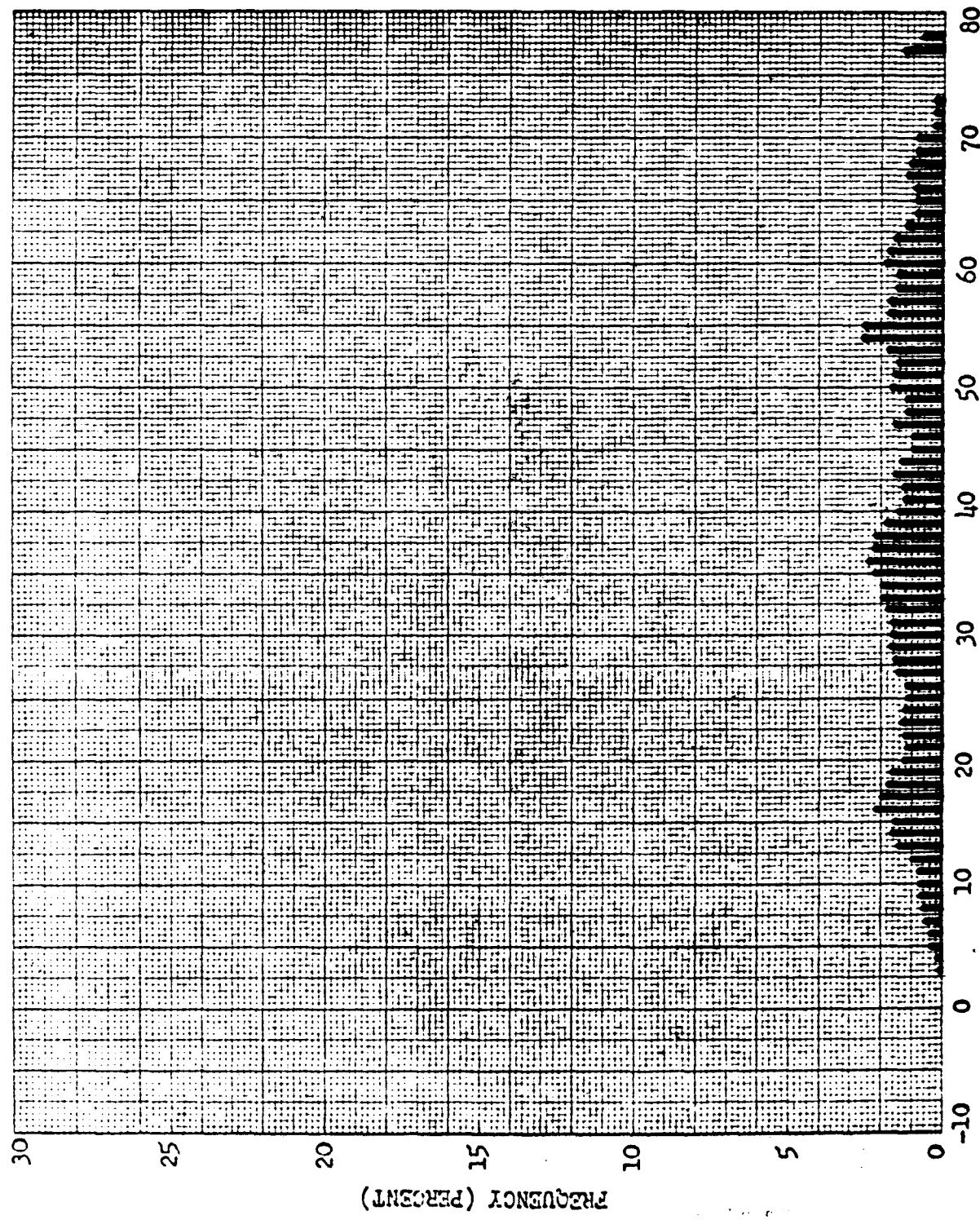
NO.

SOLAR AZIMUTH FREQUENCY DISTRIBUTION



NO.

SOLAR ELEVATION FREQUENCY DISTRIBUTION



TOP SECRET C [REDACTED]

Figure 8-3

NO.

SOLAR AZIMUTH FREQUENCY DISTRIBUTION

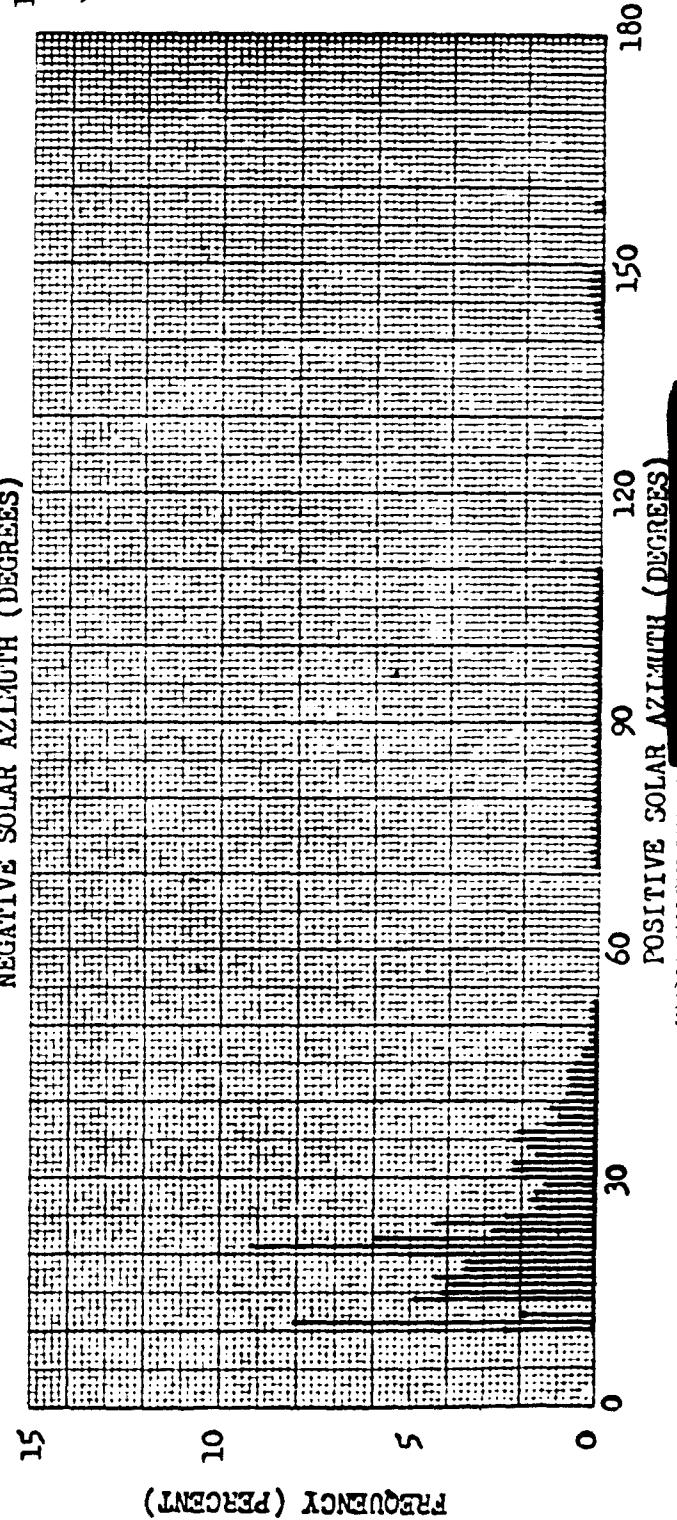
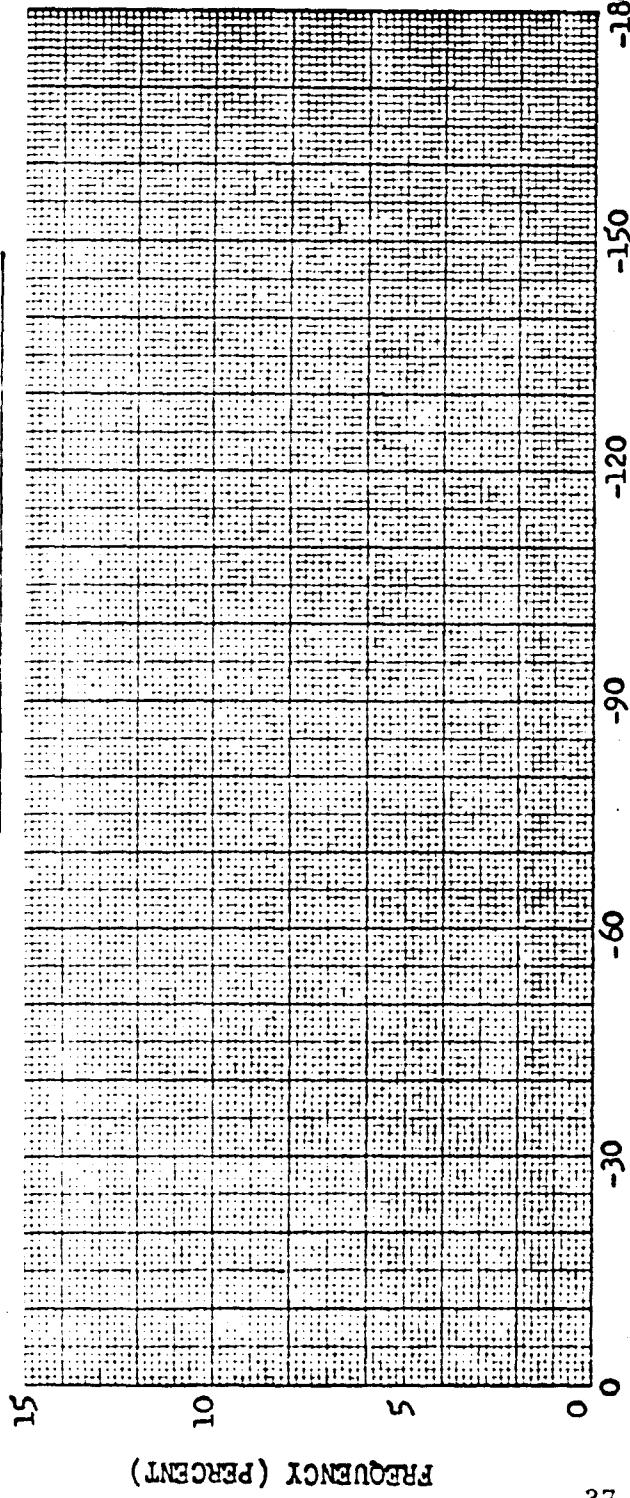
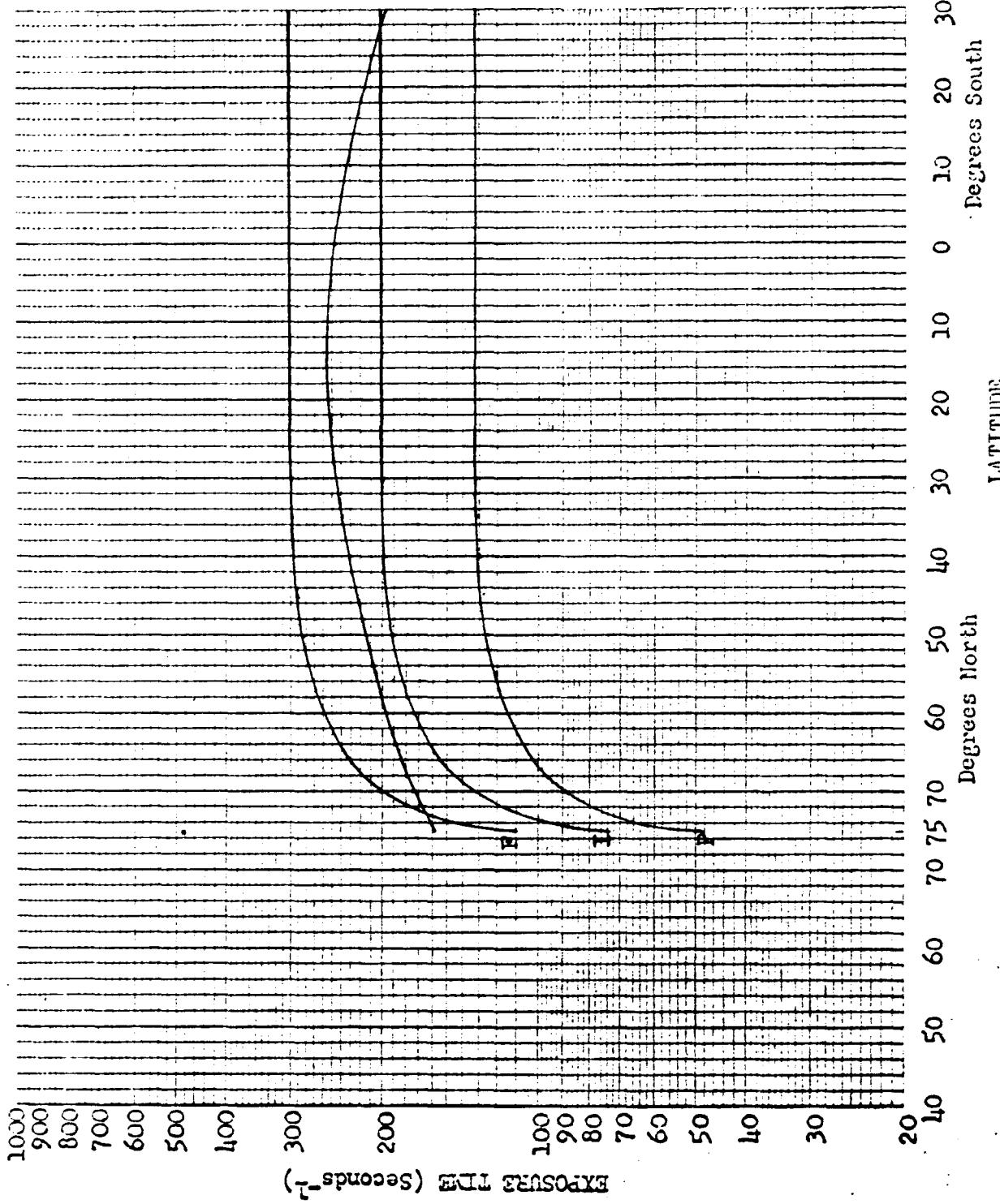


Figure 8-4

EXPOSURE POINTS



Mission No: 1930

Payload No: J-29

Camera No: 132

Pass No: 8

Launch Date: 3/9/66

Launch Time: 2202 Z

Slit Width: .275

Filter Type: Wratten 25

Film Type: 35mm

EXPOSURE POINTS

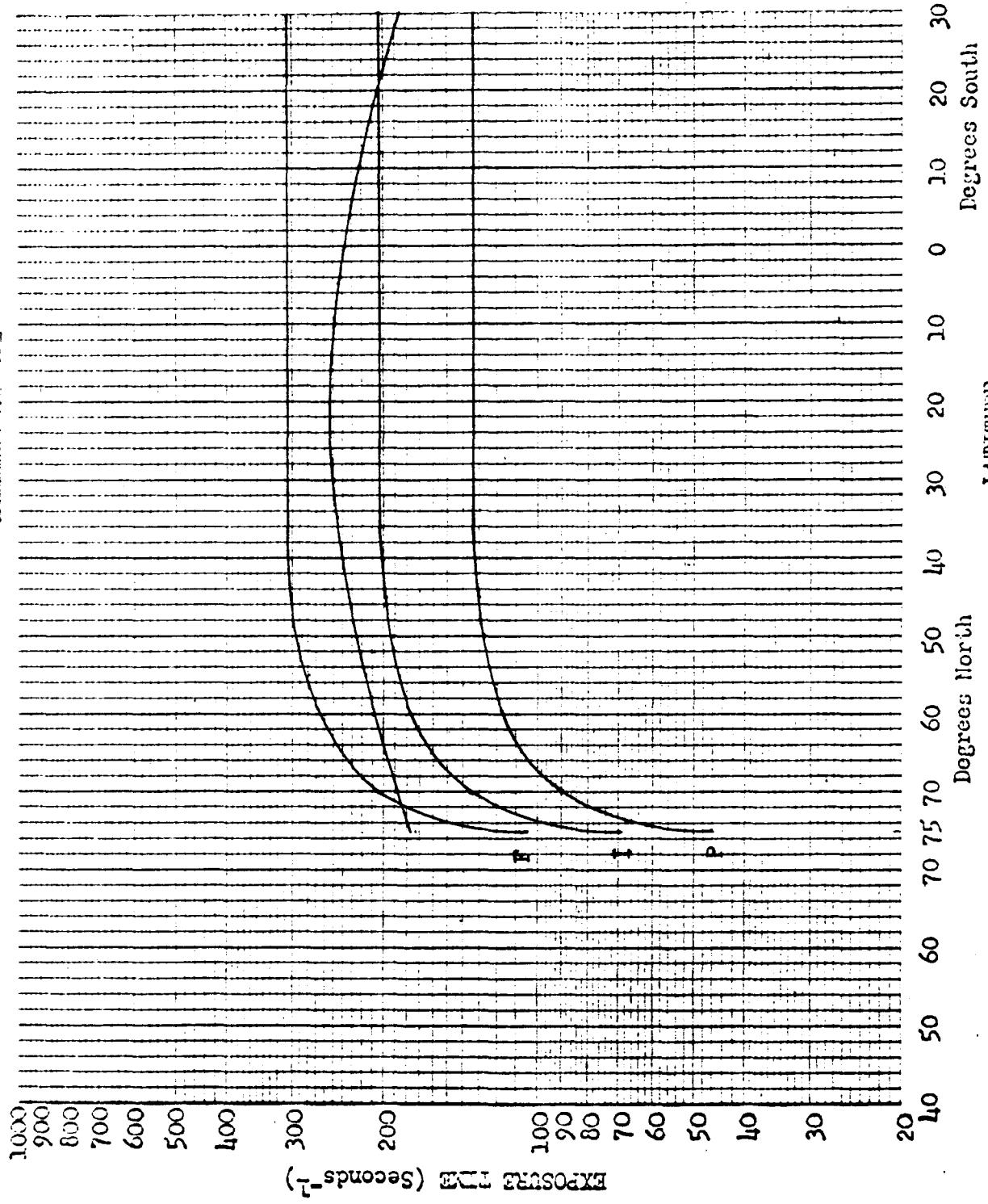
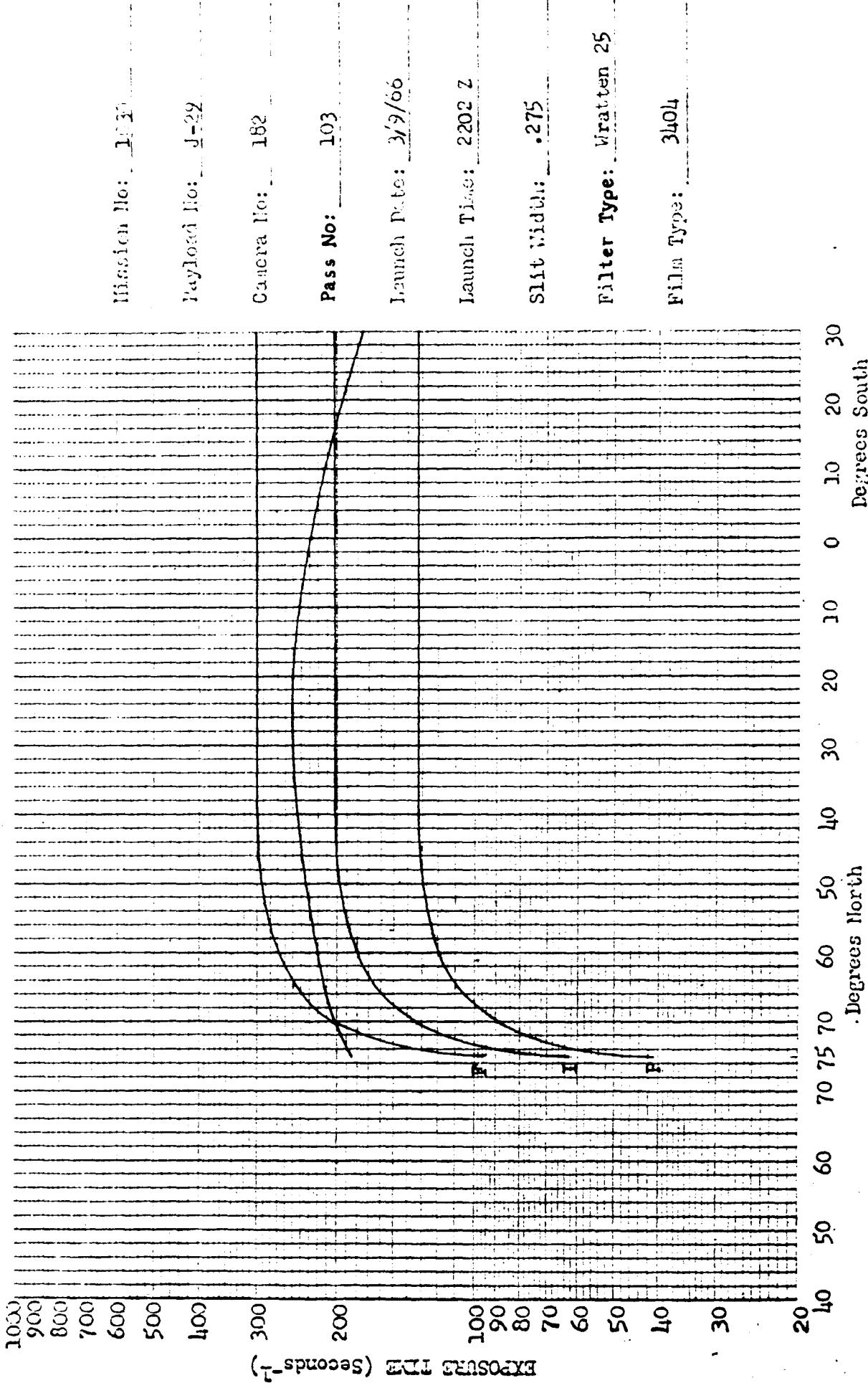


Figure 4-1

40 35 30 25 20 15 10 5 0 5 10 15 20 25 30 35 40

~~SECRET~~ EXPOSURE POINTS

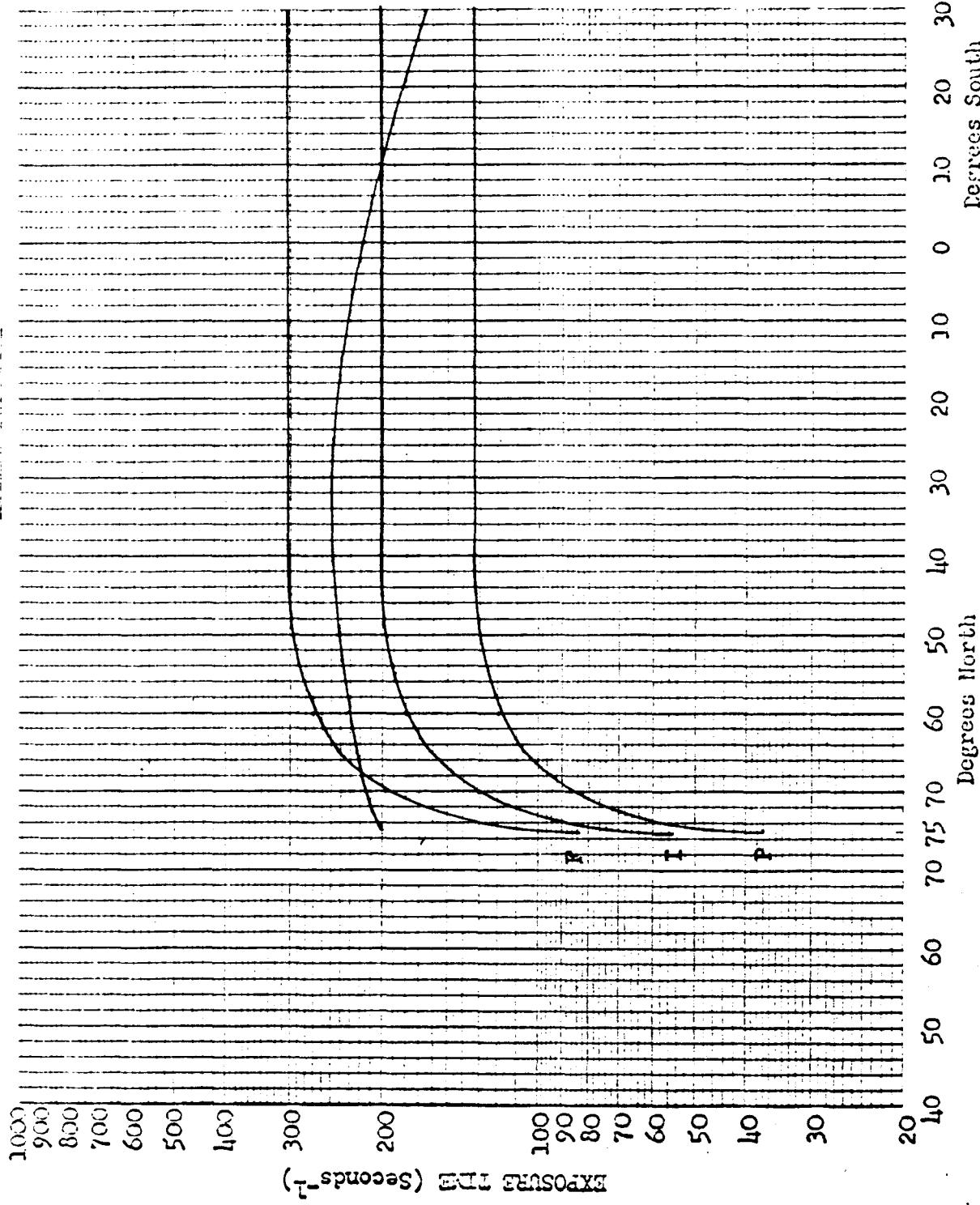


~~SECRET~~ 102

~~SECRET~~ 102

~~SECRET~~ 102

EXPOSURE POINTS



Mission No: 1.2.0

Payload No: 6-29

Camera No: 132

Pass No: 151

Launch Date: 3/9/66

Launch Time: 2202 2

Slit Width: .275

Filter Type: Wratton 25

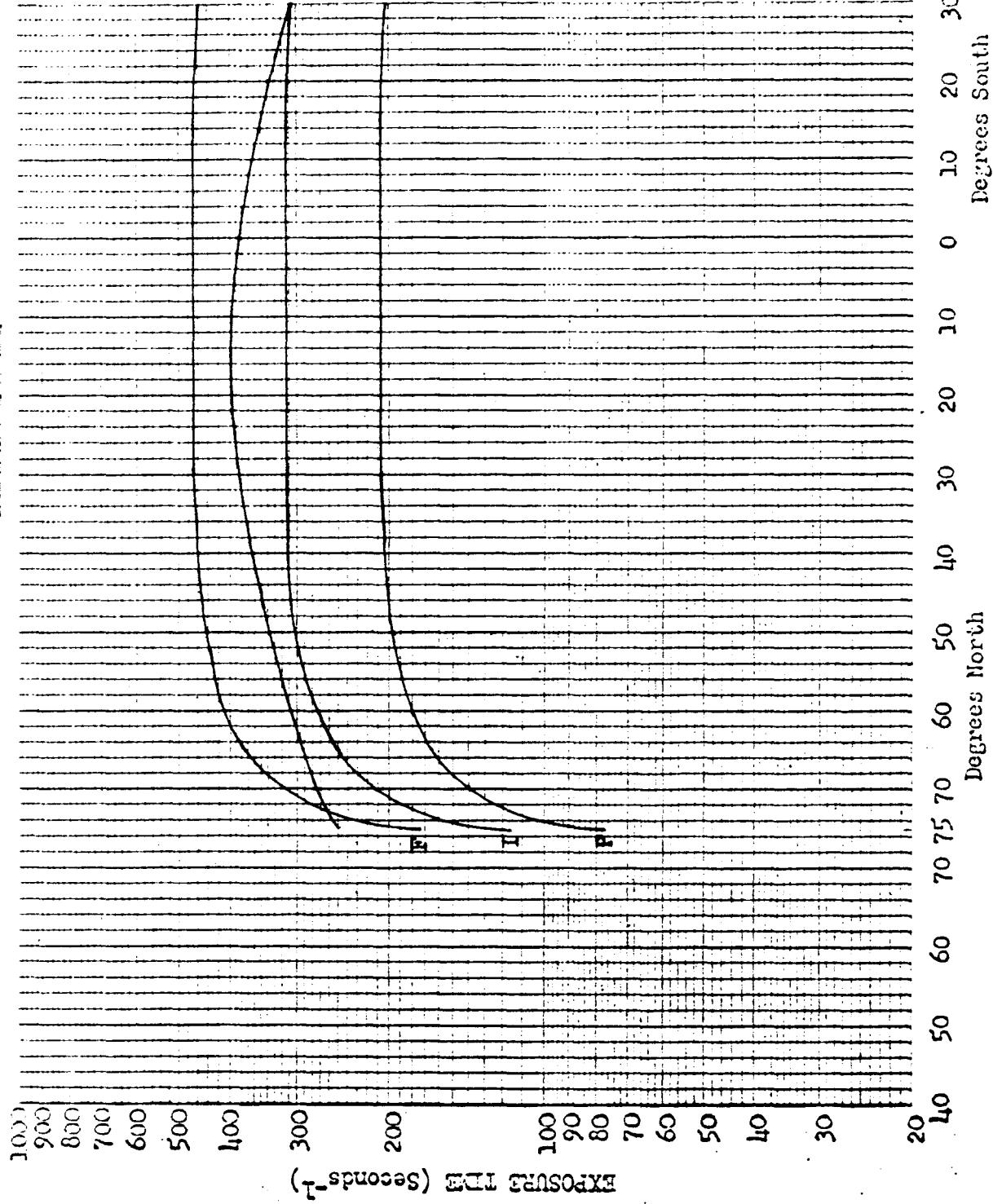
Film Type: 3404

Flight Log

LATITUDE

TIME SEPARATE C

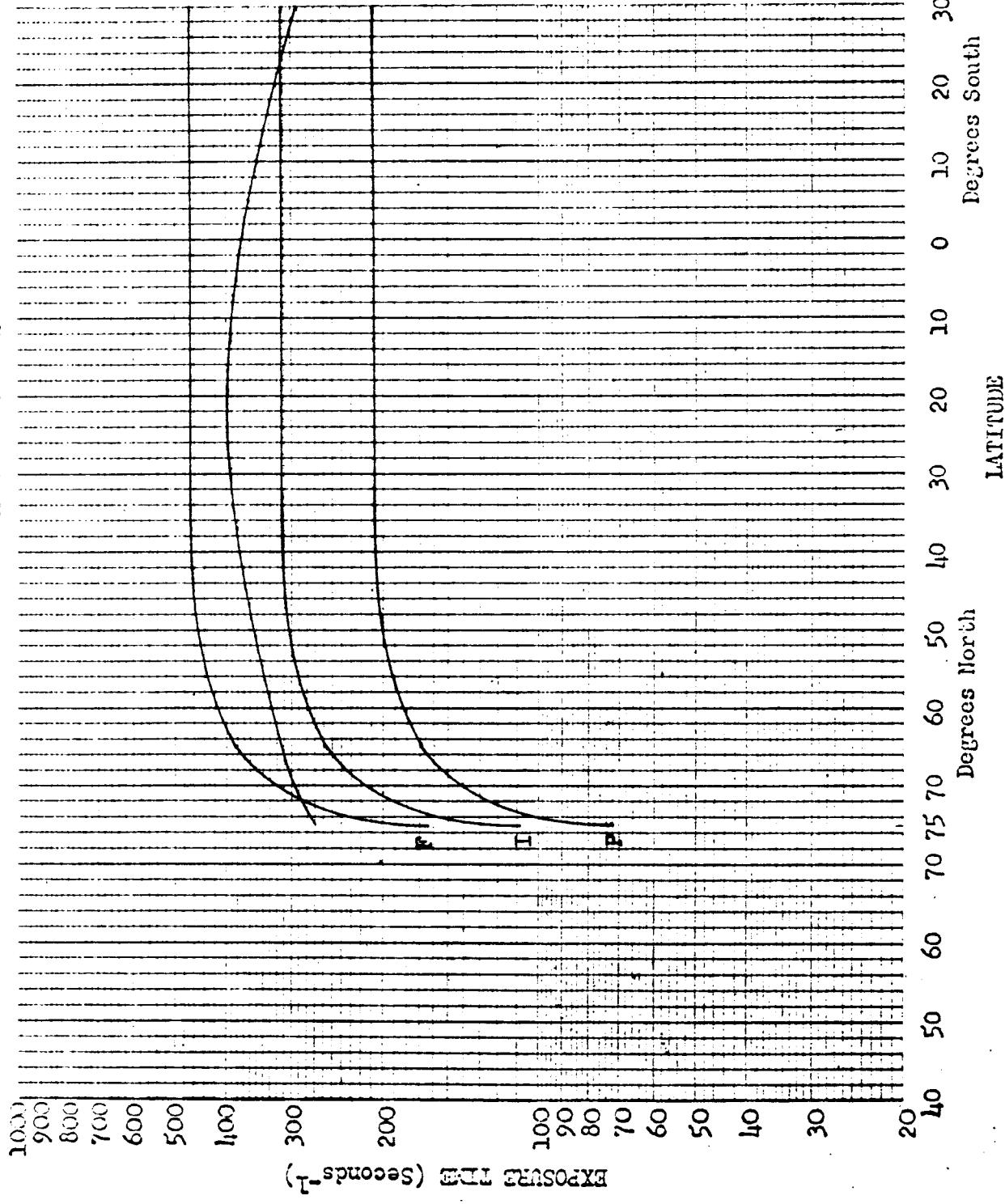
EXPOSURE POINTS



113 30

40 45 50

## EXPOSURE POSITION



Mission No.: 103D

Payload No: J-22

Camera No: 163

P. Job No: 56

Launch Date: 3/9/58

Launch Time: 2202 Z

Slit Width: .175

Filter type: Watten 21

Film Type: 3404

NO.

