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CORONA J

FLIGHT REPORT

MISSION 1034

AGENA 1626/PAYLOAD J-31

5 July 1966

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In Accordance with E. O. 12958
on NOV 26 1997

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1.0 INTRODUCTION

FTV 1626 was an Agena (S301B) and the booster was an improved THOR (LV2A-SN466). The Agena/Payload had the capability for dual recovery and deactivate/reactivate. The flight was a tail-first in orbit configuration.

The payload system was a standard J1 reconnaissance camera system. Major payload component serial numbers are shown in Figure 1-1.

The flight consisted of five day first mission and a five day second mission with the deactivate/reactivate capability not being utilized.

FTV 1626 was launched on 21 June 1966 at 14:31 PDT with first recovery terminated by air catch on Rev 81 and second recovery terminated by air catch on Rev 161.

2.0 SUMMARY

All launch, ascent, and injection events occurred as programmed which resulted in achieving the desired orbit. For the first time, the tape recorder was turned on during the ascent sequence to record the payload system temperature environment.

Both panoramic cameras operated satisfactorily throughout the flight. Average cycle rates on both instruments deviated from the pre-flight calibrated values by less than 2 per cent.

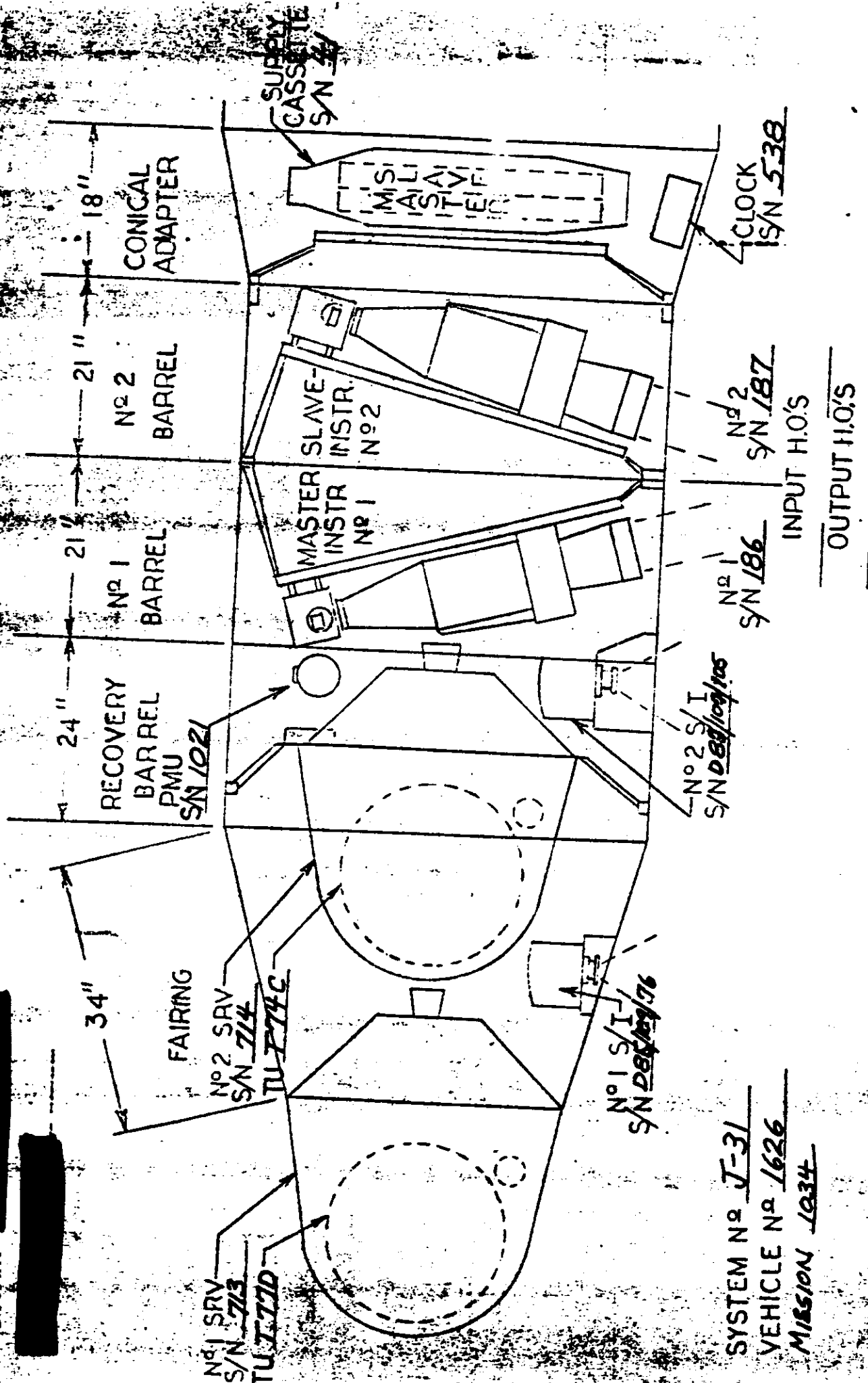
The V/H programmer failed on the end of Rev 4 or the beginning of Rev 5 and did not operate for the remainder of the flight. This resulted in FMC match errors greater than 5 per cent (Refer to 3.5).

The pressure make-up system developed a high pressure leak and gas depletion occurred on Rev 32 (Refer to 8.0).

The -1 and -2 stellar/index cameras operated satisfactory throughout the flight.

