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CORONA J

PERFORMANCE EVALUATION REPORT

MISSION 1034-1 and 1034-2

FTV 1626, J-31

16 June 1967

Declassified and Released by the N R O

In Accordance with E. O. 12958

on NOV 26 1997

Approved

[REDACTED] Manager
Advanced Projects

Approved

[REDACTED]
Program

Mgr.

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No.

6 September 1967

TO:

THRU:

FROM:

SUBJECT: MISSION 1034-1 AND 1034-2 FINAL REPORT

Enclosed is the Final Performance Evaluation Report for
Mission 1034-1 and 1034-2.

Manager
Advanced Projects

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FOREWORD

This report details the performance of the payload system during the operational phase of the Program [REDACTED] Flight Test Vehicle 1626.

Lockheed Missiles and Space Company has the responsibility for evaluating payload performance under the Level-of-Effort and "J" System contracts.

This document is the final payload test and performance evaluation report for Missions 1034-1 and 1034-2 which was launched on 21 June 1966.

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INTRODUCTION

This report presents the final performance evaluation of Missions 1034-1 and 1034-2 of the Corona Program. The purpose of this report is to define the performance characteristics of the J-31 payload system and to identify the source of in-flight anomalies.

The performance evaluation was jointly conducted by representatives of Lockheed Missiles and Space Company (LMSC) and ITEK at the facilities of NPIC and AFSPPF. The off-line evaluation using Corona engineering photography acquired over the United States was performed at the individual contractors plants.

The quantitative data used for this report is obtained from government organizations. The diffuse density data, and MTF/AIM resolution are produced by AFSPPF. The vehicle attitude error values, frame correlation times are made at NPIC who also supply the Processing Summary reports published by [REDACTED]

Computer programs developed by A/P are utilized to calculate and plot the frequency distribution of the various contributors to image smear to permit analysis and correlation of the conditions of photography to the information content and quality of the acquired pictures. Computer analysis of the exposure, processing and illumination data provides the necessary data to analyze the exposure criteria selected for the mission.

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SECTION 1
SYSTEM PERFORMANCE

A. MISSION OBJECTIVES

The payload section of Mission 1034, placed into orbit by Flight Test Vehicle #1626 and LV-2A booster #466, consisted of two panoramic cameras, two Stellar-Index cameras, two Mark 5A recovery capsules and a space structure to enclose the cameras and provide mounting surfaces for all equipments. Figure 1-1 presents an inboard profile of the J-31 payload system. This Corona "J" system is designed to acquire search and reconnaissance photography of selected areas of the earth from orbital altitudes. The planned mission was a 4 day and a 5 day photographic period with no deactivate.

B. MISSION DESCRIPTION

The payload was launched from Vandenberg Air Force Base (VAFB) at 2131:00 Z (1431:00 PDT) on 21 June 1966. Ascent and injection were nominal and the achieved orbit was within nominal tolerances. Tracking and command support was effected by the Air Force Satellite Control Facility consisting of tracking and command stations at [REDACTED]

[REDACTED] under central control of the Satellite Test Center at Sunnyvale, California. Mission 1034-1 consisted of a 5 day operation and was completed by air recovery on 26 June 1966. Mission 1034-2 was completed with an air recovery on 1 July 1966 following a 5 day photographic operation.

The comparison of the planned and actual orbit parameters is tabulated as follows:

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ORBITAL PARAMETERS

<u>Parameter</u>	<u>Predicted</u>	<u>Orbit 40 Actuals</u>	<u>Orbit 130 Actuals</u>
Period (Min.)	90.07	90.148	90.028
Perigee (N. M.)	109.5	105.37	106.591
Apogee (N. M.)	192.5	199.59	188.410
Inclination (Deg.)	80.00	80.106	80.104
Perigee Latitude (Deg. N.)	19.00	18.245	38.170
Eccentricity	0.0116	0.01310	0.01278

C. PANORAMIC CAMERAS

The image quality was not up to J system standards. Sources of degradation were a decrease in scale, V/h programmer failure and atmospheric conditions.

The master instrument starboard horizon imagery was veiled from pass 8 to 35.

D. STELLAR-INDEX CAMERAS

Both units produced star imagery adequate to determine the vehicle attitude. The terrain frames were of acceptable quality.

The hot wire film cutter on the -2 mission operated prematurely in the recovery sequence.

E. OTHER SUBSYSTEMS

The clock instrumentation, command and thermal control systems performed satisfactorily. The pressure make-up system developed a leak and the gas supply was depleted by Rev 38.

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Schematic Diagram - CORONA J SYSTEM

MISSION 1034

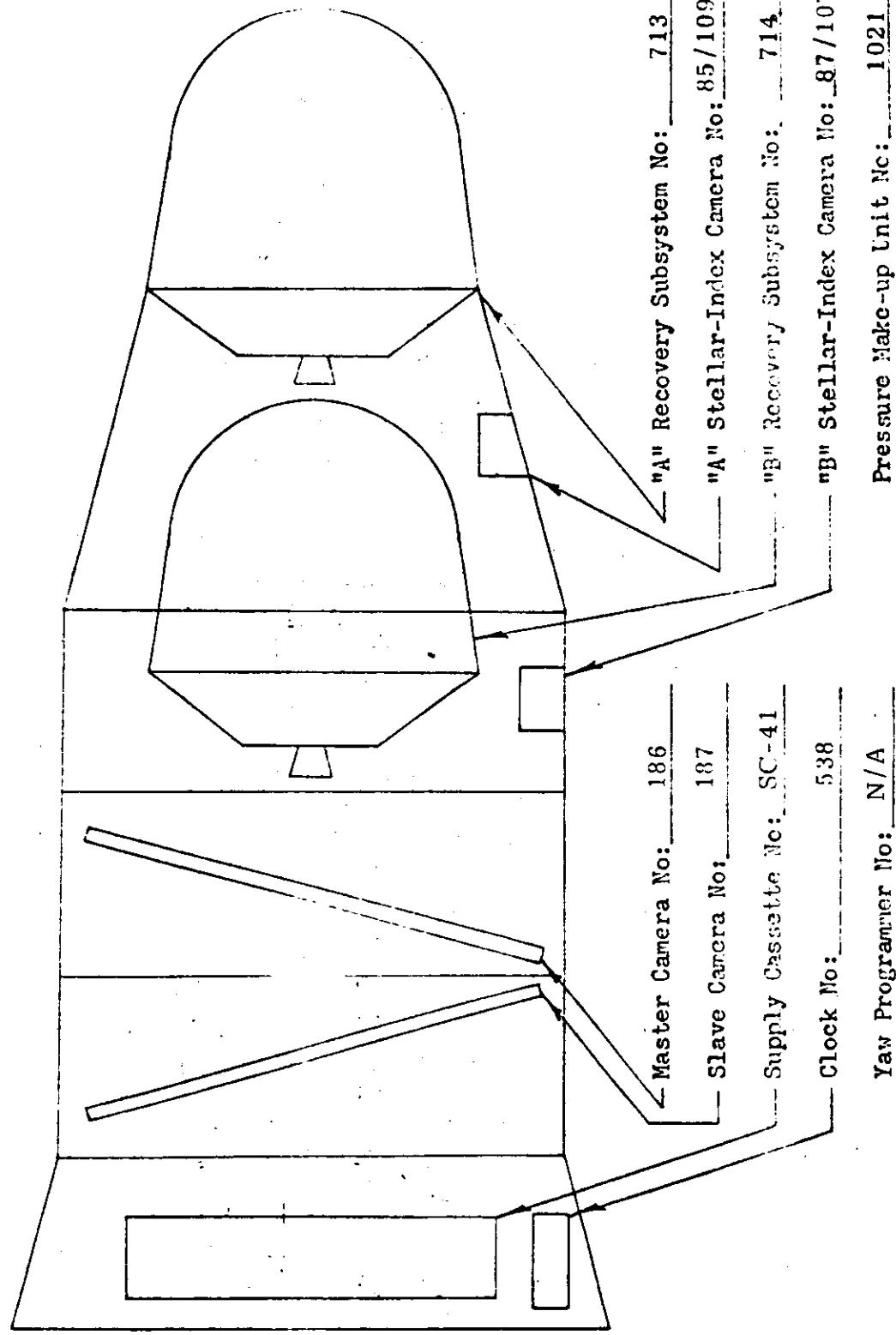


FIGURE 1-1

SECTION 2

PRE-FLIGHT SYSTEMS TEST

A. ENVIRONMENTAL TESTING

1. Test Objective

As a standard procedure, the J payload systems are subjected to thermal/altitude environmental testing which simulates orbital environment. One of the purposes of this test is to demonstrate the system susceptibility to corona discharge. Such discharge fogs the film thus degrading the operational photography.

2. Test Summary

The J-31 payload system was sent to the Sunnyvale TASC chamber for a simulated orbital test. The test was conducted from December 7, 1965 to December 14, 1965. On the seventh of December a special sub-test was initiated in which the "A" bucket heaters were allowed to raise the bucket and system internal temperatures to slightly over one hundred degrees. Normally programmed instrument operations were conducted during the first portion of this special test. The average instrument temperatures during this time ranged from 86 and 82 to approximately 98 and 93 for the master and slave instruments respectively. During this special sub-test approximately 400 cycles of instrument operation were taken in ramps 4-1, 5-8, and 7-7. The maximum average bucket temperature during this time was about 88 degrees. The instruments were not operated for the next two regularly scheduled orbits and the temperatures continued to increase. From the afternoon of the seventh the heating program was altered to allow the bucket temperatures to continue to rise and to allow the average instrument temperatures to drop. During the morning of the eighth the bucket temperatures rose to an average of 99 degrees - the peak temperature during the test - and the instrument temperatures were in the low eighties. Four stereo operations of approximately 350 cycles were performed during this period of maximum bucket temperatures. System performance during the elevated bucket temperatures was normal.

An additional innovation to the TASC test plan was the monitoring of +28 reg current and +24 unreg current. J-31 was the first payload system to monitor the current demands on the system for simulated orbital operations.

Analysis of the panoramic camera data indicates cycle rate errors which were fast and exceeding 2% deviation from the calibrated values. These excessive cycle rate errors were confined predominantly to the master instrument. The master and slave instruments on many occasions had excessive coasting after an instrument off command. On more than one occasion after an off command the lens cells coasted into the clamp position of the next operation's first frame.

The slave instrument failed-safe during orbit 11 in the "B" mode.

Prior to the fail-safe the panoramic instruments had been cycling slightly faster than the calibrated data, but the T/M data indicated normal mechanical and electrical operations until approximately 19 secs prior to the fail-safe. At this time the slave instrument take-up idler indicated an inexplicably brief slowdown, then a very fast take-up. The lens rotation time duration was approximately one-third of the preceding normal lens rotation time durations. The slave instruments supply and take-up idlers metered erratically from this time. Four seconds prior to the fail-safe the slave instrument's supply and take-up idlers stopped metering. One second prior to the fail-safe the take-up and supply idlers started metering until the fail-safe switch was encountered and power was removed.

The tape recorder status and temp data were recorded satisfactorily; however, during the cut and wrap the master and slave take-up idlers, channels AP 9 and AP 10, were attenuated.

The J-31 payload system is the second system to incorporate the new film footage pot design. The T/M output voltage is characteristically a hump backed curve. Only the "A" bucket master and slave take-up spools have the new pot characteristics.

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Table 2-1 shows the cycle rates, times up ramp, ramp amplitude settings, and cycle rate percentage deviations from calibrated data. Table 2-2 shows the clock correlation with IRIG time.

The current monitors installed in the J-31 test console were monitored on Sanborn 4 during the latter part of the "A" mode and during the "B" mode of the test.

The following are current levels observed for certain functions of the system operation. They were derived from commands given in the "A" mode; and from a mono 1 and mono 2 operation of orbit 9 in the "B" mode.

Commands

	<u>Unreg.</u>
Brush 27 and delay'	0.8A
Brush 17	0.2A
Brush 29	0.2A
RTC 6	1.0A
RTC 8, 9, 10, 11, 12	0.8A
RTC 15	.4A Spike

Reg. Unreg.

Ascent		5A
Standby (7 Sec.)	.95A	5.75A
Power No. T/M No. Op.	.5A	1.0A
T/M On	.65A	1.2A

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Instrument #1

Cycle period approximately 2.20 seconds.

<u>Event</u>	<u>+24 Reg.</u>	<u>+24 Unreg.</u>
Turn-on	1.05A	3.2A
Clamp	-	1.2A
Center Format		
Horizon Optics Fiducials	0.86A	4.8A
H. O. Shutter	0.6A	-
Pan Data Block	0.85A	-
Pan Fiducials	0.85A	-
S/I Fiducials	-	0.8A
S/I Commands	-	1.6A
Drive Current	-	0-4.0A
Maximum During M1 OP	4.1	14.2
Minimum During M1 OP	1.3	3.2

Instrument #2

Cycle period approximately 2.25 seconds.

<u>Event</u>	<u>+28 Reg.</u>	<u>+24 Reg.</u>
Turn-on	1.05A	1.6A
Clamp	-	1.2A
Center Format		
Horizon Optics Fiducials	0.8A	4.8A
Horizon Optic Shutter	0.6A	-
Pan Data Block	0.85A	-
Pan Fiducials	0.85A	-
Drive Current	-	0-4.3
Maximum During M2 OP	4.2	10.4
Minimum During M2 OP	1.5	1.6

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An 83 CPS noise was present on the unregulated current monitor during either instrument motor drive current demand. The maximum amplitude of the noise signal .8A peak to peak.

Upon return of the J-31 payload system from the first TASC test, series of tests were conducted to simulate the conditions that resulted in the "fail-safe" in the chamber. Conclusions drawn from the results of the first TASC test and the special post-TASC tests indicated an erratic magnetic amplifier unit in the slave instrument. The magnetic amplifier was then replaced and the master and slave instrument cycle rates were readjusted.

The J-31 payload system was returned to the TASC chamber on January 3, 1966. The second test was conducted from January 4, and the cut and wrap was performed on January 5, 1966 after 8 orbits and approximately 1300 stereo cycles of payload. The "B" mode was initiated and completed on January 6, 1966, after 5 orbits and approximately 600 stereo cycles of payload. The "failsafe" problem encountered in the first TASC test was not present in the second test.

The cycle rates for both instruments present the following problems. Numerous instances in which the cycle rate errors exceed 2% fast; and on four occasions the 2.15 second cycle period limit was exceeded. An examination of the temperatures shows that the first three occasions in which the master and slave instruments exceeded 2.15 seconds-during the "A" mode - the master instrument was at approximately 95°F. and the slave instrument was at approximately 90°F. The fourth occasion was in the "B" mode, and the master instrument was at approximately 76°F., and the slave instrument was at approximately 72°F. Table 2-1 tabulates the cycle rates for the test.

The clock - system time correlation is not as consistent as the first TASC test, but there were some power interrupts that introduce some instability in the initial reference readings of each delta correlation period. Table 2-2 shows the clock-system time correlation. The clock is considered to be acceptable for flight.

Examination of the TASC payload from both altitude tests indicate that instrument #187, S/I 85/109/76 and S/I 87/107/105 are acceptable for flight relative to tracking, cut and wrap, frame length and metered pitch, electrostatic corona and auxiliary data recording.

B. RESOLUTION TEST

Resolution and theodolite tests were performed on 14 January 1966. Results of the thru-focus resolution tests of pan instruments 186 and 187 show the following characteristics:

Master Pan Instrument No. 186

Maximum high contrast resolution 162 lines/mm at 0.000 focal position.

Maximum low contrast resolution 104 lines/mm at 0.000 focal position.

Slave Instrument No. 187

Maximum high contrast resolution 168 lines/mm at +.001 focal position.

Maximum low contrast resolution 109 lines/mm at +.001 focal position.

The test data for both instruments is shown in Figures 2-1 and 2-2. Both instruments met the system requirements specification.

C. LIGHT LEAK TEST

J-31 was subjected to the system light leak test on 4 February 1966 and again on 9 February 1966 using 3401 type film.

The first light leak test revealed acceptable master and slave instrument drum light leak fog. In addition, the slave film from instrument 187 exhibited heavy fogging attributed to the output horizon camera rubber boot. Visual examination of the suspect boot revealed a fairly large hole between the boot and horizon door interface. The boot leak was repaired. A second system light leak test demonstrated that the subject horizon boot leak had been repaired as evidenced by the absence of light fog.

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D. FLIGHT CERTIFICATION

Processed film from the flight readiness operation of J-31 contained a minus density line 1/8" wide the full length of each fogged format from the master camera (186). No anomalies were found in film from the slave camera (187).

Boston personnel inspected the master camera and found some foreign matter on the filter. After cleaning the filter, a second flight readiness operation was performed on the master camera only with satisfactory results.

In accordance with a formal request from Performance Evaluation, the slave camera starboard H/O boot was painted with "velvet" paint. After drying, the surface gave the appearance of black velvet with no smooth or bright spots. The adjacent master camera H/O boot did show some reflected light.

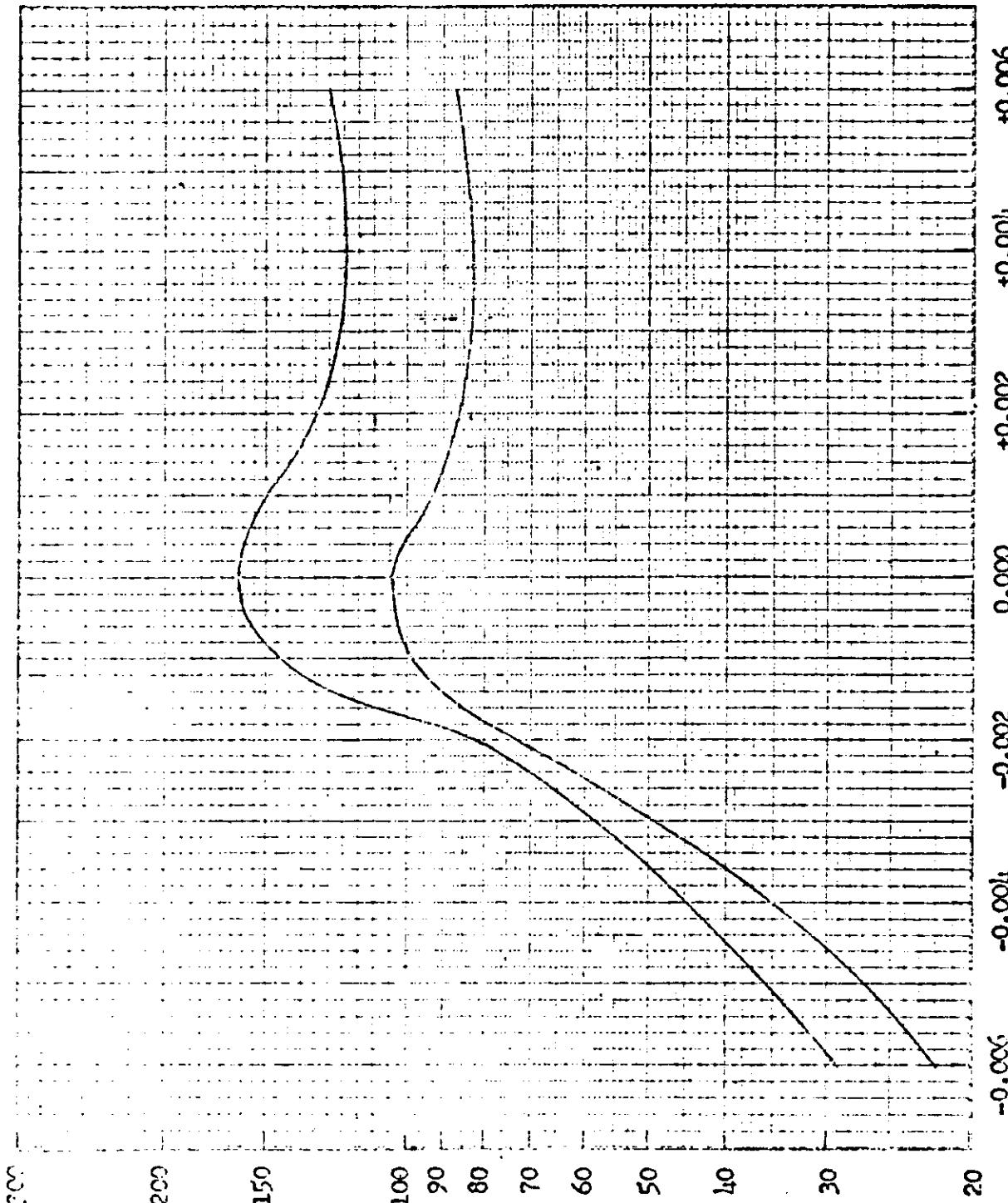
Flight loading of film and stray voltage and resistance checks were accomplished on 16 June 1966.

Tracking checks were performed on 17 June 1966 and the system was certified for flight.

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PRE-FLIGHT DYNAMIC RESOLUTION



Camera No: 186

Payload No: J-31

Resolution (l/mm)

High Contrast: 162

Low Contrast: 101

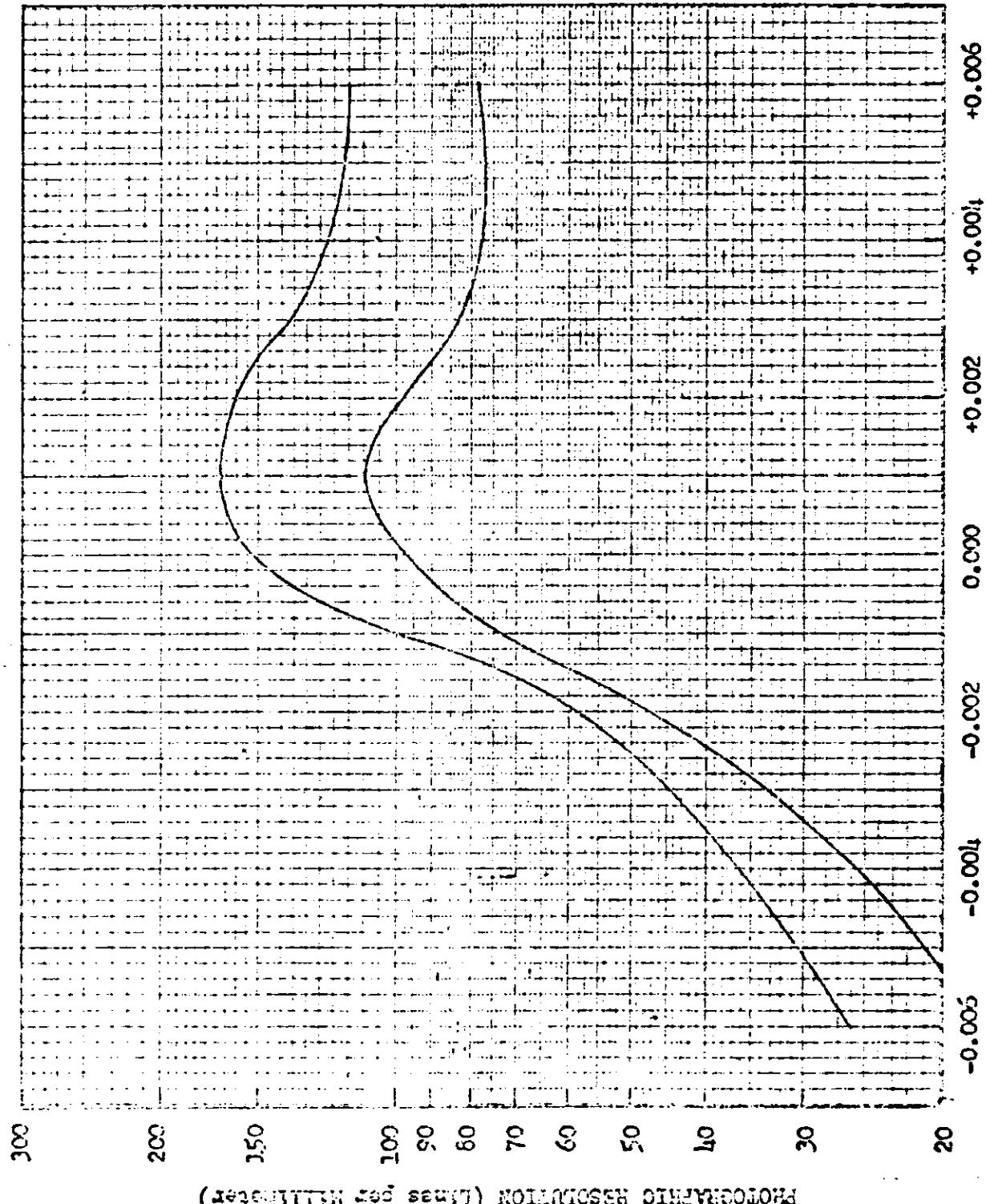
Film Type: 3404

Test Date: 1/11/66

Figure 2-1

TEST REPORT NO.