EXPOSURE POLARIS

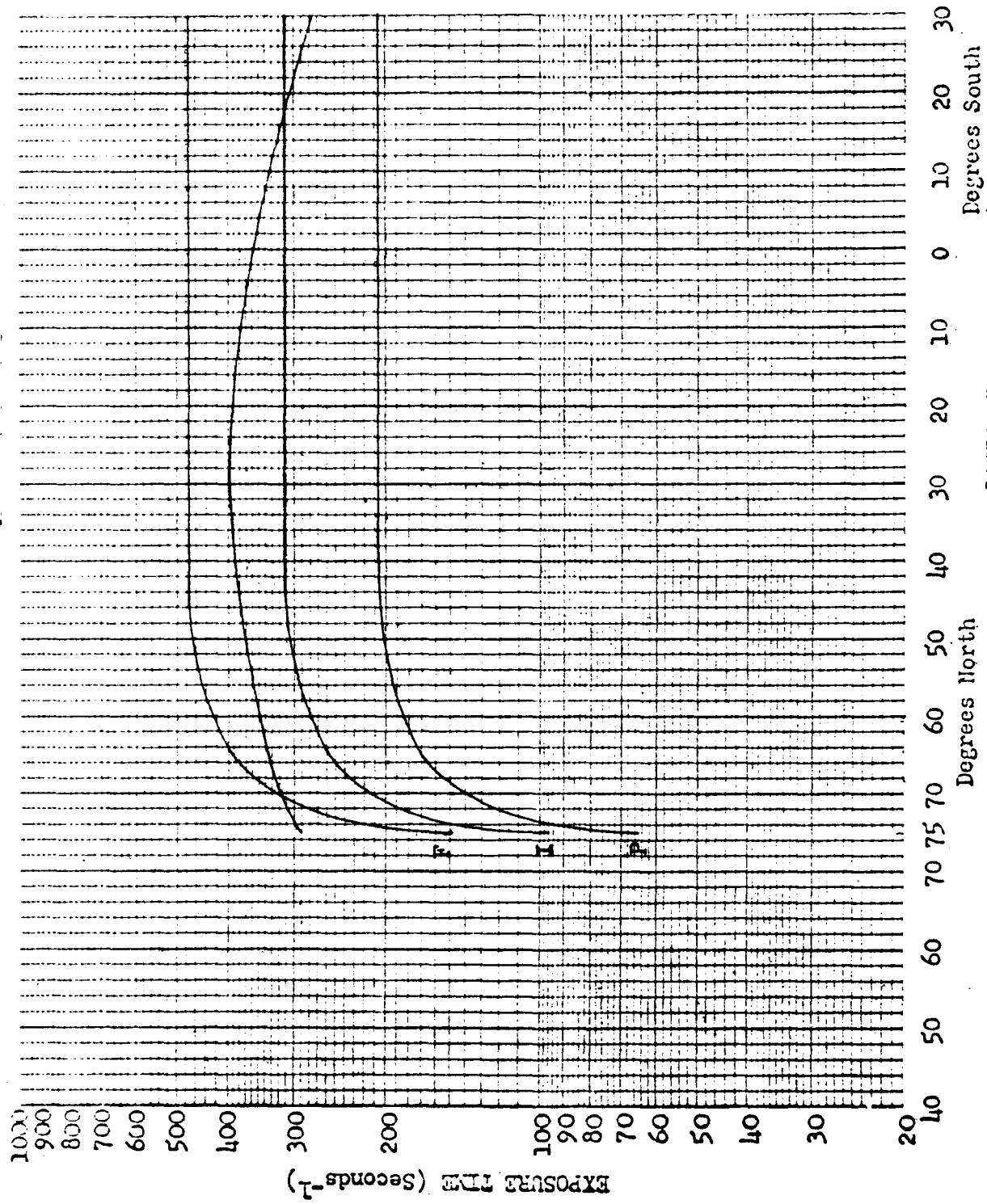


Figure 8-11

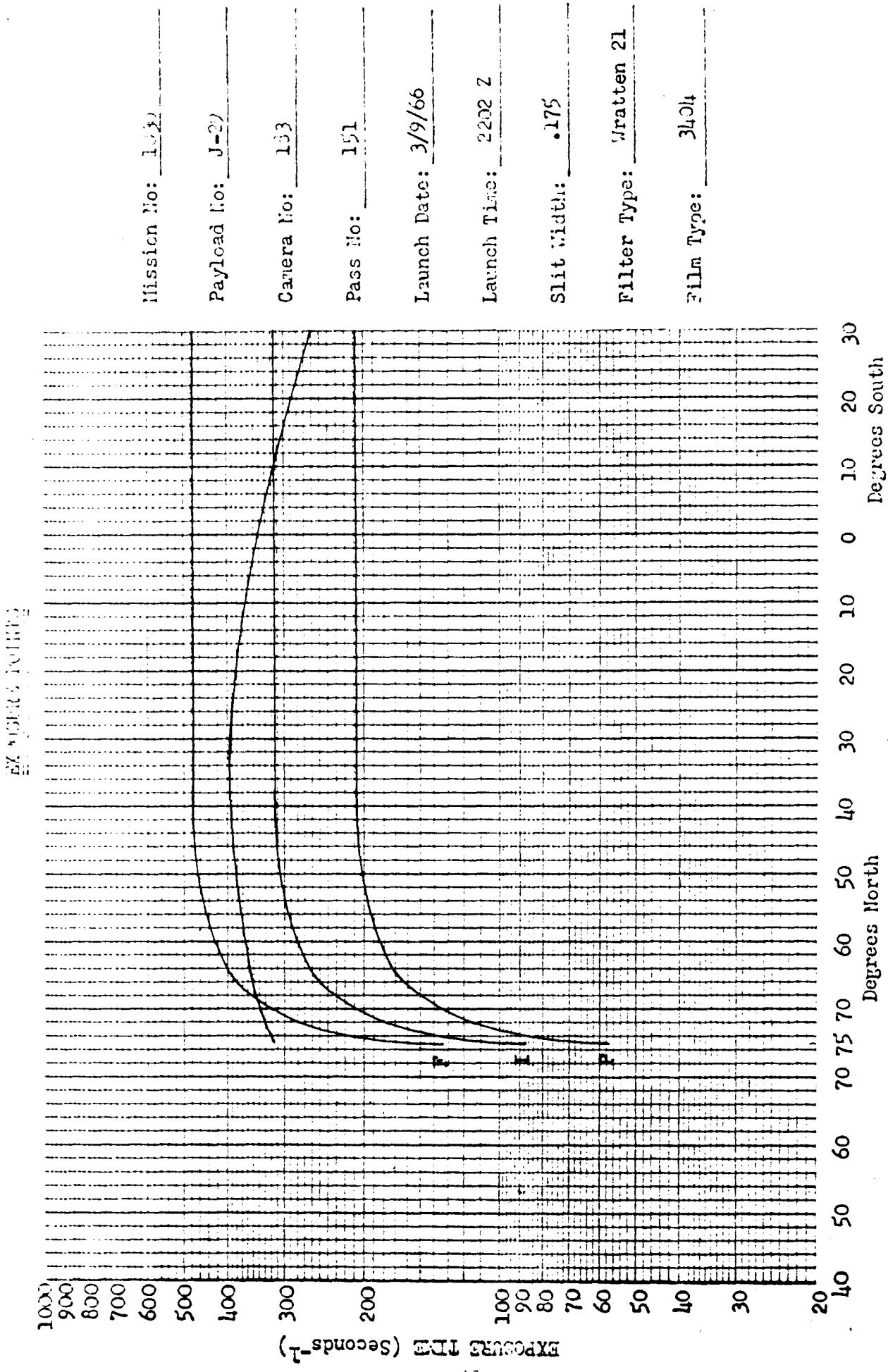


Figure B 12

~~HOT SPOT MAP C~~

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NO.

## SECTION 9

### DIFFUSE DENSITY MEASUREMENTS

The diffuse density measurements made by AFSPPF were computer sorted at A/P to permit analysis of the density ranges encountered at the three processing levels. A study of sorting techniques showed that no absolute method was available to separate the density values as the accuracy of the Processing History published by [REDACTED] appears rather low and processing transition phases are not accounted for. The sorting technique selected uses the base plus fog density values where measurements up to 0.09 density are considered as having received Primary processing, 0.10 to 0.17 as Intermediate and above 0.17 density as Full. The percentage of original negative that was processed at each level, based on the computer sort, is tabulated below with the predicted and reported processing percentages.

<u>Mission</u>	<u>Camera</u>		<u>Primary</u>	<u>Intermediate</u>	<u>Full</u>
1030-1	FWD	Predicted	0%	58	42
		Reported	3	31.7	65.3
		Computed	0.8	51.7	47.5
1030-1	AFT	Predicted	0	53	47
		Reported	0.2	45.6	54.2
		Computed	0	71	29
1030-2	FWD	Predicted	1	42	57
		Reported	0.1	52.5	47.4
		Computed	0	70	30
1030-2	AFT	Predicted	1	23	76
		Reported	0.2	28.3	71.5
		Computed	0	30	70

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The tabulations of density frequency distributions for Missions 1030-1 and 1030-2 are included in Appendix A, Table A-1 thru A-4. The graphical presentation of the density distribution are computer plotted in Appendix A Figures A-1 thru A-39.

A summary of the processing and exposure analysis is shown in Table 9-1. The terrain D-Min criteria, (range) for proper exposure and processing is 0.40 to 0.90 density units. The area measured for D-Min is selected subjectively and is not necessarily the absolute D-Min in the photography.

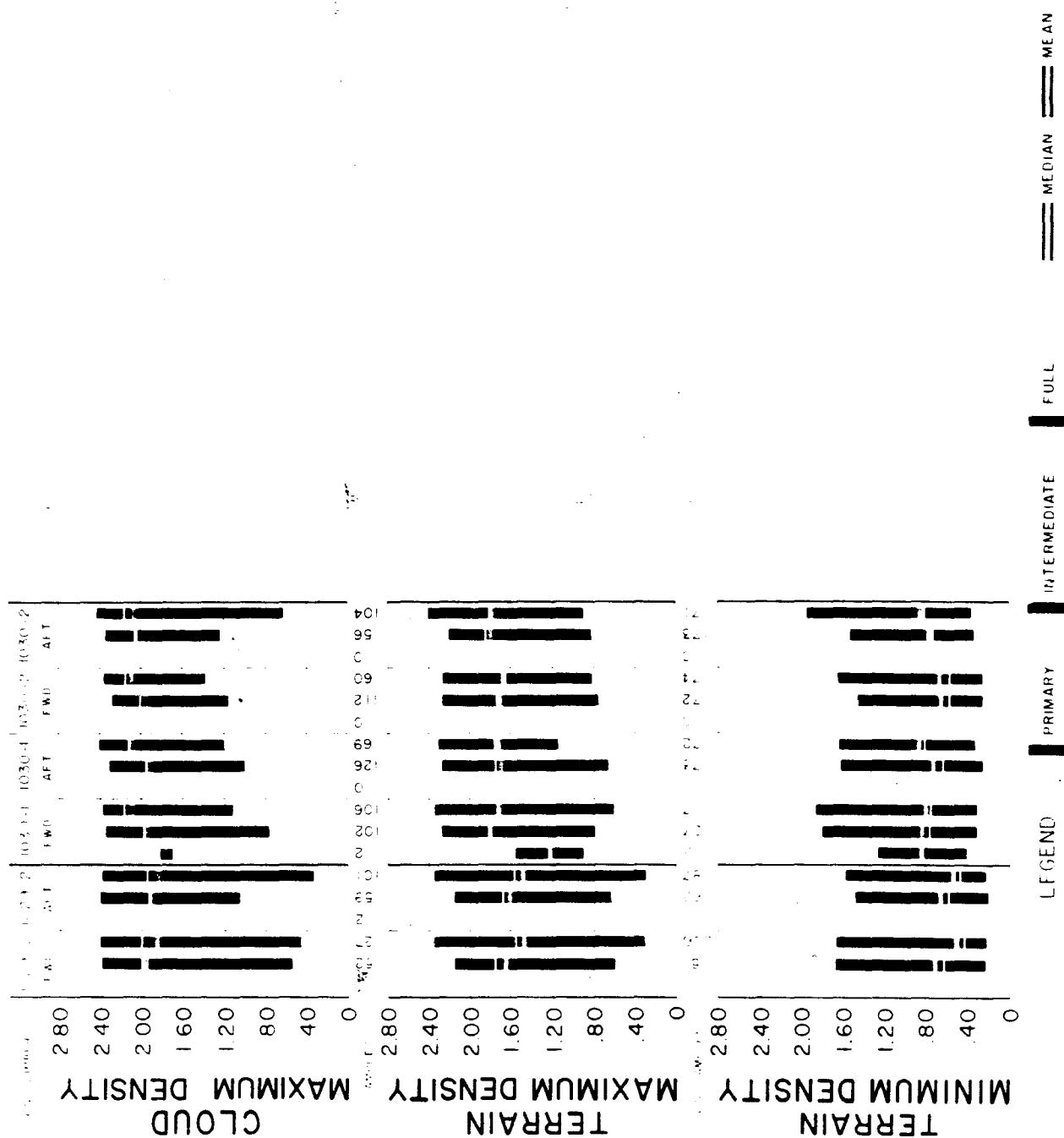
A density range chart, Figure 9-1 is included in this report. This type of chart for missions 1004 to 1031 is included in the A/P Final Report for Mission 1031.

These charts are produced from the same density measurements previously mentioned in this section. The computer produced the mean, median and range figures for the various processing levels used. The chart includes the number of frames (samples) in which the density measurements were made. These measurements are made on approximately every tenth frame throughout the mission.

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# J MISSION DENSITY RANGES

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MISSION DATE		INSTR - FWD		8/25/06		PROCESSING AND EXPOSURE ANALYSIS			
ITEM	SAMPLE	UNDER EXPOSED	UNDER PROCESSED	CURRENT EXP+PROC	OVER PROCESSED	OVER EXPOSED			
PRIMARY	112	3 PC	2 PC	50 PC	0 PC	50 PC	50 PC	50 PC	
INTERMEDIATE	113	3 PC	6 PC	53 PC	27 PC	50 PC	50 PC	50 PC	
FULL	117	3 PC	2 PC	62 PC	22 PC	1 PC	1 PC	1 PC	
AVERAGE	248	4 PC	3 PC	61 PC	28 PC	5 PC	5 PC	5 PC	
MISSION DATE		INSTR - AFT		8/25/06		PROCESSING AND EXPOSURE ANALYSIS			
ITEM	SAMPLE	UNDER EXPOSED	UNDER PROCESSED	CURRENT EXP+PROC	OVER PROCESSED	OVER EXPOSED			
PRIMARY	112	3 PC	2 PC	30 PC	0 PC	0 PC	0 PC	0 PC	
INTERMEDIATE	113	3 PC	12 PC	55 PC	17 PC	0 PC	0 PC	0 PC	
FULL	117	3 PC	0 PC	61 PC	36 PC	0 PC	0 PC	0 PC	
AVERAGE	248	2 PC	3 PC	54 PC	22 PC	4 PC	4 PC	4 PC	
MISSION DATE		INSTR - FWD		8/25/06		PROCESSING AND EXPOSURE ANALYSIS			
ITEM	SAMPLE	UNDER EXPOSED	UNDER PROCESSED	CURRENT EXP+PROC	OVER PROCESSED	OVER EXPOSED			
PRIMARY	112	1 PC	2 PC	0 PC	0 PC	0 PC	0 PC	0 PC	
INTERMEDIATE	113	1 PC	13 PC	73 PC	12 PC	3 PC	3 PC	3 PC	
FULL	117	15 PC	0 PC	55 PC	18 PC	0 PC	0 PC	0 PC	
AVERAGE	248	15 PC	3 PC	71 PC	13 PC	2 PC	2 PC	2 PC	
MISSION DATE		INSTR - AFT		8/25/06		PROCESSING AND EXPOSURE ANALYSIS			
ITEM	SAMPLE	UNDER EXPOSED	UNDER PROCESSED	CURRENT EXP+PROC	OVER PROCESSED	OVER EXPOSED			
PRIMARY	112	0 PC	0 PC	0 PC	0 PC	0 PC	0 PC	0 PC	
INTERMEDIATE	113	0 PC	1 PC	75 PC	19 PC	4 PC	4 PC	4 PC	
FULL	117	0 PC	0 PC	53 PC	35 PC	1 PC	1 PC	1 PC	
AVERAGE	248	0 PC	0 PC	66 PC	30 PC	2 PC	2 PC	2 PC	
MISSION DATE		INSTR - FWD		8/25/06		PROCESSING AND EXPOSURE ANALYSIS			
ITEM	SAMPLE	UNDER EXPOSED	UNDER PROCESSED	CURRENT EXP+PROC	OVER PROCESSED	OVER EXPOSED			
PRIMARY	112-113	0.01-0.13	0.14-0.39	0.40-0.90	-----	0.91 AND UP			
INTERMEDIATE	113-117	0.01-0.29	0.21-0.39	0.40-0.90	0.91-1.34	1.35 AND UP			
FULL	117	0.01-0.39	-----	0.40-0.90	0.91-1.69	1.70 AND UP			

Table 9-1

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NO.

## SECTION 10

### PERFORMANCE MEASUREMENTS

The photography acquired by both panoramic cameras during Missions 1030-1 and 1030-2 received a MIP rating of 85. A summary is tabulated below of the MTF/AIM resolution values measured by AFSPPF and [REDACTED]. The microdensitometer slit used by AFSPPF and [REDACTED] was 80 microns by one micron.

<u>Mission</u>	<u>Camera</u>	<u>AFSPPF</u>	[REDACTED]
1030-1	FWD	81	66
1030-1	AFT	74	77
1030-2	FWD	73	71
1030-2	AFT	86	71

The details of the measurement and computing techniques, targets measured and target locations are fully reported in the evaluation report published by AFSPPF and are not normally included in this report.

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## SECTION 11

### OBSERVED DATA

Mission 1030 contained an unusually high percentage of photography that was degraded by atmospheric conditions, the PEIR report states that for Mission 1030-1 only 2% was clear terrain, and Mission 1030-2 contained 11% clear terrain. Consequently, only a very small amount of photography from engineering operations is suitable for evaluating the system performance capability.

Pass D47 covered Indian Springs and Pahrump Fixed CORN targets. Indian Springs had solid cloud cover. Pahrump was degraded by thin clouds or haze, but the high contrast fixed target was read to 12 feet ground resolution. A mobile T Bar Target of low contrast was deployed near the fixed target. The largest group (16 feet) could not be resolved. Obviously, the system capability is much better than shown under this atmospheric condition.

The other 2 resolution targets photographed on this mission were even less useful. The Fort Huachuca target on pass D31 was in the bonus area and out of focus. A mobil medium T-Bar target was deployed at Lompoc, California for pass D126. This target appeared 2 inches from the end of the format and thus suffered loss of scale. The forward camera resolved 16 feet on the ground and the aft camera resolved 12 feet.

Pass D126 did contain a few square miles of clear terrain around Ventura, California with no detectable haze. At a sewage treatment plant the catwalks and spray arms on the clarifier tanks were detected by both cameras, representing a detection capability of 5 feet. A few miles away, at Oxnard AFB, the 3 foot spaces of the runway threshold markers could not be seen, in spite of a 15:1 aspect ratio.

The only conclusion that can be drawn from the foregoing is that this particular system was capable of resolving less than 12 feet on the ground, but probably could not resolve 6 feet.

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NO.

## SECTION 12

### MISSION 1030-1 STELLAR-INDEX CAMERA

#### A. COMPONENT ASSIGNMENT

<u>Component</u>	<u>Serial Number</u>
Camera	D-94
Index Reseau	100
Stellar Reseau	107

#### B. CAMERA DATA AND FLIGHT SETTINGS

##### Stellar Camera:

Lens	85 mm f/1.8
Exposure Time	2 seconds
Filter Type	None
Film Type	Eastman Type 3401

##### Index Camera:

Lens	38 mm f/4.5
Exposure Time	1/500 second
Filter Type	Wratten 21
Film Type	Eastman Type 3400

#### C. POST FLIGHT PERFORMANCE EVALUATION

The -1 mission instruments each produced 422 frames of good quality photography. Plus density streaks, multidirectional, appeared intermittently through frame 78 of the stellar material. To determine the source of these particles would be difficult and since they have a minimal effect on data reduction, there will be no further action taken.

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NO.

## SECTION 13

### MISSION 1030-2 STELLAR-INDEX CAMERA

#### A. COMPONENT ASSIGNMENT

<u>Component</u>	<u>Serial Number</u>
Camera	D-82
Index Reseau	195
Stellar Reseau	102

#### B. CAMERA DATA AND FLIGHT SETTINGS

##### Stellar Camera:

Lens	85 mm f/1.8
Exposure Time	2 seconds
Filter Type	None
Film Type	Eastman Type 3401

##### Index Camera:

Lens	38 mm f/4.5
Exposure Time	1/500 second
Filter Type	Wratten 21
Film Type	Eastman Type 3400

#### C. POST FLIGHT EVALUATION

The -2 mission instruments each produced 444 frames of good quality for data reduction.

In many target areas there was a severe haze layer that drastically reduced contrast and image quality. An analysis of the index material shows that only 15% of the -1 mission and 17% of the -2 mission had clear weather (10% or less cloud cover).

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## SECTION 14

## VEHICLE ATTITUDE

The vehicle attitude errors for both Mission 1030-1 and 1030-2 were derived from the reduction of the Stellar camera photography. This attitude data is supplied to A/P by NPIC.

The attitude errors for each frame and the attitude control rates are calculated at the A/P computer facility. The computer also plots the frequency distribution of the rates and errors. Figures 14-1 through 14-6 show these distributions for Mission 1030-1 and Figures 14-7 through 14-12 for Mission 1030-2.

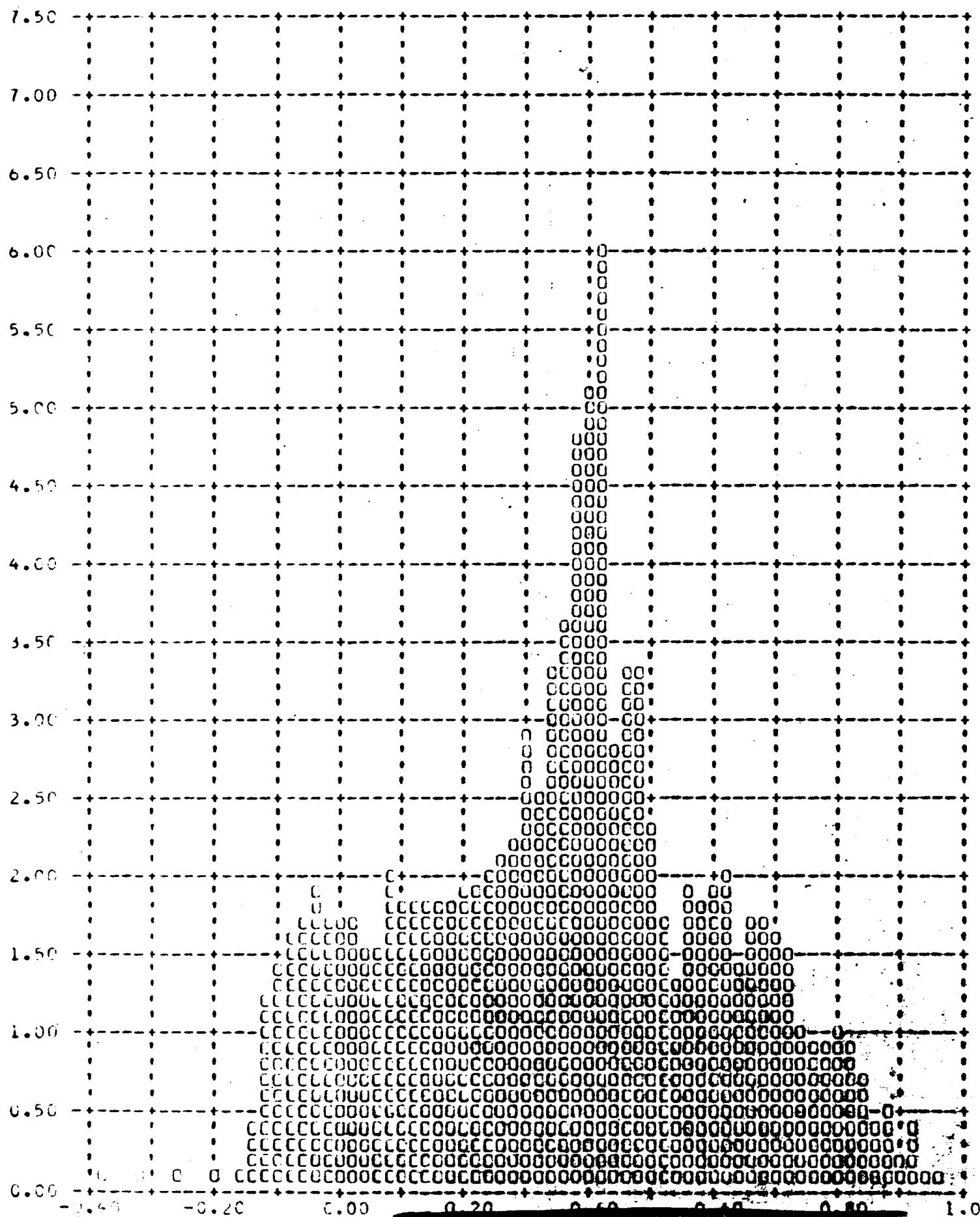
The summary table below lists the maximum attitude errors and rates that were experienced during 90% of the FWD photographic operations, excluding the first six frames of each operation, and the total range of the errors and rates.