The clock, instrumentation, and command system functioned properly throughout the flight.

CORONA J PROFILE



SYSTEM Nº J-31
VEHICLE Nº 1626
MISSION 1034

FIGURE 1.1

TOP SECRET

The thermal environment was within tolerance. The ascent temperature data from the tape recorder is included in Figure 9.1 and 9.2.

Both recovery systems operated satisfactorily with the exception of the -2 flashing light. This was the second -2 recovery system which the flashing light equipment was inoperative. (Ref. 10.2)

3.0 MISSION DESCRIPTION SUMMARY

3.1 Orbital Parameters - ORBIT #1

<u>Parameters</u>	<u>Predicted</u>	<u>Actual</u>
Period - Min.	90.07	90.20
Apogee - N.M.	192.5	201.82
Perigee - N.M.	109.5	106.45
Eccentricity	.0116	.0133
Inclination - Deg.	80.00	80.11
Argument of Perigee - Deg.	161	170.3

3.2 Programmed Mission

	<u>Programmed</u>	<u>Actual</u>
Launch Time - PDT	1430-1530	14:31
-1 Duration - Days	4	5
Deactivation - Days	0	0
-2 Duration - Days	5	5

3.3 Panoramic Film Consumption

	<u>Actual</u>	
	<u>Master</u>	<u>Slave</u>
Pre-launch	102	105
-1 Mission	2896	2930
-2 Mission	3039	2995
Total	6037	6030

3.4 Camera Settings and Film Types

3.4.1 Panoramic Camera

	<u>Master</u>	<u>Slave</u>
Film Type	3404	3404
Slit Width - Inches	.200	.150
Filter Type - Wratten	23A	21

3.4.2 Horizon Optics

	<u>Master</u>		<u>Slave</u>	
	<u>Take-Up</u>	<u>Supply</u>	<u>Take-Up</u>	<u>Supply</u>
Aperture	F8.0	F6.3	F6.3	F8.0
Exposure Time - Sec.	1/100	1/100	1/100	1/100
Filter Type - Wratten	25	25	25	25

3.4.3 Stellar/Index

	<u>-1</u>		<u>-2</u>	
	<u>Stellar</u>	<u>Index</u>	<u>Stellar</u>	<u>Index</u>
Film Type	4401	4400	4401	4400
Aperture	F1.8	F4.5	F1.8	F4.5
Exposure Time - Sec.	2.0	1/500	1.0	1/500
Filter Type - Wratten	None	21	None	21

3.5 FMC Match

The V/H programmer failed to cycle after Rev 04 of the mission. Telemetry indicated that the programmer started properly on the beginning of Rev 04 but was inoperative during Rev 05. This failure caused the two panoramic camera systems to operate at a constant cycle rate regardless of the time up ramp position.

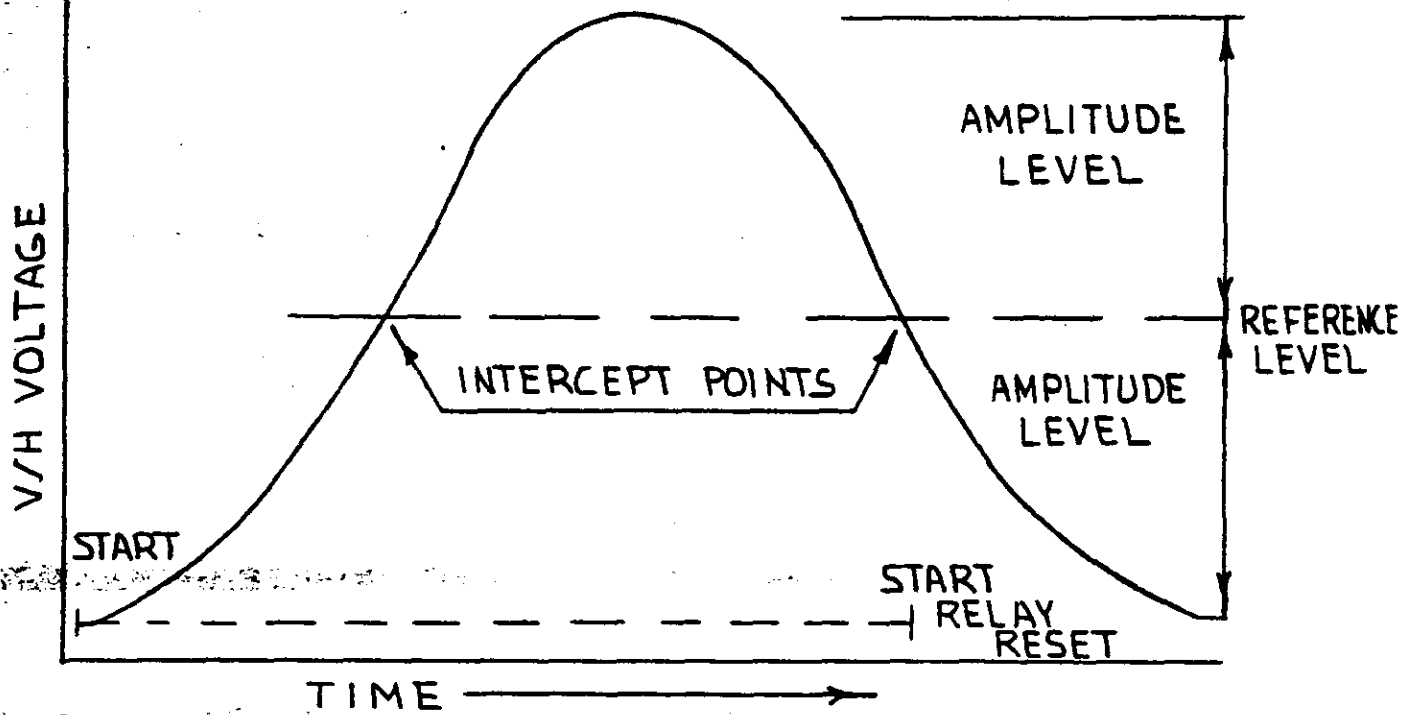
Telemetry data indicated the V/H Programmer had stopped at a position equivalent to the Reference Level voltage (See Figure 3.5). With the programmer in this position the Amplitude Command setting had no effect on the output voltage and only the Reference Command settings could be used to minimize FMC errors. Operational control under the above restrictions produced FMC errors of generally less than 10 per cent. However, FMC error on a few operations exceeded 20 per cent.