PHOTOGRAPHIC RESOLUTION



THROUGH FOCUS INCREMENTS (Inches)

TEST STRUCTURE

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NO.

J-31 186/187

TASC TEST 2

REV/MODE	RAMP	T.U.R.	ACT.	INST 186			INST 187			186/187 DIFF.
				CAL.	DEV.	ACT.	CAL.	DEV.		
CO A	10	2	0	6.625	6.571	0.82S	6.575	6.547	0.43S	-0.75
CO A	7	7	0	3.565	3.610	1.24F	3.558	3.603	1.25F	-0.20
CO A	7	7	0	3.540	3.610	1.93F	3.568	3.603	0.97F	0.79
CI A	7	7	392	3.400	3.468	2.52F	3.418	3.482	1.84F	0.53
CI A	7	7	2215	2.487	2.509	0.86F	2.499	2.512	0.51F	0.48
CO A	4	1	1427	2.140	2.194	2.47F				
CO A	4	1	1617				2.162	2.191	1.31F	
CO A	4	1	2027	2.11C	2.168	2.68F	2.143	2.184	2.86F	1.56
CO A	5	8	0	2.983	3.085	3.30F	3.020	3.083	2.03F	1.24
CO A	7	7	2462	2.587	2.649	2.32F	2.627	2.650	0.88F	1.55
CO A	7	7	3532	3.415	3.530	3.25F	3.460	3.524	1.81F	1.32
CO A	5	2	237	5.050	5.294	4.62F	5.135	5.276	2.68F	1.68
CO A	6	2	1727	2.163	2.206	1.94F				
CO A	8	2	2247				2.220	2.243	1.04F	
CO A	11	1	1452	2.590	2.623	1.27F	2.607	2.625	0.70F	0.66
CO A	11	1	1932	2.223	2.240	0.77F	2.233	2.246	0.58F	0.45
CO A	5	8	1090	2.624	2.647	0.87F	2.650	2.649	0.04S	0.99
CO A	5	8	1441	2.420	2.456	1.46F	2.440	2.459	0.79F	0.83
CO A	7	7	2173	2.783	2.830	1.66F	2.803	2.830	0.96F	0.72

Table 2-1

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REV/MODE	RAMP	T.U.R.	INST 186			INST 187			186/18 DIFF.	
			ACT.	CAL.	DEV.	ACT.	CAL.	DEV.		
C7 A	7	7	1586	2.483	2.530	1.86F	2.507	2.533	1.02F	0.97
C8 A	7	7	2426	2.587	2.623	1.38F	2.613	2.625	0.47F	1.01
C9 A	4	1	1009	2.610	2.652	3.05F	2.633	2.694	2.25F	0.88
C9 A	4	1	1739	(2.112	2.171	2.71F	(2.130	2.185	2.53F	0.85
C10 A	6	5	1970	2.207	2.249	1.85F	2.240	2.254	0.63F	1.50
C11 S	6	6	0	3.613	3.642	0.81F	3.625	3.636	0.29F	0.33
C12 S	7	7	363	3.425	3.493	1.95F	3.455	3.486	0.94F	0.88
C13 S	7	7	2213	2.500	2.508	0.31F	2.507	2.511	0.16F	0.28
C14 S	4	1	1425	2.154	2.194	1.84F				
C15 S	4	1	1617				2.150	2.191	1.86F	
C16 S	4	1	2025	2.128	2.168	1.85F	2.148	2.184	1.63F	0.94
C17 S	6	2	0	5.340	5.502	2.95F	5.410	5.483	1.32F	1.31
C18 S	7	7	0	3.520	3.610	2.48F	3.560	3.603	1.20F	1.14
C19 S	2	2	239	5.158	5.251	2.51F	5.173	5.273	1.89F	0.29
C20 S	8	2	1724	2.163	2.206	1.95F				
C21 S	6	2	2259				2.235	2.253	0.81F	

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THE (-) SIGN INDICATES THAT INST 1 IS SLOWER THAN INST 2
 F=FAST AND S=SLOW

Table 2-1

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J-31 TASC 2 CLOCK CHECK

IRIG REV	DAY	HR	MIN	SEC	IRIG SECCNDS	CLOCK SECONDS	DELTA IRIG	DELTA CLOCK	ERRC
001	4	9	25	38.275	379538.275	52735.513	---	---	---
002	4	10	56	10.310	384973.310	58170.558	5435.035	5435.045	0.01
003	4	15	12	43.390	393163.390	66360.670	8190.080	8190.112	0.03
004	4	15	59	43.395	395983.395	69180.641	2820.005	2819.971	-0.03
005	4	15	32	8.560	401528.560	74725.809	5545.165	5545.168	0.00
	0	6	6	30.285	DELTA TIME		TOTAL ACCUM. ERROR	0.01	
006	5	9	21	56.045	465716.045	240905.578	---	---	---
007	5	11	1	41.100	471701.100	246890.640	5985.055	5985.062	0.00
008	5	11	43	51.040	474231.040	249420.552	2529.940	2529.912	-0.02
	0	2	21	54.995	DELTA TIME		TOTAL ACCUM. ERROR	-0.02	
001	6	7	59	26.795	547166.795	115218.570	---	---	---
4	6	14	4	36.595	569076.595	137128.403	21909.800	21909.833	0.03
5	6	14	33	26.560	570806.560	138858.372	1729.965	1729.969	0.00
6	6	25	16	3.730	573363.730	141415.504	2557.170	2557.132	-0.03
	0	7	16	36.935	DELTA TIME		TOTAL ACCUM. ERROR	-0.00	

Table 2-2

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SECTION 3

FLIGHT OPERATIONS

A. SUMMARY

All launch, ascent, and injection events occurred as programmed which resulted in achieving the desired orbit. For the first time, the tape recorder was turned on during the ascent sequence to record the payload system temperature environment.

Both panoramic cameras operated satisfactorily throughout the flight. Average cycle rates on both instruments deviated from the pre-flight calibrated values by less than 2 per cent.

The V/h programmer failed on the end of Rev 4 or the beginning of Rev 5 and did not operate for the remainder of the flight. This resulted in FMC match errors greater than 5 percent.

The pressure make-up system developed a high pressure leak and gas depletion occurred on Rev 32.

The -1 and -2 stellar/index cameras operated satisfactorily throughout the flight. The clock, instrumentation, and command system functioned properly throughout the flight.

The thermal environment was within tolerance. The ascent temperature data from the tape recorder is included in Figure 3-1 and 3-2.

Both recovery systems operated satisfactorily with the exception of the -2 flashing light. This was the second -2 recovery system which the flashing light equipment was inoperative.

B. PANORAMIC CAMERA PERFORMANCE

Camera system dynamics were normal throughout the -1 and -2 missions. The film transport of both camera systems were normal. Cycle rate data (Table 3-1) indicates that the camera systems were generally less than 2.0 percent from the calibrated systems value. The master and slave instruments were generally less than 1.0 percent apart throughout most of the flight. The 99/101

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average clutch ratio was 6/6 for the master instrument and 6/6 for the slave instrument. Film depletion on the slave camera occurred prior to the engineering operation on Rev 159.

Panoramic Film Consumption (Frames)

	<u>Actual</u>	
	<u>Master</u>	<u>Slave</u>
Pre-launch	102	105
-1 Mission	2896	2930
-2 Mission	3039	2995
Total	6037	6030

FMC Match

The V/h programmer failed to cycle after Rev 04 of the mission. Telemetry indicated that the programmer started properly on the beginning of Rev 04 but was inoperative during Rev 05. This failure caused the two panoramic camera systems to operate at a constant cycle rate regardless of the time up ramp position.

Telemetry data indicated the V/h programmer had stopped at a position equivalent to the Reference Level voltage (see Figure 3-3). With the programmer in this position the Amplitude Command setting had no effect on the output voltage and only the Reference Command settings could be used to minimize FMC errors. Operational control under the above restrictions produced FMC errors of generally less than 10 per cent. However, FMC error on a few operations exceeded 20 per cent.

Analysis of this failure indicated that the most probable cause was the failure of the programmer self-energize switch (S201), See Figure 3-3. Failure of this switch to make contact resulted in loss of 400 cps voltage to the drive motor at the time S-202 applied reset voltage to the start relay. With S-202 retaining voltage on the reset coil, subsequent start commands were ineffective. This drive design has been used since the start of the Corona Program without a failure and this failure was considered to be random. The only corrective action was to review test procedures to assure proper operation of S-201.

~~TOP SECRET~~ [REDACTED]

C. STELLAR/INDEX CAMERA PERFORMANCE

The -1 stellar/index camera operation was normal throughout the mission with telemetry indicating proper metering and shutter operation.

The -2 stellar/index camera operation was also normal throughout the mission with no abnormalities noted on telemetry.

D. INSTRUMENTATION AND COMMAND SYSTEM PERFORMANCE

The instrumentation and command systems operated satisfactorily throughout the -1 and -2 missions with no abnormalities evident. The mono delay time was within the specified tolerance and operated satisfactorily.

E. CLOCK SYSTEM PERFORMANCE

The payload clock system performed satisfactorily during both phases of the mission. The clock/system time correlation data obtained from the [REDACTED] acquisitions are included in Table 3-2 and 3-3.

F. PRESSURE MAKE-UP SYSTEM PERFORMANCE

The pressure make-up system (PMU) developed a high pressure leak and gas depletion occurred on Rev 32 as indicated by Figure 3-4. This high pressure leak most probably occurred on the supply side of the on-off solenoid.

A review of the PMU design and the performance from the previous 25 flight units indicated the design was adequate. This failure was considered to be random and no further corrective action was taken.

G. THERMAL ENVIRONMENT

The temperature data obtained from the [REDACTED] acquisitions are contained in Table 3-4. Average panoramic camera temperatures for the master camera varied from 77° F to 61° F and the slave camera varied from 71° F to 55° F during the mission.

The ascent thermal environment was recorded on the tape recorder and is included in Figures 3-1 and 3-2.

~~TOP SECRET C~~

NO.

J-31 FLIGHT

I-----INST. 186-----I-----INST. 187-----I

REV.	CP	RAMP	TUR	SYSTEM	ACTUAL	UNIT	SYSTEM	ACTUAL	UNIT	SYSTEM	186/187	
NO.		R	A	SECS	CALIB.		DEV.	DEV.		DEV.	DEV.	DIFF.
69	A	7	6	2740	2.890	2.893	0.10S	0.11S	2.909	0.67S	0.66S	0.55
10	A	5	11	2740	2.638	2.650	0.50S	0.47S	2.680	1.57S	1.60S	1.13
32	A	3	11	2740	2.427	2.440	0.61S	0.52S	2.451	0.90S	0.98S	0.45
47	A	3	11	2740	2.427	2.450	1.02S	0.94S	2.450	0.85S	0.94S	-0.09
63	A	3	11	2740	2.427	2.426	0.03S	0.05F	2.443	0.57S	0.65S	0.70
79	A	3	11	2740	2.427	2.455	1.22S	1.14S	2.445	0.65S	0.73S	-0.41
80	B	5	11	2740	2.638	2.672	1.34S	1.30S	2.665	1.00S	1.03S	-0.26
95	B	3	11	2740	2.427	2.451	1.06S	0.98S	2.430	0.03S	0.11S	-0.86
111	B	3	11	2740	2.427	2.465	1.64S	1.55S	2.453	0.98S	1.06S	-0.49
127	B	2	11	2740	2.336	2.380	1.90S	1.79S	2.380	1.69S	1.79S	-0.00
143	B	2	11	2740	2.338	2.390	2.32S	2.22S	2.370	1.26S	1.36S	-0.84
159	B	2	11	2740	2.336	2.369	1.43S	1.32S	2.367	1.13S	1.24S	-0.08

DEV. AND DIFF. ARE IN PERCENT

THE (-) SIGN INDICATES THAT INST 1 IS SLOWER THAN INST 2

F=FAST AND S=SLOW

Table 3-1

~~TOP SECRET C~~

~~TOP SECRET C~~

NO.

J-31 1626 1034

ORDER FIT .1

SYS TIME I/P	CL TIME I/P	COMP SYS TM	DELTA ST	REV	STA
0.385114380 05	0.1571769910 06	0.3851144910 05	-0.0111	9	
0.779639780 05	0.1966295390 06	0.7796399030 05	-0.0123	16	
0.592196180 05	0.2382853730 06	0.3321981710 05	0.0009	24	
0.781216710 05	0.2831872340 06	0.7812167040 05	0.0006	32	
0.333876830 05	0.3248532550 06	0.3338768420 05	-0.0012	40	
0.726721680 05	0.3643377390 06	0.7267216140 05	0.0066	47	
0.335190760 05	0.4113846600 06	0.3351907430 05	0.0017	56	
0.729926410 05	0.4508582290 06	0.7299263650 05	0.0045	63	
0.336449480 05	0.4979105530 06	0.3364495240 05	-0.0044	72	
0.730941200 05	0.4886040000 06	0.7309410860 05	0.0114	79	
0.337371550 05	0.4753185100 05	0.3373714750 05	0.0075	88	
0.731267480 05	0.8692144000 05	0.7312672970 05	0.0183	95	
0.338080930 05	0.1340028060 06	0.3380808760 05	0.0054	104	
0.731993480 05	0.1733940740 06	0.7319934880 05	-0.0008	111	
0.338746110 05	0.2204693490 06	0.3387461570 05	-0.0047	120	
0.730629530 05	0.2596576980 06	0.7306295790 05	-0.0049	127	
0.339014050 05	0.3068561560 06	0.3390140780 05	-0.0028	136	
0.730364750 05	0.3463012350 06	0.7330648000 05	-0.0050	143	
0.339096530 05	0.3933045970 06	0.3390983390 05	-0.0009	152	
0.732530500 05	0.4326478290 06	0.7325305910 05	-0.0091	159	

AO=-0.11866551460 06 AI= 0.9999998277000 00

SIGMA=0.00716 NC. POINTS= 20

RATIO OF CLOCK TIME TO SYS TIME= 0.1000000172300 01

Table 3-2

~~TOP SECRET C~~

~~TOP SECRET C~~

NO.

J-31 1626 1034

ORDER FIT 2

SYS TIME I/P	CL TIME I/P	COMP SYS TM	DELTA ST	REV	STA
0.385114380 05	0.1571769910 06	C.3851143910 05	-0.0011	9	
0.779639780 05	0.1966295390 06	0.7796398330 05	-0.0053	16	
0.332198180 05	0.2382853730 06	0.3321981290 05	0.0051	24	
0.781216710 05	0.2831872340 06	0.7812166880 05	0.0022	32	
0.335876830 05	0.3248532550 06	0.3336768470 05	-0.0017	40	
0.728721680 05	0.3643377390 06	0.7287216350 05	0.0045	47	
0.335190760 05	0.4113846600 06	0.3351907800 05	-0.0020	56	
0.729926410 05	0.4508582290 06	0.7299264120 05	-0.0002	63	
0.336449460 05	0.4979105530 06	0.3364495790 05	-0.0099	72	
0.730941200 05	0.4888046000 03	0.7309411450 05	0.0055	79	
0.337371550 05	0.4753185100 05	0.3373715340 05	0.0016	88	
0.731267480 05	0.8692144000 05	0.7312673530 05	0.0127	95	
0.338080930 05	0.1340028060 06	0.3380809240 05	-0.0006	104	
0.731993480 05	0.1733940740 06	0.7319935260 05	-0.0046	111	
0.338746110 05	0.2204693490 06	0.3387461800 05	-0.0070	120	
0.730629530 05	0.2596576980 06	0.7306295860 05	-0.0056	127	
0.339014050 05	0.3068561560 06	0.3390140610 05	-0.0011	136	
0.733064750 05	0.3463012350 06	0.7330647600 05	-0.0010	143	
0.339098330 05	0.3933045970 06	0.3390982680 05	0.0062	152	
0.732530500 05	0.4326478290 06	0.7325304910 05	0.0009	159	

A0=-0.11866553950 06 A1= 0.999999936404D 00

A2=-6.9657944836711D-13

SIGMA=0.00499 NC. POINTS= 20

Table 3-3

~~TOP SECRET C~~

TABLE 3-hJ-21 TEMPERATURE SUMMARY

SUSP.

ORBITS ACQUIRED

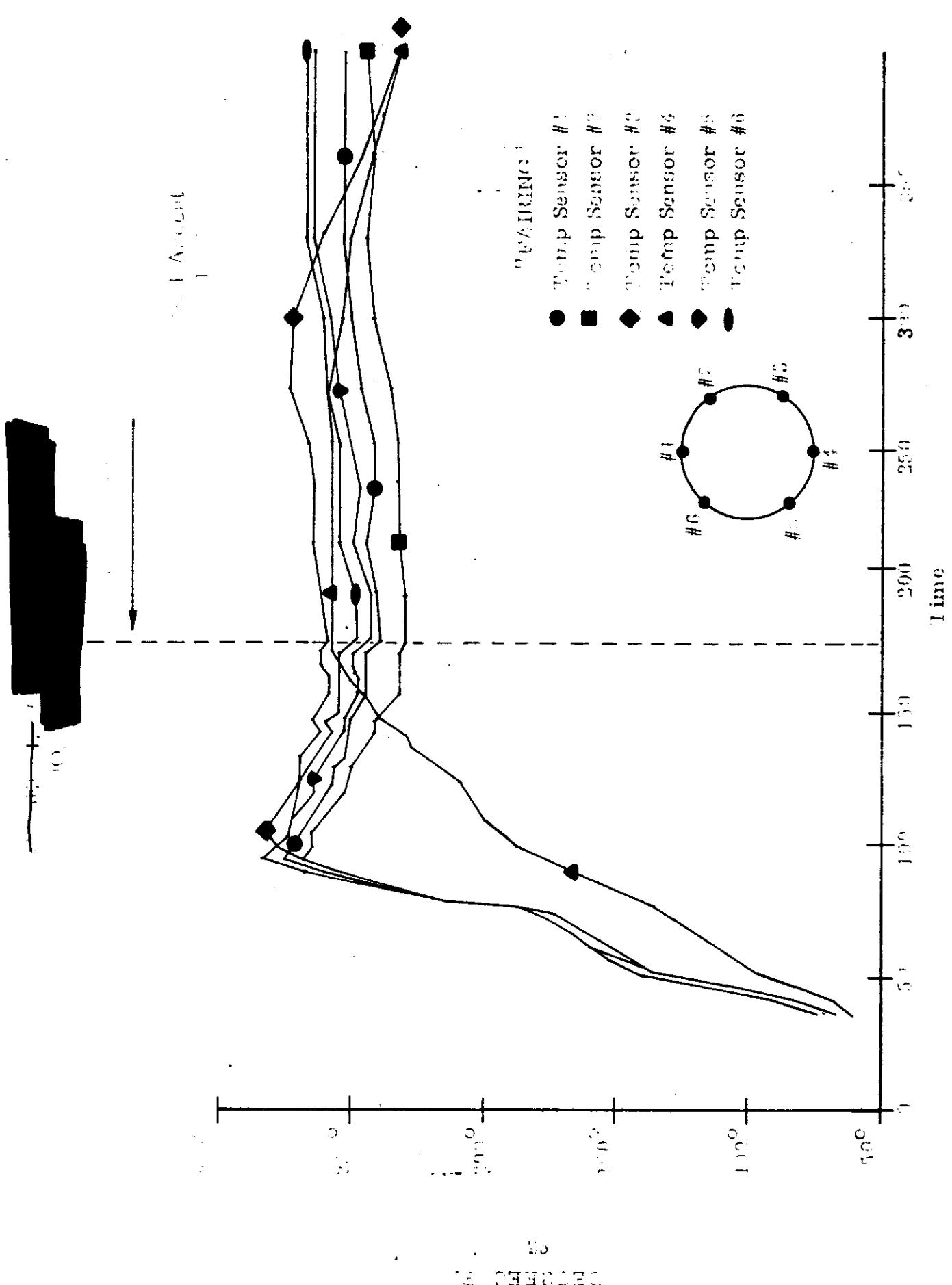
<u>Orbit</u>	<u>L/O Pad</u>	<u>29</u>	<u>16</u>	<u>24</u>	<u>32</u>	<u>40</u>	<u>47</u>	<u>56</u>	<u>63</u>	<u>72</u>	<u>83</u>	<u>92</u>	<u>101</u>	<u>120</u>	<u>121</u>	<u>135</u>	<u>143</u>	<u>152</u>		
3	65	70	63	70	67	70	63	66	67	65	65	60	60	53	64	57	63	59	63	
4	64	76	71	75	74	71	78	75	77	73	74	71	71	66	62	66	61	62	66	
5	59	78	74	74	74	76	76	75	75	72	72	70	69	66	66	67	65	67	67	
6	59	78	76	76	77	75	77	75	77	72	72	70	69	66	66	65	65	65	65	
7	64	78	75	75	77	74	77	75	77	73	73	71	71	67	67	63	63	67	67	
8	63	80	76	77	77	75	78	76	76	76	76	75	75	70	64	59	61	61	61	
9	63	71	67	67	67	67	78	76	76	76	76	73	73	70	64	64	66	69	69	
10	64	71	67	67	67	67	78	76	76	76	76	73	73	70	64	64	66	69	69	
11	67	78	76	76	76	76	77	75	75	75	75	71	71	67	67	63	63	67	67	
12	71	78	73	73	74	73	77	73	73	73	73	71	71	67	67	64	64	67	67	
13	59	76	75	75	72	74	75	74	74	74	74	72	72	70	67	67	63	63	67	
Avg	64	77	74	74	76	73	75	74	74	74	74	71	71	70	67	67	63	61	61	
Master Square																				
1	61	64	69	69	72	71	69	69	69	69	69	66	65	63	62	59	57	57	55	
2	54	54	59	59	76	72	75	71	73	73	73	69	71	68	69	56	57	50	53	
3	57	59	59	59	75	71	75	71	73	73	73	70	70	65	67	52	52	62	64	
4	67	55	55	55	74	72	74	71	72	72	72	67	67	63	64	60	60	64	65	
5	57	57	57	57	72	67	70	67	70	70	70	69	69	66	66	62	62	62	62	
6	57	57	57	57	73	69	73	71	73	73	73	70	70	67	67	63	63	63	65	
7	57	57	57	57	74	72	74	71	73	73	73	70	70	67	67	63	63	63	65	
8	57	57	57	57	72	67	70	67	70	70	70	67	67	63	63	60	60	64	64	
9	58	58	58	58	73	69	73	68	72	72	72	69	69	66	66	63	63	63	65	
10	-	-	-	-	71	67	71	68	72	72	72	69	69	67	67	-	-	-	-	
11	62	62	67	63	66	63	65	63	63	63	63	61	61	59	59	55	55	55	55	
12	57	69	66	69	64	67	61	67	61	67	61	63	63	60	58	58	52	52	52	
13	53	66	64	65	64	65	65	63	63	63	63	60	60	58	58	55	55	55	55	
Avg	63	71	68	71	67	69	67	69	67	69	67	65	65	64	64	59	59	57	57	
Supply Spool																				
1	59	62	59	62	58	62	62	62	62	62	62	60	61	60	59	55	57	53	56	55
2	59	63	60	63	60	62	61	62	61	62	61	58	59	52	55	57	54	49	53	51

NOTE: All data corrected for self-heating, except injection.