<u>Value</u>	Mission 1030-1		Mission 1030-2	
	<u>90%</u>	<u>Range</u>	<u>90%</u>	<u>Range</u>
Pitch Error ( $^{\circ}$ )	0.67	-0.38 to +0.96	0.70	-0.06 to +1.0
Roll Error ( $^{\circ}$ )	0.25	-0.26 to +0.80	0.27	-0.35 to +1.05
Yaw Error ( $^{\circ}$ )	0.89	-1.30 to +0.90	0.87	-1.35 to +1.05
Pitch Rate ( $^{\circ}/\text{hr.}$ )	29.63	-85 to +85	28.38	-56 to +76
Roll Rate ( $^{\circ}/\text{hr.}$ )	22.70	-65 to +75	22.66	-90 to +80
Yaw Rate ( $^{\circ}/\text{hr.}$ )	36.09	-50 to +85	36.29	-50 to 62

MISSION 1030A1 ~~TOP SECRET~~

J-29 A-PUCKET FORWARD INSTRUME FRAMES 1-6 OF EACH OP OMITTED 90 PERCENT = .0.67

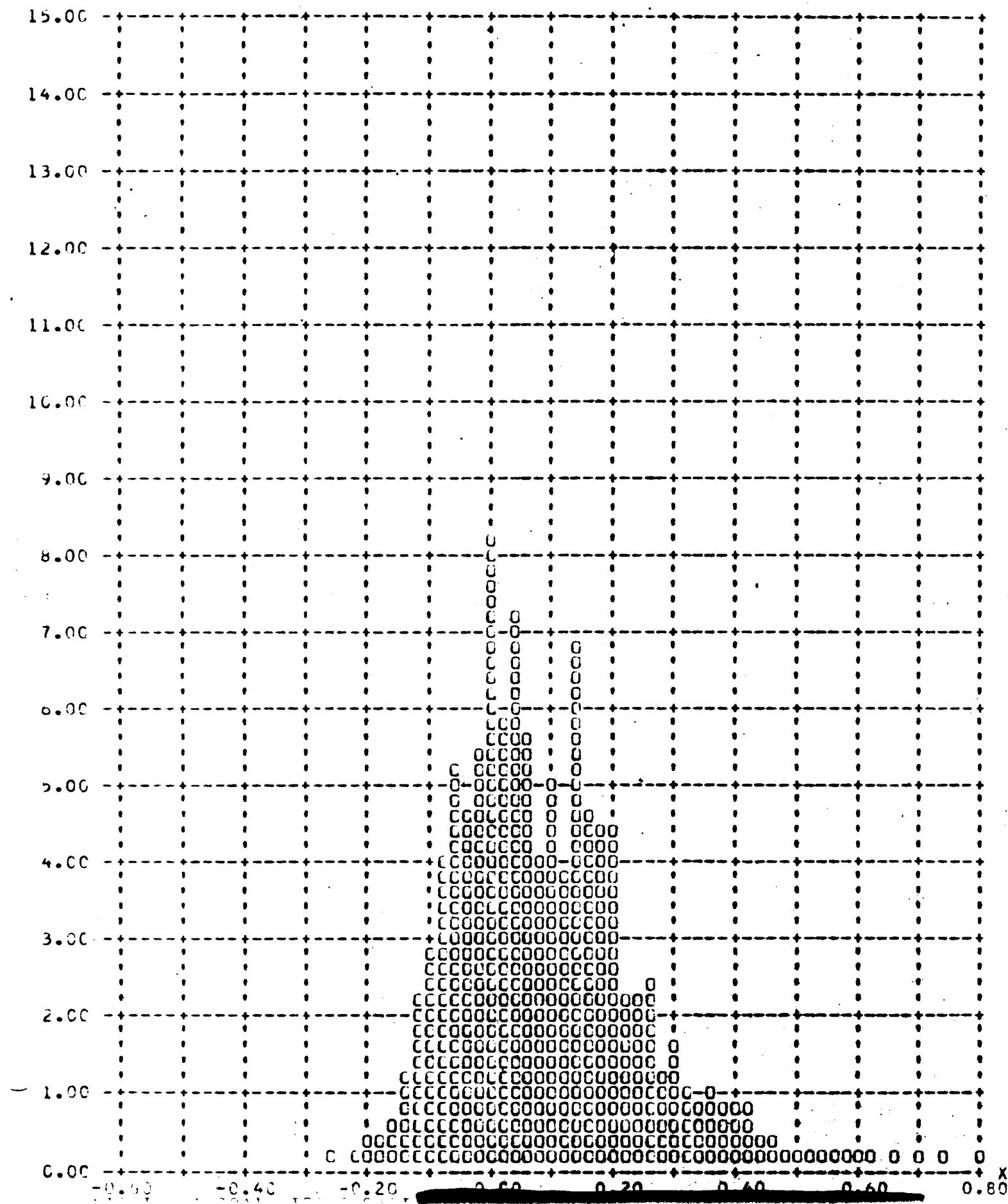
Y PITCH ANGLE ERROR - DEGREES (X) VERSUS FREQUENCY - PERCENT (Y)



MISSION 1030A1 TEF SECRET

-29 A-PUCKET FORWARD INSTRUME FRAMES 1-6 OF EACH OP OMITTED 90 PERCENT = 0.25

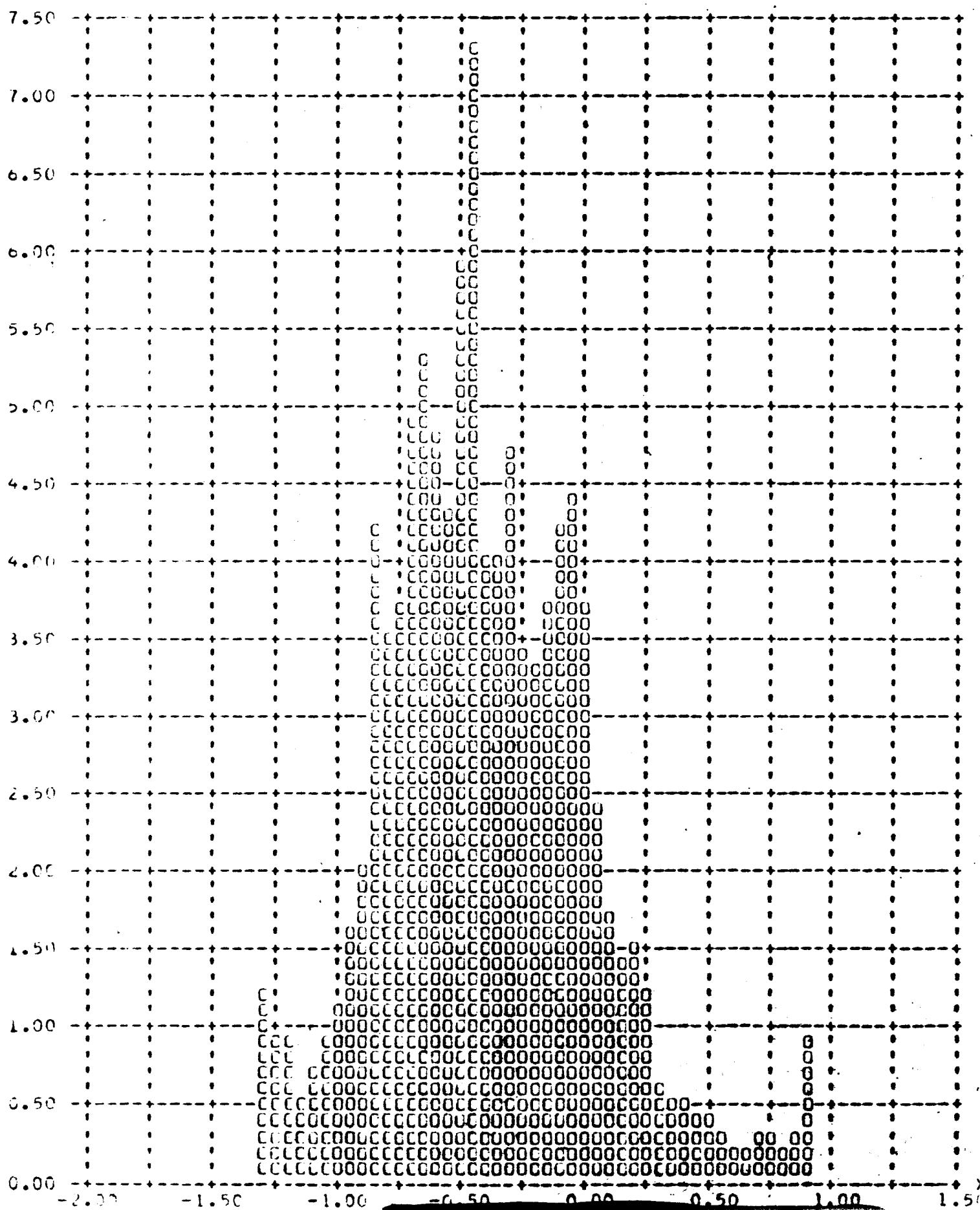
Y ROLL ANGLE ERROR - DEGREES (X) VERSUS FREQUENCY - PERCENT (Y)



MISSION 1030A1 ~~REF SECRE~~

1-29 A-PUCKET FORWARD INSTRUME FRAMES 1-6 OF EACH OP OMITTED 90 PERCENT = 0.89

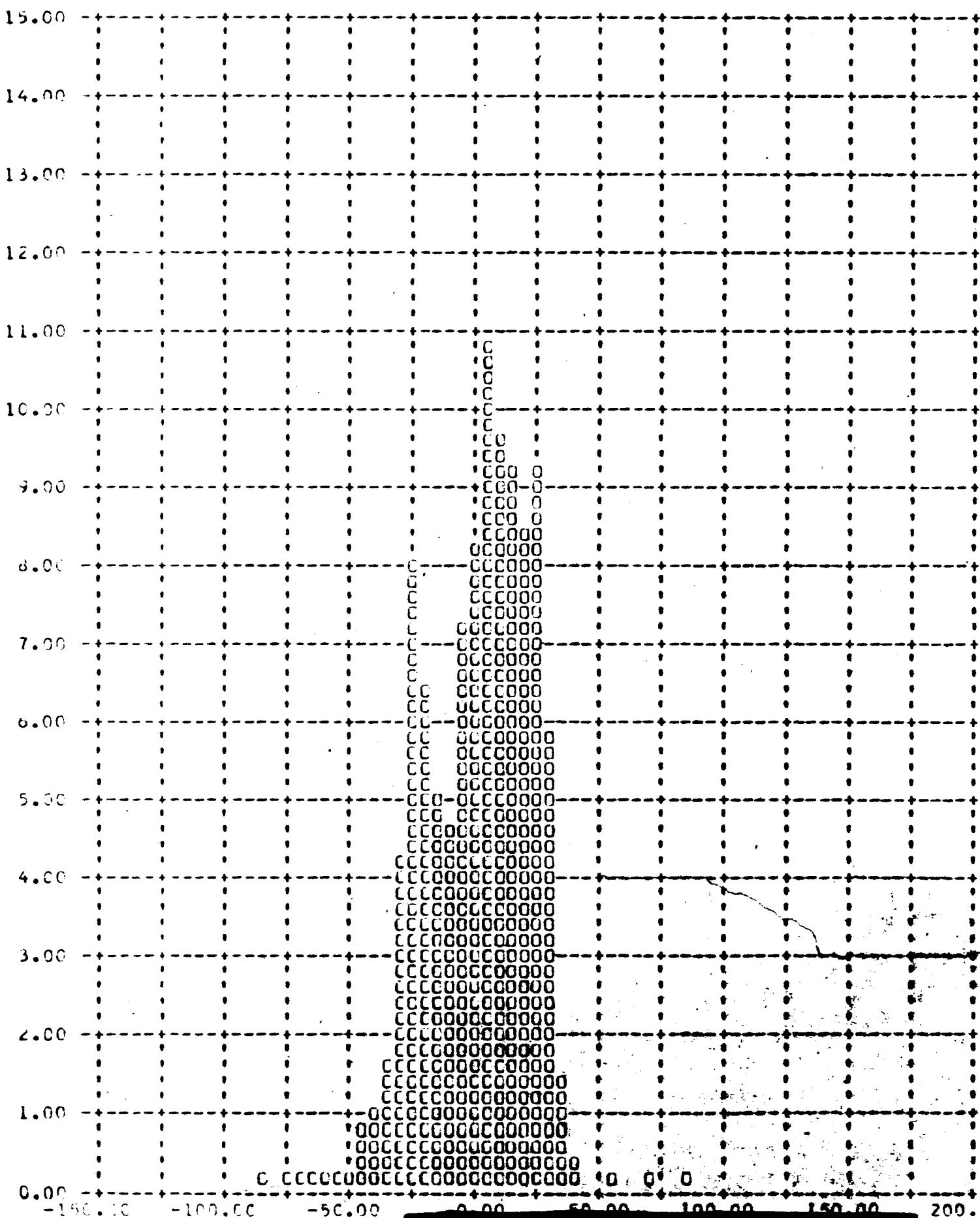
Y YAW ANGLE ERROR - DEGREES (X) VERSUS FREQUENCY - PERCENT (Y)



MISSION 1030A1 TOP SECRET

J-29 A-BUCKET FORWARD INSTRUME FRAMES 1-6 OF EACH OP OMITTED 90 PERCENT = 29.6

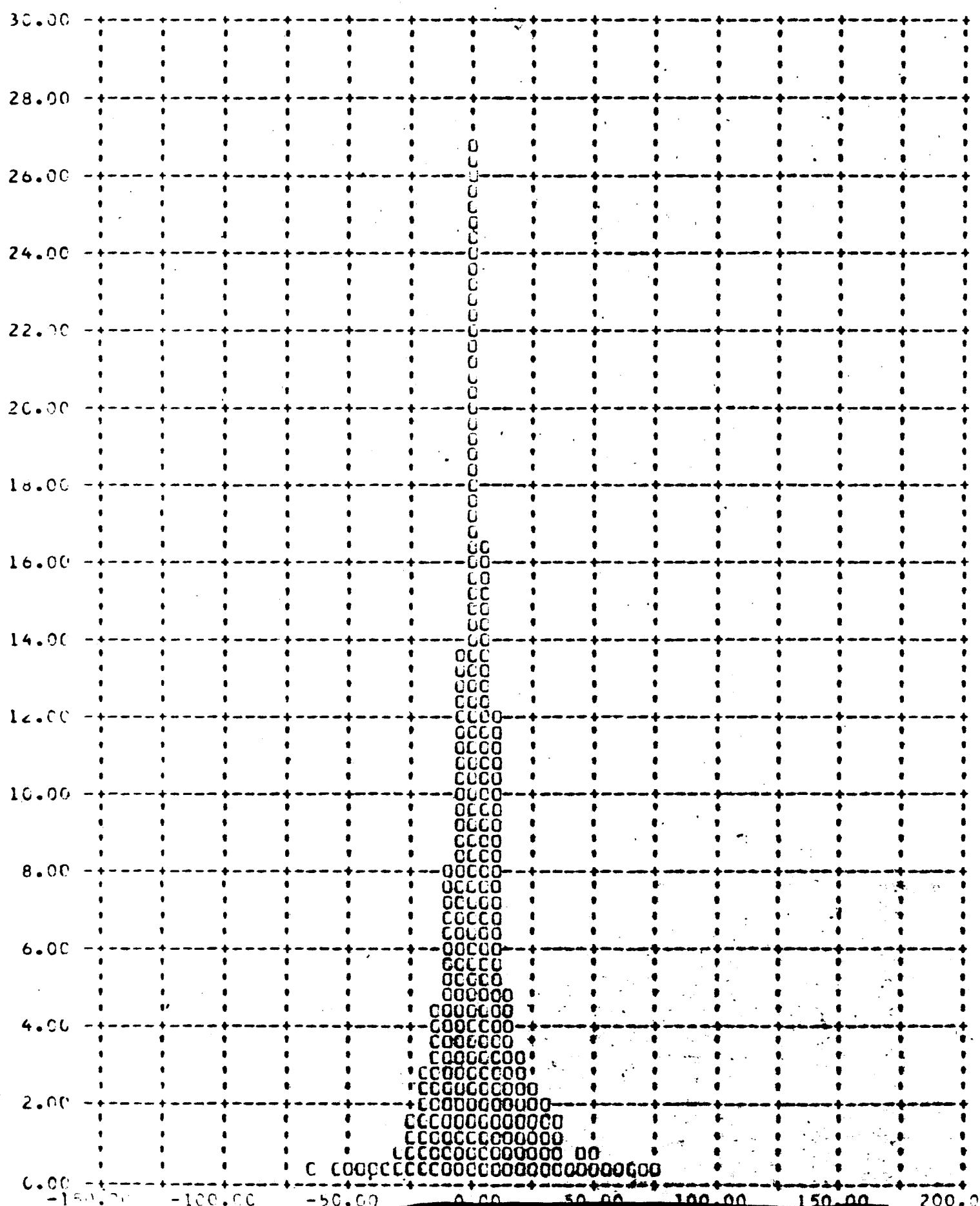
Y PITCH RATE ERROR - DEG/HOUR (X) VERSUS FREQUENCY - PERCENT (Y)



MISSION 1030A1 ~~TOP SECRET~~

-29 A-BUCKET FORWARD INSTRUMF FRAMES 1-6 OF EACH UP OMITTED 90 PERCENT = 22.70

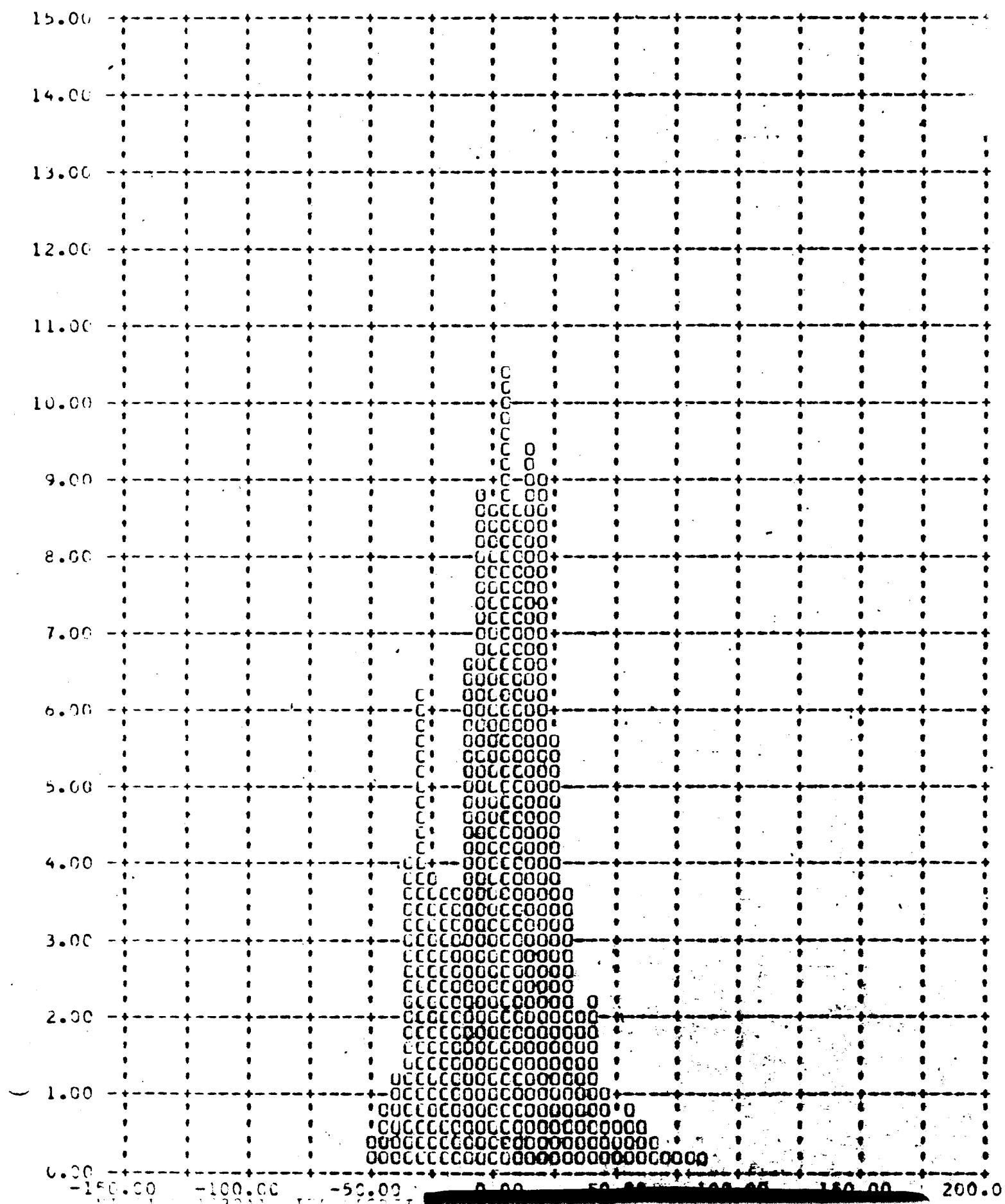
Y ROLL RATE ERRCR - DEG/HCUR (X) VERSUS FREQUENCY - PERCENT (Y)



MISSION 1030A1 ~~TOP SECRET~~

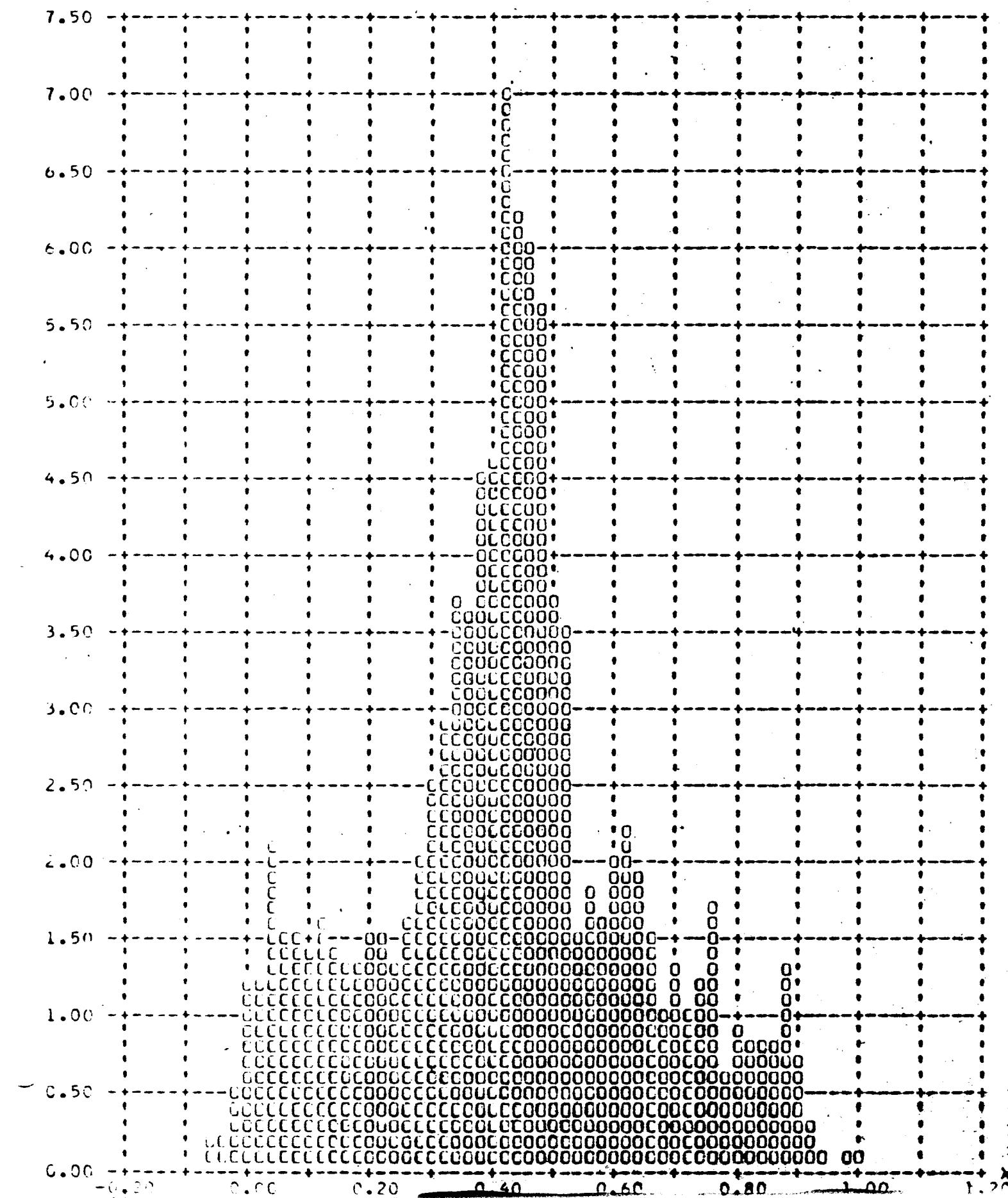
J-29 A-MEASURE FORWARD INSTRUME FRAMES 1-6 OF EACH OP OMITTED 90 PERCENT = 36.0

Y YAW RATE ERROR - DEG/FLUR (X) VERSUS FREQUENCY - PERCENT (Y)



29 B-BUCKET FORWARD INSTRUMEN FRAMES 1-6 OF EACH UP OMITTED 90 PERCENT = 0.70

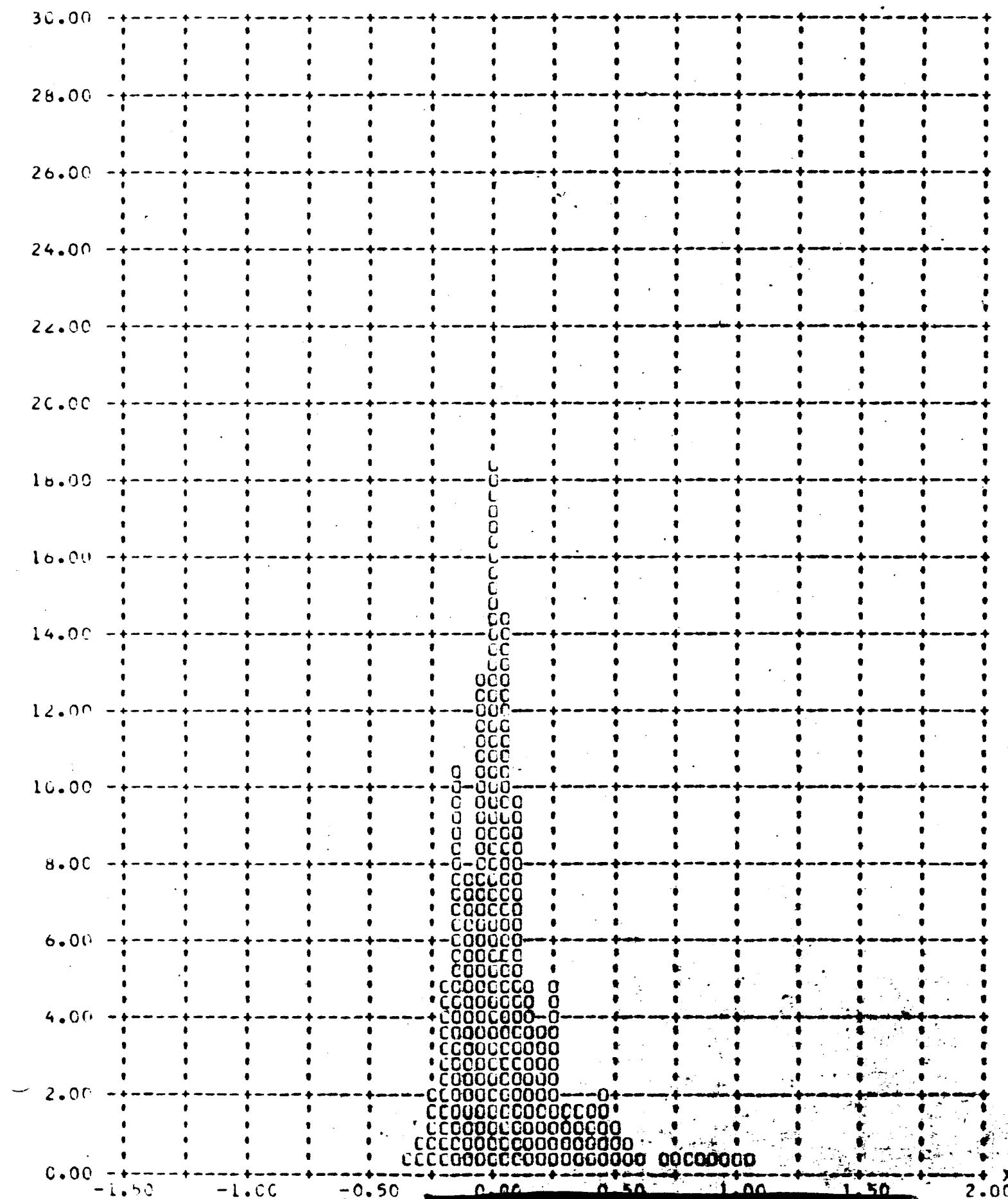
Y PITCH ANGLE ERROR - DEGREES (X) VERSUS FREQUENCY - PERCENT (Y)



MISSION 103081 ~~TOP SECRET~~

29 e-BUCKET FORWARD INSTRUMEN FRAMES 1-6 OF EACH OP OMITTED 90 PERCENT = .0.27

Y - ROLL ANGLE ERPCR - DEGREES (X) VERSUS FREQUENCY - PERCENT (Y)



Digitized by srujanika@gmail.com

MARION • 1030-1 • INSTRUMENT • FWNO

9/25/66 DENSITY FREQ DISTR

DENSITY PRIMARY INTERMEDIATE FULL ALL LEVELS  
Value MIN MAX LIM MIN MAX LIM MIN MAX LIM MIN MAX LIM

1. *Chlorophytum comosum* (L.) Willd. (Asparagaceae) (Fig. 1)

וְיִמְכַרְתָּם כֵּן כַּאֲשֶׁר־יָמַרְתָּ לְפָנֵינוּ בְּבָבְלָן

وَالْمُؤْمِنُونَ الْمُؤْمِنَاتُ وَالْمُؤْمِنُونَ الْمُؤْمِنَاتُ

وَالْمُؤْمِنُونَ الْمُؤْمِنَاتُ وَالْمُؤْمِنُونَ الْمُؤْمِنَاتُ

وَالْمُؤْمِنُونَ الْمُؤْمِنَاتُ وَالْمُؤْمِنُونَ الْمُؤْمِنَاتُ

وَمِنْهُمْ مَنْ يَرْجُو أَنْ يُنْصَتَ إِلَيْهِ مُؤْمِنًا وَمَنْ يَرْجُوا  
أَنْ يُنْكَثَ عَوْنَى وَمَنْ يَرْجُوا أَنْ يُنْكَثَ فَلَا يُنْكَثُ

وَالْمُؤْمِنُونَ الْمُؤْمِنَاتُ وَالْمُؤْمِنُونَ الْمُؤْمِنَاتُ

the first time in the history of the world that a man had been born who could not be controlled by any power on earth.

~~TOP SECRET~~ [REDACTED]

**REVIEW ARTICLE**

Table A-1

A-5

Table A-1

~~TOP SECRET~~ MISSION 1030-1 \* INSTRUMENT \* FRWD 8/25/66 DENSITY FREQ DISTR

QUALITY VALUES	PRIMARY		INTERMEDIATE		FULL		ALL LEVELS	
	MIN	MAX	MIN	MAX	MIN	MAX	MIN	MAX
• 51	0	1	0	1	0	1	0	1
• 52	0	1	0	1	0	1	0	1
• 53	0	1	0	1	0	1	0	1
• 54	0	1	0	1	0	1	0	1
• 55	0	1	0	1	0	1	0	1
• 56	0	1	0	1	0	1	0	1
• 57	0	1	0	1	0	1	0	1
• 58	0	1	0	1	0	1	0	1
• 59	0	1	0	1	0	1	0	1
• 60	0	1	0	1	0	1	0	1
• 61	0	1	0	1	0	1	0	1
• 62	0	1	0	1	0	1	0	1
• 63	0	1	0	1	0	1	0	1
• 64	0	1	0	1	0	1	0	1
• 65	0	1	0	1	0	1	0	1
• 66	0	1	0	1	0	1	0	1
• 67	0	1	0	1	0	1	0	1
• 68	0	1	0	1	0	1	0	1
• 69	0	1	0	1	0	1	0	1
• 70	0	1	0	1	0	1	0	1
• 71	0	1	0	1	0	1	0	1
• 72	0	1	0	1	0	1	0	1
• 73	0	1	0	1	0	1	0	1
• 74	0	1	0	1	0	1	0	1
• 75	0	1	0	1	0	1	0	1
• 76	0	1	0	1	0	1	0	1
• 77	0	1	0	1	0	1	0	1
• 78	0	1	0	1	0	1	0	1
• 79	0	1	0	1	0	1	0	1
• 80	0	1	0	1	0	1	0	1
• 81	0	1	0	1	0	1	0	1
• 82	0	1	0	1	0	1	0	1
• 83	0	1	0	1	0	1	0	1
• 84	0	1	0	1	0	1	0	1
• 85	0	1	0	1	0	1	0	1
• 86	0	1	0	1	0	1	0	1
• 87	0	1	0	1	0	1	0	1
• 88	0	1	0	1	0	1	0	1
• 89	0	1	0	1	0	1	0	1
• 90	0	1	0	1	0	1	0	1
• 91	0	1	0	1	0	1	0	1
• 92	0	1	0	1	0	1	0	1
• 93	0	1	0	1	0	1	0	1
• 94	0	1	0	1	0	1	0	1
• 95	0	1	0	1	0	1	0	1
• 96	0	1	0	1	0	1	0	1
• 97	0	1	0	1	0	1	0	1
• 98	0	1	0	1	0	1	0	1
• 99	0	1	0	1	0	1	0	1
SUM	1	1	1	1	1	1	1	1
TOTAL	1	1	127	127	102	117	117	106
							246	246
								210