Analysis of this failure indicated that the most probable cause was the failure of the programmer self-energize switch (S201), See Figure 3.5. Failure of this switch to make contact resulted in loss of 400 cps voltage to the drive motor at the time S-202 applied reset voltage to the start relay. With S-202 retaining voltage on the reset coil, subsequent start commands were ineffective. This drive design has been used since the start of the Corona Program without a failure and this failure was considered to be random. The only corrective action was to review test procedures to assure proper operation of S-201.

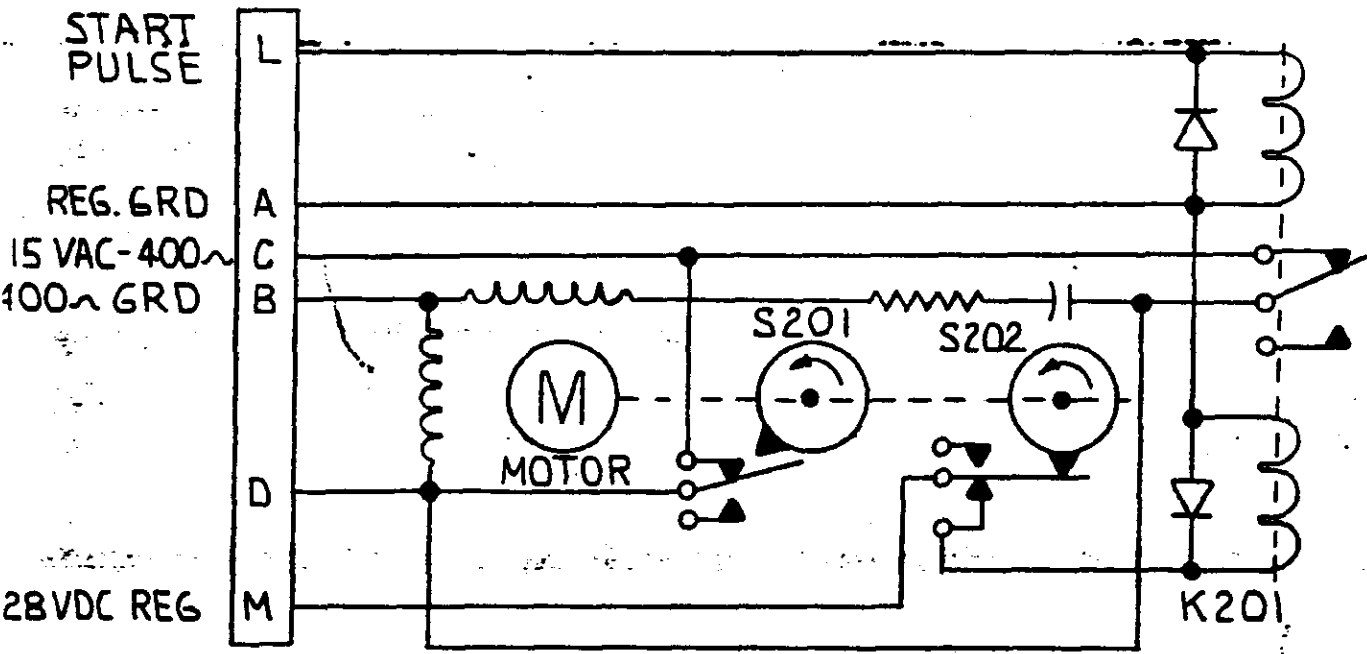
4.0 PANORAMIC CAMERA PERFORMANCE

Camera system dynamics were normal throughout the -1 and -2 missions. The film transport of both camera systems were normal. Cycle rate data (Table 4-1) indicates that the camera systems were generally less than 2.0 per cent from the calibrated systems value. The master and slave instruments were generally less than 1.0 per cent apart throughout most of the flight. The 99/101 average clutch ratio was 6/6 for the master instrument and 6/6 for the slave instrument. Film depletion on the slave camera occurred prior to the engineering operation on Rev. 159.