TABLE 3-4
TEMPERATURE SUMMARY

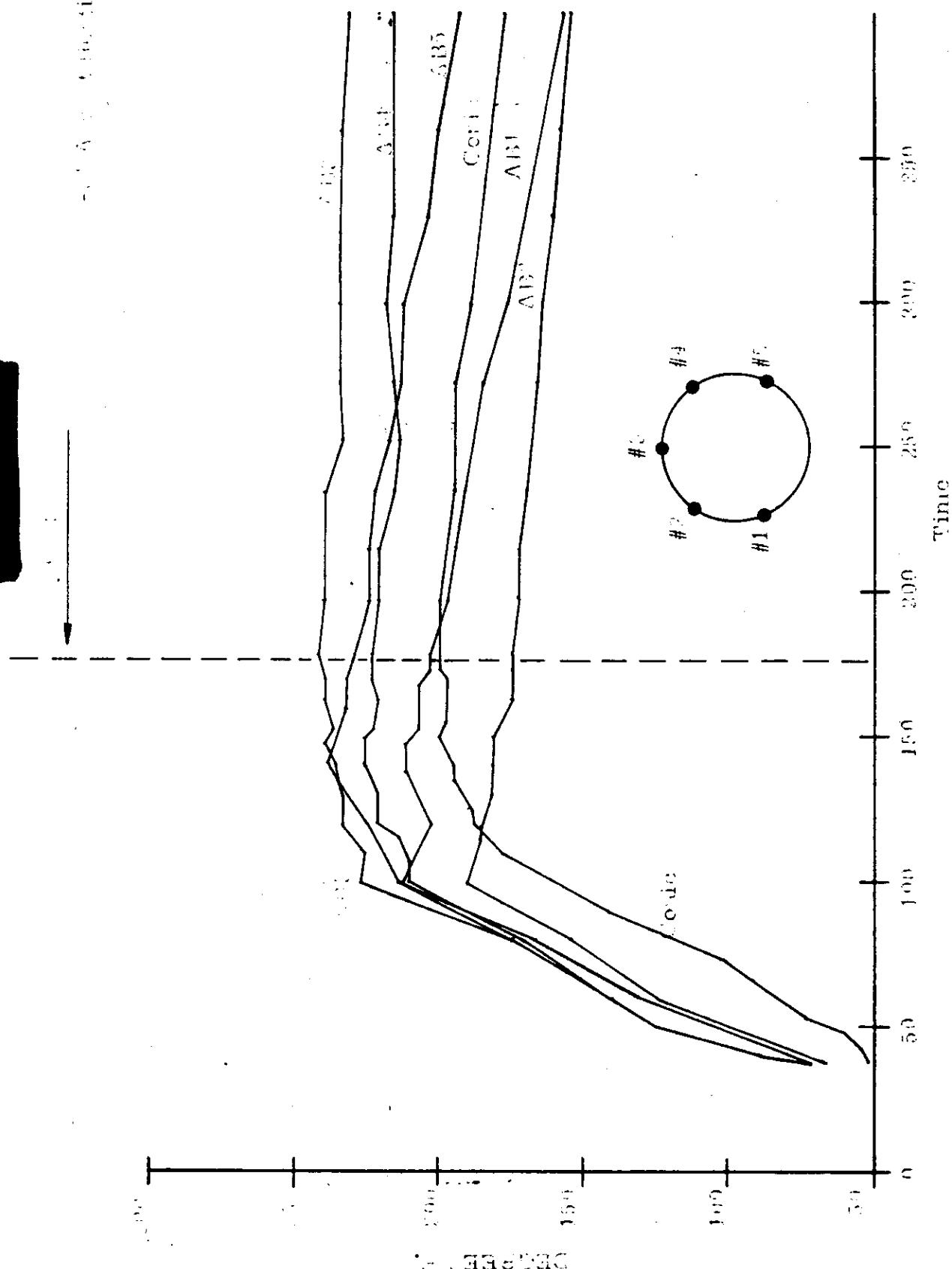
STATION		ORBITS ACQUIRED																					
Pair	(A)	(B)	L/O Pad	09	16	24	32	40	47	55	63	72	79	88	95	104	111	120	127	135	143	152	
1	--	22	81	22	78	19	81	22	78	15	71	21	44	21	44	18	41	21	44	21	44	21	
2	--	0	13	0	10	0	16	0	16	-4	29	56	78	53	78	53	84	59	90	90	93	93	
3	227	-13	15	-9	8	-9	13	-9	15	-13	15	58	143	58	146	55	148	58	146	58	146	49	
4	223	35	52	35	42	32	52	45	48	26	45	19	68	19	59	19	59	16	52	13	49	10	
5	--	44	51	41	47	37	54	37	44	34	44	22	28	22	35	16	25	16	25	16	25	9	
6	--	35	63	35	77	32	74	62	71	25	61	--	--	--	--	--	--	--	--	--	--	--	
<u>Parity</u>																							
1	144	39	54	33	48	30	51	30	45	27	42	24	36	21	30	18	24	18	27	18	27	12	
2	144	31	29	51	81	24	81	28	76	21	70	21	61	21	53	15	49	15	46	15	46	12	
3	--	50	149	54	140	50	143	50	140	44	137	54	134	50	131	50	137	50	137	50	137	44	
4	216	48	61	55	61	51	74	51	74	48	77	55	74	55	77	55	83	55	83	55	89	51	
5	191	46	69	64	61	45	64	42	64	42	64	38	55	38	51	38	51	42	58	58	58	38	
<u>Conic Angle</u>																							
1	161	26	39	29	36	23	36	23	29	16	26	13	16	10	10	6	6	6	6	6	6	3	
<u>Clock</u>																							
1	90	61	63	61	63	61	63	61	63	61	59	61	55	51	51	49	51	47	51	51	51	49	
2	94	60	60	62	60	60	62	60	60	60	58	58	58	54	52	50	48	50	46	50	50	48	
<u>Trust Curve "A" to "B" SRV</u>																							
1	116	37	34	33	33	40	33	33	32	32	32	32	32	32	32	32	32	32	32	32	32	32	
2	72	53	35	47	43	44	42	43	41	37	37	37	37	37	37	37	37	37	37	37	37	37	
<u>Steiner/Index "A" to "B"</u>																							
1	84	51	43	51	48	48	45	51	42	48	54	51	42	48	51	42	48	48	45	48	45	48	
2	71	48	48	45	45	45	45	45	45	45	45	45	45	45	45	45	45	45	45	45	45	43	
<u>Recovery Battery "B" SRV</u>																							
1	69	67	63	63	63	63	63	63	63	63	62	63	61	62	63	62	63	62	63	62	63	62	
2	91	67	64	65	66	66	66	66	66	66	65	66	66	66	66	66	66	66	66	66	66	66	
<u>Master Cassette "A" SRV</u>																							

NOTE: Only Thrust Cone Data recorded from first orbit.

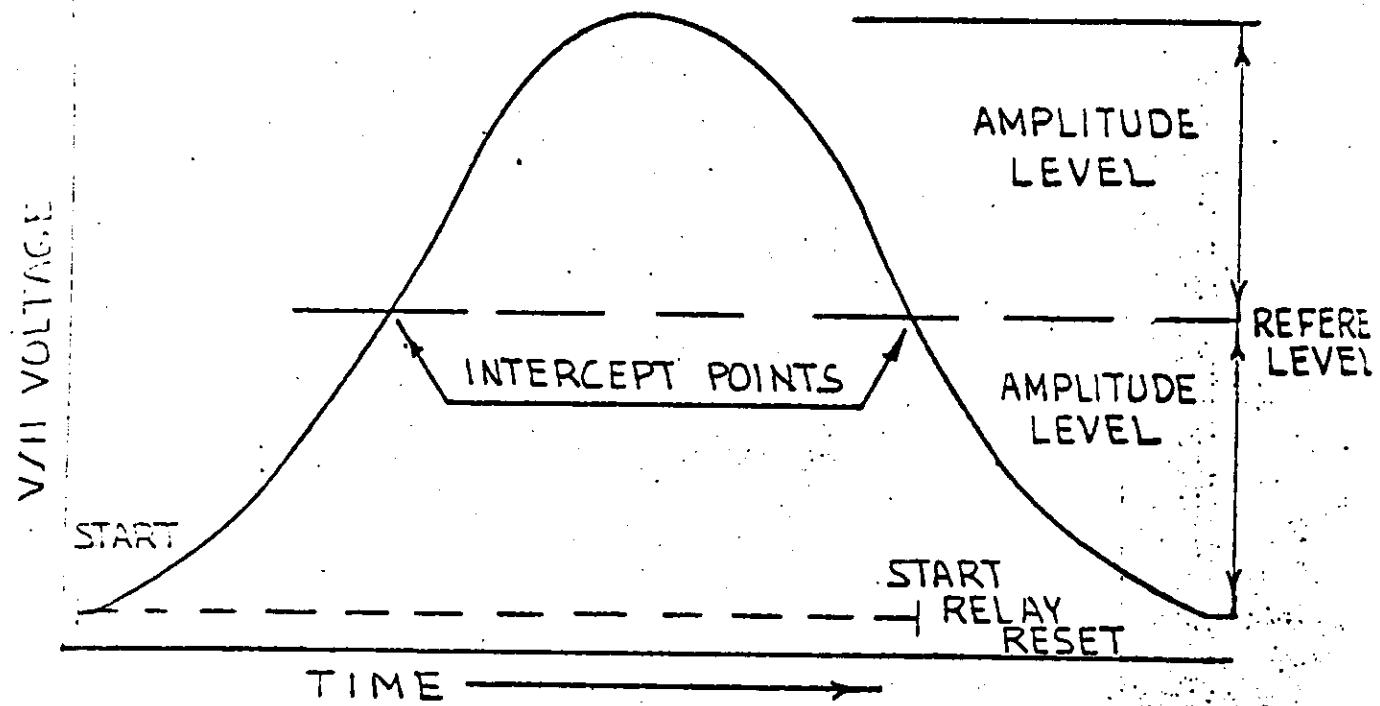


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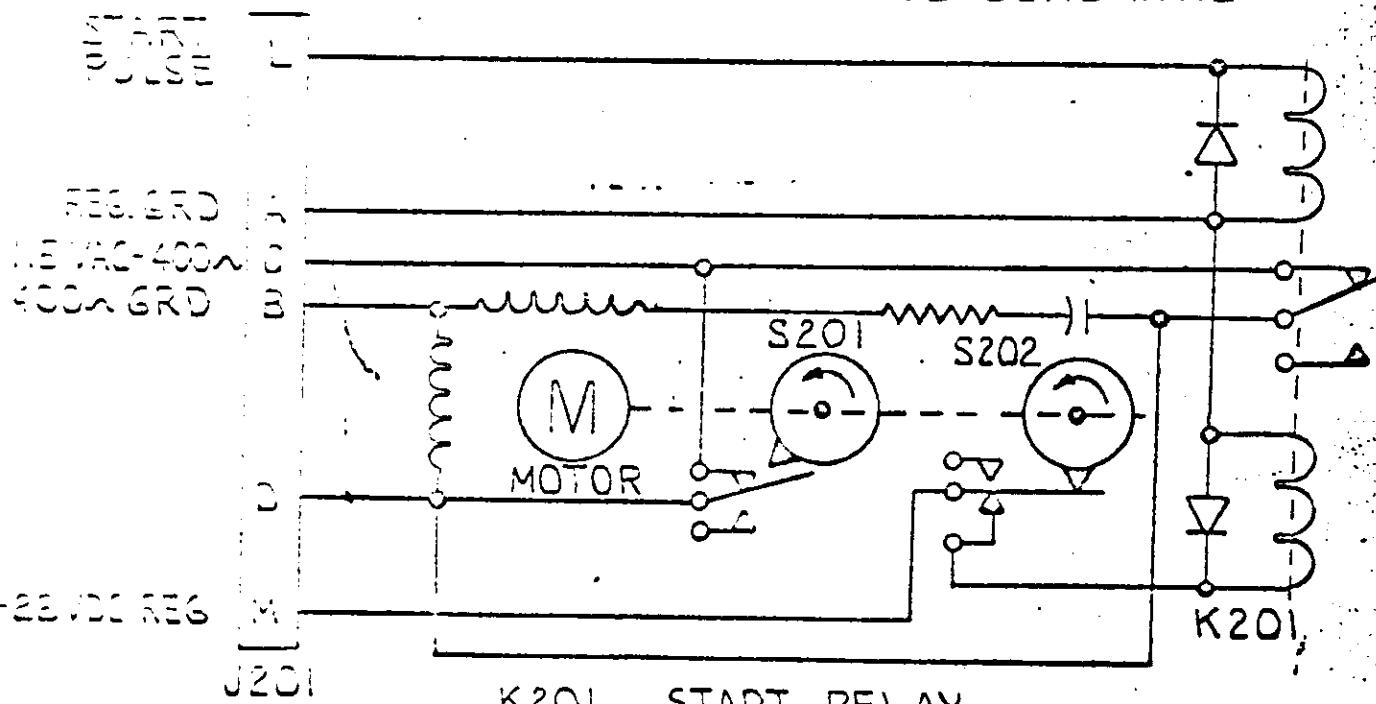
2.5 Å (100% PEG)



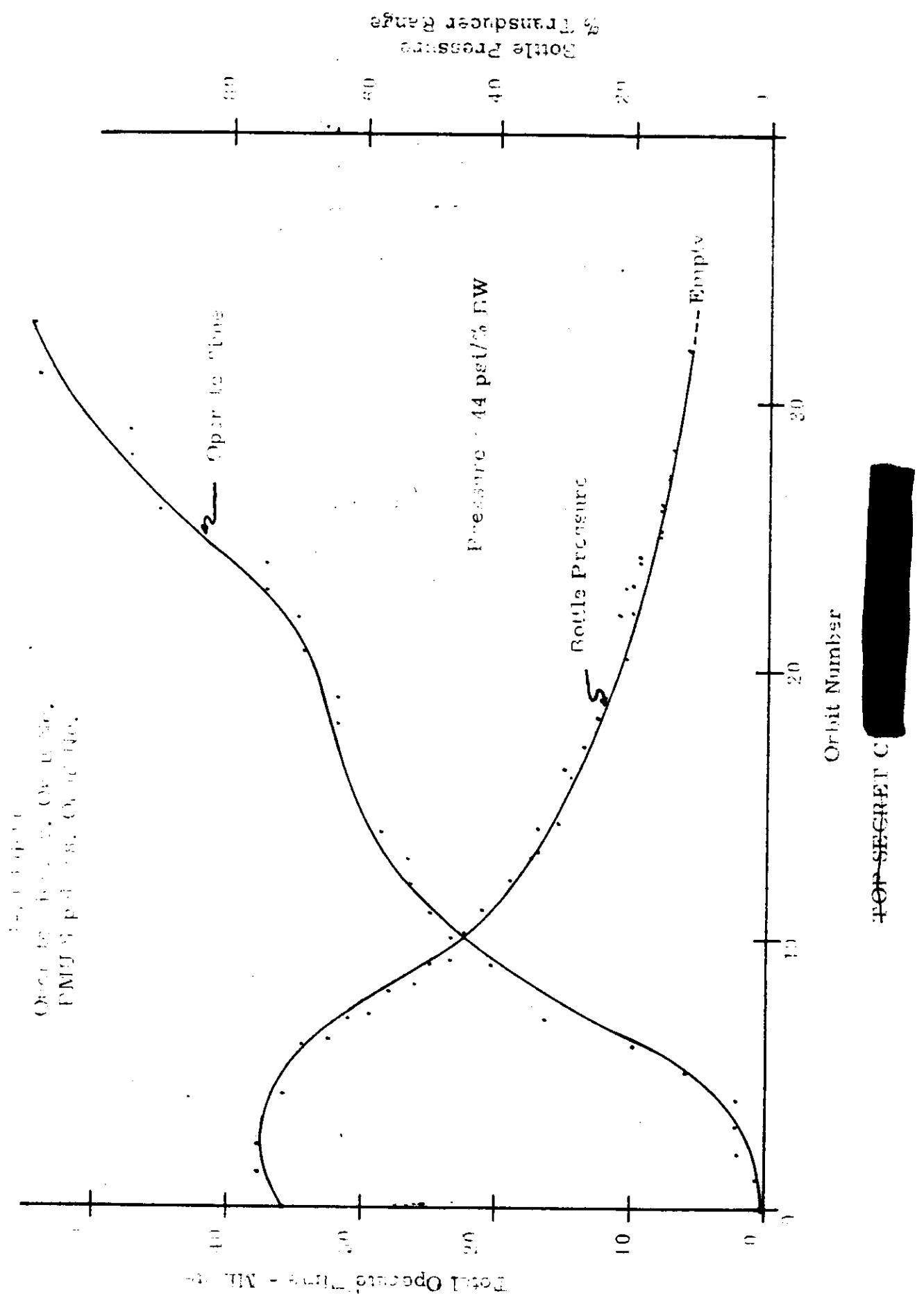
VSH PROGRAMMER VOLTAGE PROFILE



VSH PROGRAMMER DRIVE SCHEMATIC



K201 START RELAY
 S201 SELF ENERGIZE SWITCH
 S202 START RELAY RESET SWITCH



~~TOP SECRET C~~

'NO.

SECTION 4

MISSION 1034-1 RECOVERY SYSTEM

SRV #713 was received at A/P on 23 August 1965. The receiving weight was 148.9 pounds. After modifications and incorporation of outstanding E.O.'s, the SRV was delivered to Systems Test for incorporation into the J-31 system.

The capsule was shipped to VAFB on 18 May 1966.

The -1 recovery system was successfully recovered by air catch from orbit 81 on 26 June 1966. The impact point was as follows:

Predicted Impact $25^{\circ}02'N/156^{\circ}59'W$

Actual Impact $25^{\circ}00'N/157^{\circ}02'W$

The conditions of the recovered capsule was satisfactory with no damage other than normal paint blistering due to the re-entry environment.

Event times are shown in Table 4-1.

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~~TOP SECRET C~~

NO.

MISSION 1034-1

RECOVERY SEQUENCE OF EVENTS

Event	Delta Time (Seconds)	
	Actual	Nominal
*Arm	76.97	77.0 ± 1.0
*Transfer	2.01	2.0 ± 0.25
Electrical Disconnect	0.64	$0.900 \begin{matrix} +0.430 \\ -0.400 \end{matrix}$
Separation	---	---
*#Spin	3.4	3.4 ± 0.30
Retro	7.49	7.55 ± 0.45
Despin	10.60	10.75 ± 0.59
T/C Separation	1.52	1.5 ± 0.15
***"G" Switch Open	527.45	526.6
Parachute Cover Off	33.80	34.0 ± 1.5
Drogue Chute Deployed	0.67	0.68 ± 0.08
Main Chute Bag Separate	10.19	10.25 ± 1.5
Main Chute Deployed	0.55	0.62 ± 0.13
Main Chute Disreef	4.51	4.5 ± 0.80

* From Separation

** From Electrical Disconnect

*** From Retro

TABLE 4-1

~~TOP SECRET C~~

SECTION 5

MISSION 1034-2 RECOVERY SYSTEM

SRV #714 was received at A/P on 23 August 1965. The receiving weight was 151.7 pounds. After modifications and incorporation of outstanding E.O.'s the unit was delivered to Systems Test for mating to the J-31 system.

The capsule was shipped to VAFB on 18 May 1966.

The -2 recovery system was successfully recovered by air catch from orbit 161 on 1 July 1966. The impact point was as follows:

Predicted Impact $24^{\circ}36'N/170^{\circ}16'W$

Actual Impact $24^{\circ}38.4'N/169^{\circ}59.4'W$

Event times are shown in Table 5-1.

The condition of the recovered capsule indicated no abnormal re-entry effects.

It was reported by the recovery aircraft that the flashing light was working during descent. However, after the recovery system was caught and being reeled into the aircraft the flashing light was inoperative. Post recovery tests indicated satisfactory operation of all equipment. The unit was returned to G. E. for a detailed analysis. G. E. located the component that caused the intermittent failure.

~~TOP SECRET C~~

NO.

MISSION 1034-2

RECOVERY SEQUENCE OF EVENTS

<u>Event</u>	<u>Delta Time (Seconds)</u>	
	<u>Actual</u>	<u>Nominal</u>
*Arm	76.96	77.0 ± 1.0
*Transfer	1.96	2.0 ± 0.25
Electrical Disconnect	0.90	$0.900 \begin{matrix} +0.430 \\ -0.400 \end{matrix}$
Separation	--	--
**Spin	3.41	3.4 ± 0.30
Retro	7.63	7.55 ± 0.45
Despin	10.73	10.75 ± 0.59
T/C Separation	1.51	1.5 ± 0.15
***"G" Switch Open	534.94	534.0
Parachute Cover Off	34.08	34.0 ± 1.5
Drogue Chute Deployed	0.63	0.63 ± 0.08
Main Chute Bag Separate	9.78	10.25 ± 1.5
Main Chute Deployed	0.44	0.52 ± 0.13
Main Chute Disreef	4.32	4.45 ± 0.80

* From Separation

** From Electrical Disconnect

*** From Retro

TABLE 5-1

~~TOP SECRET C~~

~~TOP SECRET C~~

NO.

SECTION 6

MISSION 1034 PANORAMIC CAMERAS

A. COMPONENT ASSIGNMENT

<u>Component</u>	<u>Master Serial Number</u>	<u>Slave Serial Number</u>
Main Camera	186	187
Main Camera Lens	1942435	1932435
Supply Horizon Camera	290-G6	302-G6
Supply Horizon Camera Lens	E12846	E12843
Take-up Horizon Camera	290-G5	302-G5
Take-up Horizon Camera Lens	E12875	E12833
Supply Cassette	SC-41	SC-41

B. CAMERA DATA AND FLIGHT SETTINGS

Main Camera:

Lens	24" f/3.5	24" f/3.5
Slit Width	0.200"	0.150"
Filter Type	Wratten 23A	Wratten 21
Film Type (Eastman)	3404	3404

Supply Horizon Camera:

	<u>Port</u>	<u>Starboard</u>
Lens	55 mm f/6.3	55 mm f/6.3
Aperture Setting	f/6.3 Port	f/8.0
Exposure Time	1/100 second	1/100 second
Filter Type	Wratten 25	Wratten 25

~~TOP SECRET C~~

NO.

Take-up Horizon Camera	<u>Master</u>	<u>Slave</u>
Lens	55 mm f/6.3	55 mm f/6.3
Aperture Setting	f/8.0	f/6.3
Exposure Time	1/100 second	1/100 second
Filter	Wratten 25	Wratten 25

C. POST FLIGHT PERFORMANCE EVALUATION

The overall image quality was not as good as on recent missions. The selection of the best frames for the MIP rating (80) indicates that the quality was below that expected for the J system. The average altitude was 6% higher than normally flown which decreases the obtainable ground resolution. This mission was flown in the latter part of June and it has been observed that the atmospheric conditions degrade the photography more so than in early winter or spring. Another factor that can degrade is the higher solar elevations giving rise to more specular reflections. The best ground resolution observed on several fixed targets was 14' feet.