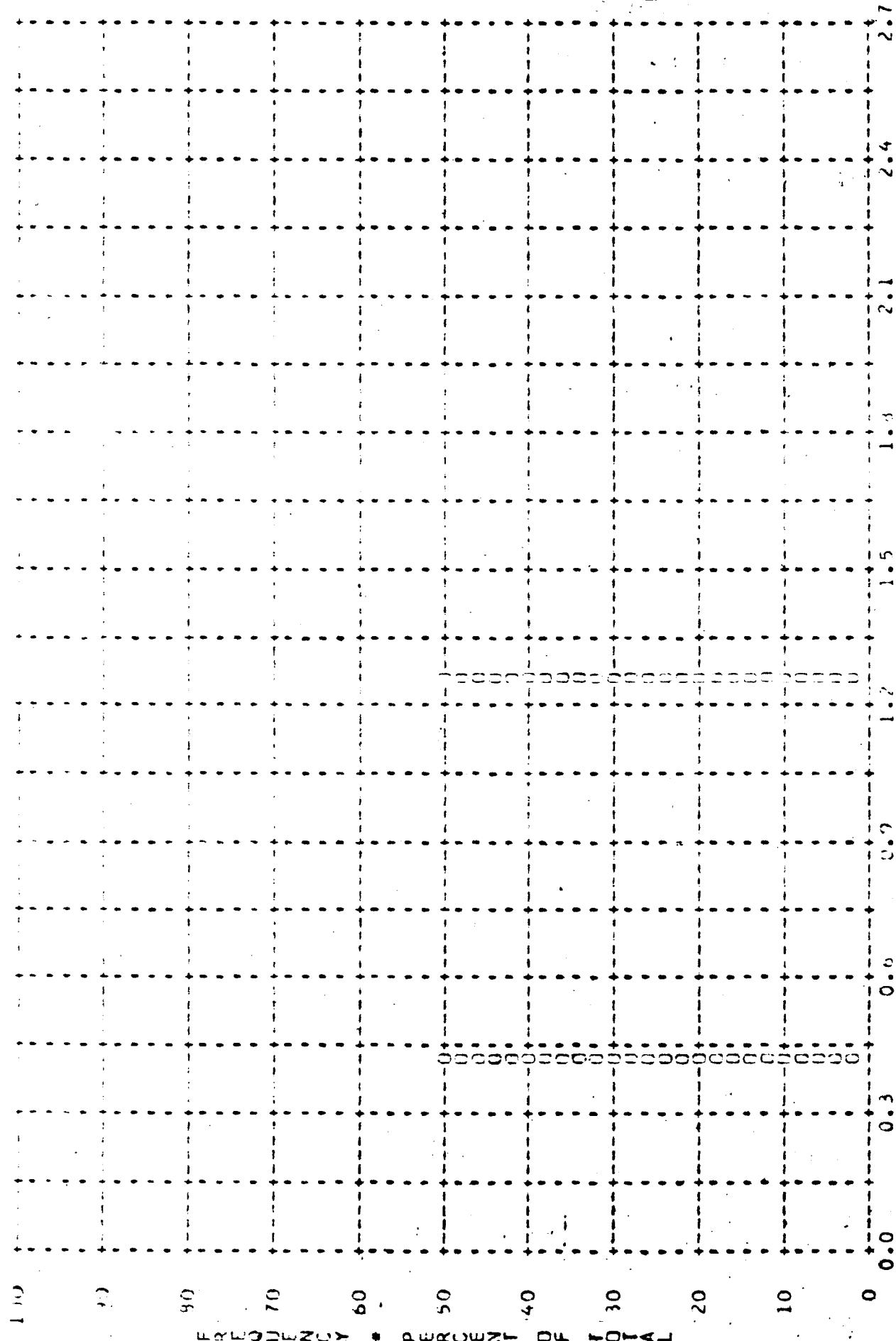
MISSION 1030-1 INSTR - FRWD 8/25/66 PROCESSING AND EXPOSURE ANALYSIS

PROJECT LEVEL	SAMPLE #	UNDER EXPOSED	UNDER PROCESSED	CORRECT EXP+PROC	OVER PROCESSED	OVER EXPOSED
PRIMARY	127	0 PC	0 PC	59 PC	0 PC	50 PC
INTERMEDIATE	127	0 PC	6 PC	59 PC	27 PC	3 PC
FULL	127	0 PC	0 PC	62 PC	23 PC	1 PC
ALL LEVELS	246	4 PC	3 PC	61 PC	28 PC	5 PC
PROJECT LEVEL	1030-1	UNDER EXPOSED	UNDER PROCESSED	CORRECT EXP+PROC	OVER PROCESSED	OVER EXPOSED
PRIMARY	0.01-0.19	0.01-0.3	0.14-0.39	0.40-0.99	-----	0.91 AND UP
INTERMEDIATE	0.01-0.17	0.01-0.25	0.21-0.39	0.40-0.99	0.91-1.34	1.05 AND UP
FULL	0.1-1.00	0.01-0.49	-----	0.40-0.99	0.91-1.57	1.75 AND UP

Table A-1

PERCENT OF INTEGRITY \* DENSITY \*

ALL 4000 VOTES FROM 1960 & 1964 STUDENTS



TOP SECRET

Figure A-1

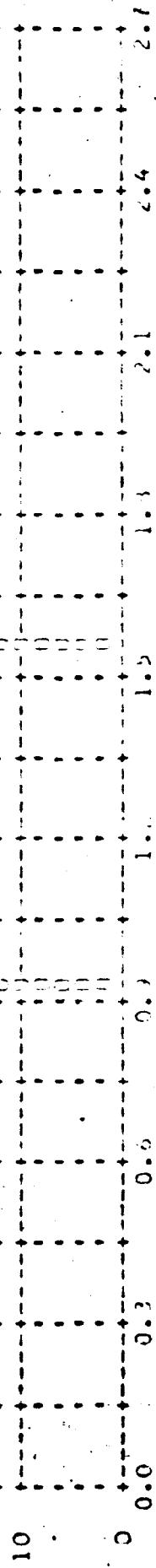
PERCENT OF POLYMER \* DENSITY \* POLYMER

ART 4 M: A4 = 1.03 & M: B4 = 1.00 & M: C4 = 1.00 & M: D4 = 1.00 & M: E4 = 1.00

100  
80  
60  
40  
20  
0

PERCENT  
POLYMER

A-8



MISSION • 17-49-1 • 1961-01-06 • 1300 • 0.5 MV • 0.045 • PRIMARY  
ADDITIONS • 1.17 • MEAN • 1.33 • THERM • 0.60 • WHICH IS 1.7 IN TABS AND 2 SAMPLES

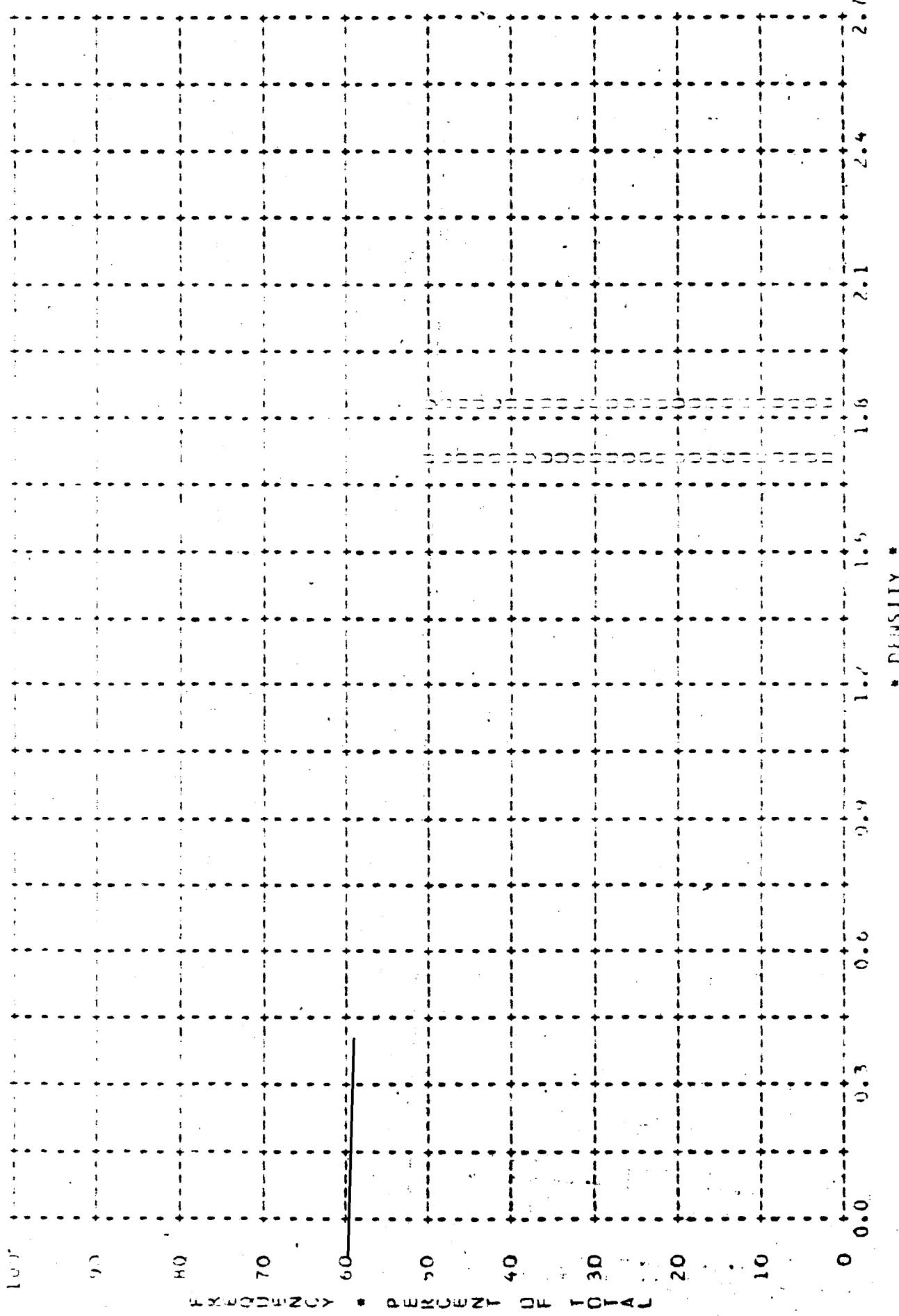


Figure A-3

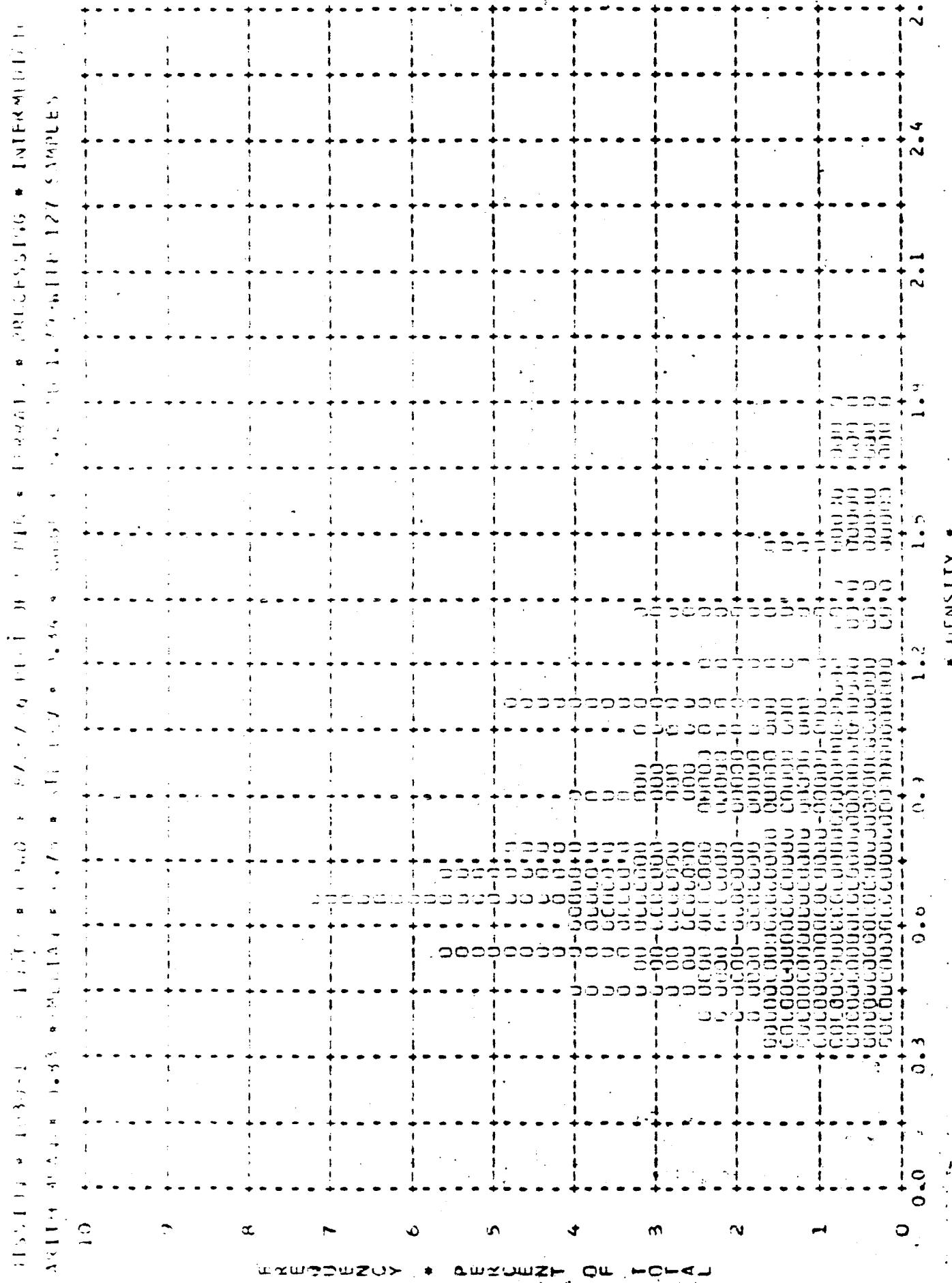


Figure A-9

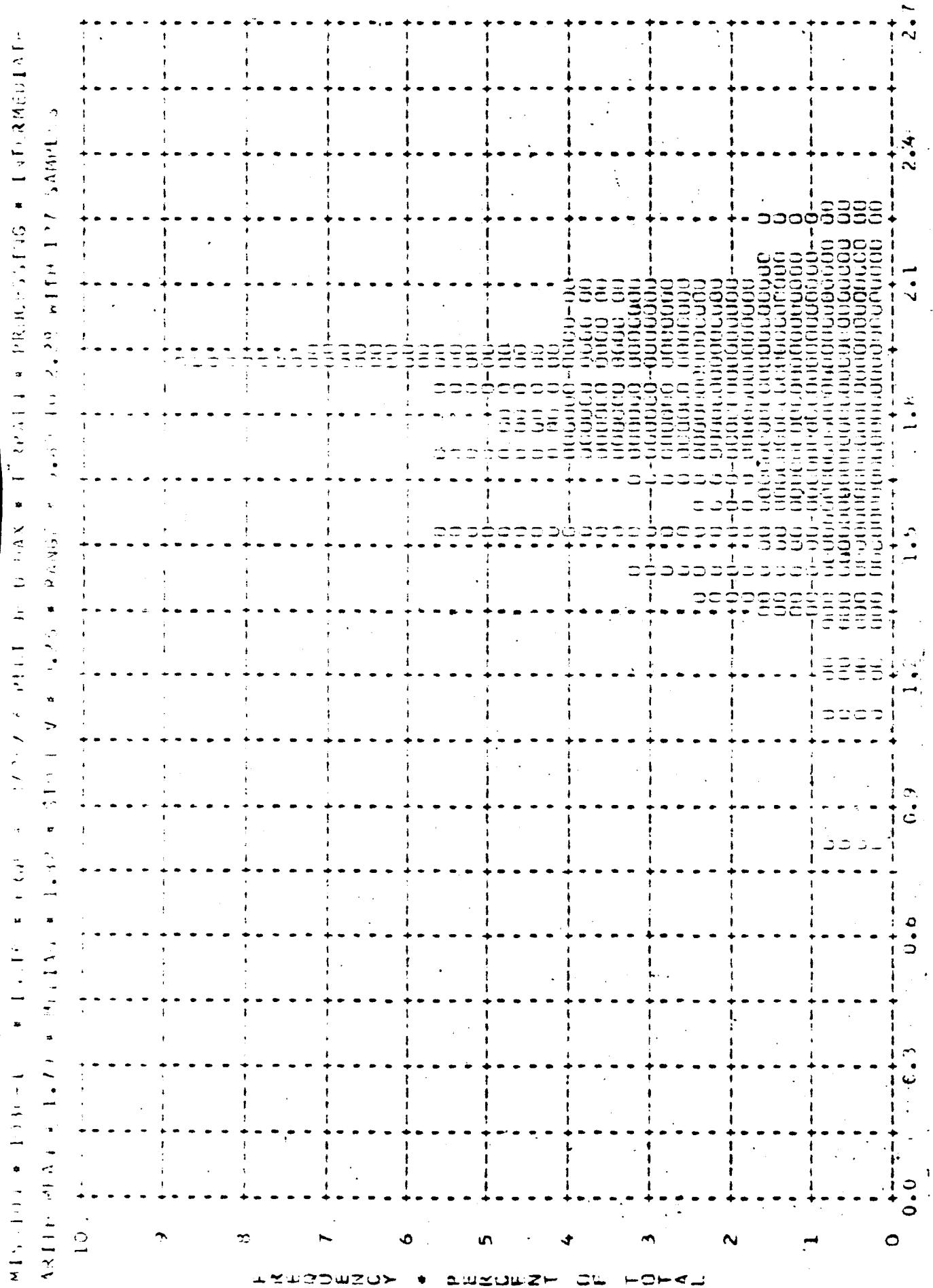
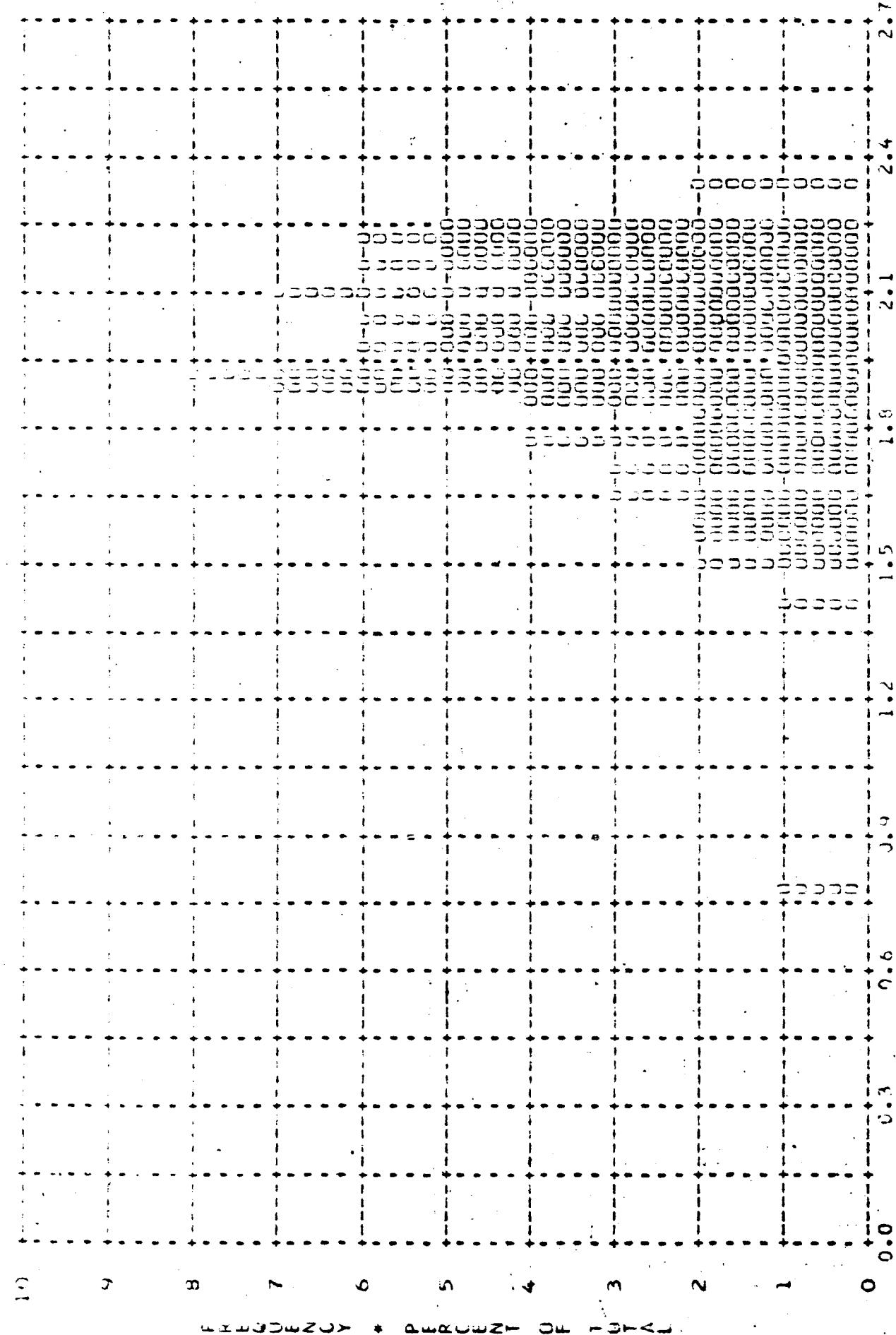


Figure A-5

FIGURE A-6. EFFECT OF EXPOSURE AND RADIATION PROCESSING ON DENSITY \* INTERMITTENCY

EXPOSED AT 1.04 & 2.04 MRAD/HR. FOR 10 HRS. IN 100°C. OVEN. 100% SAMPLES.



PERCENTAGE OF TOTAL NUMBER OF INDIVIDUALS IN EACH DENSITY CLASS

ASIDE MEAN DENSITY = 0.5175 INDIVIDUALS PER UNIT AREA

10

9

8

7

6

5

4

3

2

1

0

FREQUENCY \* PERCENT OF TOTAL

A-12

\* DENSITY \*

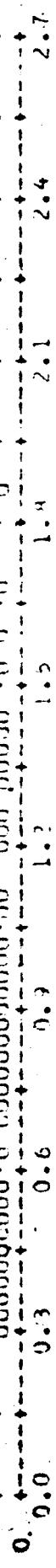


Figure A-7

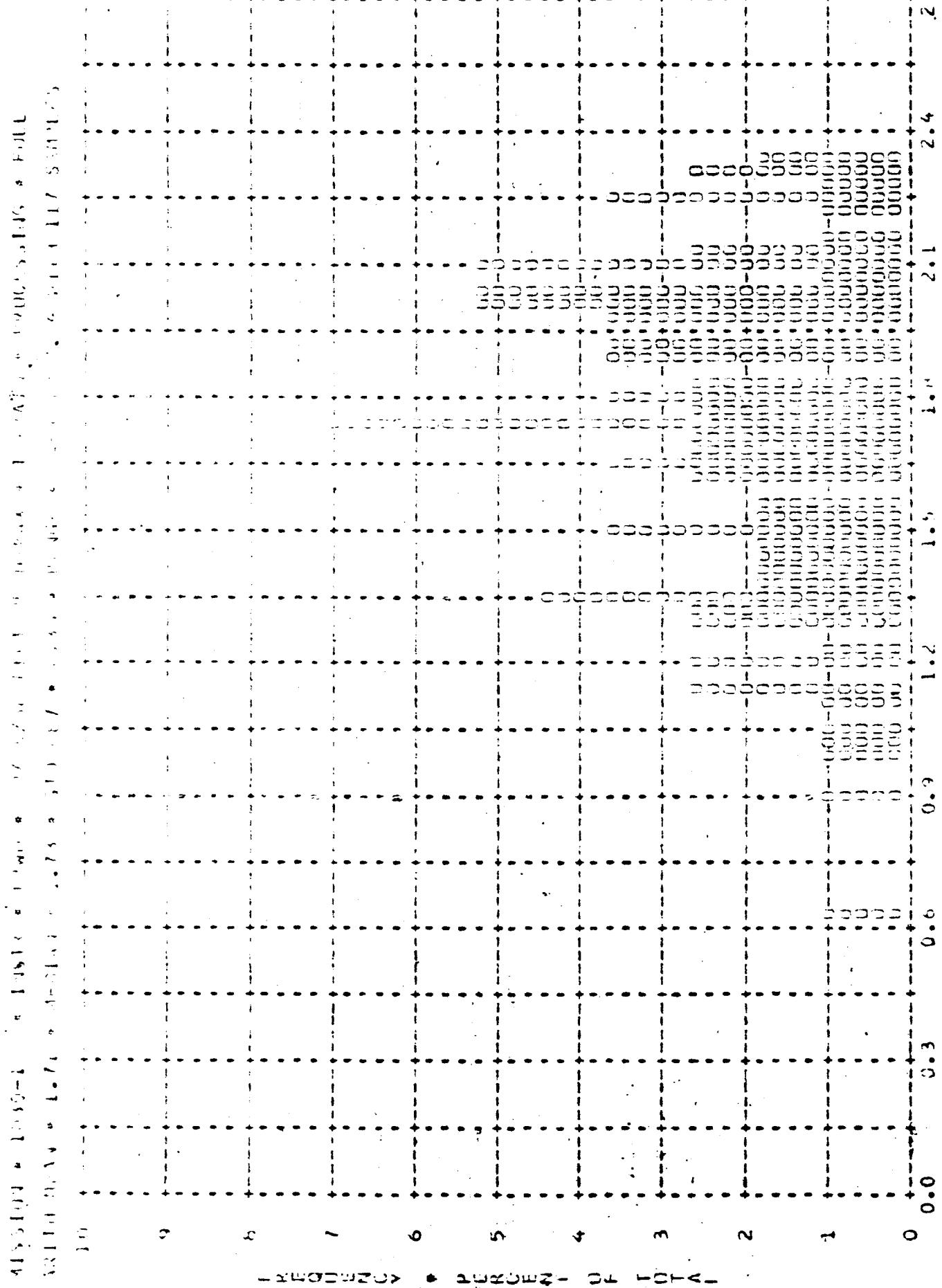


Figure A-8

~~TOP SECRET~~

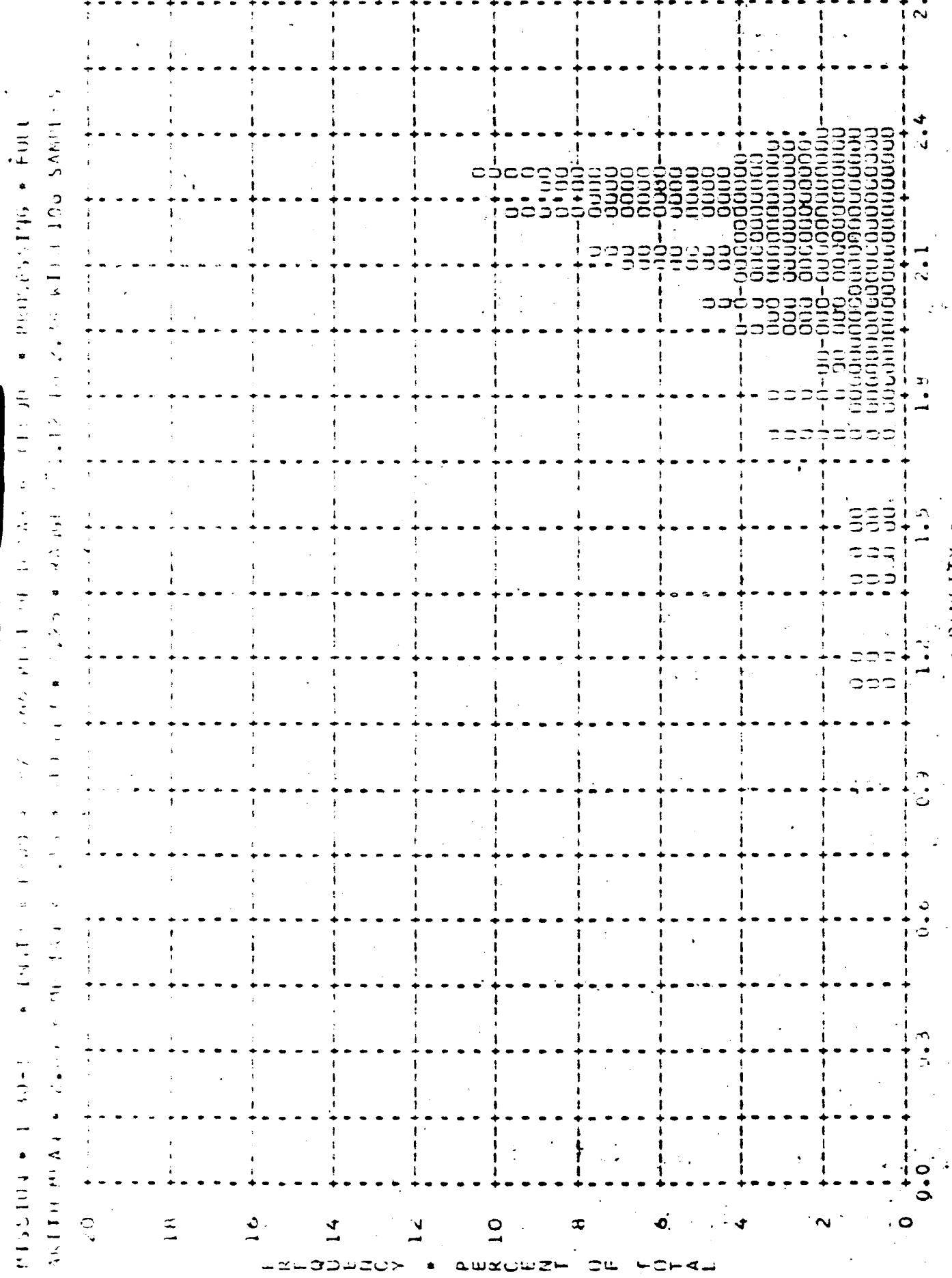
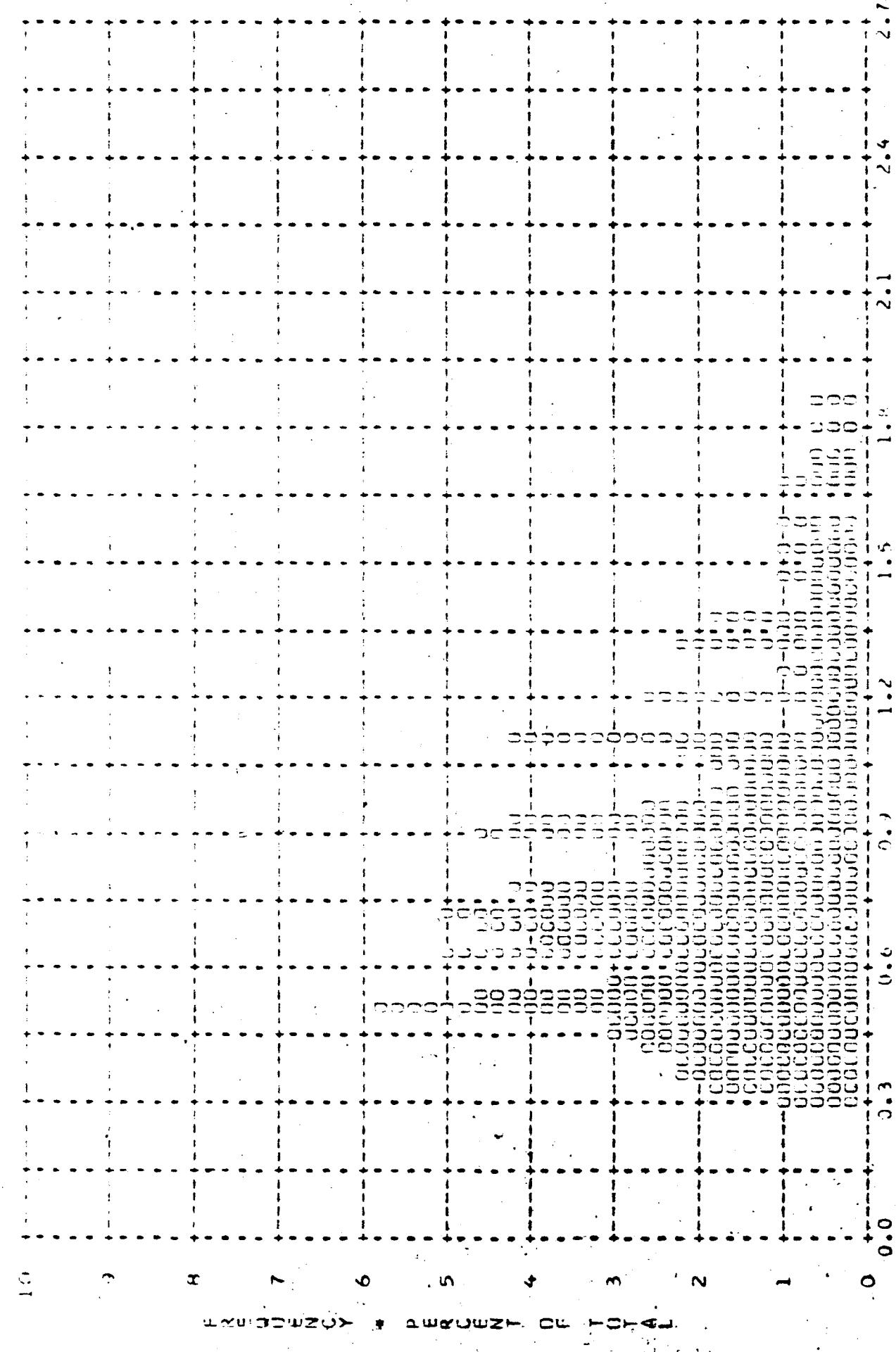