V/H PROGRAMMER VOLTAGE PROFILE



V/H PROGRAMMER DRIVE SCHEMATIC



- K201 START RELAY
- S201 SELF ENERGIZE SWITCH
- S202 START RELAY RESET SWITCH

TABLE 4-1

J-31 FLIGHT

REV. MODE	CP	RAMP R	TUR A	SYSTEM SECS CALIB.	I-----INST. 186-----I			I-----INST. 187-----I			186/187 DIFF.	
					ACTUAL	UNIT DEV.	SYSTEM DEV.	ACTUAL	UNIT DEV.	SYSTEM DEV.		
09	A	7	6	2740	2.890	2.893	0.10S	0.11S	2.909	0.67S	0.66S	0.55
16	A	5	11	2740	2.638	2.650	0.50S	0.47S	2.680	1.57S	1.60S	1.13
32	A	3	11	2740	2.427	2.440	0.61S	0.52S	2.451	0.90S	0.98S	0.45
47	A	3	11	2740	2.427	2.450	1.02S	0.94S	2.450	0.85S	0.94S	-0.00
63	A	3	11	2740	2.427	2.426	0.03S	0.05F	2.443	0.57S	0.65S	0.70
79	A	3	11	2740	2.427	2.455	1.22S	1.14S	2.445	0.65S	0.73S	-0.41
88	B	5	11	2740	2.638	2.672	1.34S	1.30S	2.665	1.00S	1.03S	-0.26
95	B	3	11	2740	2.427	2.451	1.06S	0.98S	2.430	0.03S	0.11S	-0.86
111	B	3	11	2740	2.427	2.465	1.64S	1.55S	2.453	0.98S	1.06S	-0.49
127	B	2	11	2740	2.338	2.380	1.90S	1.79S	2.380	1.69S	1.79S	-0.00
143	B	2	11	2740	2.338	2.390	2.32S	2.22S	2.370	1.26S	1.36S	-0.84
159	B	2	11	2740	2.338	2.369	1.43S	1.32S	2.367	1.13S	1.24S	-0.08

DEV. AND DIFF. ARE IN PERCENT
 THE (-) SIGN INDICATES THAT INST 1 IS SLOWER THAN INST 2
 F=FAST AND S=SLOW

5.0 STELLAR/INDEX CAMERA PERFORMANCE

The -1 stellar/index camera operation was normal throughout the mission with telemetry indicating proper metering and shutter operation.

The -2 stellar/index camera operation was also normal throughout the mission with no abnormalities noted on telemetry.

6.0 INSTRUMENTATION AND COMMAND SYSTEM PERFORMANCE

The instrumentation and command systems operated satisfactorily throughout the -1 and -2 missions with no abnormalities evident. The mono delay time was within the specified tolerance and operated satisfactorily.

7.0 CLOCK SYSTEM PERFORMANCE

The payload clock system performed satisfactorily during both phases of the mission. The clock/system time correlation data obtained from the [redacted] acquisitions are included in Table 7-1 and 7-2.

8.0 PRESSURE MAKE-UP SYSTEM PERFORMANCE

The pressure make-up system (PMU) developed a high pressure leak and gas depletion occurred on Rev 32 as indicated by Figure 8.1. This high pressure leak most probably occurred on the supply side of the on-off solenoid.

A review of the PMU design and the performance from the previous 25 flight units indicated the design was adequate. This failure was considered to be random and no further corrective action was taken.

9.0 THERMAL ENVIRONMENT

The temperature data obtained from the [redacted] acquisitions are contained in Table 9-1, -2, -3, and -4. Average panoramic camera temperatures for the master camera varied from 77° F to 61° F and the slave camera varied from 71° F to 55° F during the mission.

The ascent thermal environment was recorded on the tape recorder and is included in Figure 9.1 and 9.2.

TABLE 7-1

J-31 1626 1034

ORDER FIT 1

SYS TIME I/P	CL TIME I/P	COMP SYS TM	DELTA ST	REV	STA
0.38511438D 05	C.157176991D 06	C.385114491D 05	-0.0111	9	
0.77963978D 05	C.196629539L 06	C.779639903D 05	-0.0123	16	
0.33219818D 05	C.238285373D 06	C.332198171D 05	0.0009	24	
0.78121671D 05	C.2P3187234L 06	C.781216704D 05	0.0006	32	
0.33387683D 05	0.324853255D 06	0.333876842D 05	-0.0012	40	
0.72872168D 05	C.364337739L 06	C.728721614D 05	0.0066	47	
0.33519076L 05	C.411384660L 06	C.335190743D 05	0.0017	56	
0.72992641D 05	C.450858229D 06	C.729926365D 05	0.0045	63	
0.33644948D 05	C.497910553D 06	C.336449524D 05	-0.0044	72	
0.73094120D 05	C.488804000L 03	C.730941086D 05	0.0114	79	
0.33737155D 05	C.475318510D 05	C.337371475D 05	0.0075	88	
0.73126748D 05	0.869214400D 05	C.731267297D 05	0.0183	95	
0.33808093D 05	C.134002806D 06	C.338080876D 05	0.0054	104	
0.73199348D 05	C.173354074D 06	C.731993488D 05	-0.0008	111	
0.33874611D 05	C.220469349L 06	C.338746157L 05	-0.0047	120	
0.73062953D 05	C.259657698D 06	C.730629579D 05	-0.0049	127	
0.33901405D 05	C.306896156D 06	C.339014078D 05	-0.0028	136	
0.73306475D 05	C.346301235D 06	0.733064800D 05	-0.0050	143	
0.33909833L 05	C.393304597L 06	C.339098339D 05	-0.0009	152	
0.73253050D 05	C.432647829L 06	C.732530591D 05	-0.0091	159	