The V/h programmer failed during Rev. 04. See discussion in Section 3-B. Visual inspection of the photography at 40X magnification showed smear and/or double images in the flight direction. Flight data indicates V/h mismatch generally below 10% with some as high as 20%.

The master camera film experienced corona marking starting on pass 38D. This fog was caused by the input metering rollers at instrument starts. Three inches of film was affected at each start up. The pressure make-up system was exhausted at this time due to gas leakage.

There was minor light leak fog on a few frames which occurred during non-operate periods. The source of this light leak is at the drums of the pan cameras. An improved light seal is to be incorporated in Systems J-36 and up.

Static discharge on the film edges were less than normal. Rail scratches were minor and there were no ragged format edges. There were the normal minor scratches in the formats of both cameras.

~~TOP SECRET C~~

~~TOP SECRET C~~

NO.

The starboard looking (sun side) horizon camera on the master instrument produced veiled imagery from pass 8 D through 35D. The condition started and stopped gradually and it was not as severe as on Mission 1033. The surfaces in front of the starboard looking horizon camera of the slave instrument were painted a dull black and there was no veiled imagery. Subsequent missions will have the H.O. boot and lens mount face painted a dull black.

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NO.

SECTION 7

MISSION 1034 STELLAR-INDEX CAMERAS

A. COMPONENT ASSIGNMENT

<u>Component</u>	<u>-1 Mission Serial Number</u>	<u>-2 Mission Serial Number</u>
Camera	D-85	D-87
Index Reseau	109	107
Stellar Reseau	76	105

B. CAMERA DATA AND FLIGHT SETTINGS

Stellar Camera:

Lens	85 mm f/1.8	85 mm f/1.8
Exposure Time	2 seconds	2 seconds
Filter Type	None	None
Film Type (Eastman)	3401	3401

Index Camera:

Lens	38 mm f/4.5	38 mm f/4.5
Exposure Time	1/500 second	1/500 second
Filter Type	Wratten 21	Wratten 21
Film Type (Eastman)	3400	3400

C. POST FLIGHT PERFORMANCE EVALUATION

The -1 instruments each produced 415 frames of good photography. Light flare was present over 35% of each stellar format. The index camera correlation lamp functioned normally through frame 5 and then produced images of very low density. This anomaly was due to a loosened electrical connection. Static discharges were considered to be of the normal level. There was no exposure on frame 1 of the index photography.

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NO.

The -2 S/I unit satisfactorily produced 409 frames of stellar and 423 frames of index photography. The stellar frames contained 20 or more images and 30% flare. The film was exhausted before the end of the main camera exposure and the ends were fogged. A similar anomaly was investigated on Mission 1033 and it was discovered that the hot wire film cutter can operate before the programmed time in the recovery sequence. Corrective action has been initiated.

The percentage of index frames with less than 10% cloud cover over terrain was 12% on -1 and 22% on -2. The same analysis over snow and ice showed 4% on -1 and 2% on -2 mission.

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SECTION 8

PANORAMIC CAMERA EXPOSURE

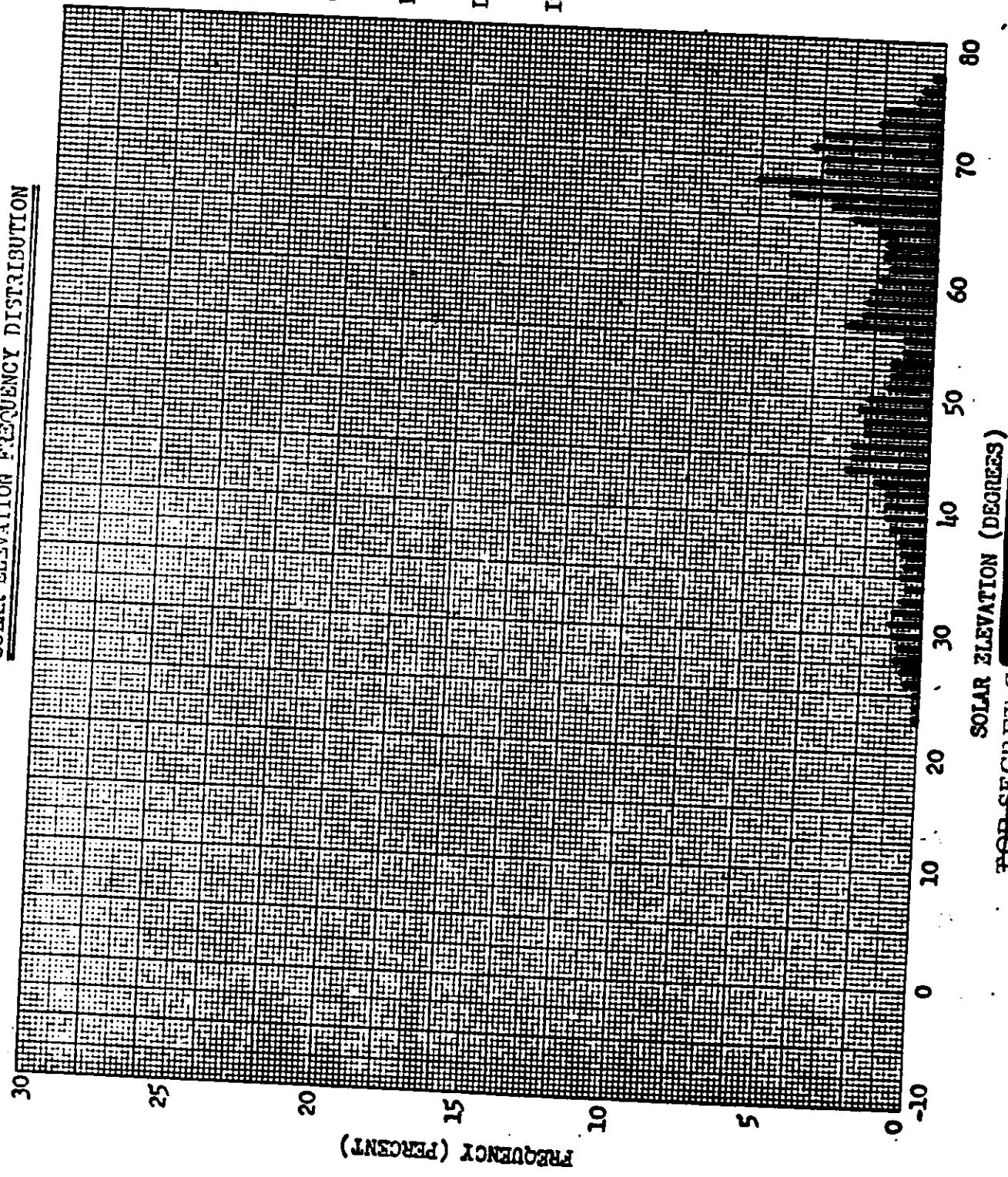
The Master camera contained a 0.200 inch slit and a Wratten 23A filter. The Slave camera had a 0.150 inch slit and a Wratten 21 filter. These conditions placed the nominal exposure on the full processing curve.

The frequency distributions of the solar elevations and solar azimuths encountered during the photographic operations are shown in Figures 8-1 to 8-4.

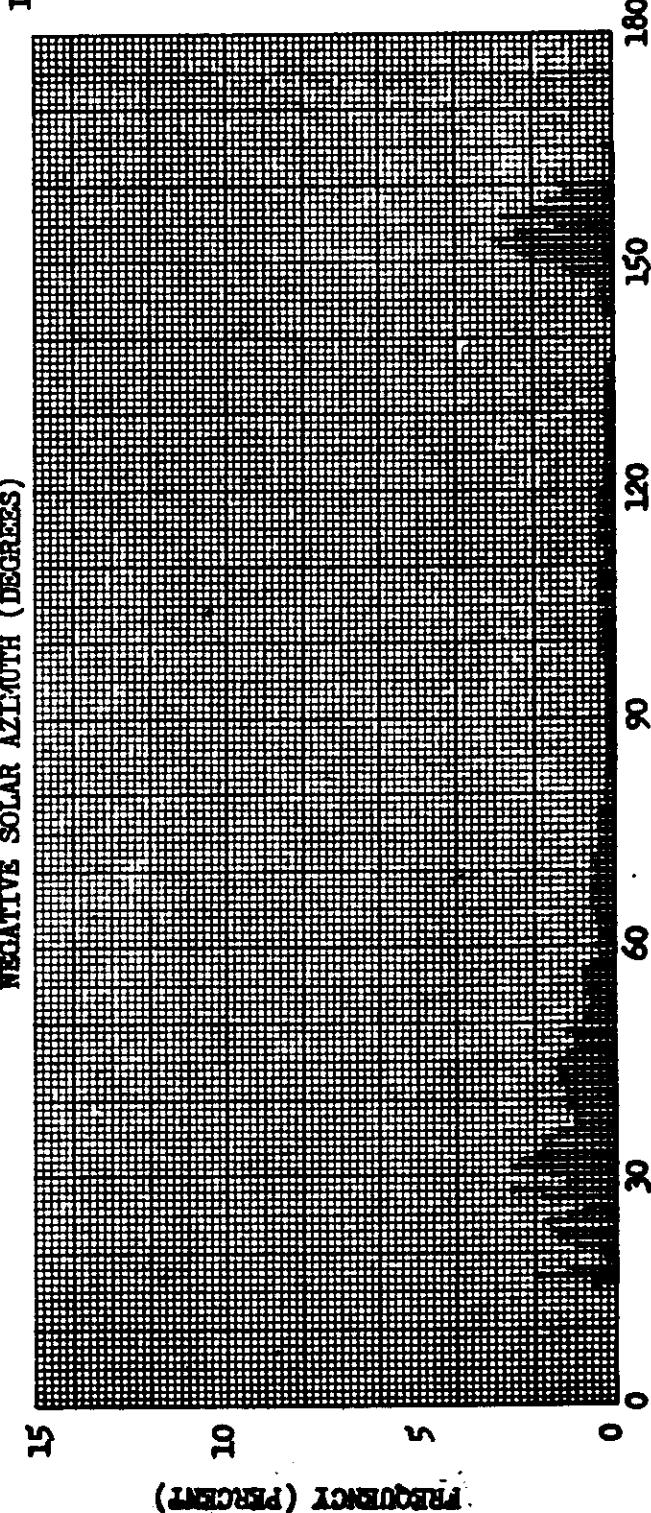
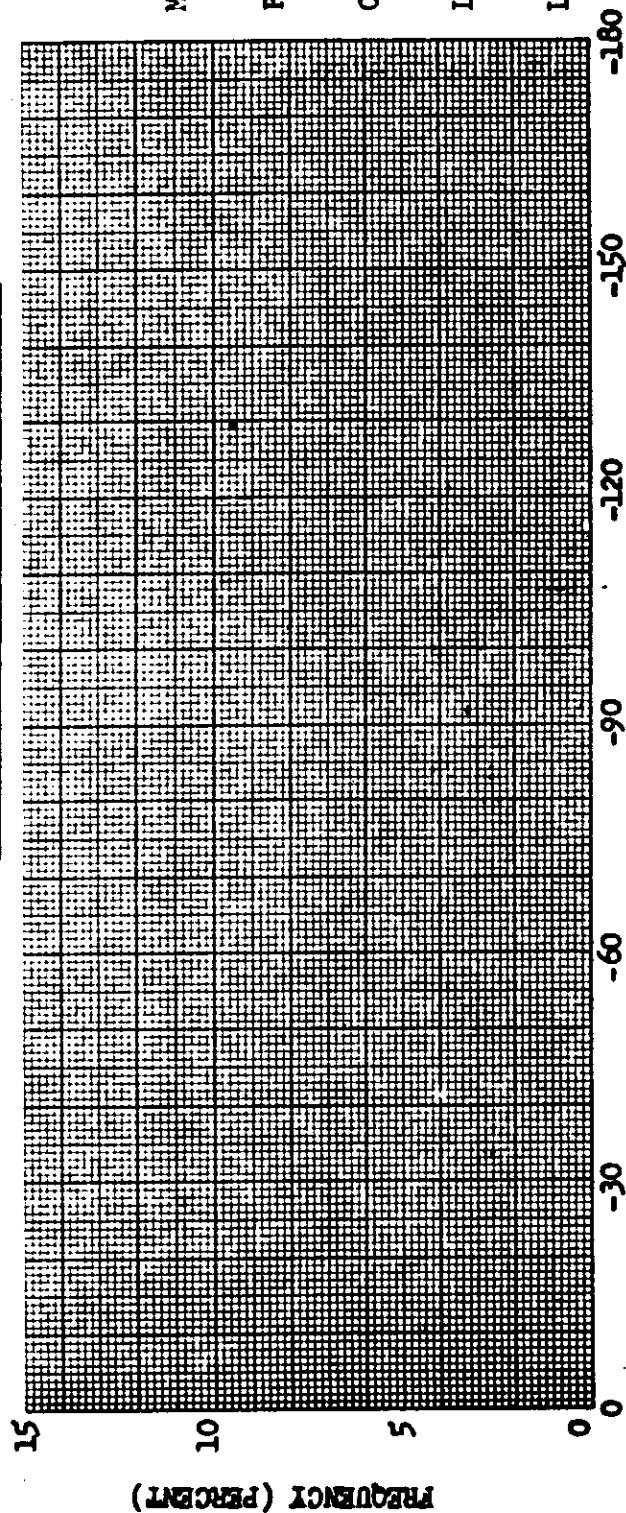
The nominal exposure times of the Master and Slave cameras are shown as a function of latitude for passes D-8, D-56, D-104 and D-152 in Figures 8-5 to 8-12. The predicted level of processing for the original negative is based on the in-flight performance estimate and is tabulated below with the processing levels reported by [REDACTED]

<u>Mission</u>	<u>Camera</u>		<u>% Primary</u>	<u>% Intermediate</u>	<u>% Full</u>
1034-1	FWD	Predicted	0	96	4
		Reported	2.6	20.9	76.5
1034-1	AFT	Predicted	0	55	45
		Reported	1.9	31.5	66.6
1034-2	FWD	Predicted	0	88	12
		Reported	8.9	25.7	65.4
1034-2	AFT	Predicted	0	41	59
		Reported	6.1	37.3	56.6

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SOLAR ELEVATION FREQUENCY DISTRIBUTION



SOLAR AZIMUTH FREQUENCY DISTRIBUTION



Mission No: 103L-1

Payload No: J-31

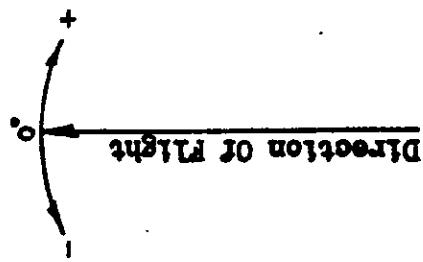
Camera No: 106

Launch Date: 6/21/66

Launch Time: 2131 Z

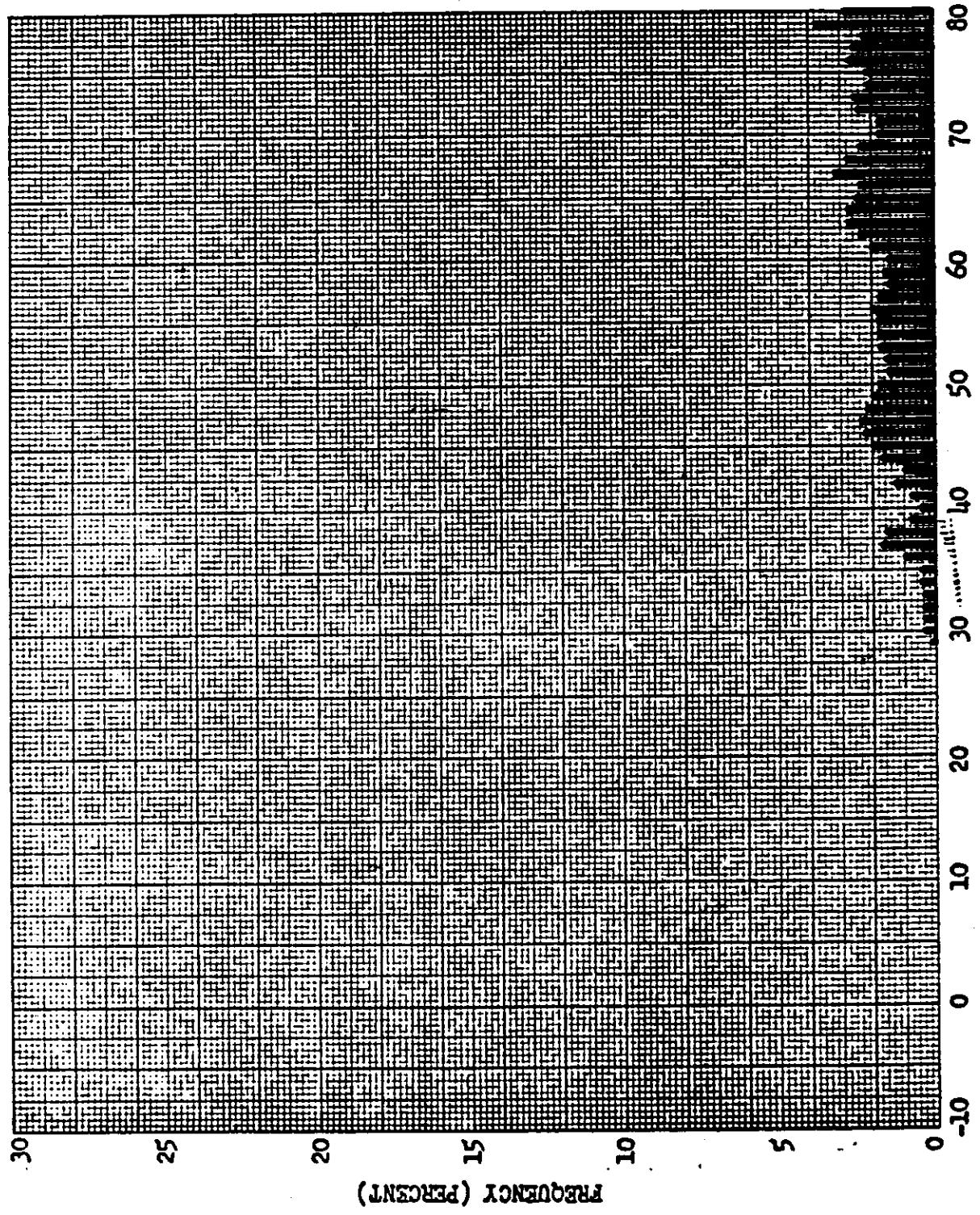
Inclination: 80°

SIGN NOTATION

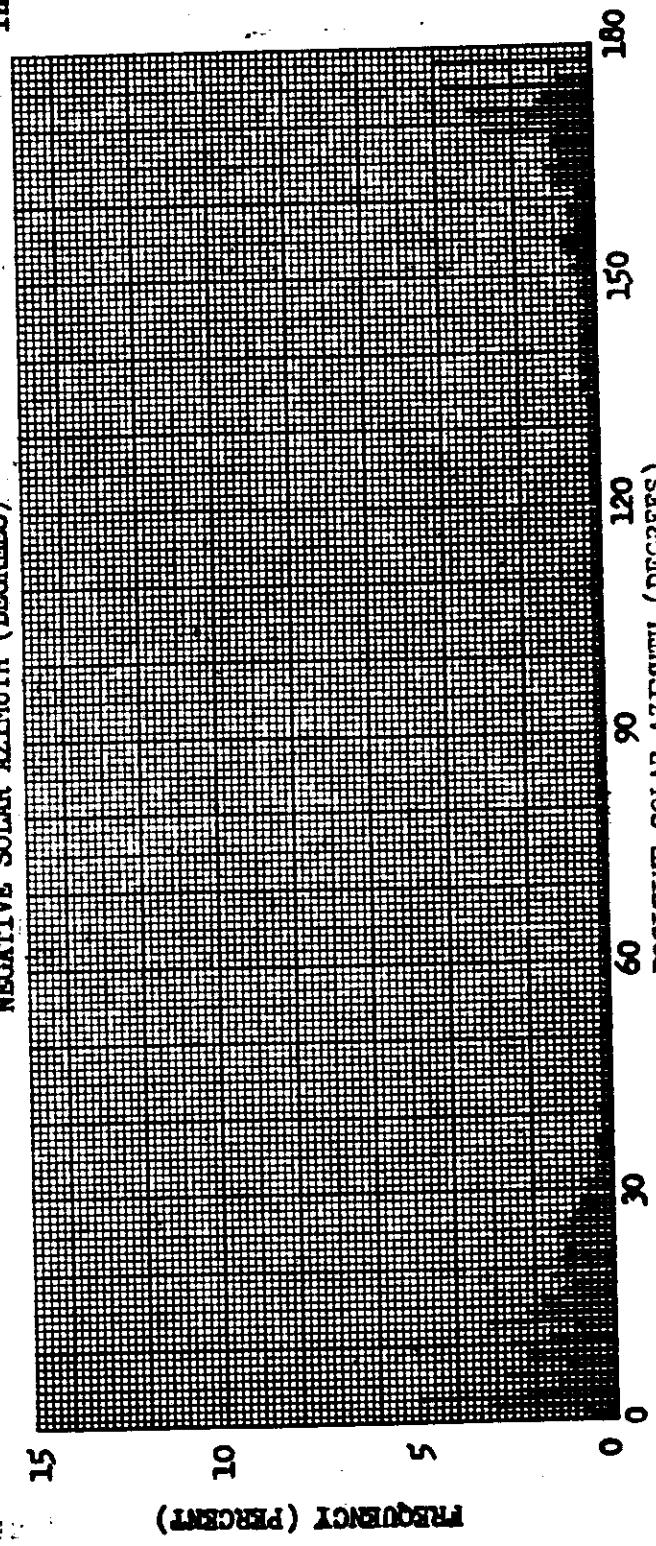
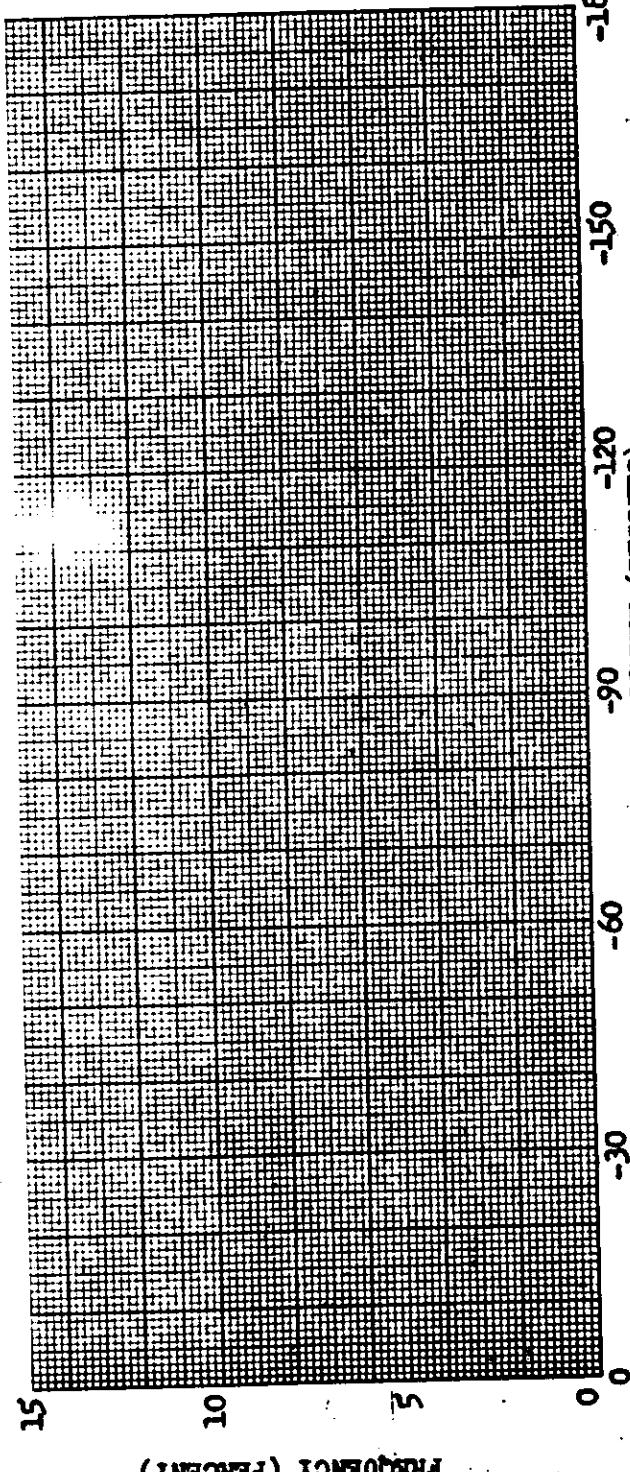