Figure A-9

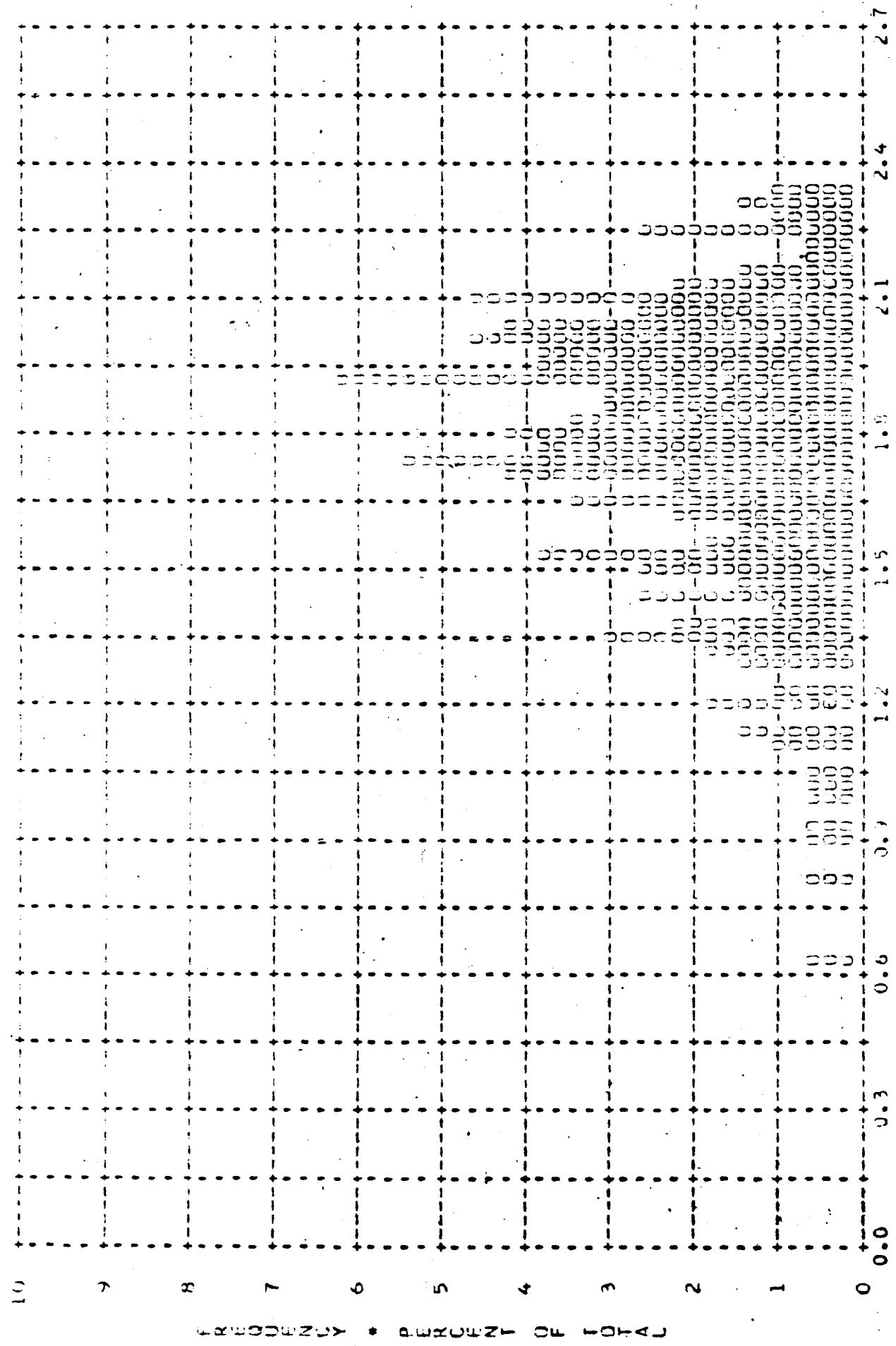
FIGURE A-10. Effect of Density on Productivity - All Units



A-15

Figure A-10

MINIMUM \* 1.0300 \* MAXIMUM \* 2.7000 \* MEAN \* 1.71 \* SD \* .36 \* RANGE \* 0.61 To 2.54 WITH 246 SAMPLES



TOP SECRET

Figure A-11

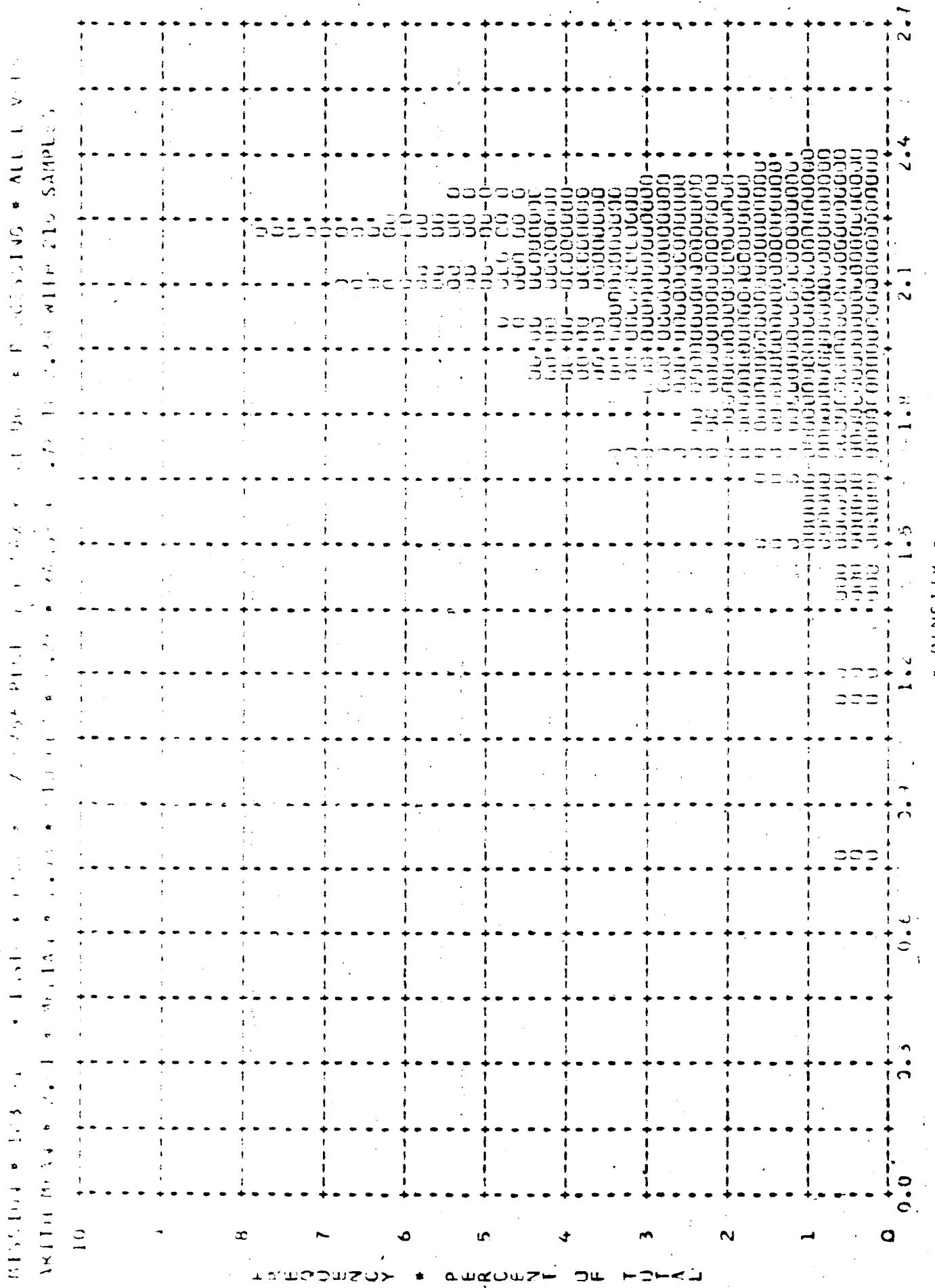


Figure A-12

\* 101 \* 15 NOV \* INSTRUMENT \* AFT

8/25/66 DENSITY FREQ DISTR.

**COLLEGE LIBRARY ENRICHMENT**

**FULL**            **ALL LEVELS**  
**MIN MAX LIM**    **MIN MAX LIM**

44  
43  
36  
33  
33  
32  
31  
30  
29  
28  
27  
26  
25  
24  
23  
22  
21  
20  
19  
18  
17  
16  
15  
14  
13  
12  
11  
10  
9  
8  
7  
6  
5  
4  
3  
2  
1

SCHEDE DI DOCUMENTAZIONE

8110 NCSCN0000000000000000

گلستانهای ادبی و فلسفی ایرانی

Table A-2

TOP SECRET

MISSION # 1934-1 INSTRUMENT # AFT

8/25/66 DENSITY FREQ DISTR

DENSITY	PRIMARY VALUE	MIN MAX LIM	INTERMEDIATE MIN MAX LIM
---------	------------------	-------------	-----------------------------

FULL : ALL LEVELS  
MIN MAX LIM : MIN MAX LIM

0.0.52  
0.0.53  
0.0.54  
0.0.55  
0.0.56  
0.0.57  
0.0.58  
0.0.59  
0.0.60  
0.0.61  
0.0.62  
0.0.63  
0.0.64  
0.0.65  
0.0.66  
0.0.67  
0.0.68  
0.0.69  
0.0.70  
0.0.71  
0.0.72  
0.0.73  
0.0.74  
0.0.75  
0.0.76  
0.0.77  
0.0.78  
0.0.79  
0.0.80  
0.0.81  
0.0.82  
0.0.83  
0.0.84  
0.0.85  
0.0.86  
0.0.87  
0.0.88  
0.0.89  
0.0.90  
0.0.91  
0.0.92  
0.0.93  
0.0.94  
0.0.95  
0.0.96  
0.0.97  
0.0.98  
0.0.99  
0.0.100

એ એ એ એ એ એ એ એ એ એ એ એ એ એ એ એ એ એ એ એ એ એ એ

תְּנַדֵּן כִּי-בָּאָה בְּעֵמֶת וְבָאָה בְּעֵמֶת

ପ୍ରକାଶନ କମିଶନ ଦ୍ୱାରା ମୁଦ୍ରଣ କରାଯାଇଥିଲା ଏହା ପରିଚୟ ପତ୍ର

oooooooooooooooooooooooooooooooooooooooooooooooooooo

2  
1  
2  
4  
9  
6  
5  
2  
4  
6  
3  
3  
4  
4  
8  
3  
1  
0  
4  
4  
6  
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2  
4  
4  
2  
3  
3  
4  
3  
2  
1  
1  
4  
1  
1  
1  
3  
5  
5  
1  
1  
2  
4  
1  
1  
0  
0  
0  
7

ପ୍ରକାଶକ ପରିଷଦଙ୍କ ମହାନ୍ ପତ୍ର ପରିଚୟ

**Table A-2**

MISSION: 1730- • INSTRUMENT • AFT E/25/66 DENSITY FREQ DISTR.

Table A-2

MISSION # 1136-2 \* INSTRUMENT # AFT 8/25/68 DENSITY FREQ DISTR

ALL LEVELS	MAX FIN LIM	FULL FIN MAX LTM	IMMEDIATE FIN MAX LTM	PRIMINARY FIN MAX LIM	ALL LEVELS
14.5	14.5	14.5	14.5	14.5	14.5
14.0	14.0	14.0	14.0	14.0	14.0
13.5	13.5	13.5	13.5	13.5	13.5
13.0	13.0	13.0	13.0	13.0	13.0
12.5	12.5	12.5	12.5	12.5	12.5
12.0	12.0	12.0	12.0	12.0	12.0
11.5	11.5	11.5	11.5	11.5	11.5
11.0	11.0	11.0	11.0	11.0	11.0
10.5	10.5	10.5	10.5	10.5	10.5
10.0	10.0	10.0	10.0	10.0	10.0
9.5	9.5	9.5	9.5	9.5	9.5
9.0	9.0	9.0	9.0	9.0	9.0
8.5	8.5	8.5	8.5	8.5	8.5
8.0	8.0	8.0	8.0	8.0	8.0
7.5	7.5	7.5	7.5	7.5	7.5
7.0	7.0	7.0	7.0	7.0	7.0
6.5	6.5	6.5	6.5	6.5	6.5
6.0	6.0	6.0	6.0	6.0	6.0
5.5	5.5	5.5	5.5	5.5	5.5
5.0	5.0	5.0	5.0	5.0	5.0
4.5	4.5	4.5	4.5	4.5	4.5
4.0	4.0	4.0	4.0	4.0	4.0
3.5	3.5	3.5	3.5	3.5	3.5
3.0	3.0	3.0	3.0	3.0	3.0
2.5	2.5	2.5	2.5	2.5	2.5
2.0	2.0	2.0	2.0	2.0	2.0
1.5	1.5	1.5	1.5	1.5	1.5
1.0	1.0	1.0	1.0	1.0	1.0
0.5	0.5	0.5	0.5	0.5	0.5
0.0	0.0	0.0	0.0	0.0	0.0

卷之三

**Table A-2**



31-111-12 130-1

1030-1 \* INSTRUMENT \* AFT 9/25/66 DENSITY FREQ DISTR

EPA-2015-0250 | INDEX - AEE | 173501 | BUSINESS AND EXPOSURE ANALYSIS

PROJECT LEVEL	NAME	UNDER EXPOSED	UNDER PROCESSED	CORRECT EXF+PROC	OVER PROCESSED	OVER EXPOSED
PRIMARY INTERMEDIATE FILE	173	3 PC	12 PC	65 PC	17 PC	6 PC
ALL LEVELS	243	11 PC	9 PC	64 PC	22 PC	4 PC
PROJECT LEVEL	BASE	UNDER EXPOSED	UNDER PROCESSED	CORRECT EXF+PROC	OVER PROCESSED	OVER EXPOSED
PRIMARY INTERMEDIATE FILE	0.31-0.39	0.21-0.12	0.14-0.39	0.48-0.39	-----	0.31 AND UP

Table A-2

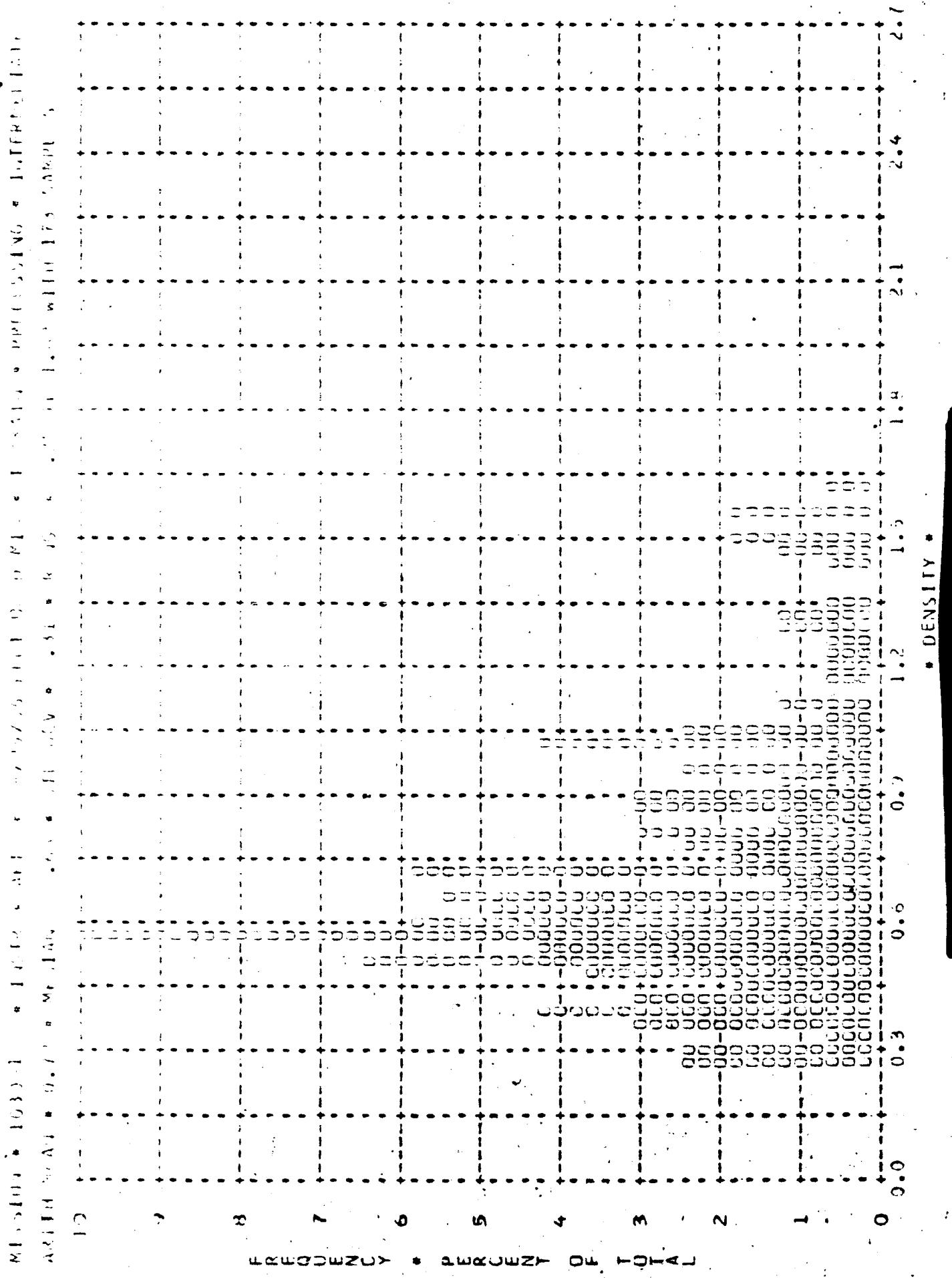
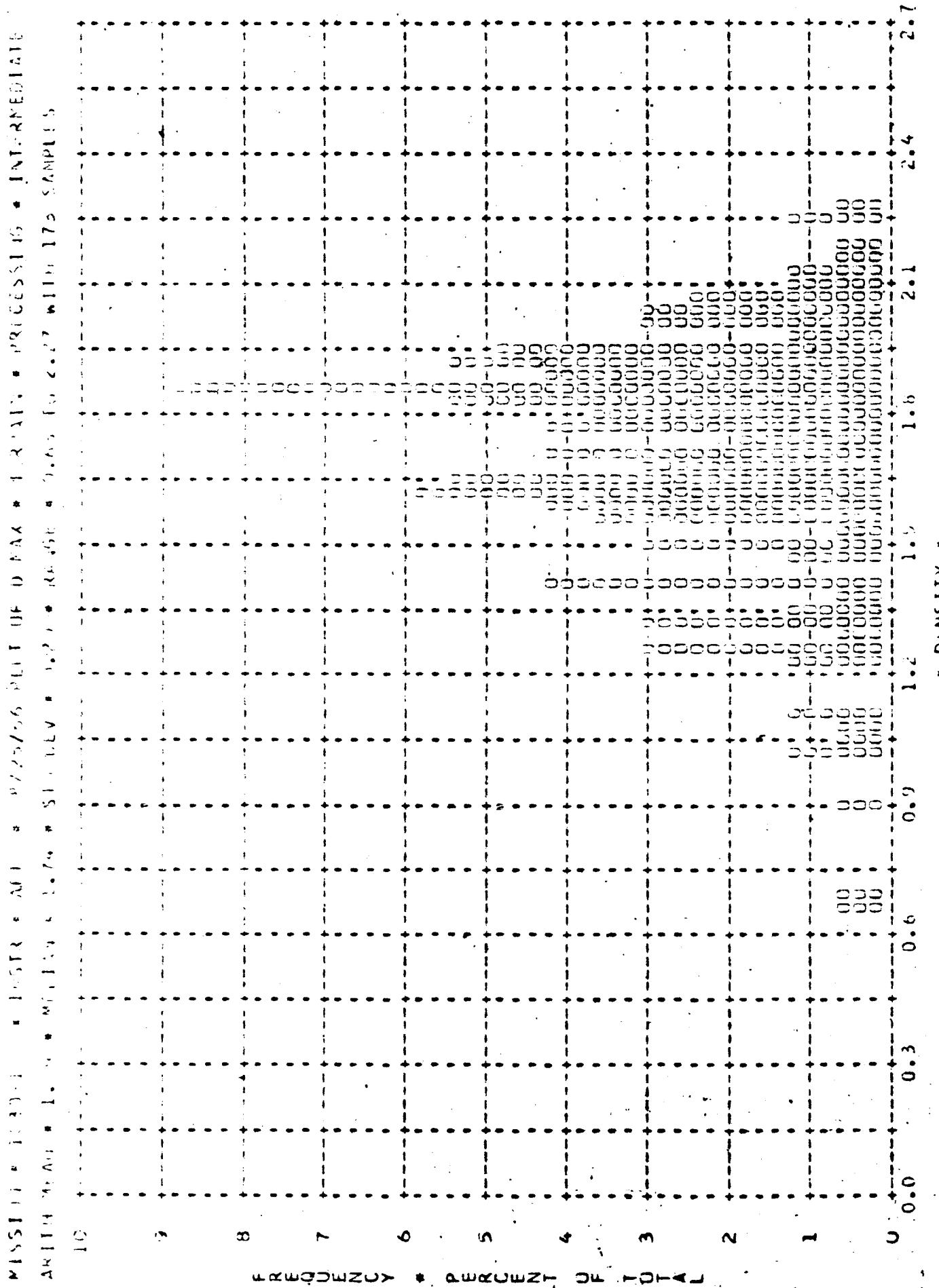
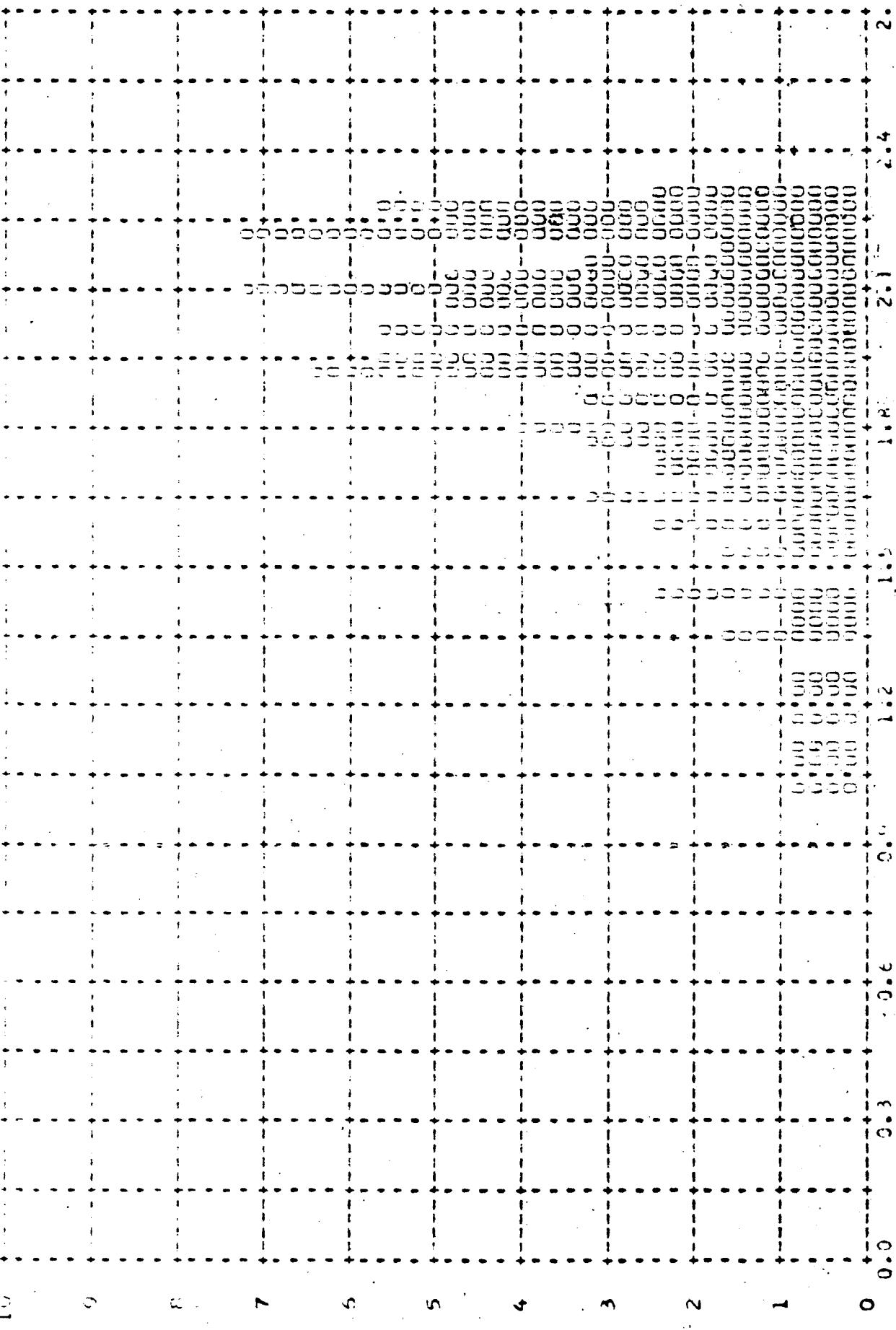


Figure A-13



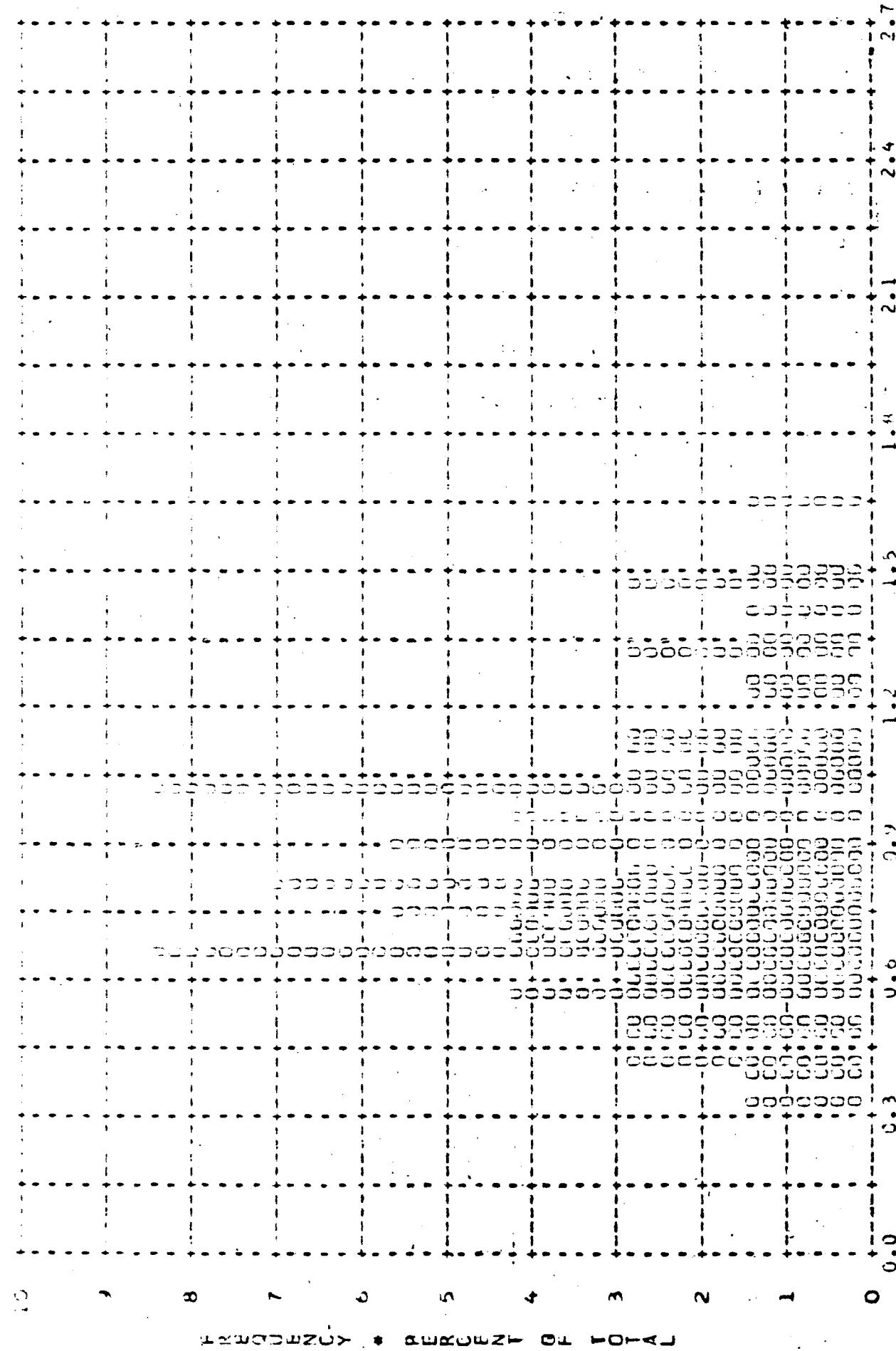
1000 \* 1000 \* 1000 \* 1000 \* 1000 \* 1000 \* 1000 \* 1000 \* 1000 \* 1000 \* 1000

1000 \* 1000 \* 1000 \* 1000 \* 1000 \* 1000 \* 1000 \* 1000 \* 1000 \* 1000 \* 1000