A0=-0.1186655148D 06 A1= 0.999999827700D 00

SIGMA=0.00716 NC. POINTS= 20

RATIO OF CLOCK TIME TO SYS TIME= 0.100000017230D 01

TOP SECRET
TABLE 7-2

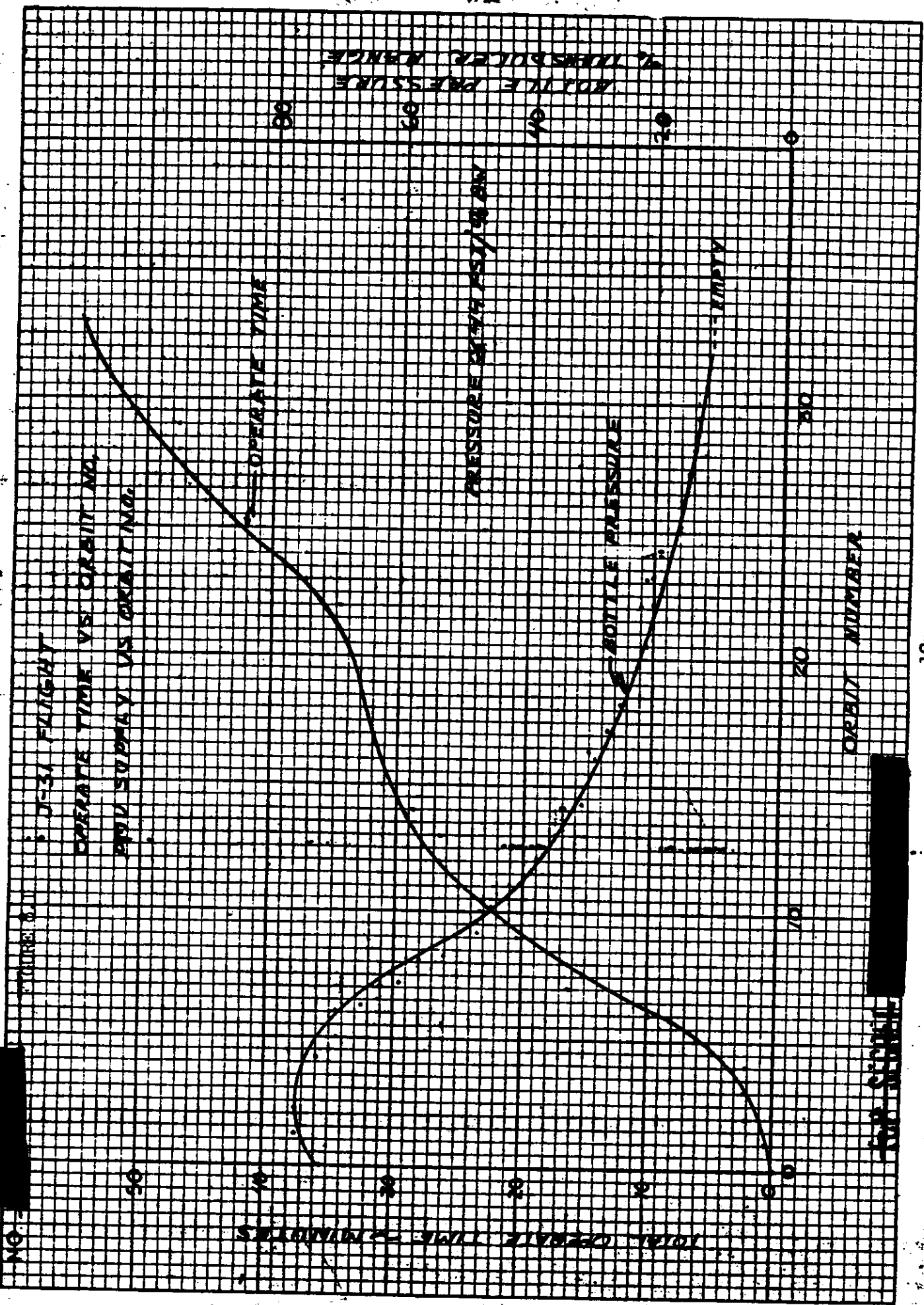
J-31 1626 1034

ORDER FIT 2

SYS TIME I/P	CL TIME I/P	COMP SYS TM	DELTA ST	REV	STA
0.385114380 05	C.157176991L 06	C.385114391D 05	-0.0011	9	
0.779639780 05	C.196629539C 06	0.779639833D 05	-0.0053	16	
0.332198180 05	C.238285373C 06	0.332198129D 05	0.0051	24	
0.781216710 05	C.283187234C 06	C.781216688D 05	0.0022	32	
0.333876830 05	C.324853255C 06	C.333876847D 05	-0.0017	40	
0.72872168L 05	C.364337739L 06	C.728721635D 05	0.0045	47	
0.33519076C 05	C.411384660C 06	C.335190780D 05	-0.0020	56	
0.72992641D 05	C.450858229C 06	C.729926412D 05	-0.0002	63	
0.33644948D 05	C.497910553C 06	C.336449579D 05	-0.0099	72	
0.73094120D 05	C.4888C4000C 03	C.730941145D 05	0.0055	79	
0.33737155U 05	C.475318510L 05	C.337371534D 05	0.0016	88	
0.73126748U 05	C.869214400C 05	C.731267353D 05	0.0127	95	
0.33808093D 05	C.1340C2806C 06	0.338080924D 05	0.0006	104	
0.73199348D 05	C.173394074C 06	C.731993526D 05	-0.0046	111	
0.33874611D 05	C.220469349C 06	0.338746180D 05	-0.0070	120	
0.73062953U 05	C.259657698L 06	C.730629586D 05	-0.0056	127	
0.33901405D 05	C.306896156C 06	0.339014061D 05	-0.0011	136	
0.73306475D 05	C.346301235D 06	0.733064760D 05	-0.0010	143	
0.33909833C 05	C.3533C4597C 06	C.339098268D 05	0.0062	152	
0.73253050D 05	C.432647829C 06	C.732530491L 05	0.0009	159	