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SOLAR ELEVATION FREQUENCY DISTRIBUTION



SOLAR AZIMUTH FREQUENCY DISTRIBUTION



Mission No: 1034-2

Payload No: J-31

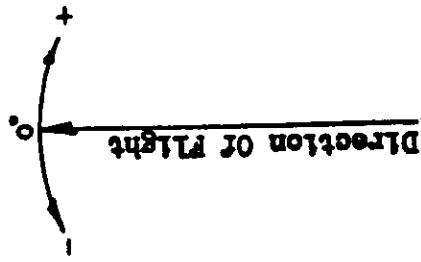
Camera No: 186

Launch Date: 6/21/66

Launch Time: 2131 Z

Inclination: 80°

SIGN NOTATION



DIRECTION OF FLIGHT

EXPOSURE POINTS

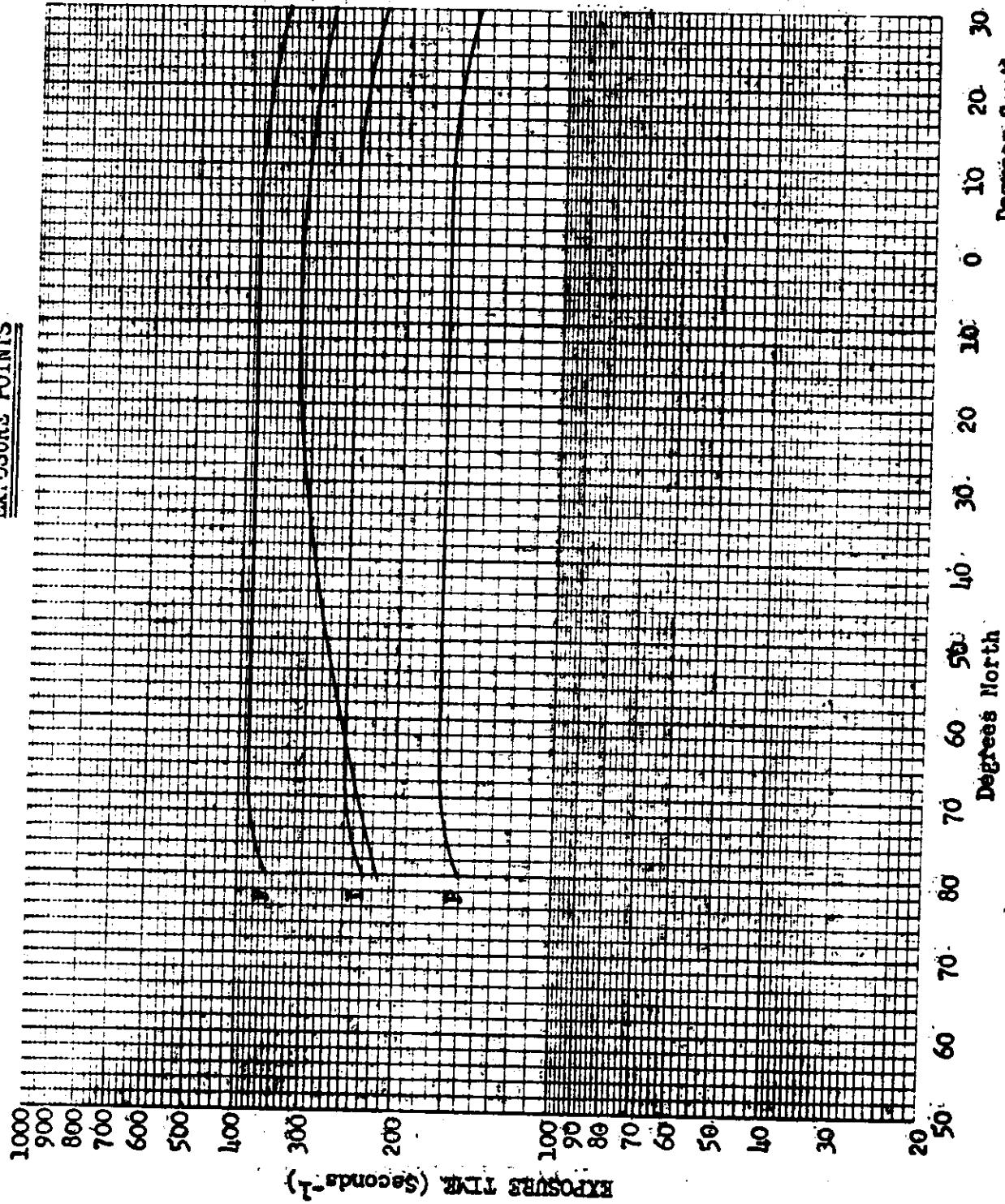
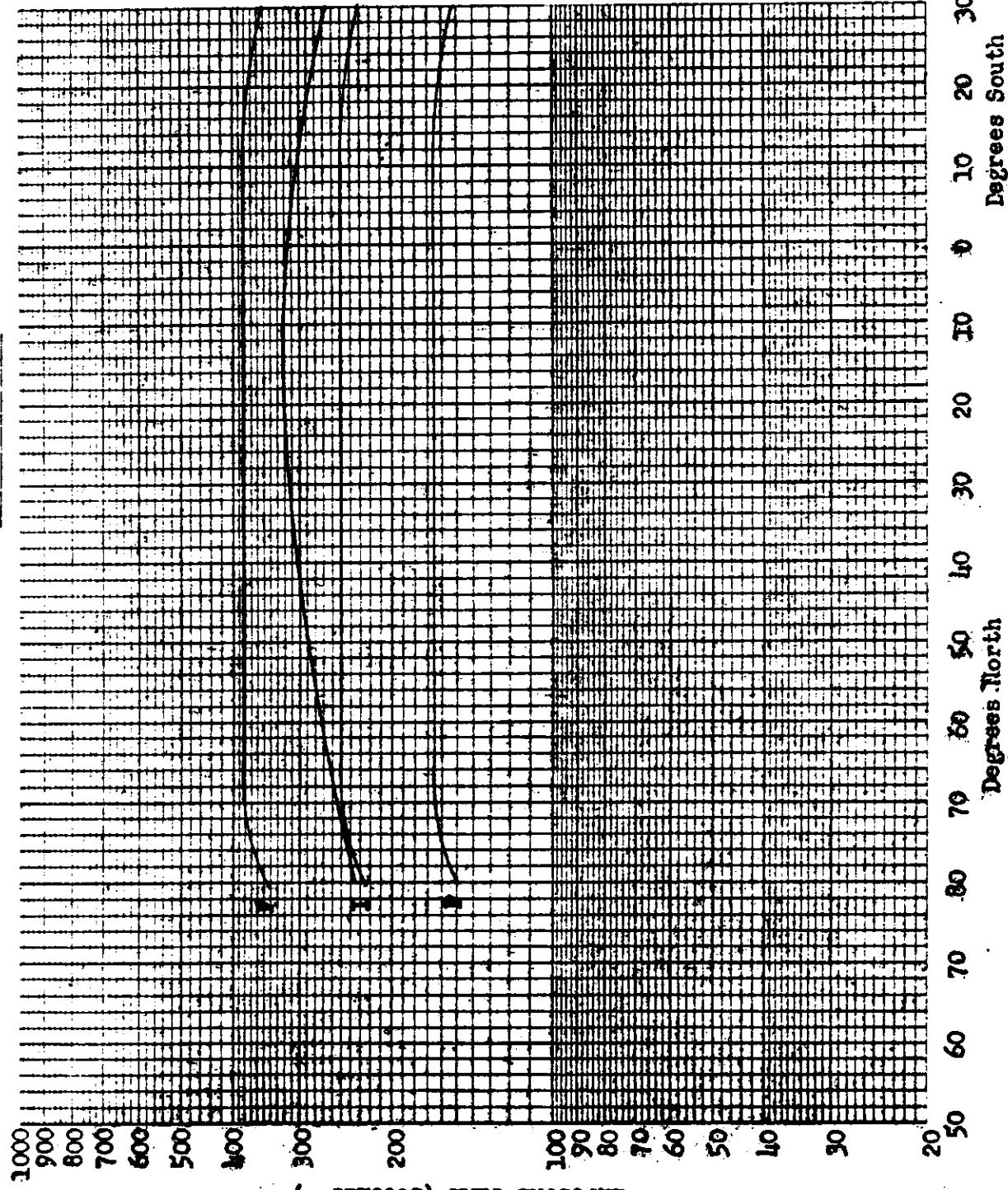


Figure 8-5

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NO. [REDACTED]

EXPOSURE POINTS



EXPOSURE TIME (Seconds-L)

NO.

EXPOSURE POINTS

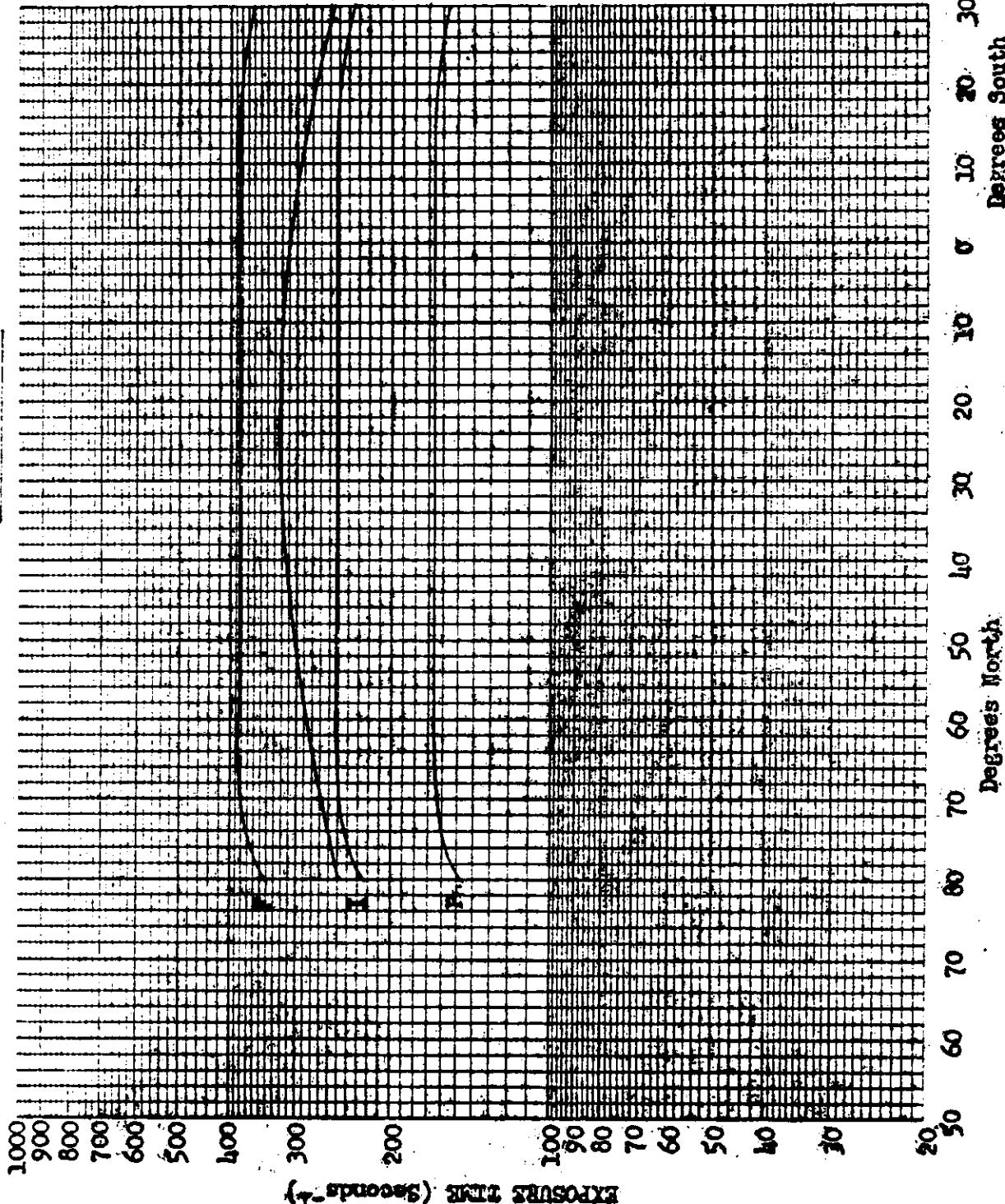


Figure 8-7

NO.