TOP OF MAXIMUM • COUNTS PER UNIT

REF ID: A110141  
MATERIAL TESTS \* POLYACRYLIC ACID \* 100% CONCENTRATION \* PRECIPITATION \* FULL



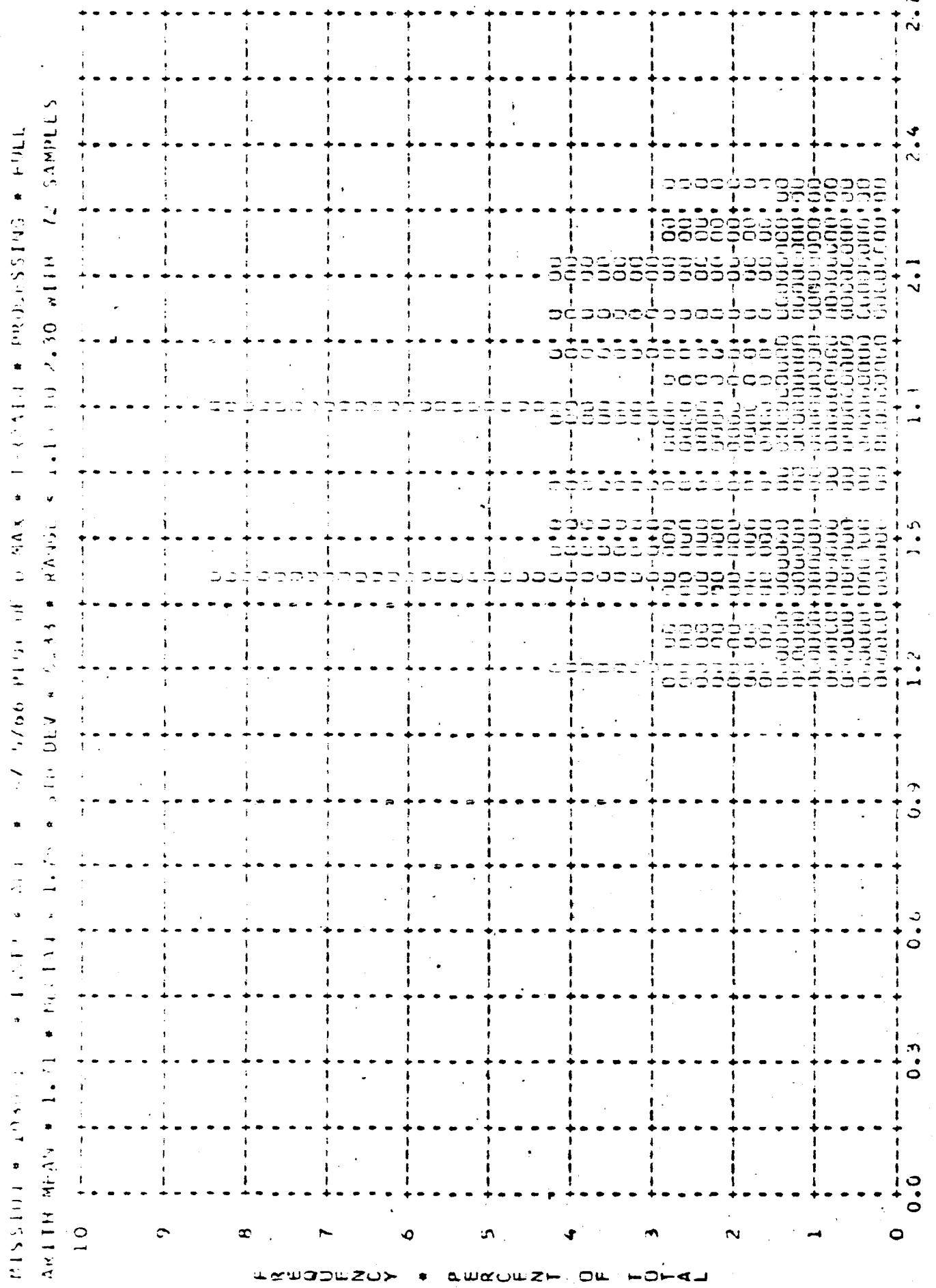


Figure A-17

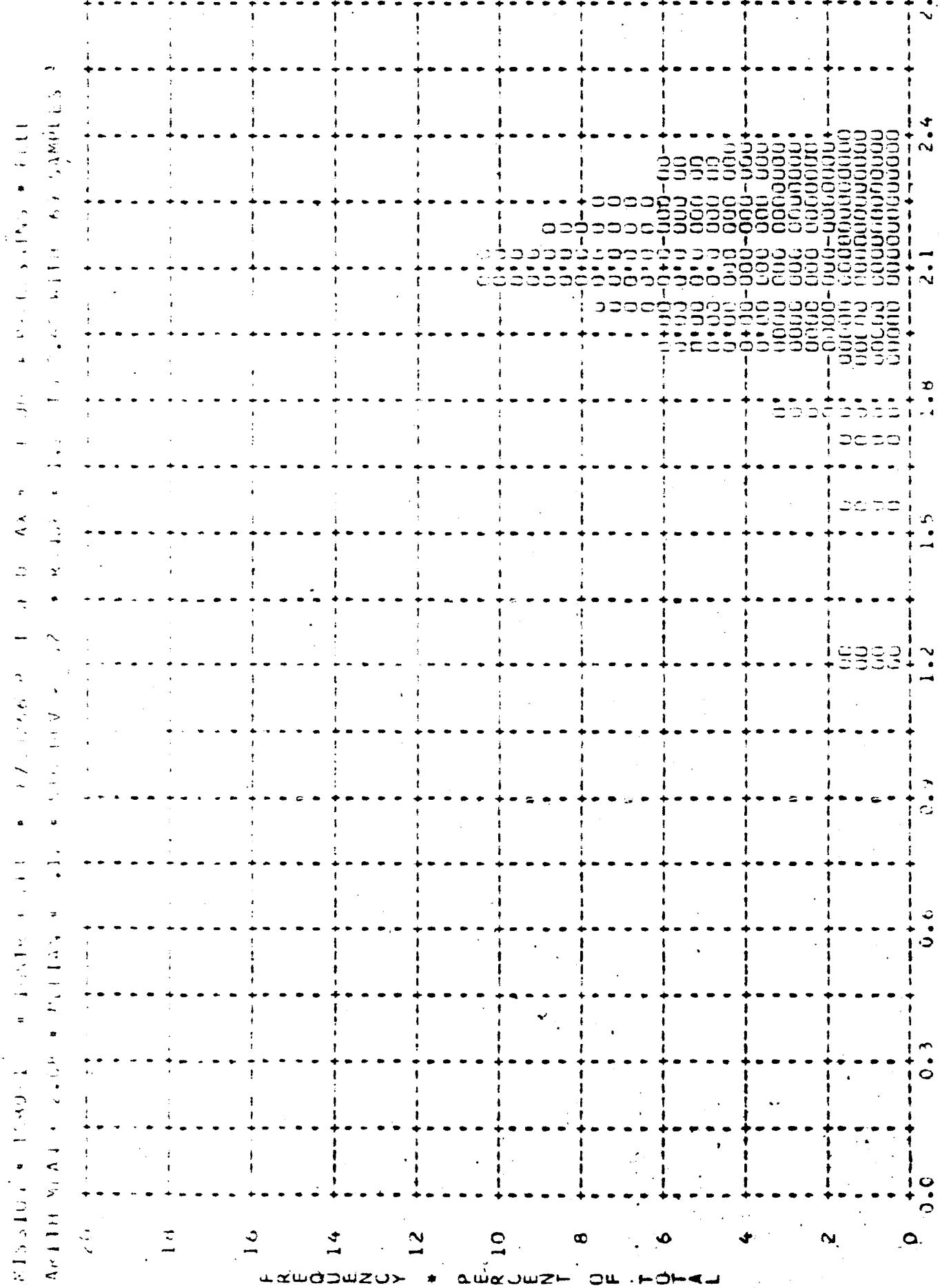
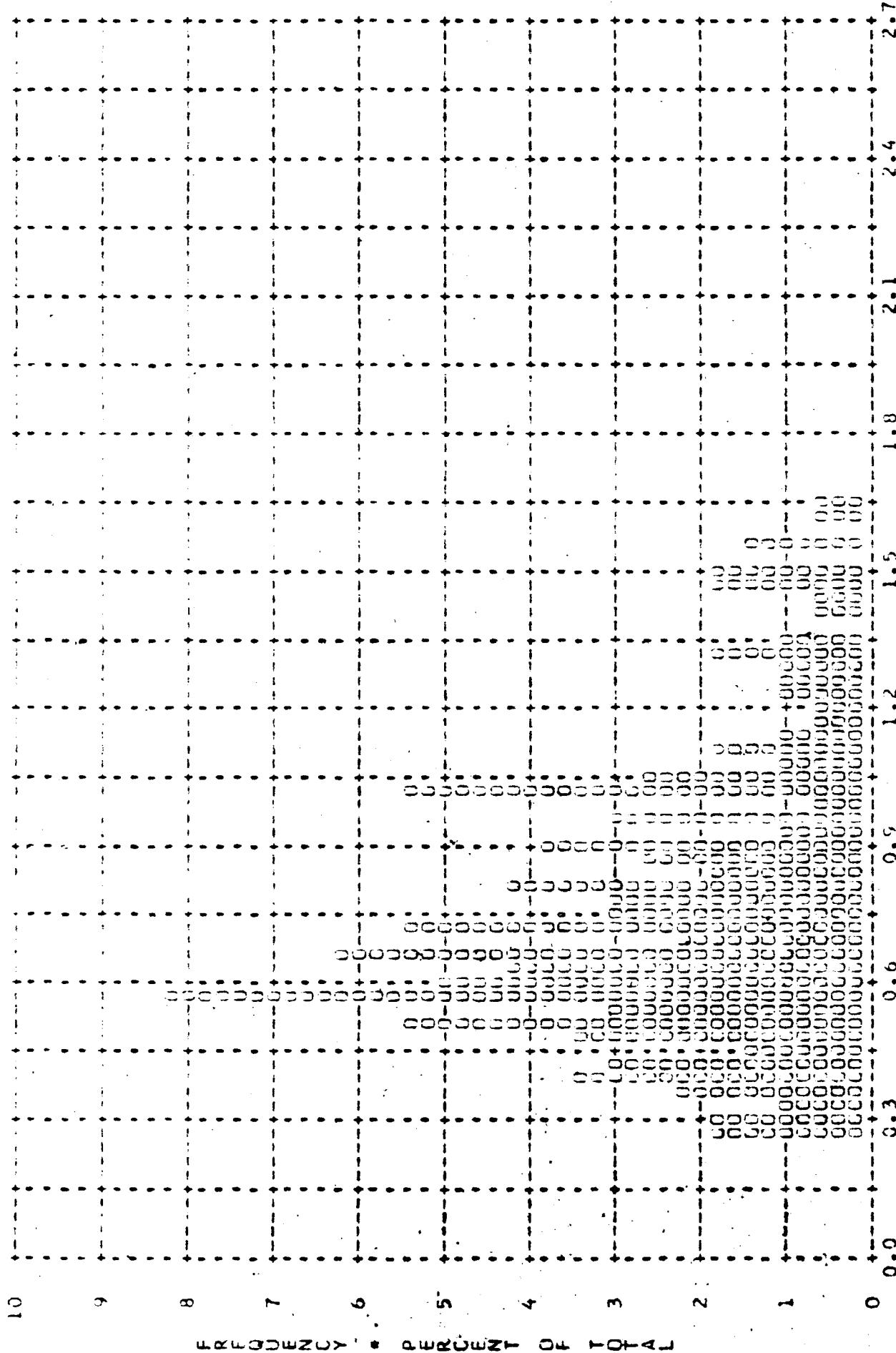


Figure A-18

MISSOURI \* IOWA \* KANSAS \* NEBRASKA \* SOUTH DAKOTA \* NORTH DAKOTA \* MONTANA

APRIL 1946 \* 6.76 P.M. EST \* 5.60 DFV \* 0.31 \* DATA FROM 1000 LBS. WITH 160 SAMPLES



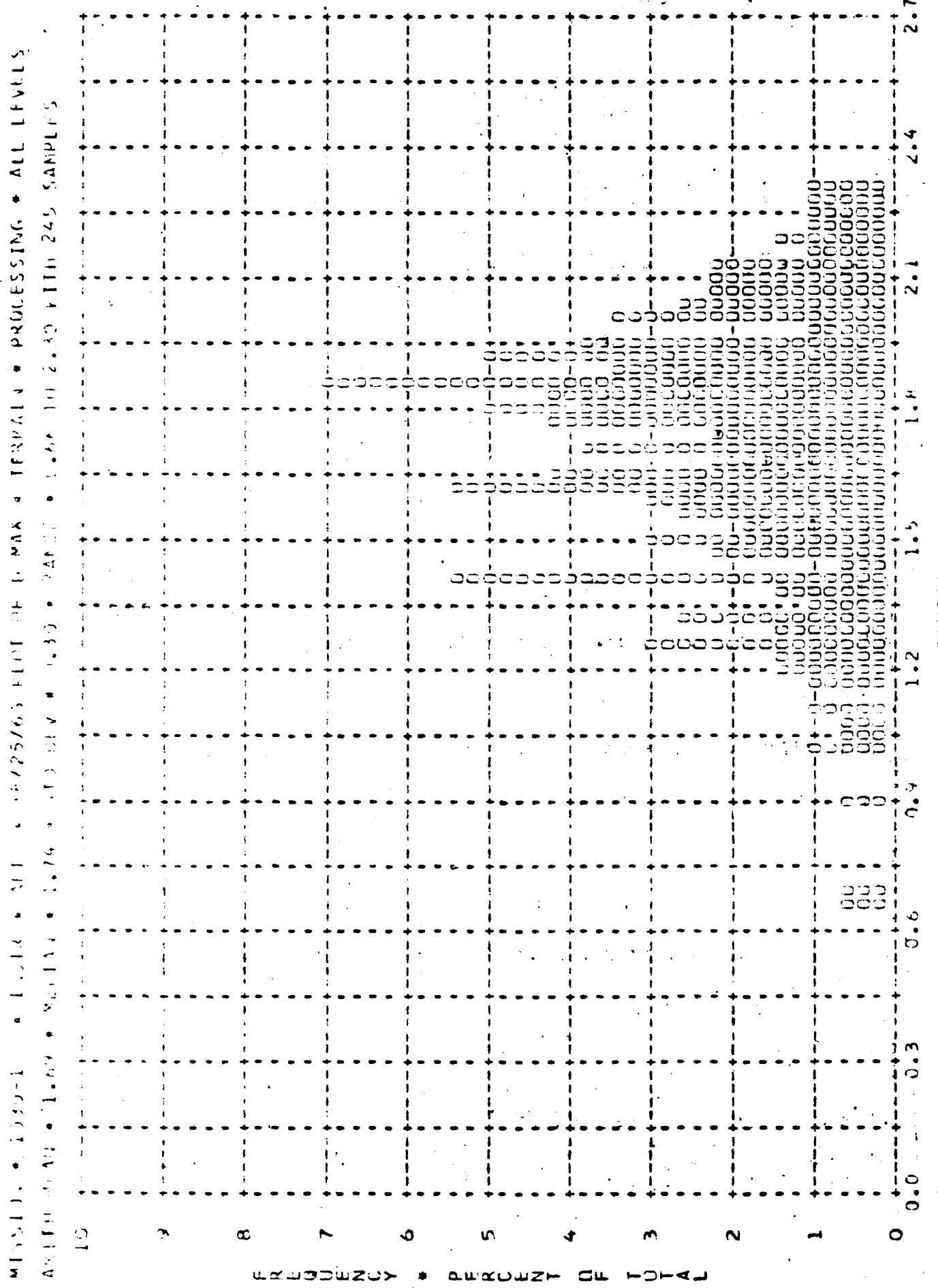


Figure A-20

SECRET

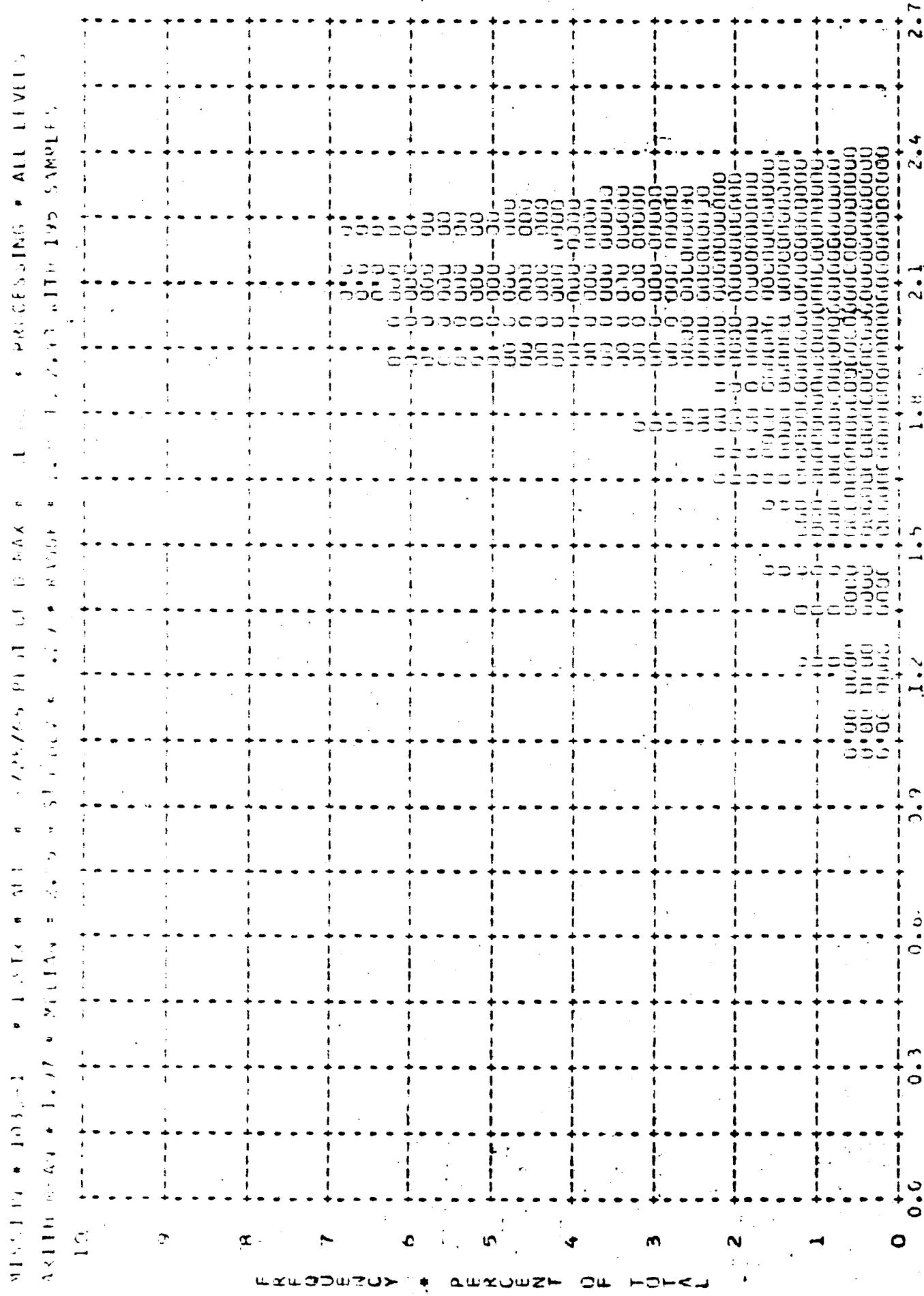


Figure A-21

~~TOP SECRET~~

MISSION # 123-1-2		INSTRUMENT # FRWD		8/25/66	DENSITY FREQ DISTR		
DENSITY VALUE	PRIMARY MIN MAX LIM	INTERMEDIATE MIN MAX LIM	FULL MIN MAX LIM		ALL LEVELS MIN MAX LIM		
6.0	6.0 6.0	6.0 6.0	6.0 6.0	6.0 6.0	6.0 6.0	6.0 6.0	
6.1	6.1 6.1	6.1 6.1	6.1 6.1	6.1 6.1	6.1 6.1	6.1 6.1	
6.2	6.2 6.2	6.2 6.2	6.2 6.2	6.2 6.2	6.2 6.2	6.2 6.2	
6.3	6.3 6.3	6.3 6.3	6.3 6.3	6.3 6.3	6.3 6.3	6.3 6.3	
6.4	6.4 6.4	6.4 6.4	6.4 6.4	6.4 6.4	6.4 6.4	6.4 6.4	
6.5	6.5 6.5	6.5 6.5	6.5 6.5	6.5 6.5	6.5 6.5	6.5 6.5	
6.6	6.6 6.6	6.6 6.6	6.6 6.6	6.6 6.6	6.6 6.6	6.6 6.6	
6.7	6.7 6.7	6.7 6.7	6.7 6.7	6.7 6.7	6.7 6.7	6.7 6.7	
6.8	6.8 6.8	6.8 6.8	6.8 6.8	6.8 6.8	6.8 6.8	6.8 6.8	
6.9	6.9 6.9	6.9 6.9	6.9 6.9	6.9 6.9	6.9 6.9	6.9 6.9	
7.0	7.0 7.0	7.0 7.0	7.0 7.0	7.0 7.0	7.0 7.0	7.0 7.0	
7.1	7.1 7.1	7.1 7.1	7.1 7.1	7.1 7.1	7.1 7.1	7.1 7.1	
7.2	7.2 7.2	7.2 7.2	7.2 7.2	7.2 7.2	7.2 7.2	7.2 7.2	
7.3	7.3 7.3	7.3 7.3	7.3 7.3	7.3 7.3	7.3 7.3	7.3 7.3	
7.4	7.4 7.4	7.4 7.4	7.4 7.4	7.4 7.4	7.4 7.4	7.4 7.4	
7.5	7.5 7.5	7.5 7.5	7.5 7.5	7.5 7.5	7.5 7.5	7.5 7.5	
7.6	7.6 7.6	7.6 7.6	7.6 7.6	7.6 7.6	7.6 7.6	7.6 7.6	
7.7	7.7 7.7	7.7 7.7	7.7 7.7	7.7 7.7	7.7 7.7	7.7 7.7	
7.8	7.8 7.8	7.8 7.8	7.8 7.8	7.8 7.8	7.8 7.8	7.8 7.8	
7.9	7.9 7.9	7.9 7.9	7.9 7.9	7.9 7.9	7.9 7.9	7.9 7.9	
8.0	8.0 8.0	8.0 8.0	8.0 8.0	8.0 8.0	8.0 8.0	8.0 8.0	
8.1	8.1 8.1	8.1 8.1	8.1 8.1	8.1 8.1	8.1 8.1	8.1 8.1	
8.2	8.2 8.2	8.2 8.2	8.2 8.2	8.2 8.2	8.2 8.2	8.2 8.2	
8.3	8.3 8.3	8.3 8.3	8.3 8.3	8.3 8.3	8.3 8.3	8.3 8.3	
8.4	8.4 8.4	8.4 8.4	8.4 8.4	8.4 8.4	8.4 8.4	8.4 8.4	
8.5	8.5 8.5	8.5 8.5	8.5 8.5	8.5 8.5	8.5 8.5	8.5 8.5	
8.6	8.6 8.6	8.6 8.6	8.6 8.6	8.6 8.6	8.6 8.6	8.6 8.6	
8.7	8.7 8.7	8.7 8.7	8.7 8.7	8.7 8.7	8.7 8.7	8.7 8.7	
8.8	8.8 8.8	8.8 8.8	8.8 8.8	8.8 8.8	8.8 8.8	8.8 8.8	
8.9	8.9 8.9	8.9 8.9	8.9 8.9	8.9 8.9	8.9 8.9	8.9 8.9	
9.0	9.0 9.0	9.0 9.0	9.0 9.0	9.0 9.0	9.0 9.0	9.0 9.0	
9.1	9.1 9.1	9.1 9.1	9.1 9.1	9.1 9.1	9.1 9.1	9.1 9.1	
9.2	9.2 9.2	9.2 9.2	9.2 9.2	9.2 9.2	9.2 9.2	9.2 9.2	
9.3	9.3 9.3	9.3 9.3	9.3 9.3	9.3 9.3	9.3 9.3	9.3 9.3	
9.4	9.4 9.4	9.4 9.4	9.4 9.4	9.4 9.4	9.4 9.4	9.4 9.4	
9.5	9.5 9.5	9.5 9.5	9.5 9.5	9.5 9.5	9.5 9.5	9.5 9.5	
9.6	9.6 9.6	9.6 9.6	9.6 9.6	9.6 9.6	9.6 9.6	9.6 9.6	
9.7	9.7 9.7	9.7 9.7	9.7 9.7	9.7 9.7	9.7 9.7	9.7 9.7	
9.8	9.8 9.8	9.8 9.8	9.8 9.8	9.8 9.8	9.8 9.8	9.8 9.8	
9.9	9.9 9.9	9.9 9.9	9.9 9.9	9.9 9.9	9.9 9.9	9.9 9.9	
10.0	10.0 10.0	10.0 10.0	10.0 10.0	10.0 10.0	10.0 10.0	10.0 10.0	

~~TOP SECRET~~

Table A-3



Digitized by Google

• DESIGN • 1930-1 • INSTRUMENT • FBHD • 8/25/66 • DENSITY FREE DISPL.

~~TOP SECRET~~

Table A-3

卷之三

MISSION = 100-2    INSTRUMENT = FRWD    8/25/66    DENSITY-FREQ DISTR

8/25/66 DENSITY-FREQ DISTR

**Table A-3**

MISSION # 1930-2 \* INSTRUMENT # FR4D E/25/06 DENSITY FREQ DISTR

Table A-3

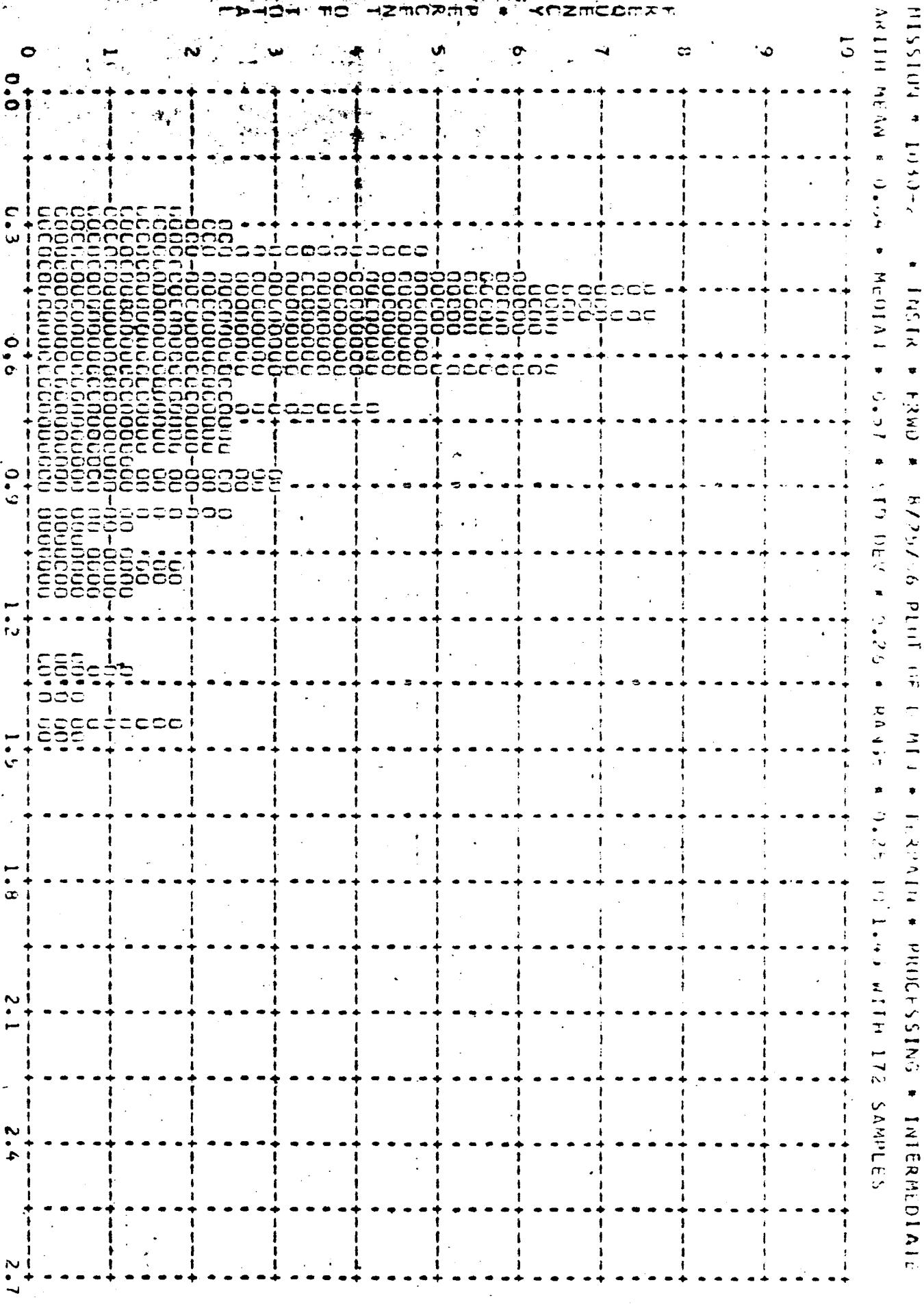
~~TOP SECRET~~

MISSION • 1030-2 • INSTRUMENT • FRWD				8/25/66 DENSITY FREQ DISTR			
DENSITY VALUE	PRIMARY MIN MAX LIM	INTERMEDIATE MIN MAX LIM	FULL MIN MAX LIM	FULL MIN MAX LIM	ALL LEVELS MIN MAX LIM	ALL LEVELS MIN MAX LIM	
2.51	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	
2.52	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	
2.53	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	
2.54	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	
2.55	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	
2.56	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	
2.57	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	
2.58	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	
2.59	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	
2.60	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	
2.61	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	
2.62	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	
2.63	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	
2.64	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	
2.65	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	
2.66	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	
2.67	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	
2.68	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	
2.69	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	
2.70	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	
SUBTOTAL	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	
TOTAL	0	0	0	172 172 112	74 74 60	246 246 172	

MISSION 1030-2		INSTR - FRWD		8/25/66 PROCESSING AND EXPOSURE ANALY			
PROCESS LEVEL	SAMPLE SIZE	UNDER EXPOSED	UNDER PROCESSED	CORRECT EXP+PROC	OVER PROCESSED	OVER EXPOSED	
PRIMARY	0	0 PC	0 PC	0 PC	0 PC	0 PC	
INTERMEDIATE	172	0 PC	13 PC	73 PC	12 PC	3 PC	
FULL	74	16 PC	30 PC	66 PC	18 PC	0 PC	
ALL LEVELS	246	5 PC	9 PC	71 PC	13 PC	2 PC	
PROCESS LEVEL	BASE + FOG	UNDER EXPOSED	UNDER PROCESSED	CORRECT EXP+PROC	OVER PROCESSED	OVER EXPOSED	
PRIMARY	0.01-0.03	0.01-0.13	0.14-0.39	0.40-0.90	-----	0.91 AND	
INTERMEDIATE	0.10-0.17	0.01-0.20	0.21-0.39	0.40-0.90	0.91-1.34	1.35 AND	
FULL	0.10-1.02	0.01-0.39	-----	0.40-0.90	0.91-1.69	1.70 AND	