A0=-0.1186655395D 06 A1= 0.999999936404D 00
A2=-0.9657944838711L-13

SIGMA=0.00499 NL. POINTS= 20



TOP SECRET

UNITED STATES GOVERNMENT

1/6 Prod.	09	16	24	32	40	47	56	63	72	79	88	95	104
3	65	70	68	67	70	68	69	66	67	65	65	60	63
4	64	76	71	71	74	74	76	69	70	68	69	64	67
5	64	80	76	75	78	75	77	73	74	71	71	66	70
6	59	78	74	74	76	74	74	72	71	70	69	65	66
7	59	78	76	75	76	76	75	73	72	72	69	66	67
8	64	78	75	74	77	76	76	72	73	72	72	65	70
9	63	80	76	75	78	76	76	72	73	71	71	67	70
10	67	78	76	76	77	75	75	71	69	69	67	62	64
11	71	78	73	73	77	73	76	71	73	70	72	66	70
12	59	76	75	74	75	74	74	72	71	70	67	64	64
13	64	77	74	73	75	74	74	73	72	70	69	65	67
14	61	73	70	69	69	69	69	66	65	63	62	58	59
15	54	69	64	62	66	64	66	60	62	59	60	53	56
16	59	76	72	71	73	68	73	69	71	68	69	63	67
17	59	75	71	71	73	73	73	70	70	70	69	64	66
18	55	74	72	71	72	73	71	69	69	69	67	63	64
19	57	72	67	66	70	67	70	64	67	63	63	59	62
20	58	73	69	68	72	69	72	68	70	67	68	63	66
21	62	67	63	63	65	63	66	61	62	59	59	55	58
22	57	69	66	64	67	64	67	61	63	60	61	54	58
23	53	66	64	64	65	63	64	62	62	60	58	55	56
24	63	71	68	67	69	67	69	65	66	64	64	59	61
25	59	62	59	58	62	62	62	60	61	60	59	55	57
26	59	63	60	60	62	61	62	59	61	58	59	52	55

NOTE: All data corrected for self-heating, except injection.

Line/Block (B)	QUIRTS ACQUIRED													
	09	16	24	32	40	47	56	63	72	79	88	95	104	
1	---	81	22	78	19	81	22	78	15	71	21	44	21	
2	---	13	0	10	0	16	0	16	-4	29	56	78	53	
3	227	-13	15	8	-9	18	-9	15	-13	15	58	143	58	
4	223	32	35	42	32	52	33	48	26	45	19	68	19	
5	---	44	41	47	37	54	37	44	34	44	22	28	22	
6	---	35	32	77	32	74	32	71	25	61	---	---	---	

Line/Block	QUIRTS ACQUIRED													
	09	16	24	32	40	47	56	63	72	79	88	95	104	
144	39	54	33	48	30	51	30	45	27	42	34	36	21	
144	31	50	31	84	24	81	28	76	21	70	21	61	21	
---	50	140	54	140	50	143	50	140	44	137	54	134	50	
216	48	64	55	64	51	74	51	74	48	77	55	74	55	
191	48	68	64	63	45	64	42	64	42	64	38	55	38	

Line	164	26	39	29	36	23	23	29	16	26	13	16	10

Line	90	61	61	63	61	63	61	61	59	61	55	51	51

Line/Block "A" to "B"	116	37	34	34	33	40	33	33	32	32	26	32	33

Line/Block "A" to "B"	84	51	48	48	51	48	45	51	42	48	54	51	51

Line/Block "A" to "B"	69	67	63	63	63	63	62	63	61	62	83	79	78

Line	91	67	64	64	65	66	66	66	65	66	66	66	---

NOTE: Only Through One Data corrected for Self-heating.