EXPOSURE POINTS

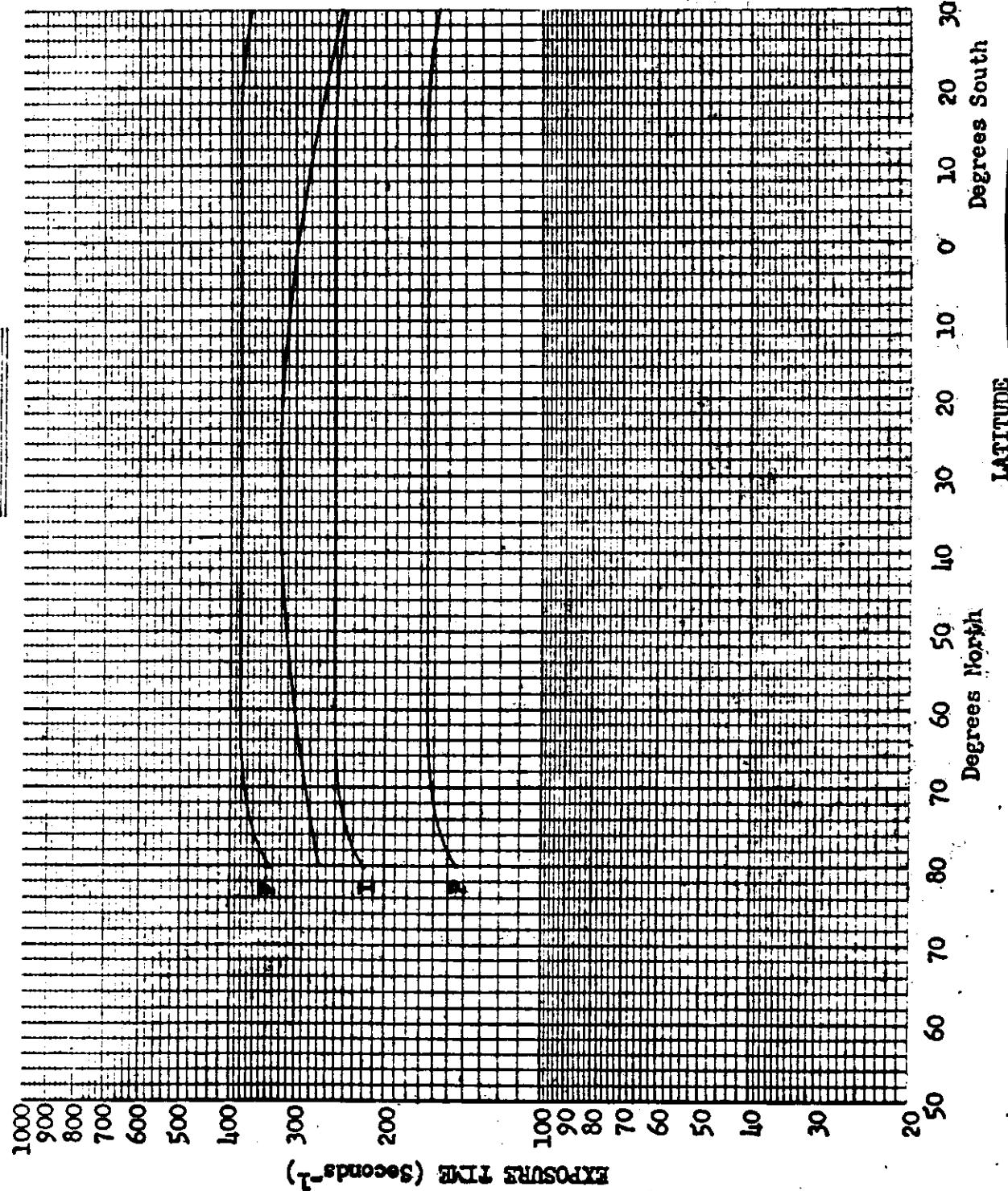


Figure 8-8

TOP SECRET C

~~SECRET C~~
EXPOSURE POINTS

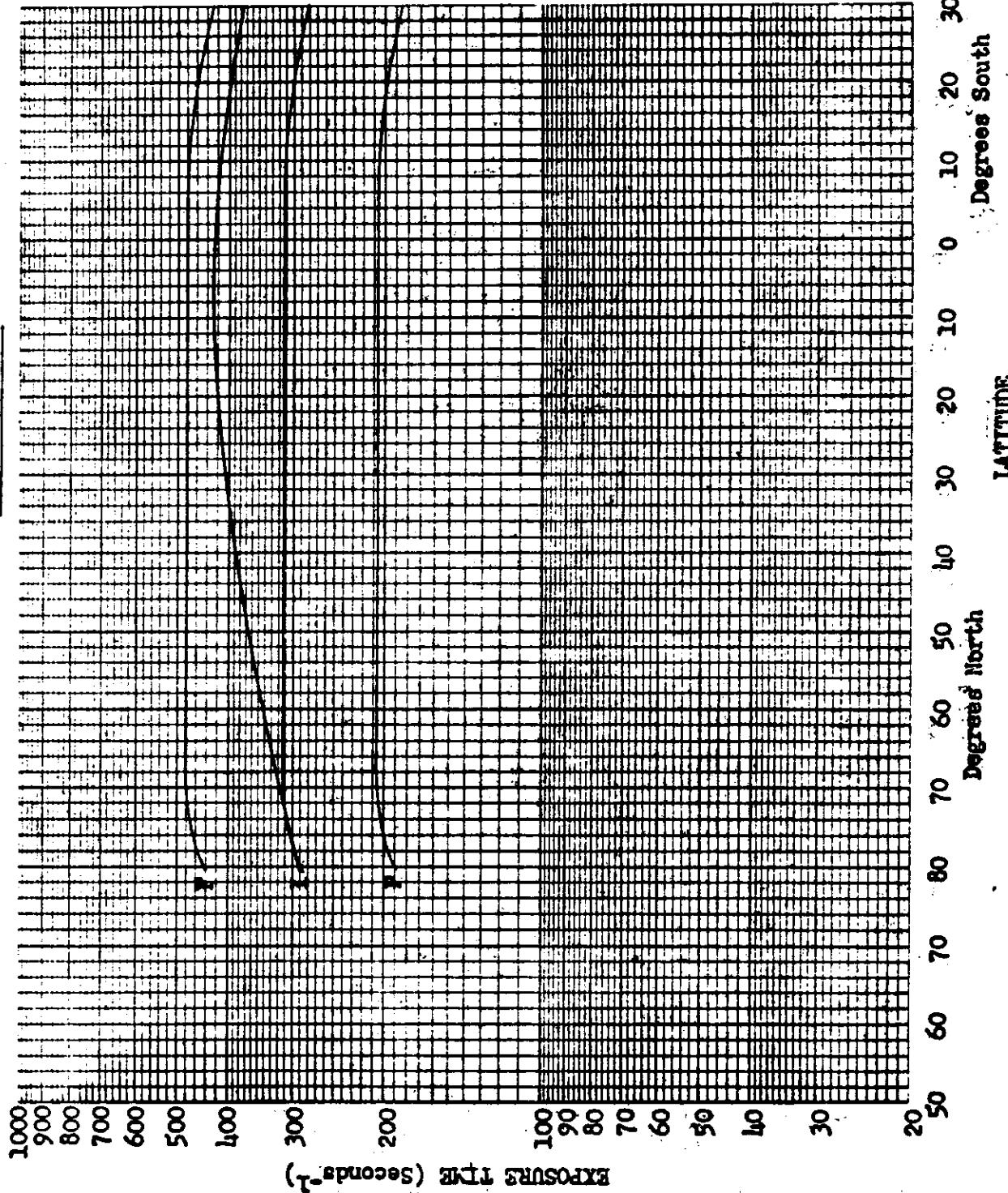


Figure 8-9

~~TOP SECRET C~~

2

EXPOSURE POINTS

Mission No: 1034

Payload No: J-31

Camera No: 187

Pass No: 56

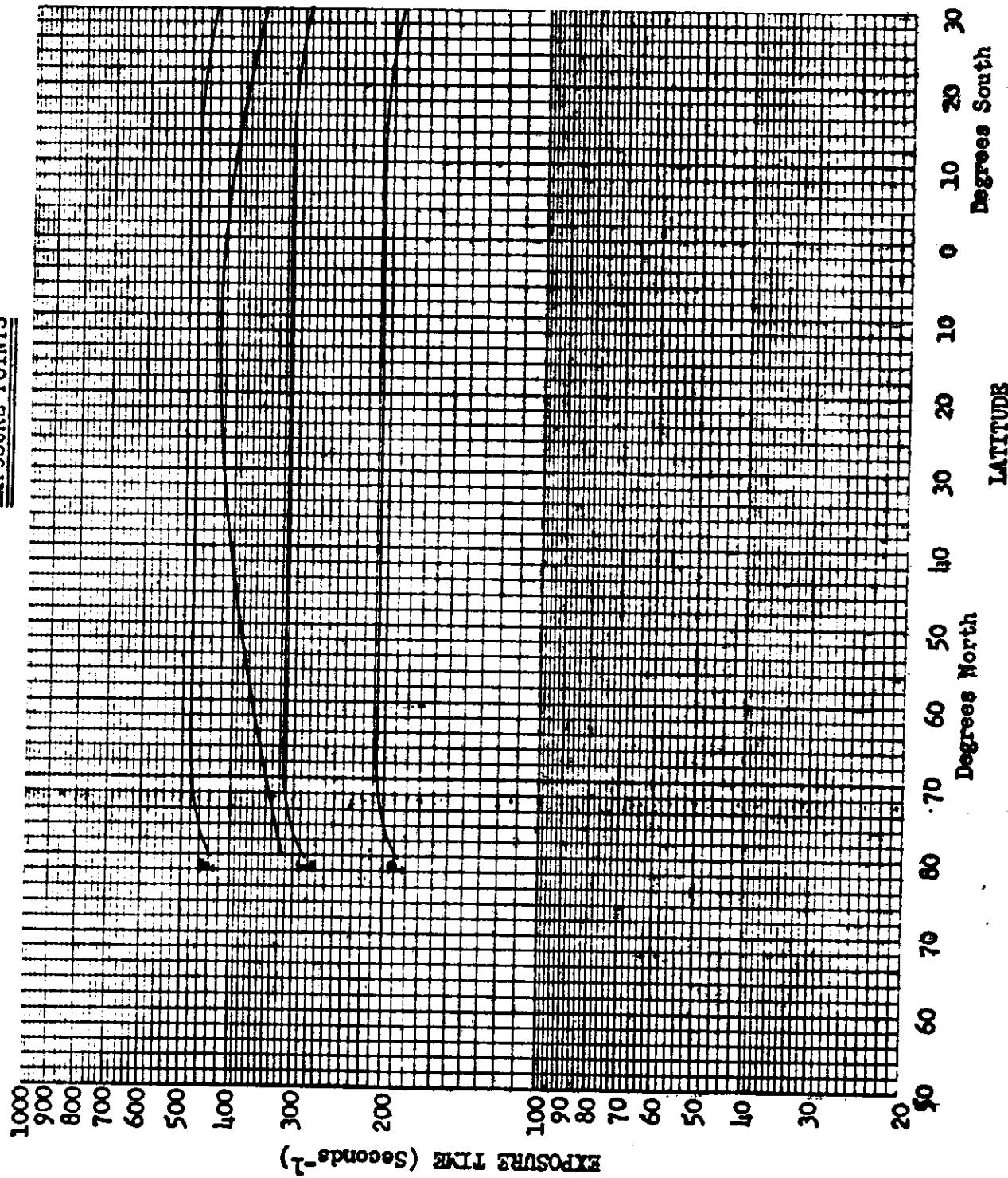
Launch Date: 6/21/66

Launch Time: 2133 3

•150

Wattson 21

310



~~SECRET~~ EXPOSURE POINTS

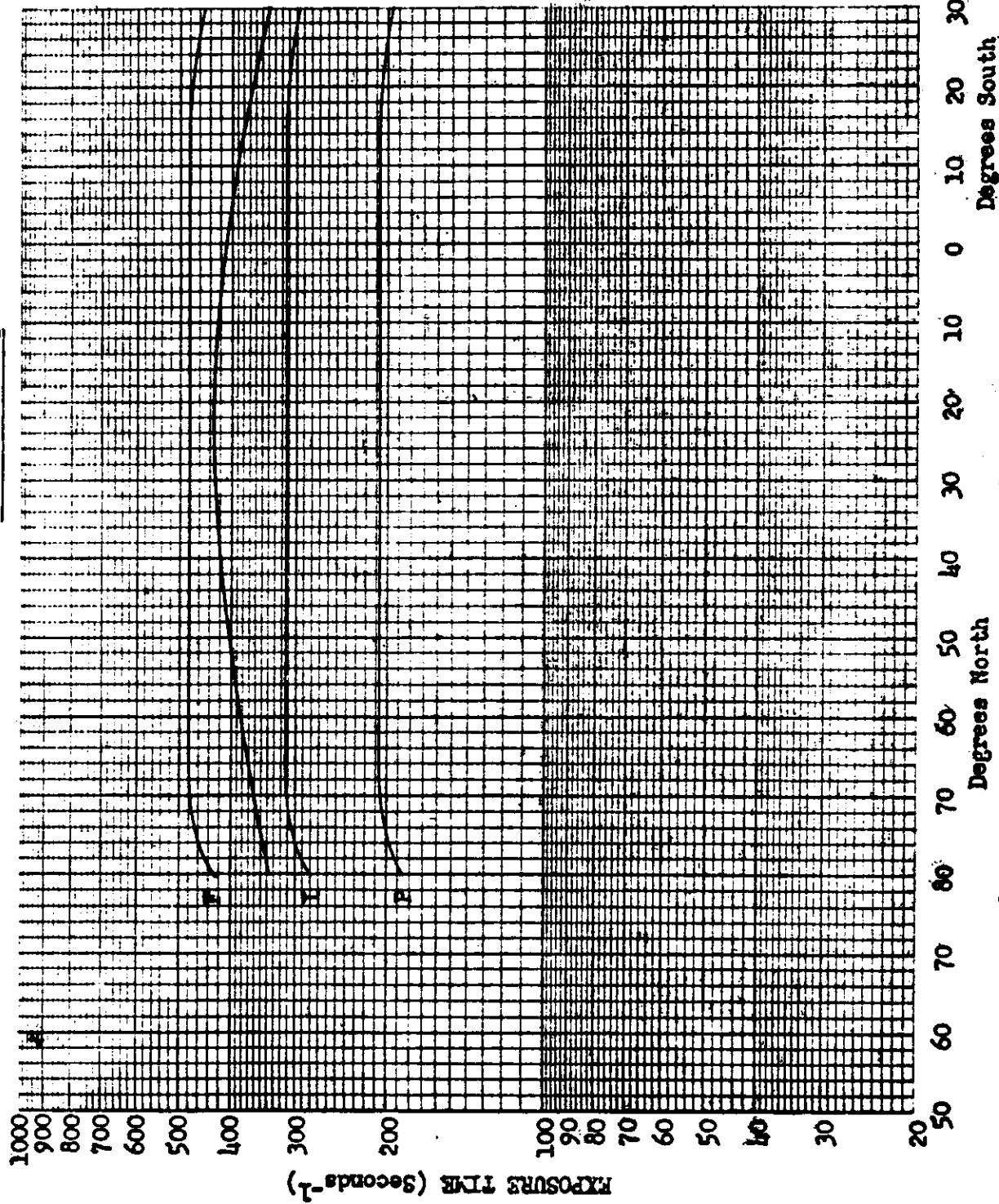


Figure 8-11

~~TOP SECRET~~

NO.

EXPOSURE POINTS

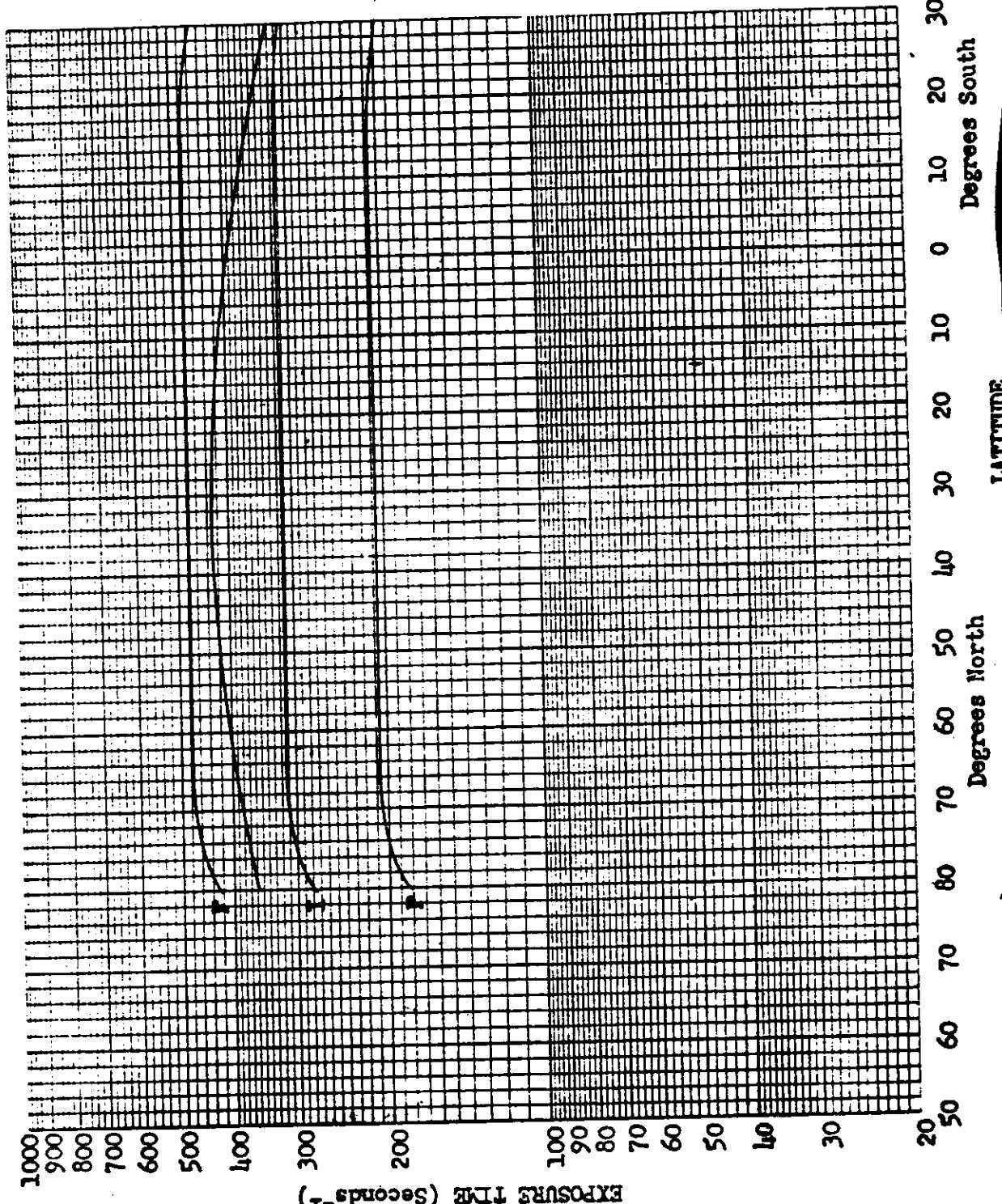


Figure 8-12

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SECTION 9

DIFFUSE DENSITY MEASUREMENTS

The diffuse density measurements made by AFSPFF were computer sorted at A/P to permit analysis of the density ranges encountered at the three processing levels. A study of sorting techniques showed that no absolute method was available to separate the density values as the accuracy of the Processing History published by [REDACTED] appears rather low and processing transition phases are not accounted for. The sorting technique selected uses the base plus fog density values where measurements up to 0.09 density are considered as having received Primary processing, 0.10 to 0.17 as Intermediate and above 0.17 density as Full. The percentage of original negative that was processed at each level, based on the computer sort, is tabulated below with the predicted and reported processing percentages.

Mission	Camera		% Primary	% Intermediate	% Full
1034-1	FWD	Predicted	0	96	4
		Reported	2.6	20.9	76.5
		Computed	0	20	80
1034-1	AFT	Predicted	0	55	45
		Reported	1.9	31.5	66.6
		Computed	0	16	84
1034-2	FWD	Predicted	0	88	12
		Reported	8.9	25.7	65.4
		Computed	0	27	73
1034-2	AFT	Predicted	0	41	59
		Reported	6.1	73.3	56.6
		Computed	0	34	66

The tabulations of density frequency distributions for Mission 1034-1 and 1034-2 are included in Appendix A, Table A-1 thru A-4. The graphical presentation of the density distribution are computer plotted in Appendix A Figures A-1 thru A-36.

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NO. [REDACTED]

A summary of the processing and exposure analysis is shown in Table 9-1. The terrain D-Min criteria, (range) for proper exposure and processing is 0.40 to 0.90 density units. The area measured for D-Min is selected subjectively and is not necessarily the absolute D-Min in the photography.

A density range chart is presented in Figure 9-1. This type of chart for Missions 1004 to 1031 is included in the A/P final report for mission 1031.

These charts are produced from the same density measurements previously mentioned in this section. The computer produced the mean, median and range figures for the various processing levels used. The chart includes the number of frames (samples) in which the density measurements were made. These measurements are made on approximately every tenth frame throughout the mission.

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J MISSION DENSITY RANGES

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NO

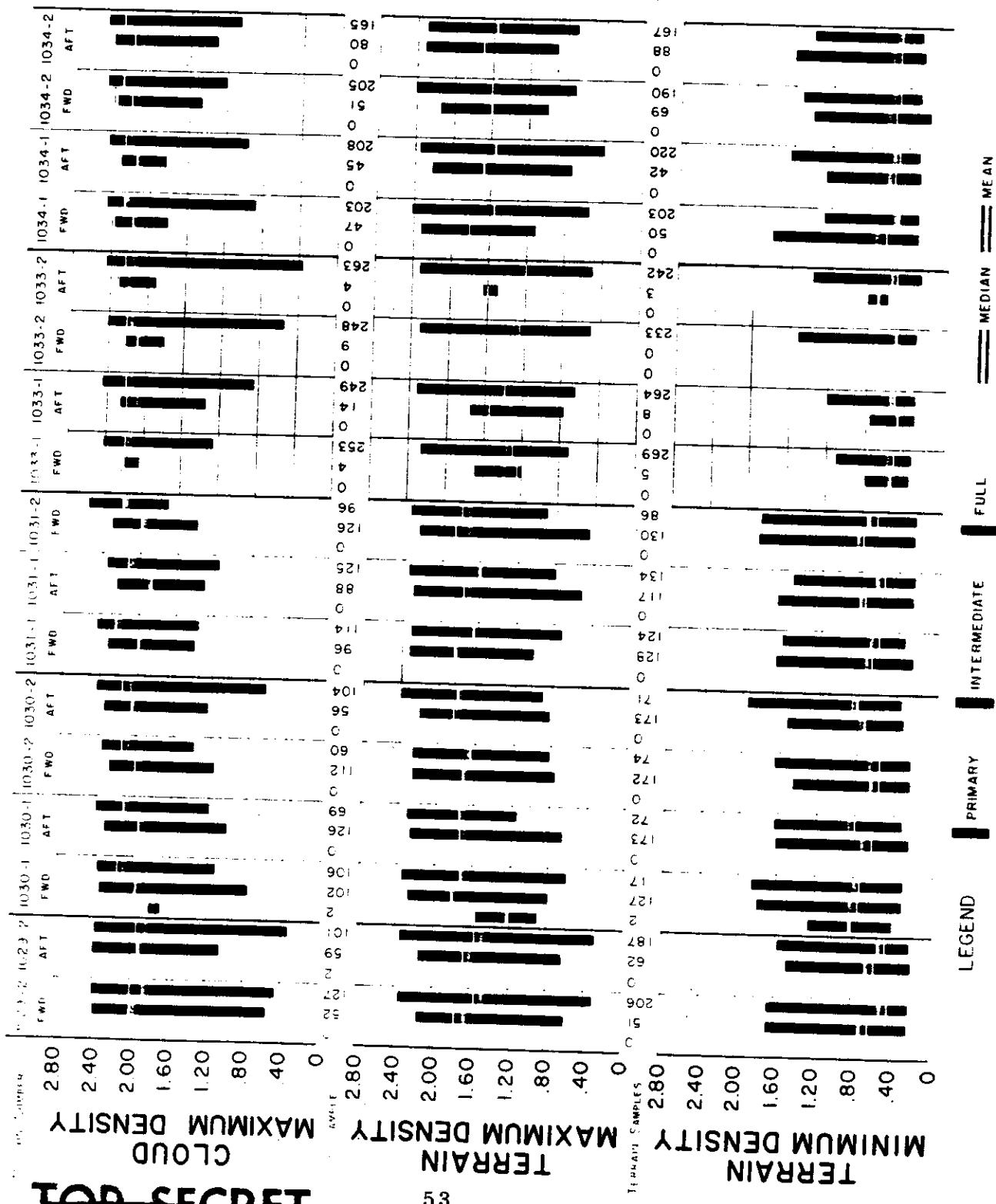


Figure 9-1

MISSION 1034-1			MISSION 1034-2			MISSION 1034-3		
PROCESS LEVEL	SAMPLE SIZE	EXPOSED	PROCESS LEVEL	SAMPLE SIZE	EXPOSED	PROCESS LEVEL	SAMPLE SIZE	EXPOSED
PRIMARY	0	0 PC	UNDER	0 PC	0 PC	CORRECT	0 PC	0 PC
INTERMEDIATE	50	50 PC	PROCESS	16 PC	56 PC	EXP+PROC	18 PC	10 PC
FULL	253	24 PC	0 PC	0 PC	73 PC		4 PC	0 PC
ALL LEVELS	253	14 PC	1 PC	1 PC	10 PC		7 PC	2 PC
MISSION 1034-1	INSTR	APT	MISSION 1034-2	INSTR	FRMD	MISSION 1034-3	INSTR	APT
PROCESS LEVEL	SAMPLE SIZE	EXPOSED	PROCESS LEVEL	SAMPLE SIZE	EXPOSED	PROCESS LEVEL	SAMPLE SIZE	EXPOSED
PRIMARY	0	0 PC	UNDER	0 PC	0 PC	CORRECT	0 PC	0 PC
INTERMEDIATE	42	42 PC	PROCESS	24 PC	60 PC	EXP+PROC	17 PC	0 PC
FULL	220	22 PC	0 PC	0 PC	73 PC		5 PC	0 PC
ALL LEVELS	262	14 PC	4 PC	4 PC	71 PC		7 PC	0 PC
MISSION 1034-1	INSTR	APT	MISSION 1034-2	INSTR	FRMD	MISSION 1034-3	INSTR	APT
PROCESS LEVEL	SAMPLE SIZE	EXPOSED	PROCESS LEVEL	SAMPLE SIZE	EXPOSED	PROCESS LEVEL	SAMPLE SIZE	EXPOSED
PRIMARY	0	0 PC	UNDER	0 PC	0 PC	CORRECT	0 PC	0 PC
INTERMEDIATE	69	1 PC	PROCESS	16 PC	67 PC	EXP+PROC	14 PC	1 PC
FULL	190	15 PC	0 PC	0 PC	79 PC		5 PC	0 PC
ALL LEVELS	259	12 PC	4 PC	4 PC	76 PC		8 PC	0 PC
MISSION 1034-2	INSTR	APT	MISSION 1034-3	INSTR	FRMD	MISSION 1034-4	INSTR	APT
PROCESS LEVEL	SAMPLE SIZE	EXPOSED	PROCESS LEVEL	SAMPLE SIZE	EXPOSED	PROCESS LEVEL	SAMPLE SIZE	EXPOSED
PRIMARY	0	0 PC	UNDER	0 PC	0 PC	CORRECT	0 PC	0 PC
INTERMEDIATE	PA	0 PC	PROCESS	30 PC	60 PC	EXP+PROC	6 PC	5 PC
FULL	167	18 PC	0 PC	0 PC	80 PC		2 PC	0 PC
ALL LEVELS	255	12 PC	10 PC	10 PC	73 PC		4 PC	2 PC
PROCESS LEVEL	PAE + FCC	EXPOSED	PROCESS LEVEL	PAE	EXPOSED	PROCESS LEVEL	PAE	EXPOSED
PRIMARY	0.01-0.02	0.01-0.13	0.01-0.39	0.01-0.39	0.01-0.90	CORRECT	0.01-0.90	0.01-0.90
INTERMEDIATE	0.10-0.17	0.01-0.20	0.21-0.39	0.21-0.39	0.40-0.90	EXP+PROC	0.91-1.34	0.91-1.34
FULL	0.18 ANC UP	0.01-0.39	-----	-----	0.40-0.90		0.91-1.69	1.35 AND UP

CONTROL NU. [REDACTED]

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SECTION 10

PERFORMANCE MEASUREMENTS

The photography acquired by both panoramic cameras during Missions 1034-1 and 1034-2 received an MIP rating of 80. A summary is tabulated below of the MTF/AIM resolution values measured by AFSPPF. The micro densitometer slit used was 1 micron by 80 microns.

<u>Mission</u>	<u>Camera</u>	<u>Cycles/mm</u>	<u>Average</u>	<u>Ground Resolution</u>
1034-1	FWD	81	84	15.3'
1034-2	FWD	89		
1034-1	AFT	90	88	14.6'
1034-2	AFT	86		

The details of the measure and computing techniques, targets measured and target locations are fully reported in the evaluation report published by AFSPPF and are not normally included in this report.

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SECTION II

VEHICLE ATTITUDE

The vehicle attitude errors for both Mission 1034-1 and 1034-2 were derived from the reduction of the Stellar camera photography. This attitude data is supplied to A/P by NPIC.

The attitude errors for each frame and the attitude control rates are calculated at the A/P computer facility. The computer also plots the frequency distribution of the rates and errors. Figures 11-1 through 11-6 show these distributions for Mission 1034-1 and Figures 11-7 through 11-12 for Mission 1034-2.

The summary table below lists the maximum attitude errors and rates that were experienced during 90% of the FWD camera photographic operations, excluding the first six frames of each operation, and the total range of the errors and rates.

<u>Value</u>	Mission 1034-1		Mission 1034-2	
	<u>90%</u>	<u>Range</u>	<u>90%</u>	<u>Range</u>
Pitch Error ($^{\circ}$)	0.20	-0.50 to +0.48	0.34	-0.48 to +0.76
Roll Error ($^{\circ}$)	0.19	-0.36 to +0.28	0.36	-0.48 to +0.46
Yaw Error ($^{\circ}$)	0.99	+0.34 to +1.22	0.33	-0.46 to +0.64
Pitch Rate ($^{\circ}/hr.$)	19.26	-60 to +50	21.06	-80 to +95
Roll Rate ($^{\circ}/hr.$)	20.41	-60 to +90	28.88	-80 to +95
Yaw Rate ($^{\circ}/hr.$)	24.86	-50 to +46	16.21	-42 to +66

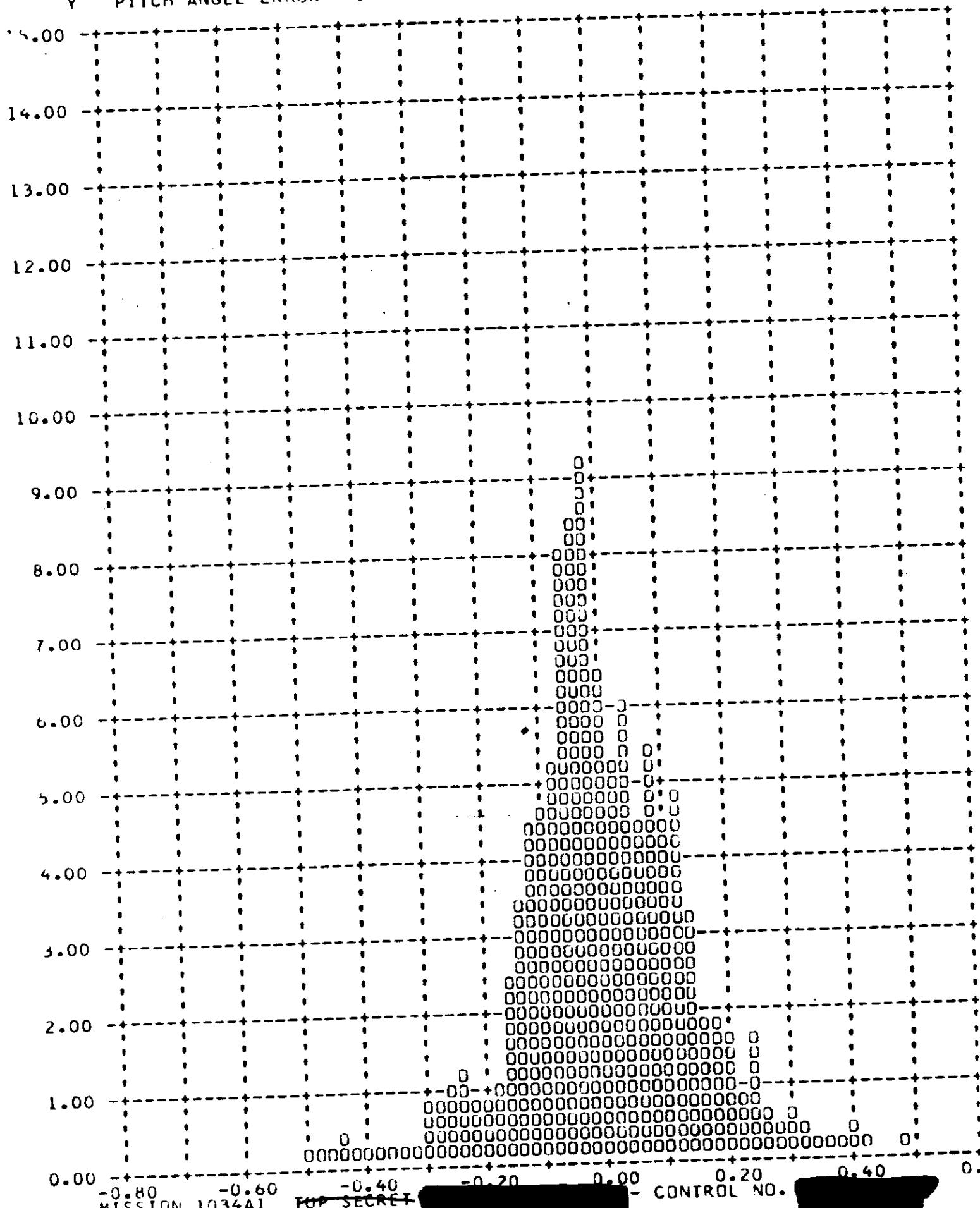
The performance of the attitude control system is better than previous missions. The panoramic photography was not degraded by the attitude control system.