~~TOP SECRET~~

Table A-3



TOP SECRET

Figure A-22

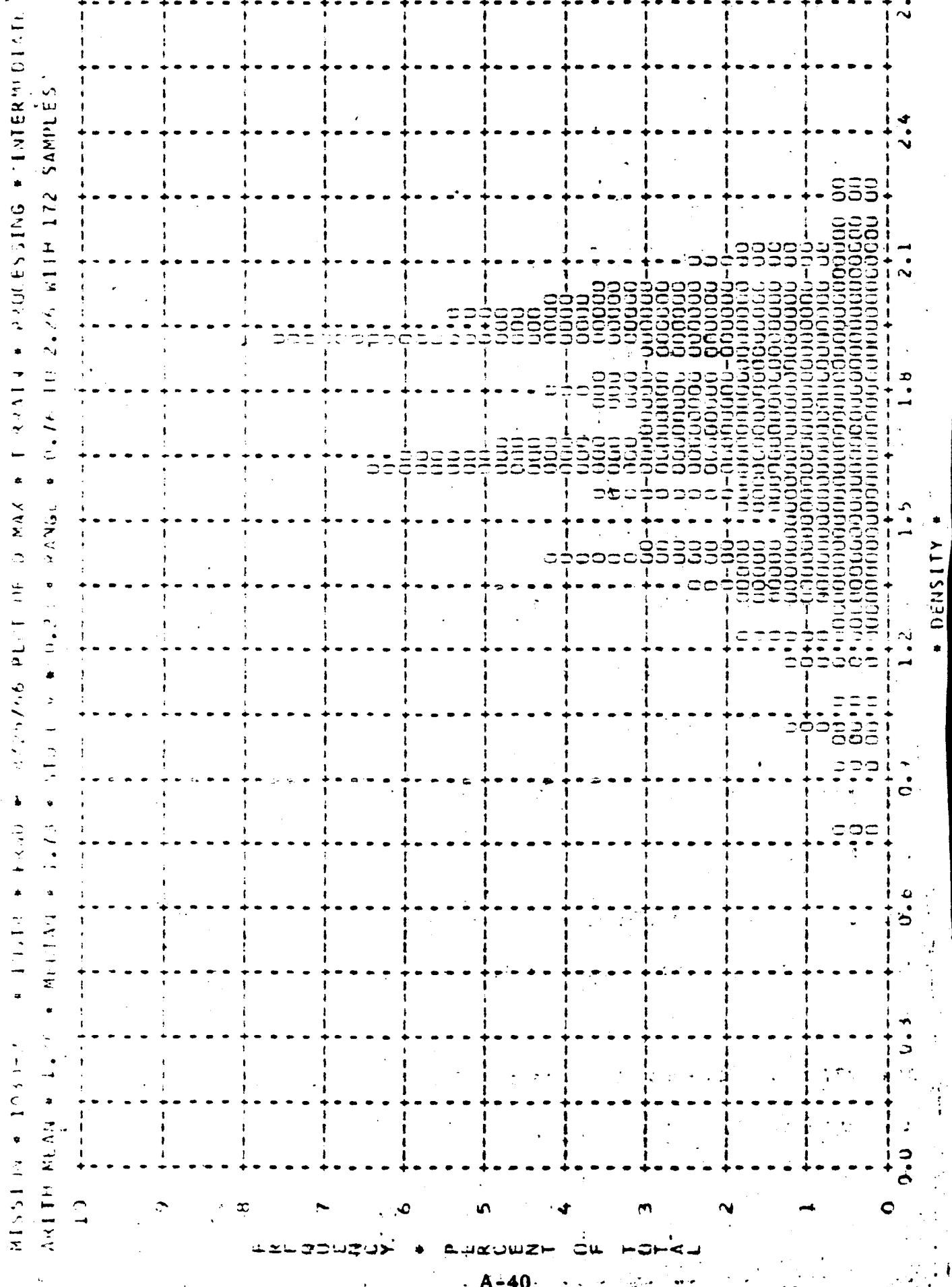
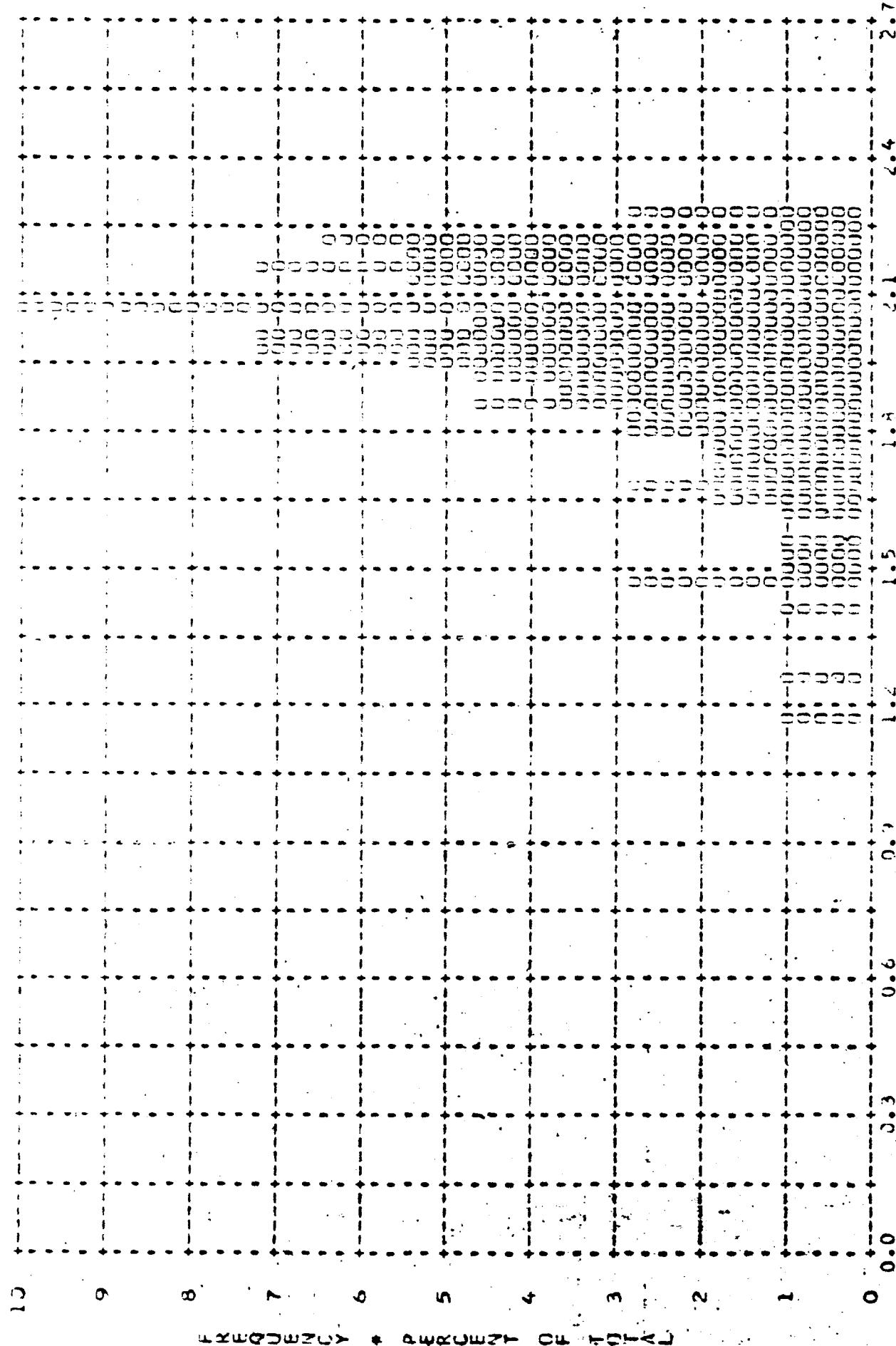


Figure A-23

MINIMUM = 1.36 \* MEAN = 1.70 \* MEDIAN = 1.70 \* RANGE = 1.17 \* STDEV = .105 \* NUMBER OF SAMPLES = 112



TOP SECRET

Figure A-94

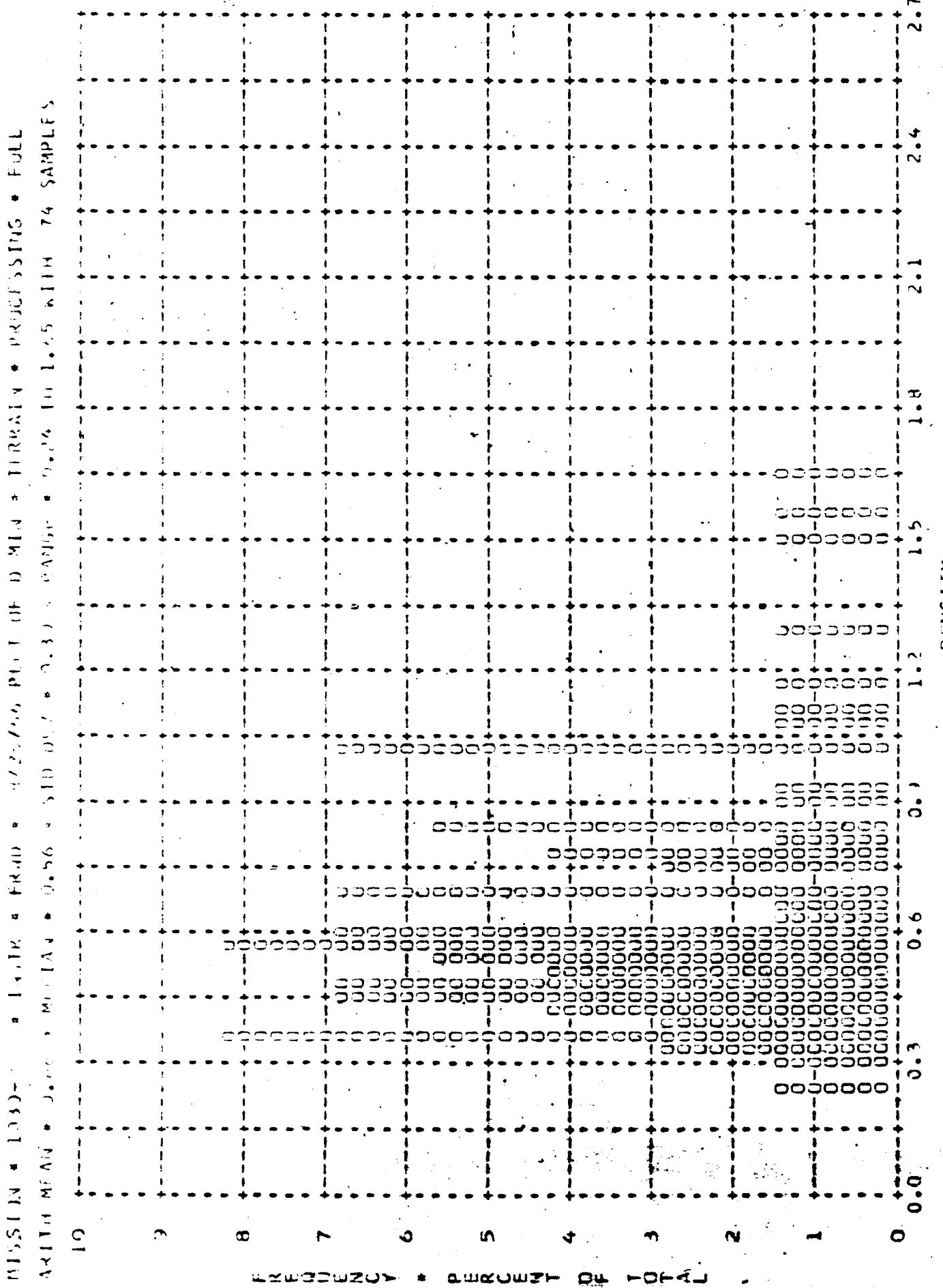


Figure A-25

MISSING = 1031-2 PLOT OFF G MAX = 1.5 PAIR  
ARITH-MEAN = 1.07 MEDIAN = 1.05 DEVI = 0.30 RANGE = 0.32 To 2.26 WITH 74 SAMPLES

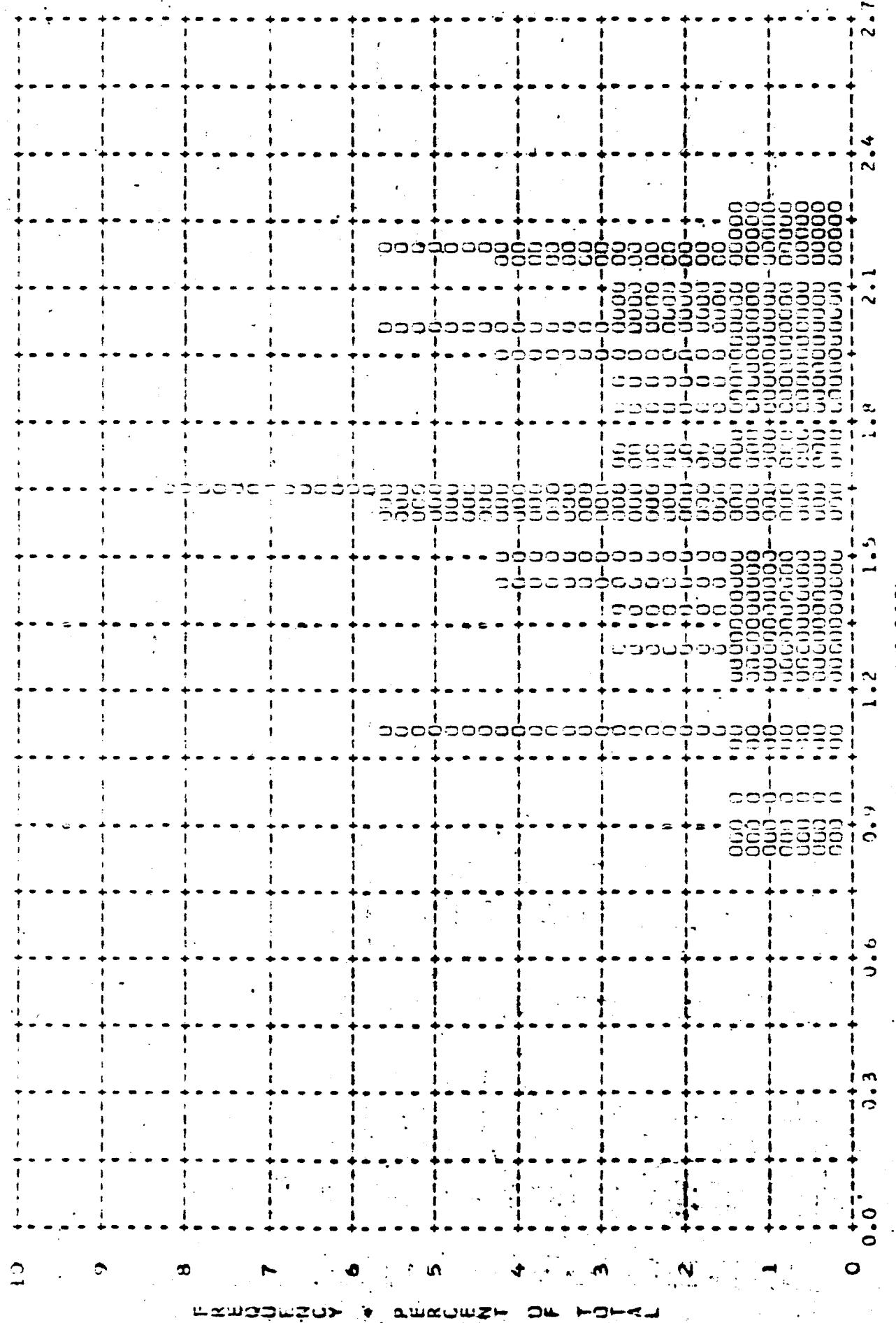
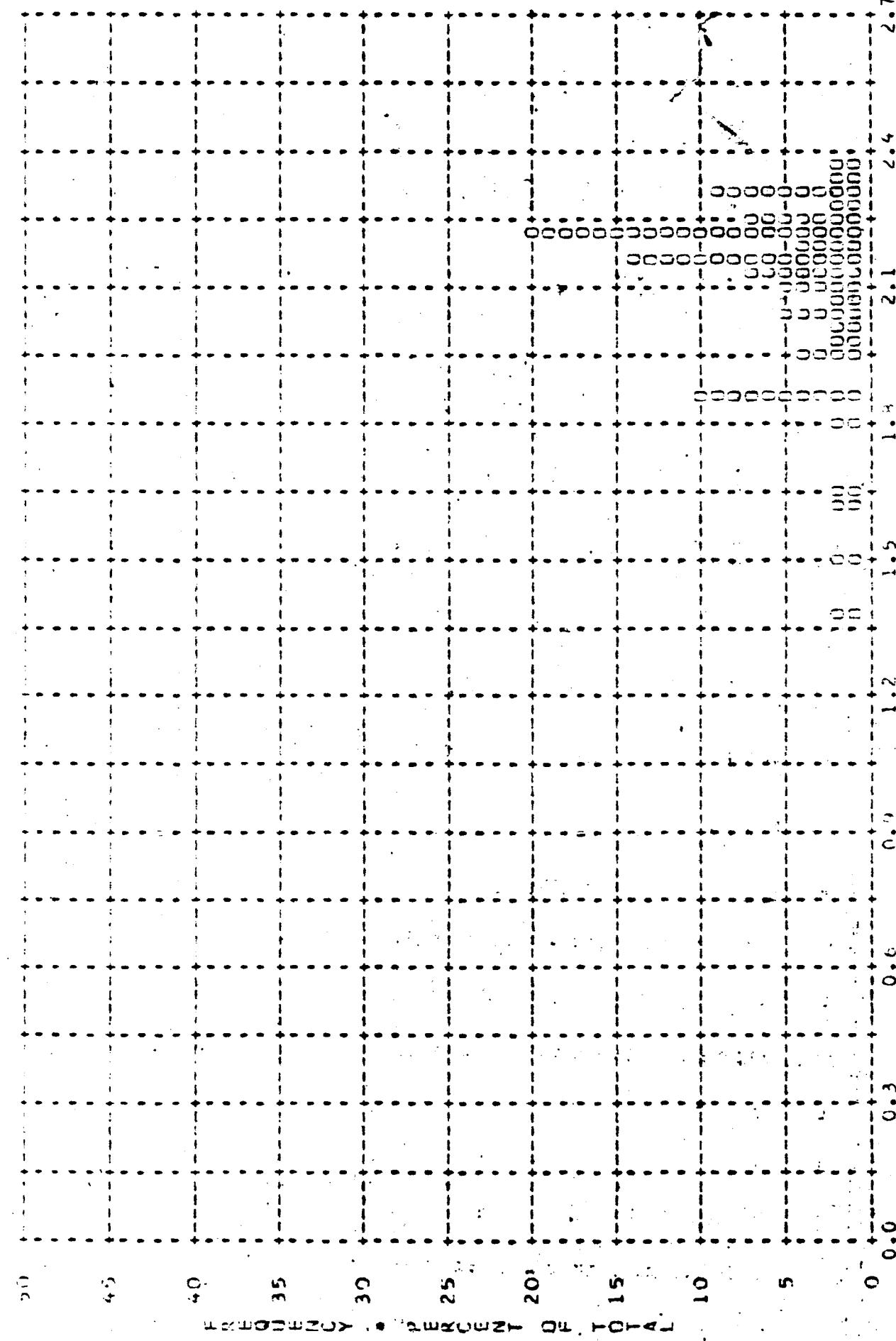


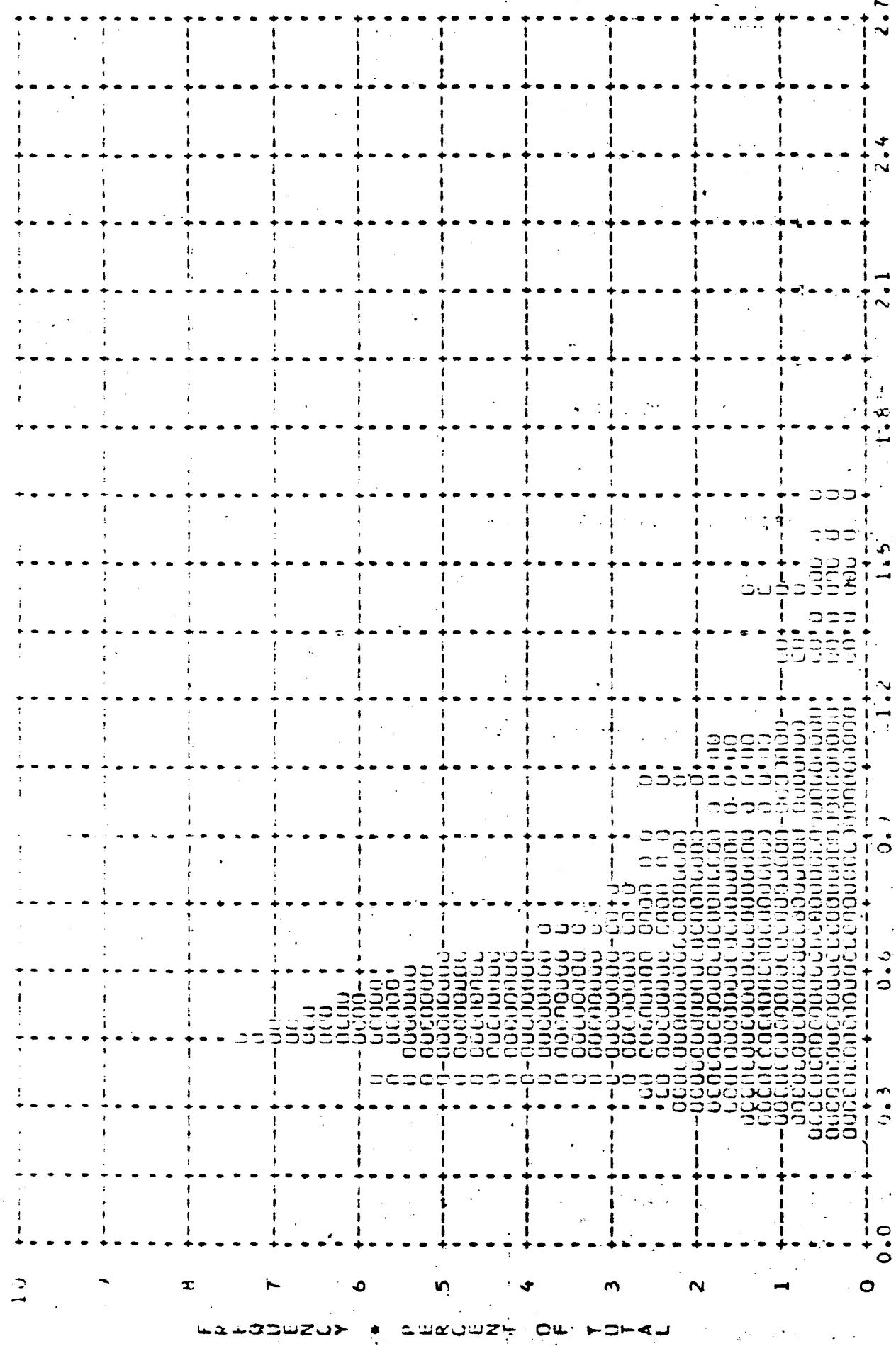
Figure A-26

MISSION # 1930-2 • DATE • FEB 1 • 1957 • PLOT OF D MAX • CUTOFF • PROCESSING • FULL

ARITHMETIC • P. 10 • MEDIAN • C. 15 • N(0,21) • PAUL • J. 35 • 1.35 WITH 60 SAMPLES



MEAN & STANDARD DEVIATION OF PERCENT PIGMENT IN ALL 246 SAMPLES



A-45

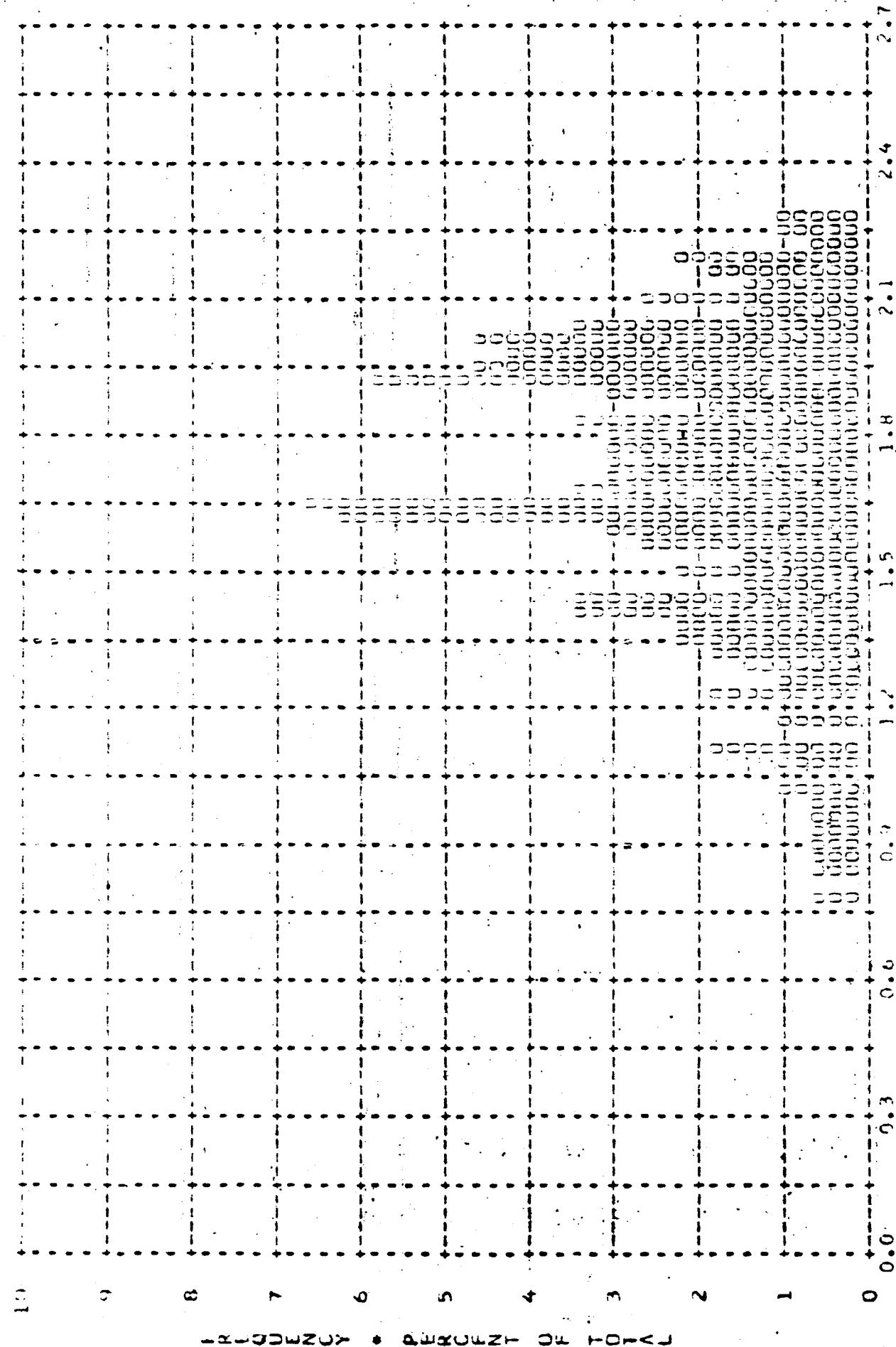
Figure A-28

\* DENSITY \*

TOP SECRET

MISSION \* 103100 \* 103100 \* 103100 \* 103100 \* 103100 \* 103100 \* 103100 \* 103100 \* 103100 \* 103100

ARITH MEAN = 1.000 \* 103100 \* 1.000 \* 103100 \* 1.000 \* 103100 \* 1.000 \* 103100 \* 1.000 \* 103100 \* 1.000 \* 103100



PLACEMENT & POSITION \* 1.000 \* 1.000 \* 1.000 \* 1.000 \* 1.000 \* 1.000 \* 1.000 \* 1.000 \* 1.000 \* 1.000

ARITH. MEAN = 1.000 MEDIAN = 1.000 \* 0.999 \* 0.999 \* 0.999 \* 0.999 \* 0.999 \* 0.999 \* 0.999 \* 0.999

2.0

1.8

1.6

1.4

1.2

1.0

0.8

0.6

0.4

0.2

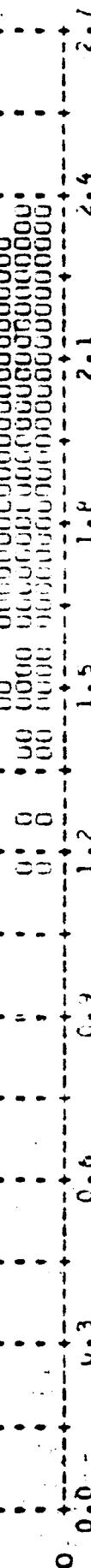
0

FREQUENCY \* PERCENT OF TOTAL

2

1

0



FOR STICKER

Figure A-30

TOP SECRET

MISSION • 1930-2 • INSTRUMENT • AFT 8/25/66 DENSITY FREQ DISTR

8/25/66 DENSITY FREQ DISTR

Table A-4

LUD. RECHT

MISSION • 1C30-2      \* INSTRUMENT • AFT      8/25/66      DENSITY FREQ DISTR

JOURNAL OF CLIMATE

**Table A-4**

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MISSION = 1130-2     INSTRUMENT = AFT     8/25/06     DENSITY FREQ DISTR

Table A-4

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LITERATURE • MARCH • INSTRUMENT • ANALYSIS

8/25/66 DENSITY FREQ LIST

DESENTRY VALUE	PRIMARY MIN MAX LIM	INTERMEDIATE MIN MAX LIM	FULL MIN MAX LIM	ALL LEVELS MIN MAX LIM
-------------------	------------------------	-----------------------------	---------------------	---------------------------

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**Table A-4**

~~TOP SECRET~~ MISSION \* 1030-2 \* INSTRUMENT \* AFT 8/25/66 DENSITY FREQ DISTR

DENSITY VALUE	PRIMARY		INTERMEDIATE		FULL	ALL LEVELS	
	MIN	MAX	MIN	MAX	MIN	MAX	LIM
1	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
2	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
3	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
4	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
5	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
6	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
7	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
8	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
9	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
N	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000

Table A-4

~~TOP SECRET~~

MISSION • 1030-2 • INSTRUMENT • AFT      8/25/66      DENSITY FREQ DISTR

DENSITY VALUE	PRIMARY			INTERMEDIATE			FULL			ALL LEVELS		
	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM
2.054	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2.055	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2.056	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2.057	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2.058	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2.059	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2.060	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2.061	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2.062	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2.063	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2.064	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2.065	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2.066	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2.067	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2.068	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2.069	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2.070	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
SUBTOTAL												
TOTAL			0	73	73	.56	171	171	104	244	244	160

MISSION 1030-2      INSTR - AFT      8/25/66      PROCESSING AND EXPOSURE ANALYSIS

PROCESS LEVEL	SAMPLE SIZE	UNDER EXPOSED		UNDER PROCESSED		CORRECT EXP+PROC		OVER PROCESSED		OVER EXPOSED	
		0 PC	1 PC	0 PC	1 PC	0 PC	1 PC	0 PC	1 PC	0 PC	1 PC
PRIMARY		0	0	0	0	0	0	0	0	0	0
INTERMEDIATE	73	0	0	1	1	75	75	19	19	4	4
FULL	171	0	2	0	2	63	63	35	35	1	1
ALL LEVELS	244	0	2	0	2	66	66	30	30	2	2
PROCESS LEVEL	BASE + FCG	UNDER EXPOSED	UNDER PROCESSED	CORRECT EXP+PROC	OVER PROCESSED	OVER EXPOSED	OVER EXPOSED	OVER EXPOSED	OVER EXPOSED	OVER EXPOSED	OVER EXPOSED
PRIMARY	0.01-0.03	0.01-0.13	0.14-0.39	0.42-0.90	-----	-----	0.91	AND UP			
INTERMEDIATE	0.10-0.17	0.01-0.20	0.21-0.39	0.42-0.90	0.71-1.34	1.35	AND UP				
FULL	0.14 AND UP	0.01-0.39	-----	0.40-0.90	0.71-1.69	1.72	AND UP				