TEMPERATURE ANALYSIS

1966

ORBITS ASSIGNED

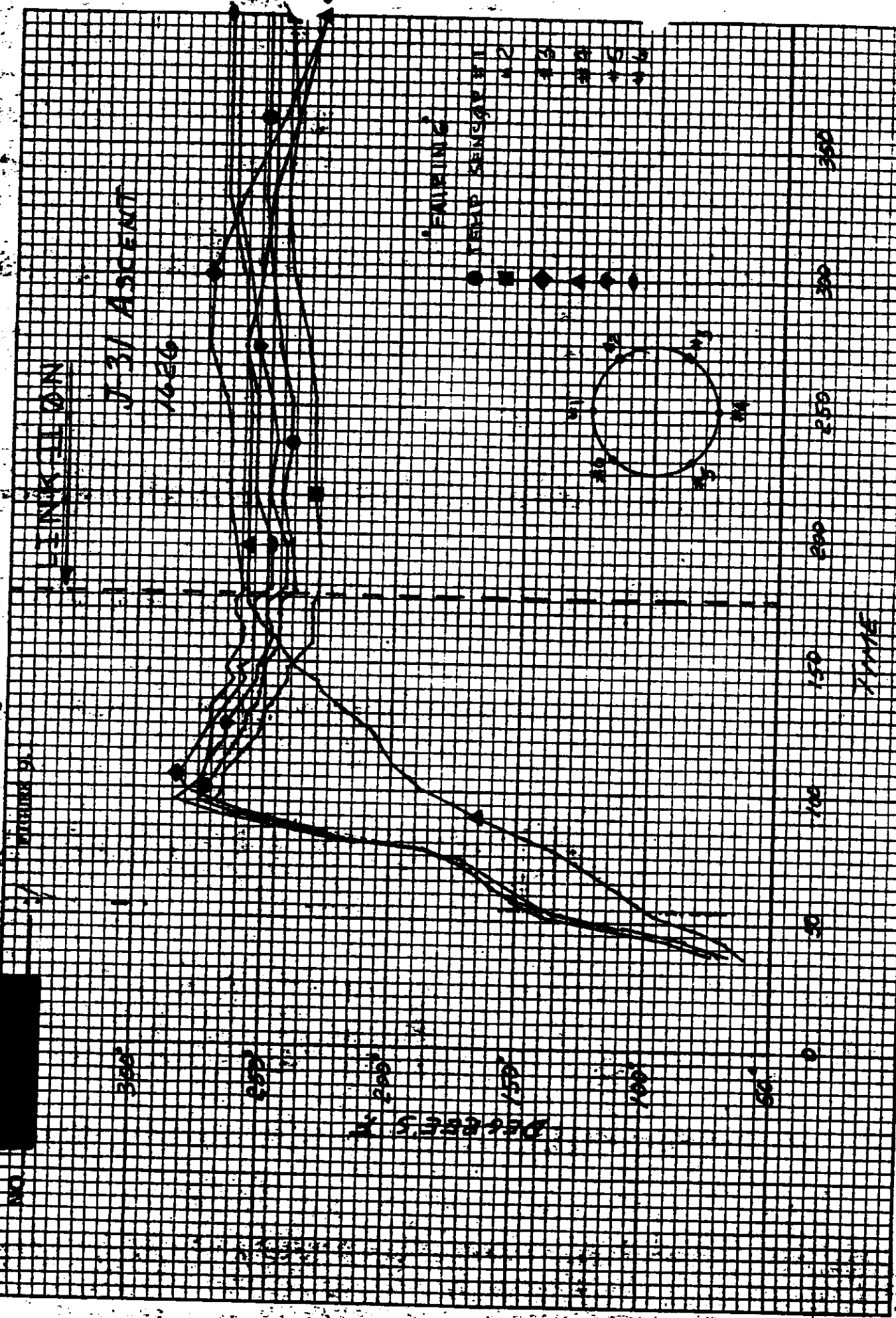
ORBIT	111	120	127	135	143	152
3	58	64	57	63	59	63
4	62	68	61	66	62	66
5	65	70	64	69	65	67
6	62	67	61	64	61	62
7	64	67	63	66	65	65
8	63	69	63	68	63	67
9	64	69	63	69	63	66
10	--	--	--	--	--	--
11	59	64	57	63	59	61
12	64	70	64	69	66	69
13	62	64	60	63	61	61
0-TEMP. TEMP.	62	67	61	66	62	65
14	55	58	53	57	65	55
15	50	57	50	55	50	53
16	62	66	62	65	62	64
17	62	66	62	66	63	65
18	60	64	60	64	62	62
19	57	63	57	61	58	61
20	61	66	61	66	62	66
21	--	--	--	--	--	--
22	53	57	52	56	53	55
23	52	57	52	56	52	54
24	54	55	50	55	53	54
0-TEMP. TEMP.	56	61	55	60	57	59
25	53	56	53	56	54	55
26	57	54	49	53	51	52

NOTE: All data corrected for self-heating, except injection.

ORBITS ACQUIRED

STATION/REMARKS	111	120	127	135	143	152
1 (B)	44	18	11	21	44	21
2	78	53	84	59	90	53
3	146	55	148	58	146	49
4	59	16	58	13	49	10
5	35	16	25	16	25	9
6	--	--	--	--	--	--
7	30	18	24	18	27	12
8	53	15	49	15	46	12
9	131	50	137	50	137	44
10	77	55	83	55	89	51
11	51	38	51	42	58	38
12	10	6	6	6	6	3
13	49	51	47	51	51	49
14	48	50	46	50	50	48
15	49	53	49	53	51	50
16	49	58	53	57	55	55
17	46	48	45	48	48	42
18	41	46	40	49	46	43
19	79	81	81	84	84	84
20	--	--	--	--	--	--

Only through case data corrected for ball-bearing.