MISSION 1034A1 TOP SECRET

- CONTROL NO.

FRAMES 1-6 OF EACH OP OMITTED 90 PERCENT = 0.20

Y PITCH ANGLE ERROR - DEGREES (X) VERSUS FREQUENCY - PERCENT (Y)



MISSION 1034A1 TOP SECRET

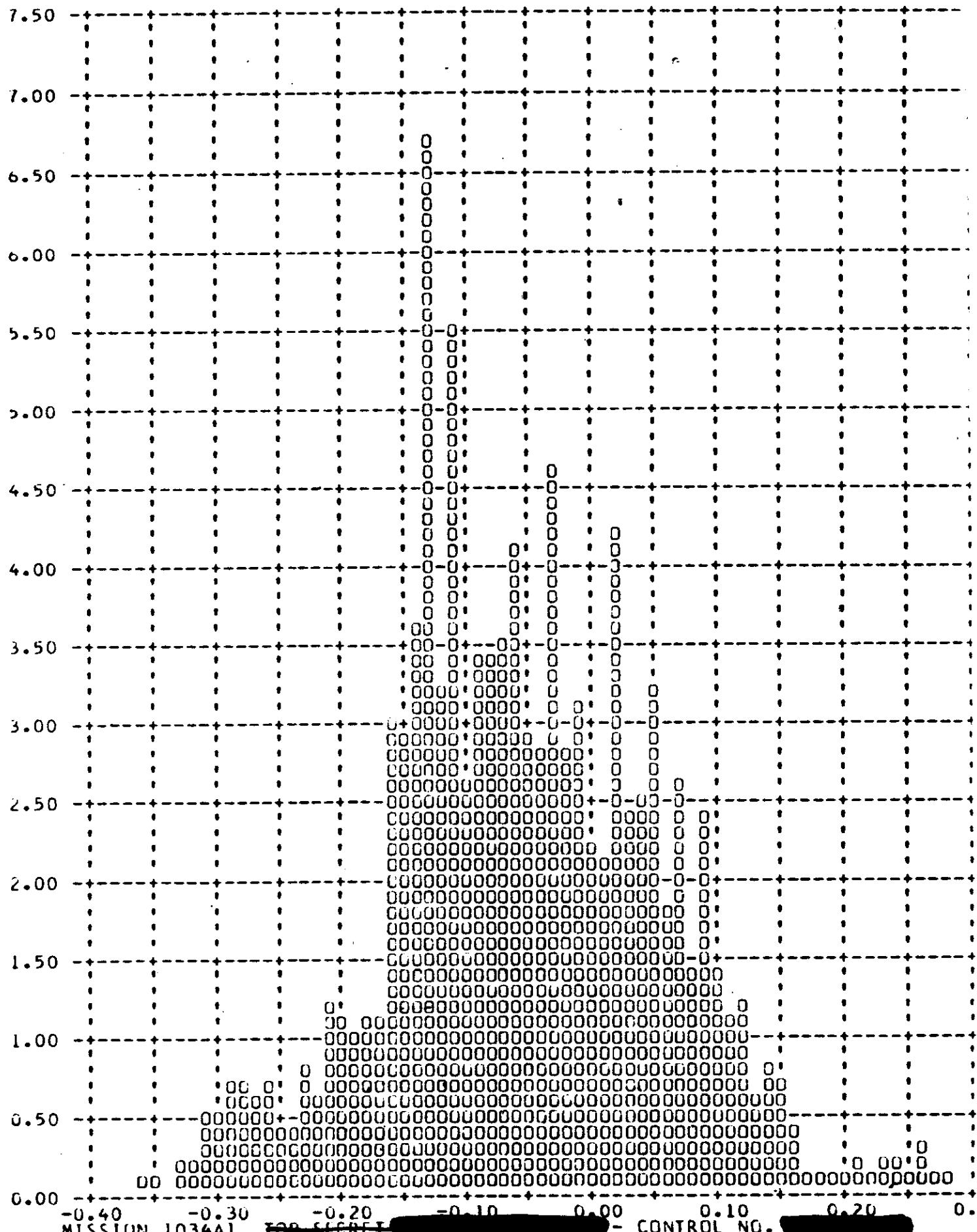
- CONTROL NO.

MISSION 1034A1 TOP SECRET

- CONTROL NO.

FRAMES 1-6 OF EACH OP OMITTED 90 PERCENT = 0.

Y ROLL ANGLE ERROR - DEGREES (X) VERSUS FREQUENCY - PERCENT (Y)



MISSION 1034A1 TOP SECRET

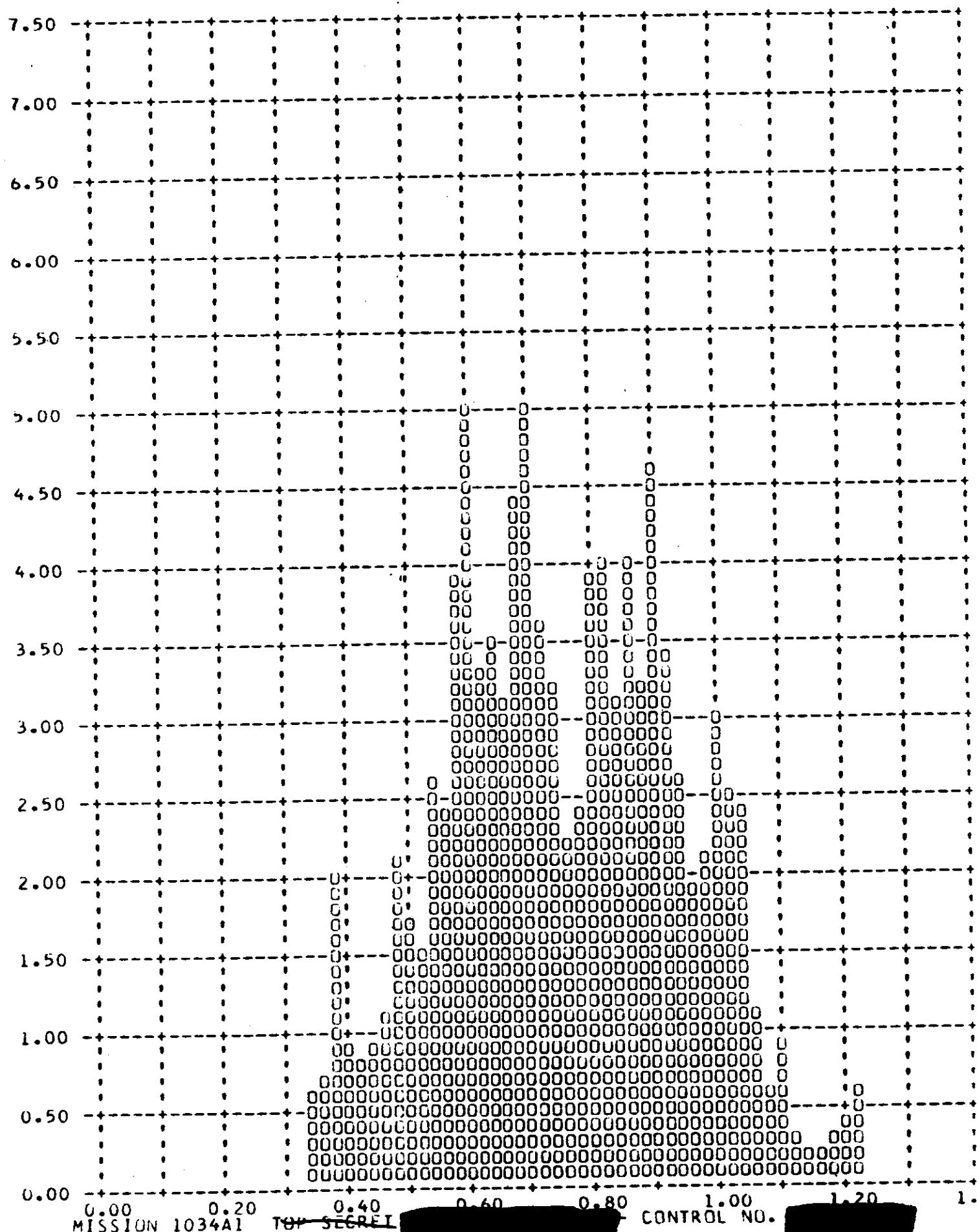
- CONTROL NO.

MISSION 1034A1 TOP SECRET

- CONTROL NO.

FRAMES 1-6 OF EACH OP OMITTED 90 PERCENT = 0.1

Y YAW ANGLE ERROR - DEGREES (X) VERSUS FREQUENCY - PERCENT (Y)

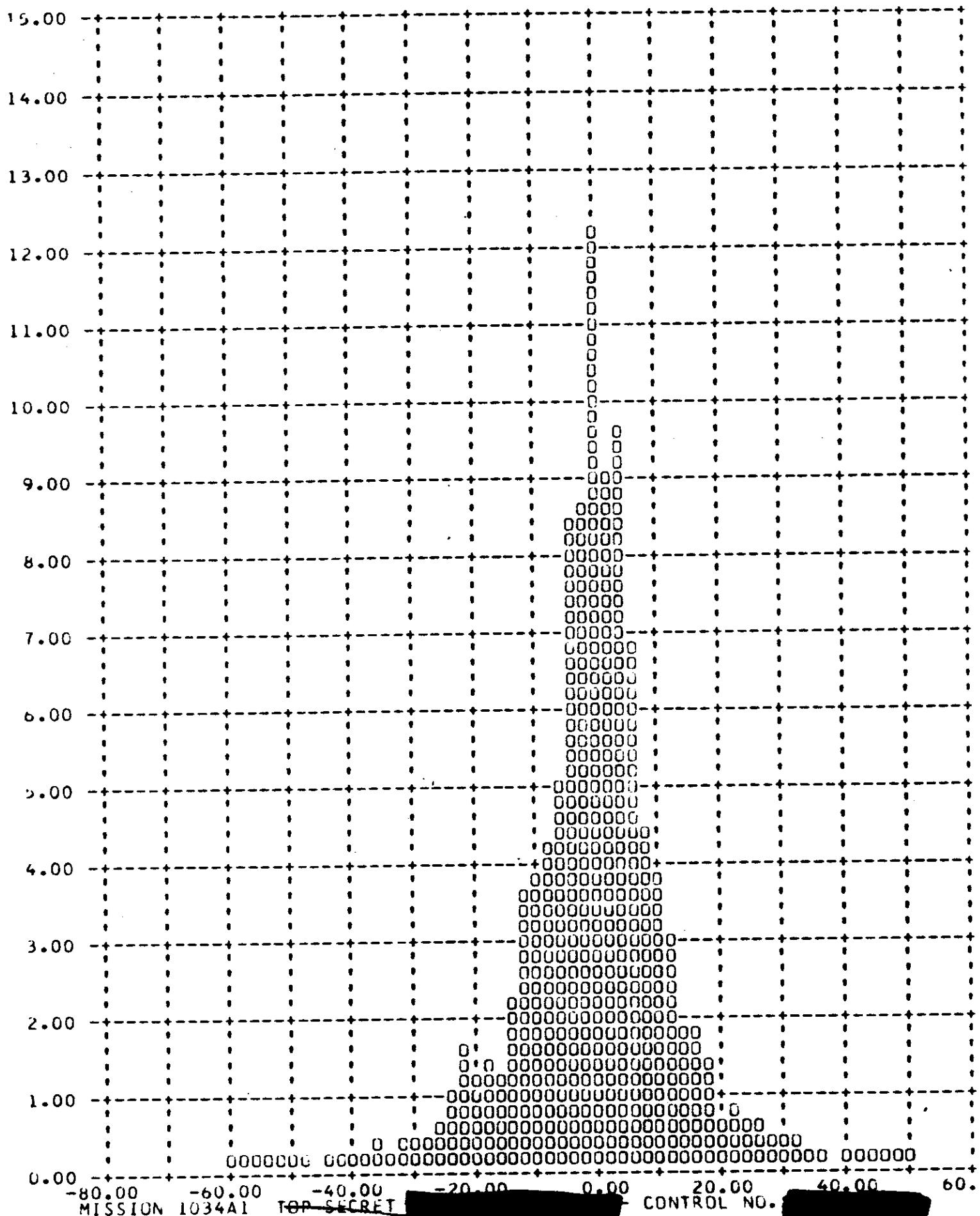


MISSION 1034A1 TOP SECRET

- CONTROL NO.

FRAMES 1-6 OF EACH OP OMITTED 90 PERCENT = 19.2

Y PITCH RATE ERROR - DEG/HOUR (X) VERSUS FREQUENCY - PERCENT (Y)



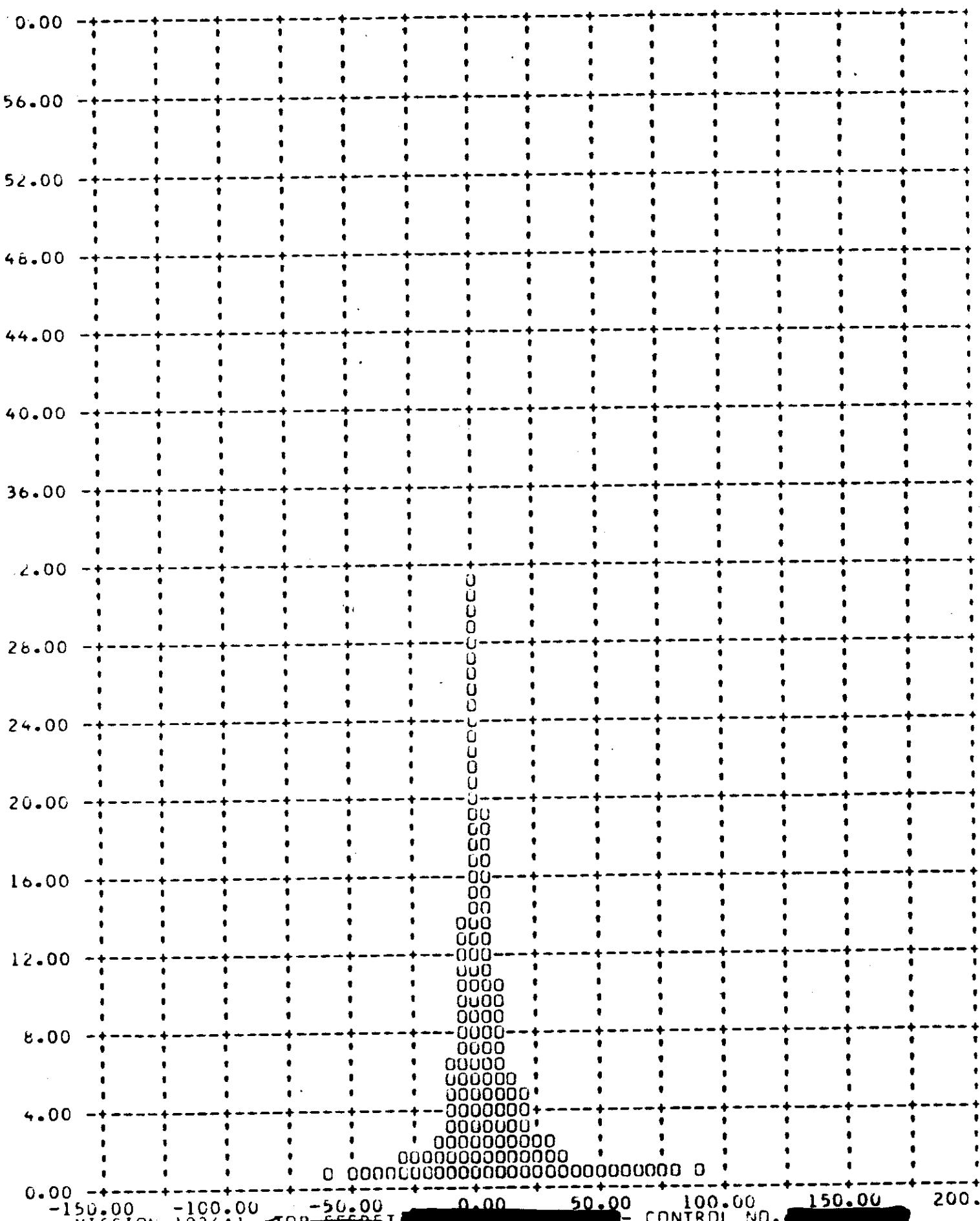
MISSION 1034A1 TOP SECRET

- CONTROL NO.

MISSION 1034A1 ~~TOP SECRET~~- CONTROL NO. ~~XXXXXXXXXX~~

FRAMES 1-6 OF EACH OP OMITTED 90 PERCENT = 20.4

Y ROLL RATE ERROR - DEG/HOUR (X) VERSUS FREQUENCY - PERCENT (Y)

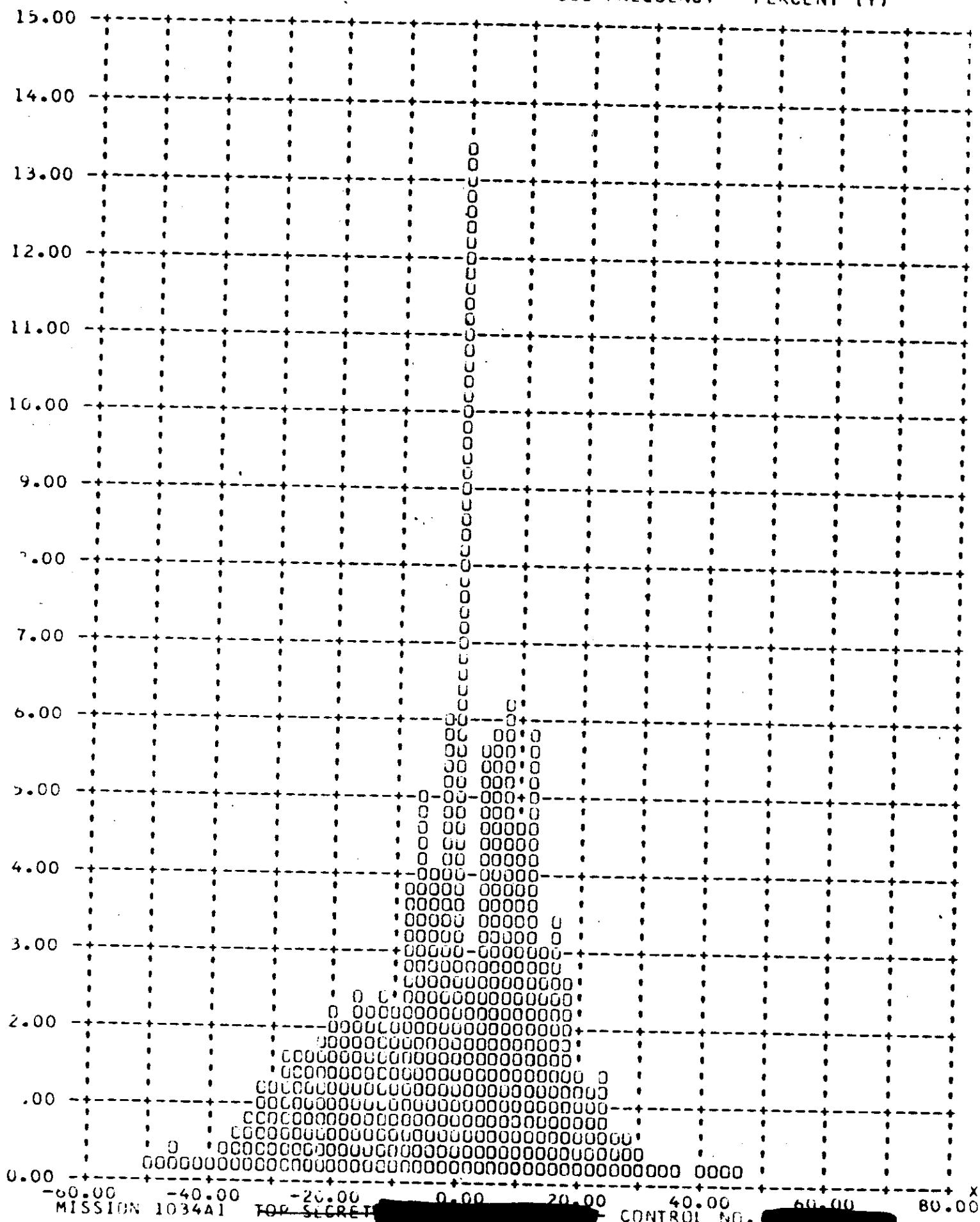


MISSION 1034A1 TOP SECRET

- CONTROL NO.

FRAMES 1-6 OF EACH UP OMITTED 90 PERCENT = 24.1

Y YAW RATE ERROR - DEG/HOUR (X) VERSUS FREQUENCY - PERCENT (Y)

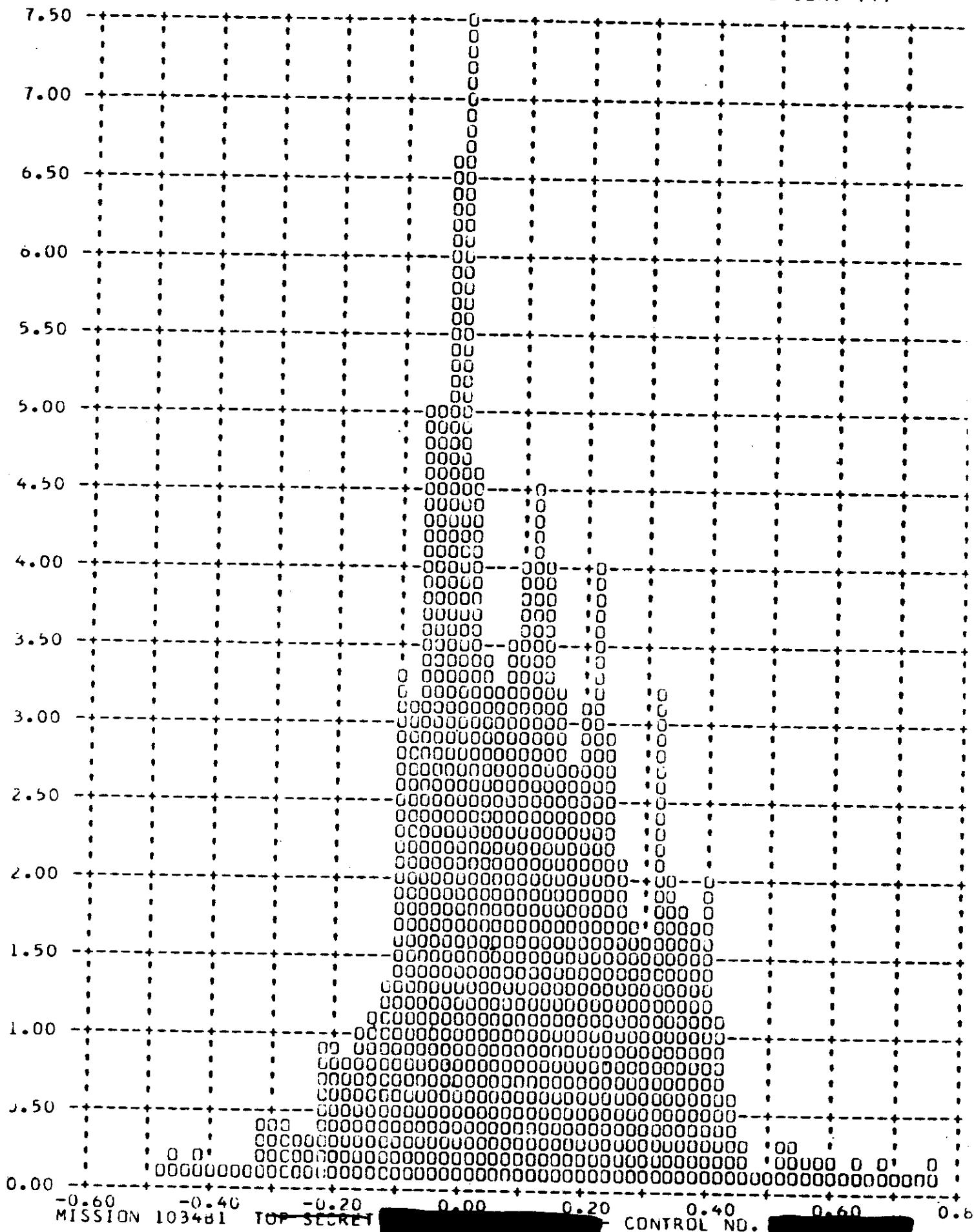


MISSION 1034A1 TOP SECRET

- CONTROL NO.