~~TOP SECRET~~

Table A-4

PROCESSING \* INTEGRITY

MEAN \* MEDIAN \* Q1 \* Q3 \* RANGE \* STDEV \* TOTAL \* COUNT \* PERCENTAGE WITH 73 SAMPLES

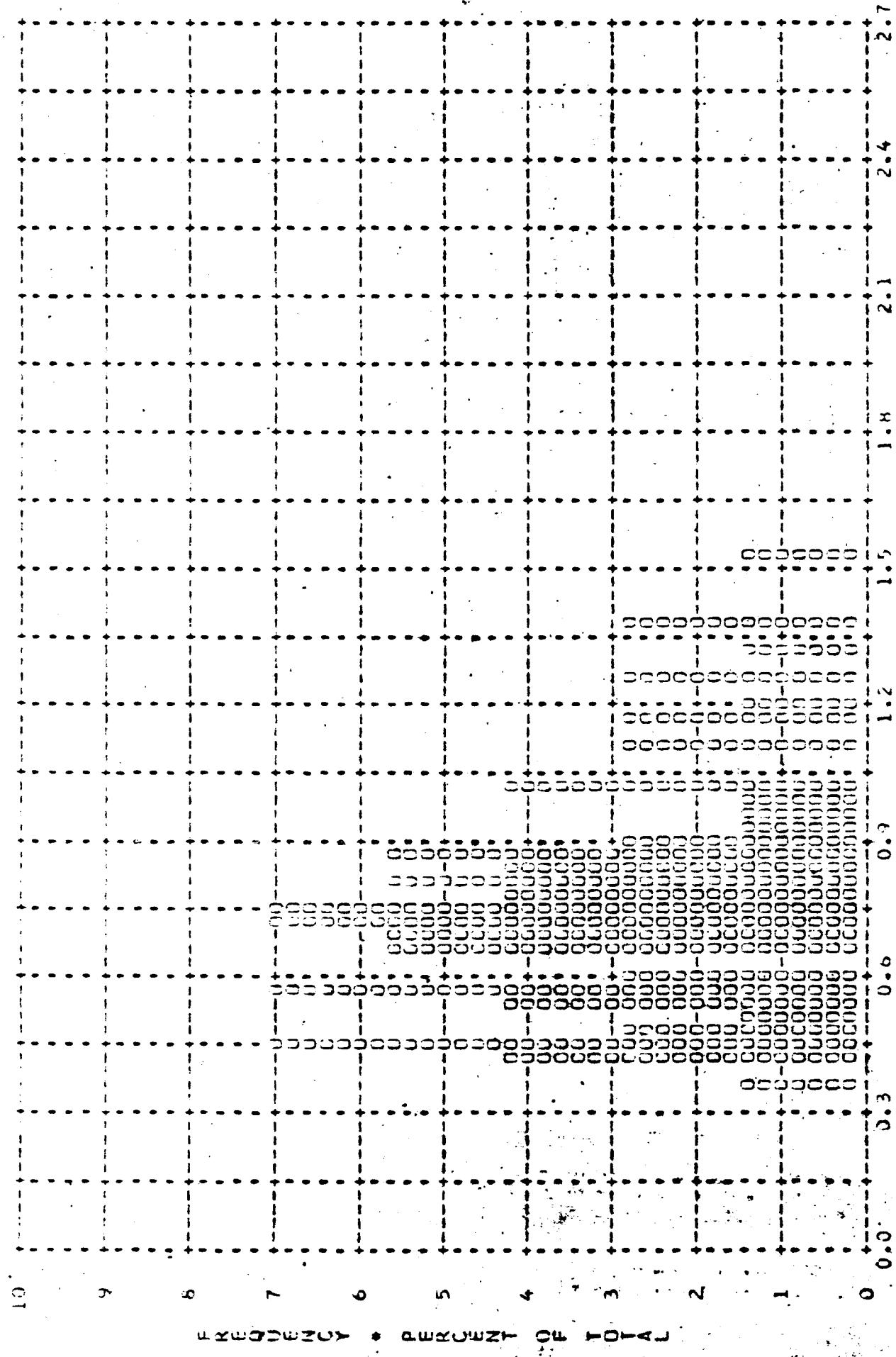
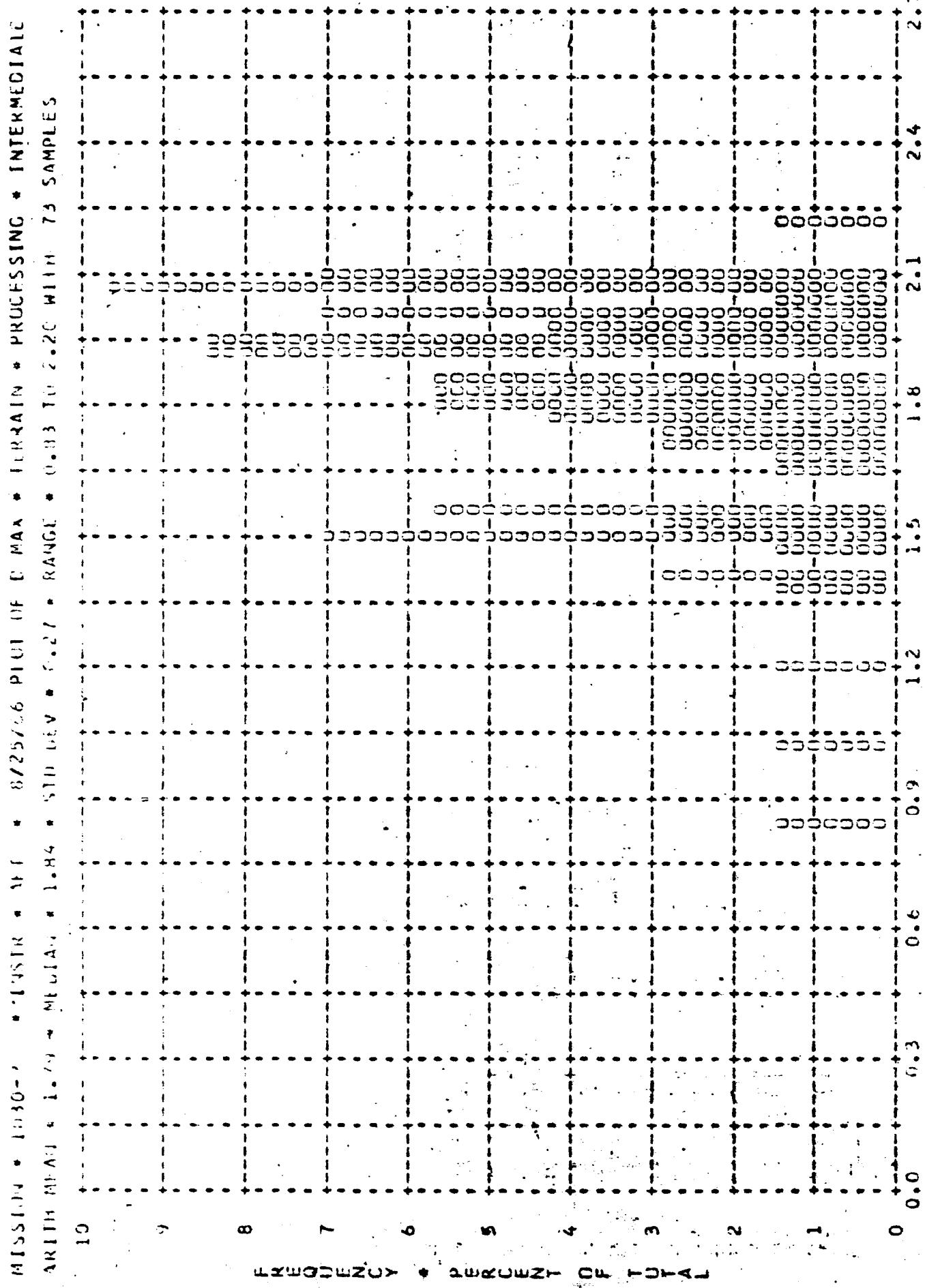


Figure A-21



A-55

REF ID: A32

Figure A-32

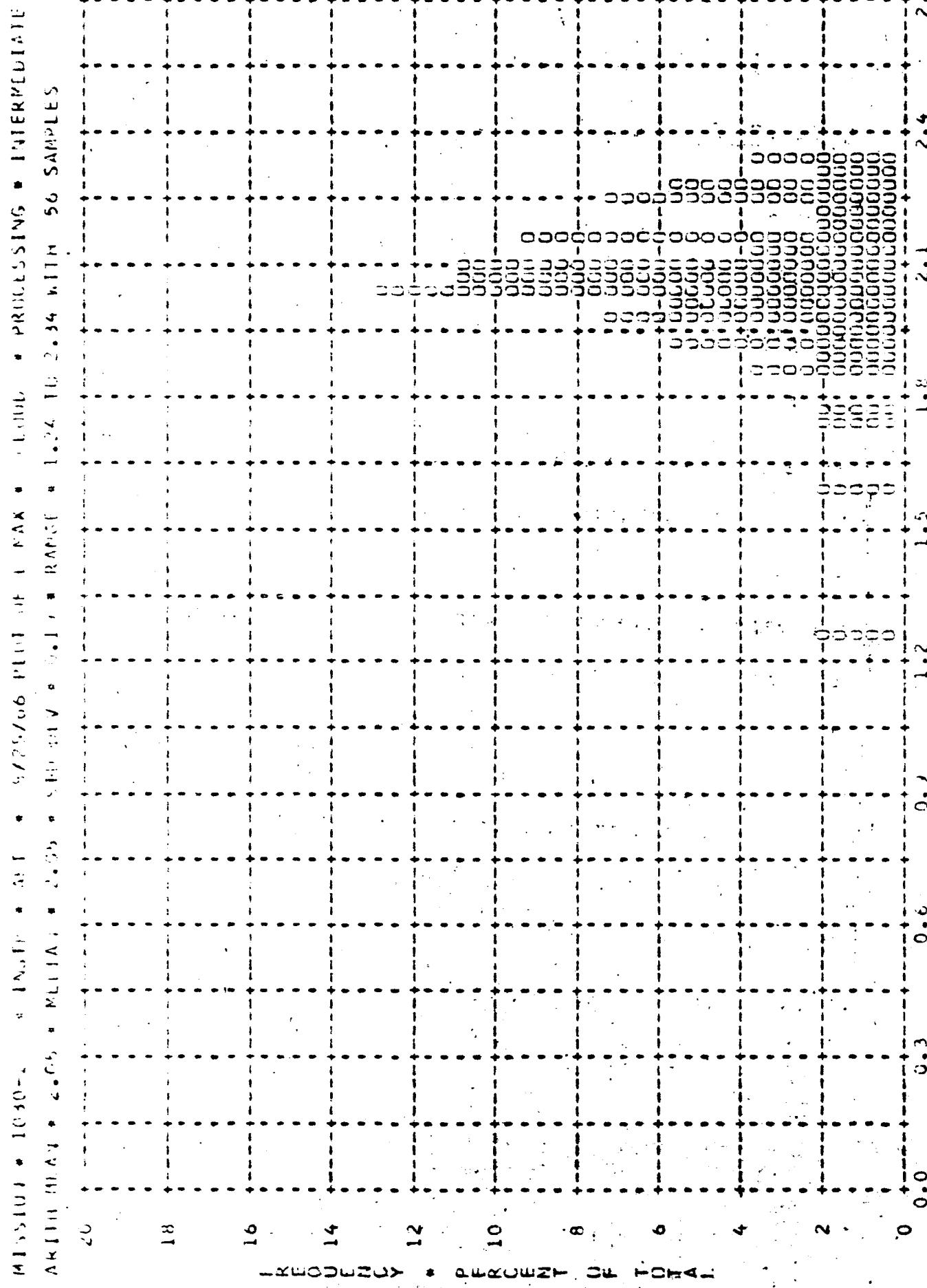


Figure A-33

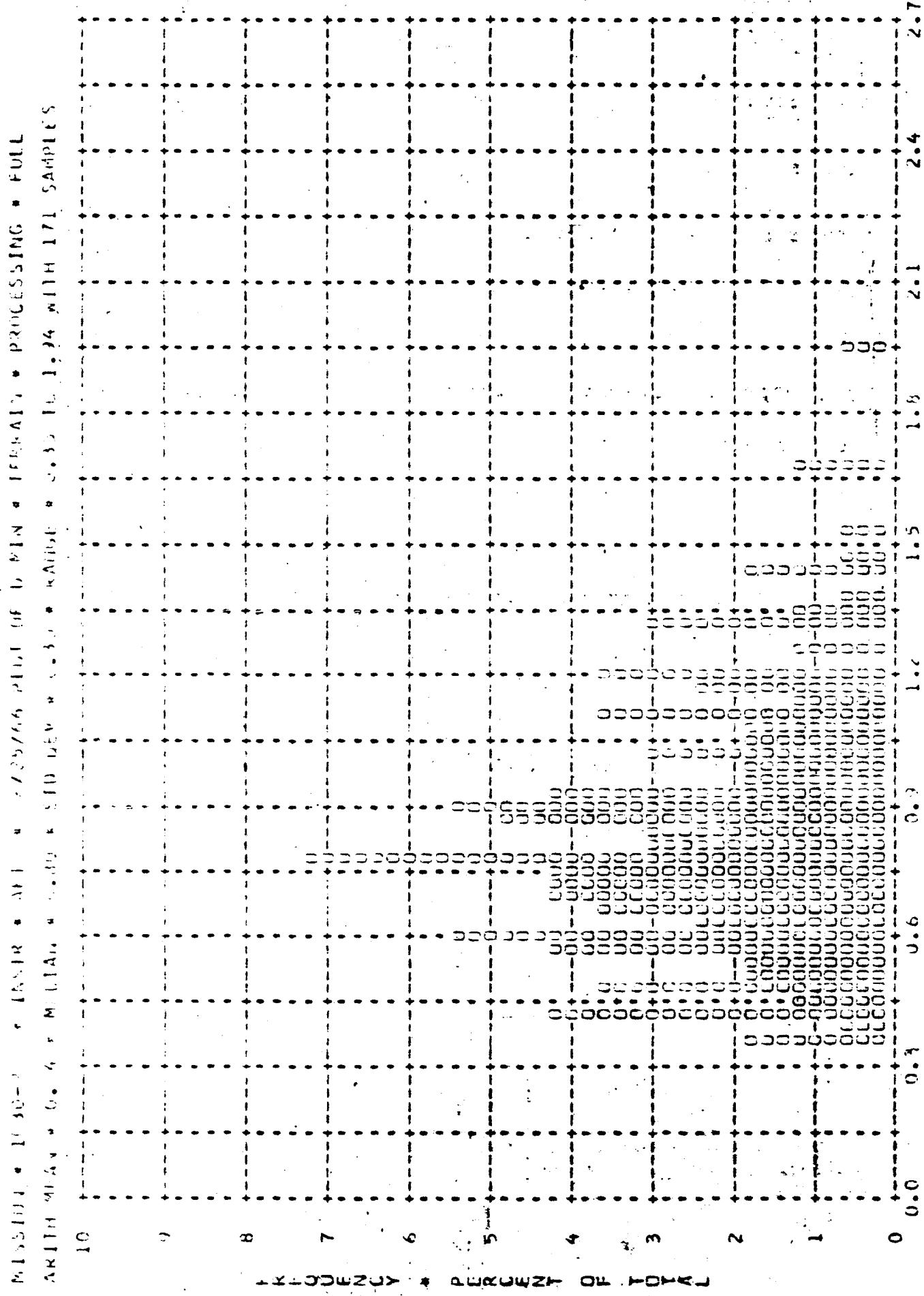
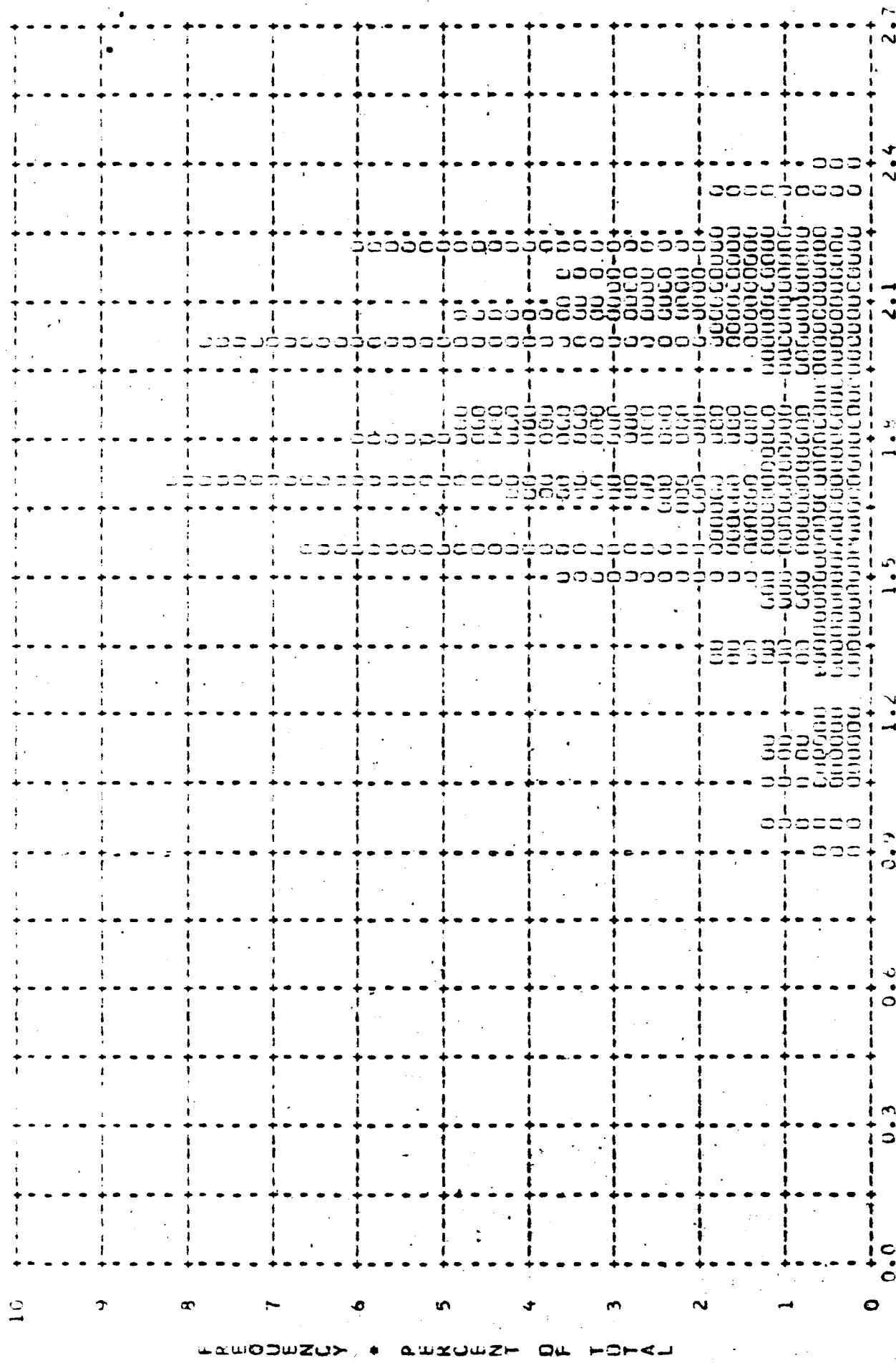


Figure A-34

卷之三

MISSION \* 163018Z \* 101100Z \* 01210600Z \* E 600 \* W 600 \* PROCESSING \* FULL  
ARLIN 3000 \* 1.00 \* MEDIAN P.H. \* 0.100000 \* PLATE # 0.002000 WITH 1/2 SAMPLES



TOP SECRET

Figure A-35

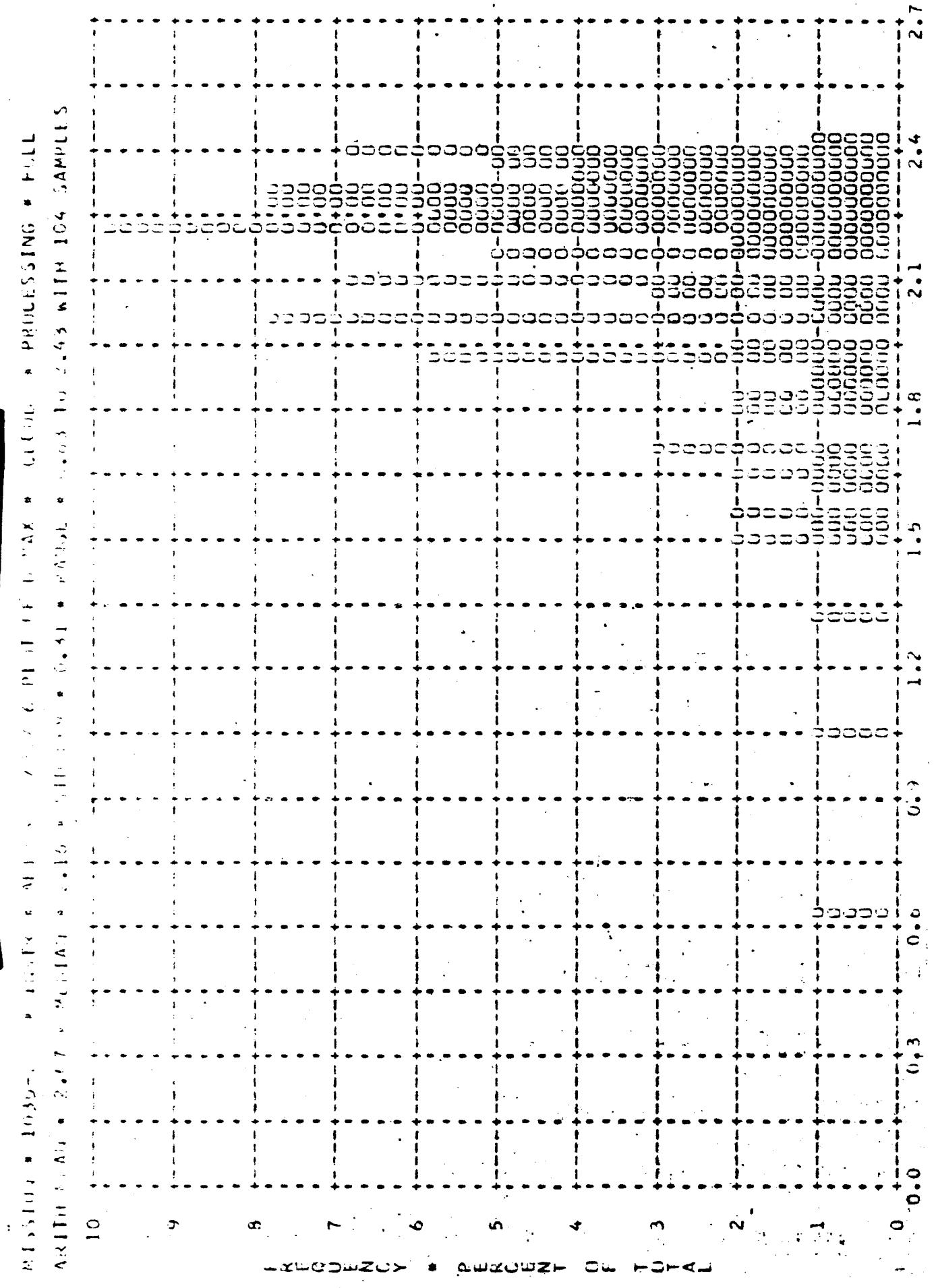
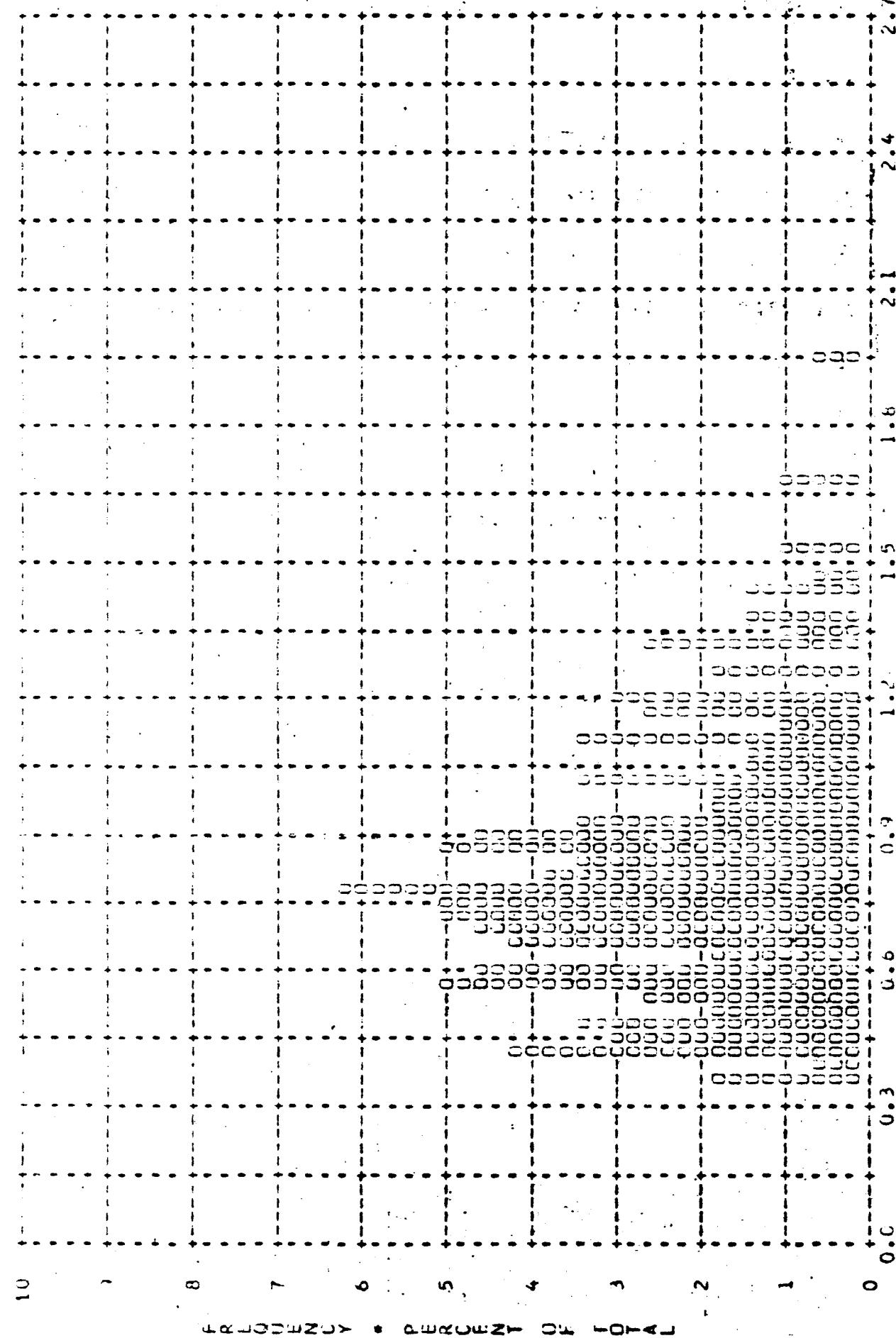


Figure A-36

四百一

110,000 \* 100 = 110,000 \* 100% \* PERCENT WORKING \* REACHING \* ALL LEVELS

88100 \* 100 = 88100 \* 100% \* PERCENT WORKING \* REACHING \* ALL LEVELS



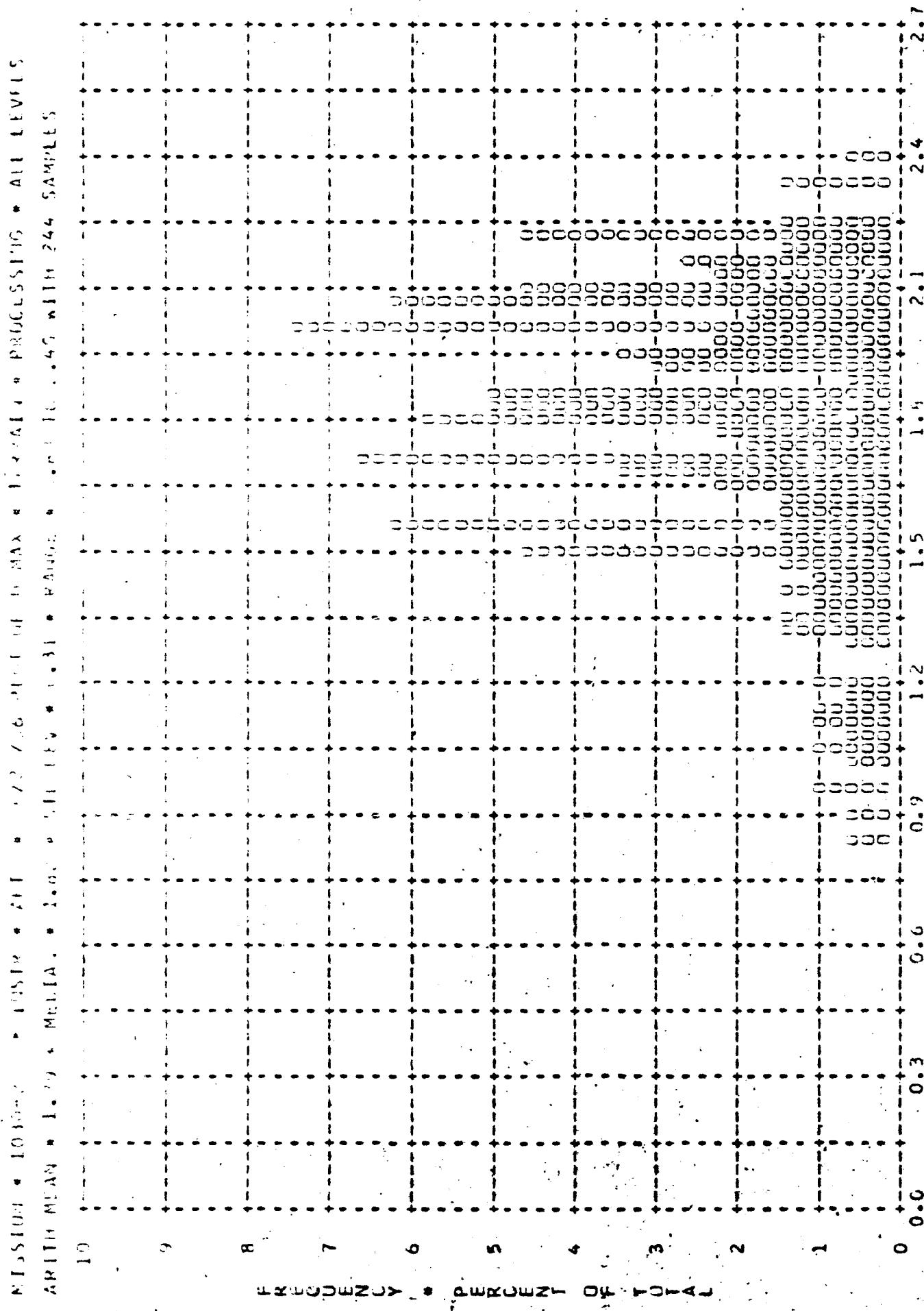


Figure A-38

TOP-ESCRIT

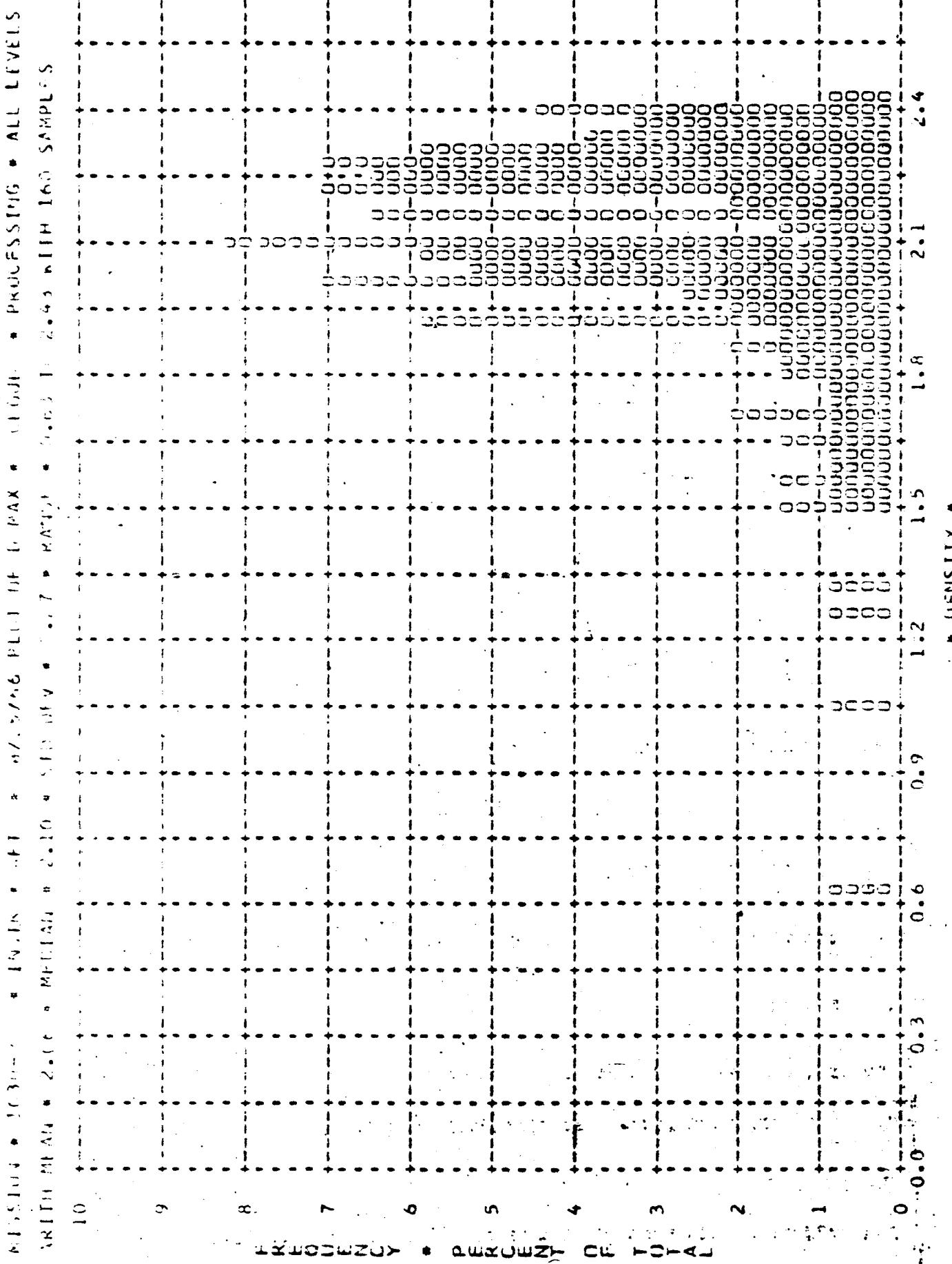


Figure A-39

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