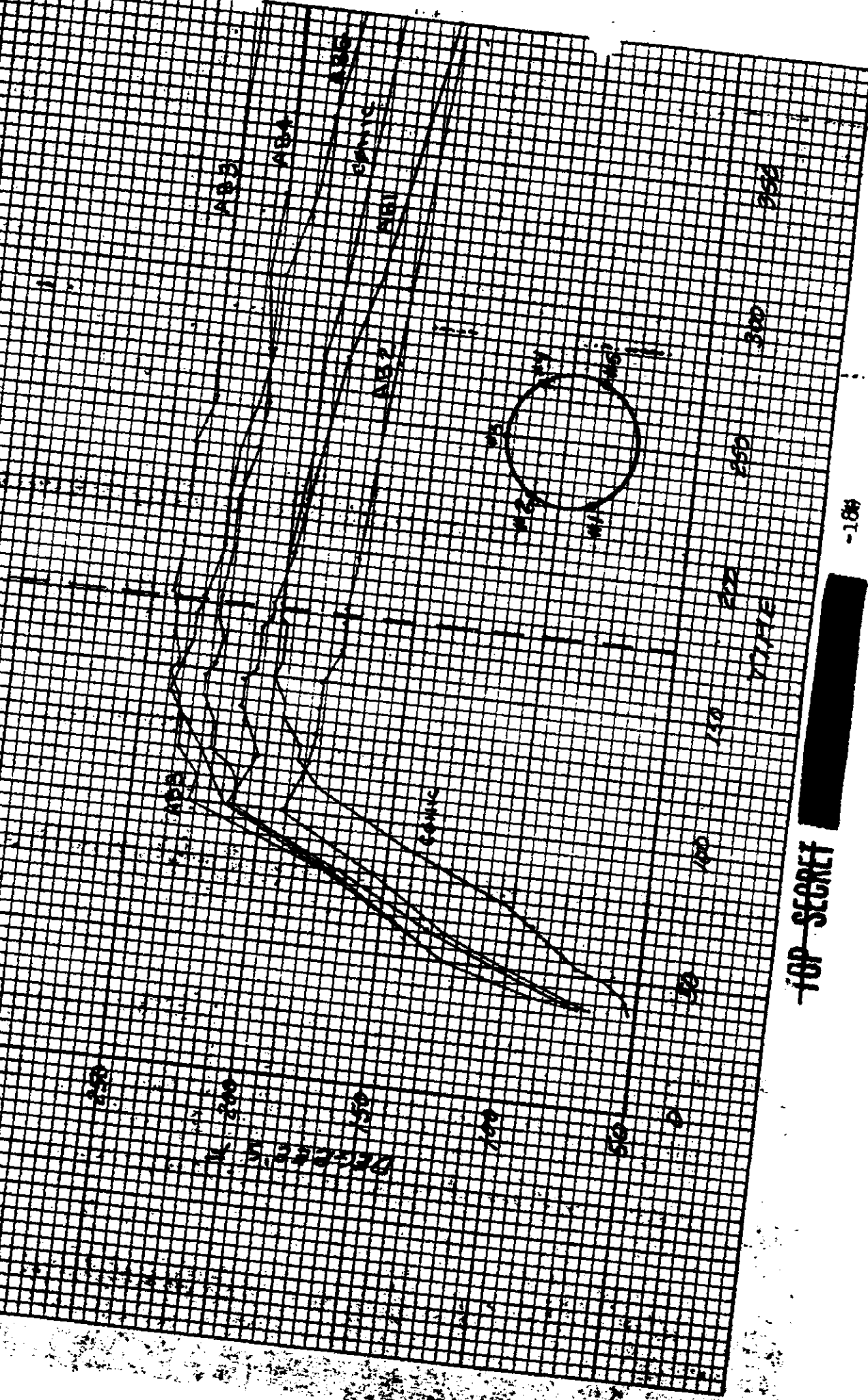
~~TOP SECRET~~

NO

FIGURE 19.2

TEST ASCENT MEASUREMENTS

11/18/57 11 AM



~~TOP SECRET~~

10.0 RECOVERY SYSTEM PERFORMANCE

10.1 -1 Mission

The -1 recovery system operated satisfactorily and was successfully recovered by air catch on 26 June 1966.

REV 81 Impact Point

<u>Predicted</u>	<u>Actual</u>
25° 02'N/156° 59'W	25° 00'N/157° 02'W

10.2 -2 Mission

It was reported by the recovery aircraft that the flashing light was working during descent. However, after the recovery system was caught and being reeled into the aircraft the flashing light was inoperative. Post recovery tests indicated satisfactory operation of all equipment. The unit is being returned to G.E. for a detailed analysis.

The -2 recovery system was successfully recovered by air catch on 01 July 1966.

REV 161 Impact Point

<u>Predicted</u>	<u>Actual</u>
24° 36'N/170° 16'W	24° 38.4'N/169° 59.4'W

Refer to Table 10-1 for the sequence of events for both -1 and -2 recoveries.

~~TOP SECRET~~

TABLE 10-1

RE-ENTRY SEQUENCE OF EVENTS

EVENT	SYSTEM TIME		DELTA TIME		
	No. 1	No. 2	No. 1	No. 2	Nominal
*Arm	83390.65	83572.33	76.97	76.96	77.0 ± 1.0
*Transfer	83465.61	83647.33	2.01	1.96	2.0 ± .25
Electrical Disconnect	83466.25	83648.23	.64	.90	.9 + .43 - .40
Separation	83467.62	83649.29			
**Spin	83469.66	83651.64	3.41	3.41	3.4 ± .30
Retro	83477.15	83659.27	7.49	7.63	7.55 ± .45
Despin	83487.75	83670.00	10.60	10.73	10.75 ± .59
T/C Separation	83489.27	83671.51	1.52	1.51	1.5 ± .15
3" Switch Open	84004.60	84194.21	527.45	534.94	528.6 ± 534.0
Parachute Cover Off	84038.40	84228.29	33.80	34.08	34.0 ± 1.5
Drogue Chute Deployed	84039.07	84228.92	.67	.63	.63 ± .08
Main Chute Bag Separate	84049.26	84238.70	10.19	9.78	10.25 ± 1.5
Main Chute Deployed	84049.81	84239.14	.55	.44	.52 ± .13
Main Chute Disreef	84054.32	84243.46	4.51	4.32	4.5 ± .80

*From separation

**From elect. disc.

***From retro