FRAMES 1-6 OF EACH OP OMITTED 90 PERCENT = .0.

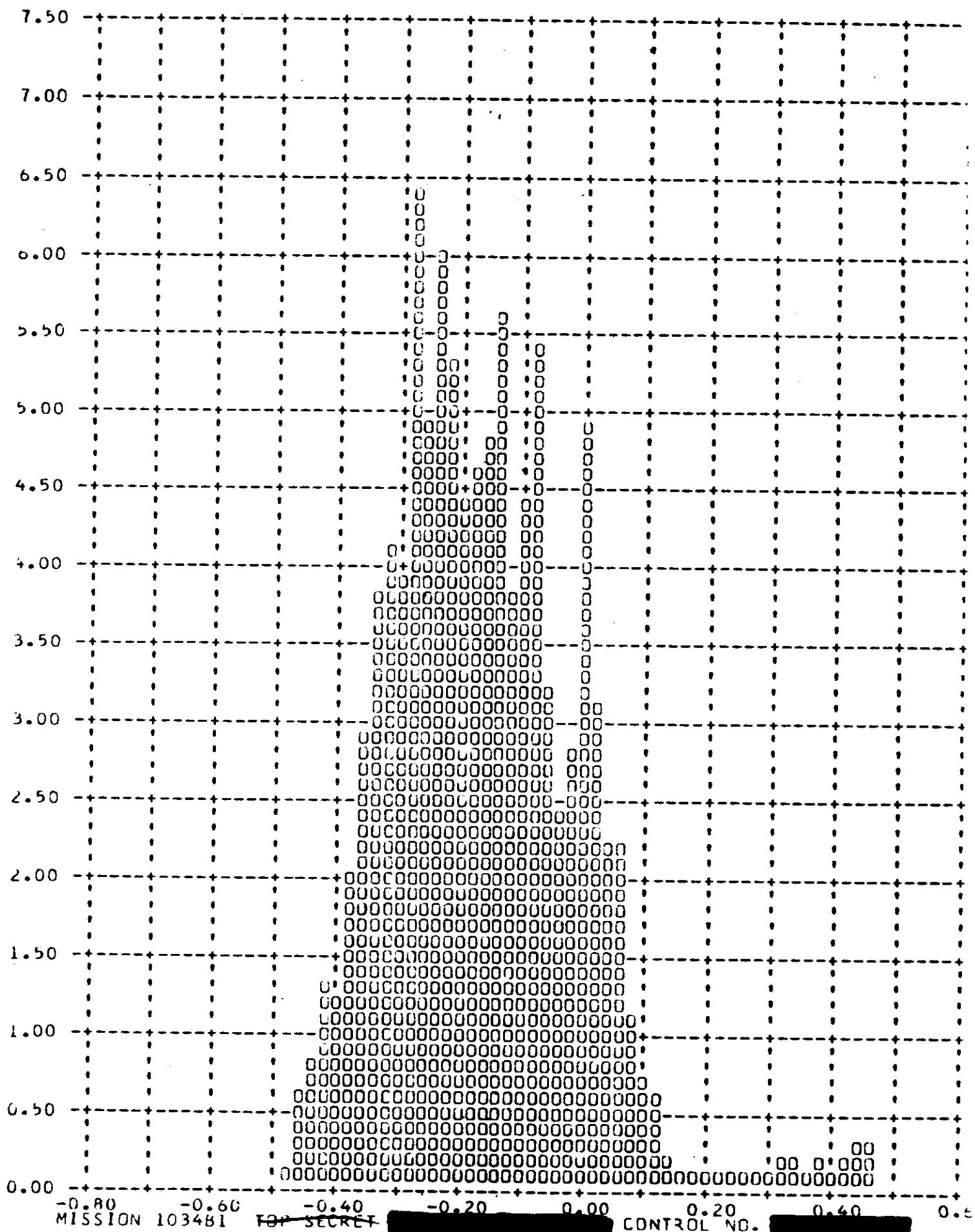
Y PITCH ANGLE ERROR - DEGREES (X) VERSUS FREQUENCY - PERCENT (Y)



MISSION 103481 ~~TOP SECRET~~- CONTROL NO.

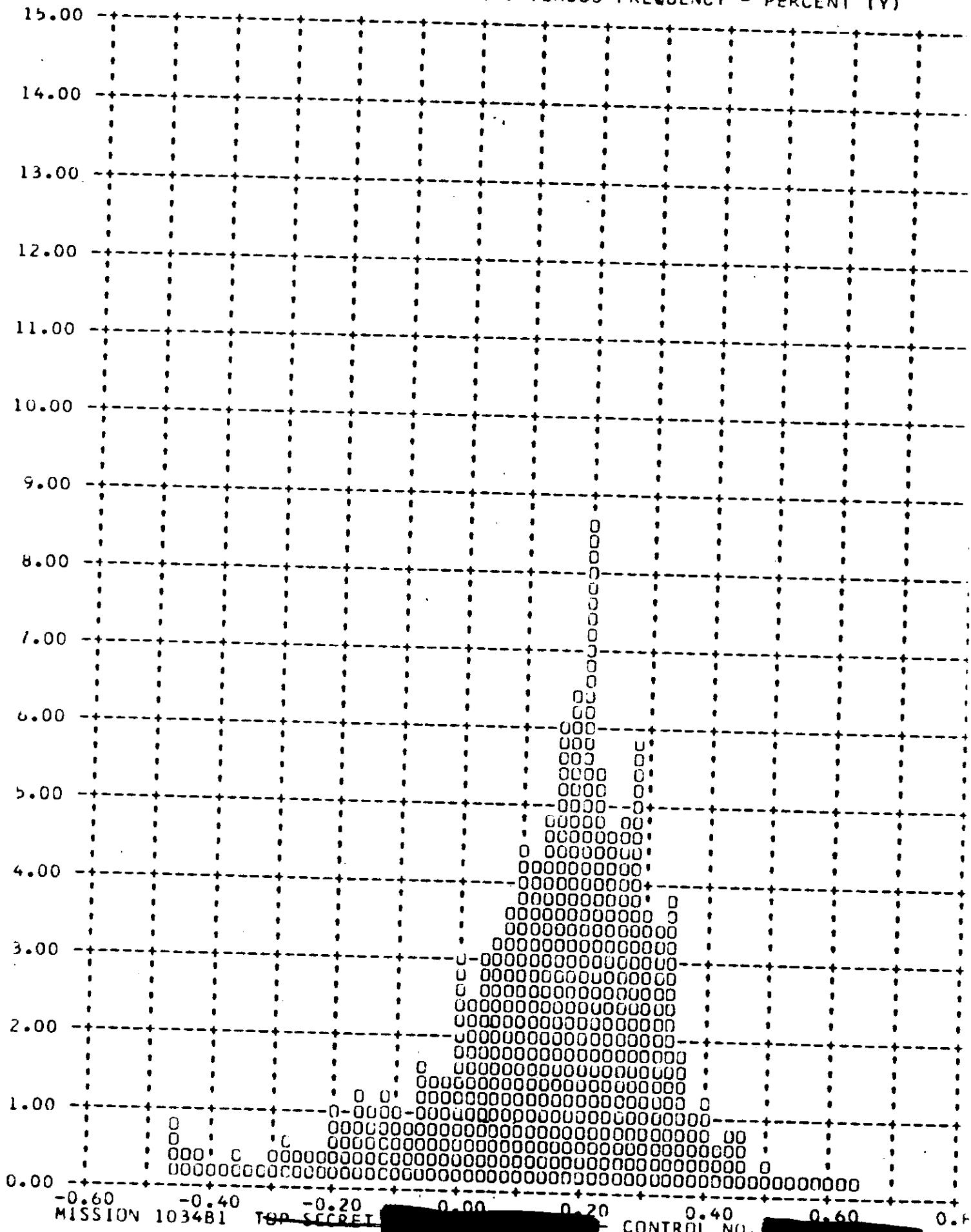
FRAMES 1-6 OF EACH OP OMITTED 90 PERCENT = 0.

Y ROLL ANGLE ERROR - DEGREES (X) VERSUS FREQUENCY - PERCENT (Y)

MISSION 103481 ~~TOP SECRET~~CONTROL NO.

FRAMES 1-6 OF EACH OP OMITTED 90 PERCENT =

Y YAW ANGLE ERROR - DEGREES (X) VERSUS FREQUENCY - PERCENT (Y)



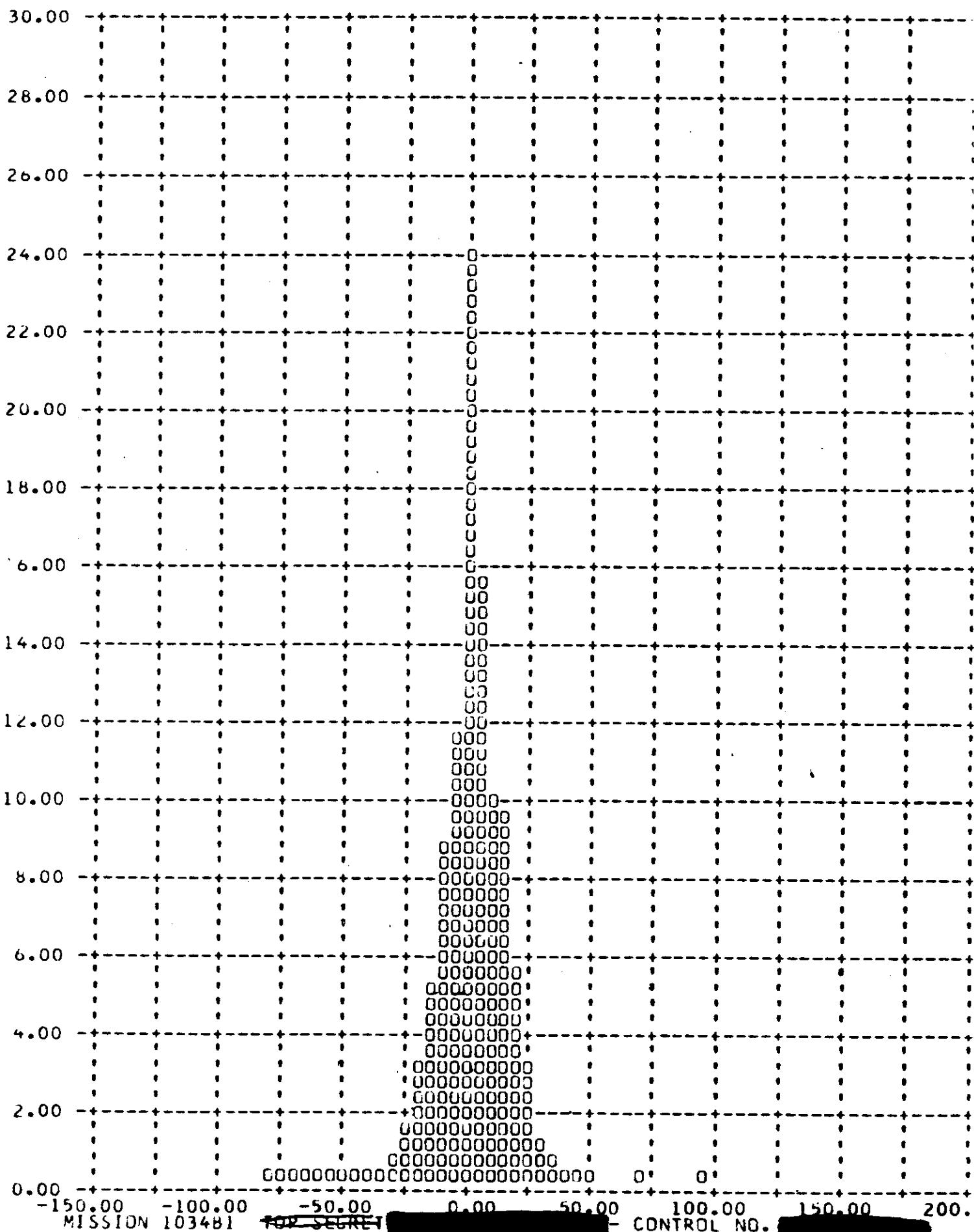
MISSION 103481

~~TOP SECRET~~

- CONTROL NO.

FRAMES 1-6 OF EACH OP OMITTED 90 PERCENT = 21.

Y PITCH RATE ERROR - DEG/HOUR (X) VERSUS FREQUENCY - PERCENT (Y)



MISSION 103481

~~TOP SECRET~~

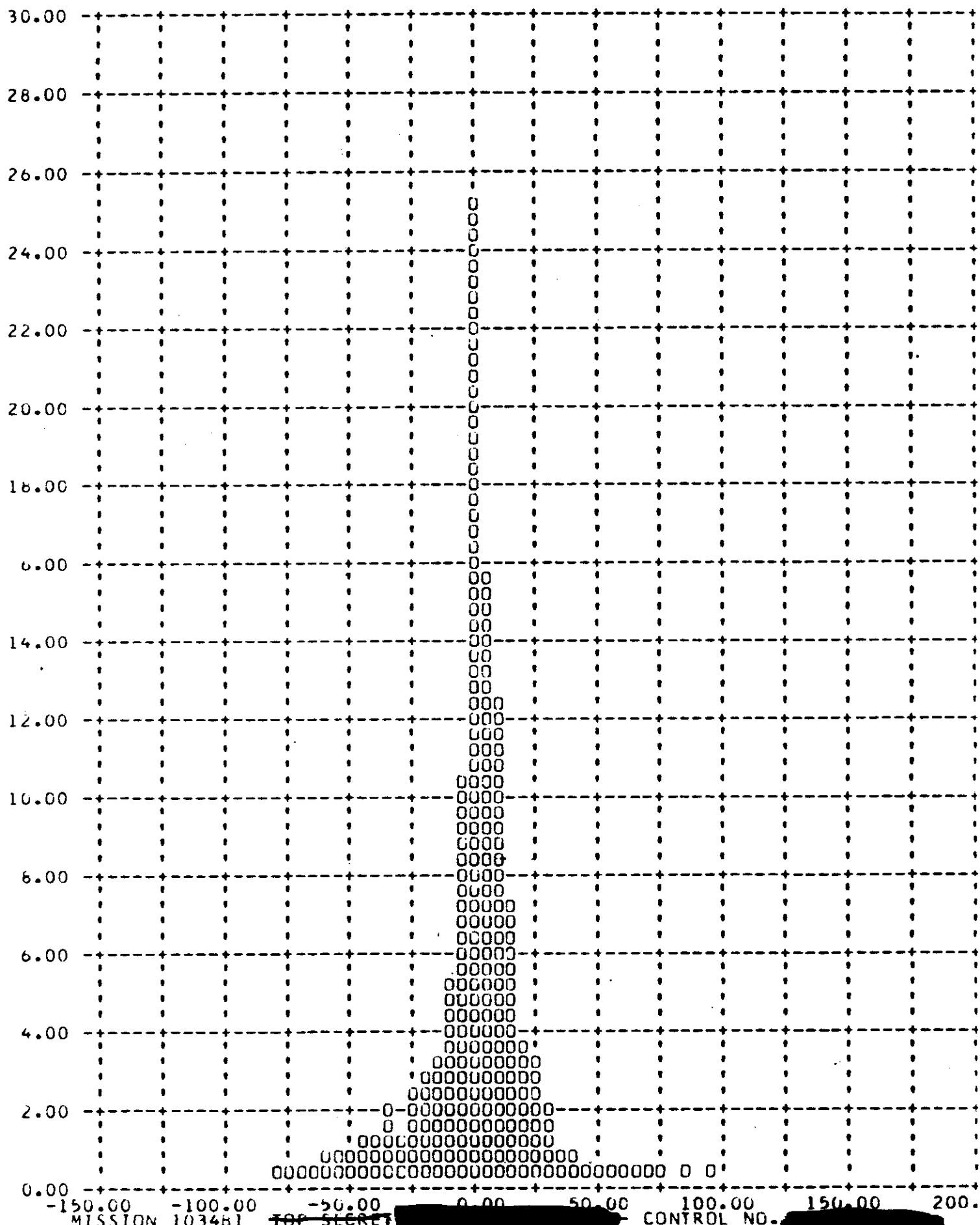
- CONTROL NO.

MISSION 103481 - TOP SECRET

- CONTROL NO.

FRAMES 1-6 OF EACH OP OMITTED 90 PERCENT = 28.0

Y ROLL RATE ERROR - DEG/HOUR (X) VERSUS FREQUENCY - PERCENT (Y)



MISSION 103481 - TOP SECRET

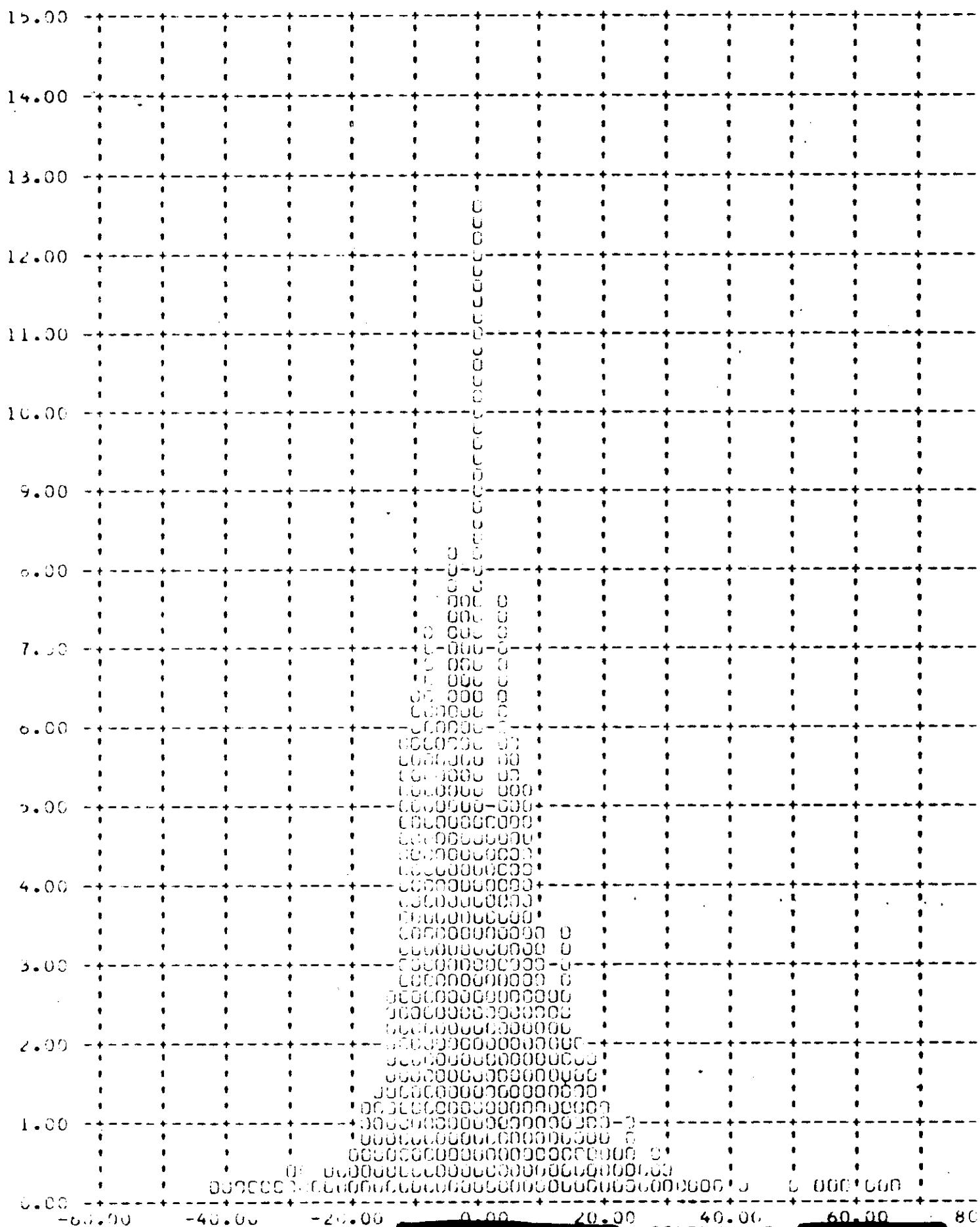
- CONTROL NO.

MISSION 103481 -TOP-SECRET

- CONTROL NO.

FRAMES 1-6 OF EACH UP OMITTED 90 PERCENT = 16.

Y YAW RATE ERROR - DEG/HOUR (X) VERSUS FREQUENCY - PERCENT (Y)



MISSION 103481 -TOP-SECRET

- CONTROL NO.

SECTION 12

IMAGE SMEAR ANALYSIS

The frame correlation tape supplied to A/P by NPIC contains the binary time word of each frame of photography. A computer program has been assembled at A/P which calculates the exposure time of each frame and compares the camera cycle rate with the ephemeris to calculate the V/h mismatch. This data is combined with the vehicle attitude error and rate values of each frame and the crab error caused by earth rotation at the latitude of each frame. The program outputs the total along track and cross track INC error and the limit of ground resolution that can be acquired by a camera regardless of focal length and system capabilities.

The computer rejects the first six frames of all operations as the large V/h error induced by camera start-up is not representative of the overall system operations. The frequency distribution of the V/h errors and resolution limits are computer plotted and are shown in Figures 12-1 through 12-12.

The summary table 12-1 presents the maximum V/h ratio errors and resolution limits that existed during 90% of the photographic operations and the total range of values during all operations that were computed.

The excessively high ground resolution values are the result of the V/h programmer failing to cycle after pass D-01. See discussion in Section 3-B.

MISSION 1034
V/H RATIO AND RESOLUTION LIMITS

VALUE	UNITS	CAMERA	MISSION 1034-1		MISSION 1034-2	
			90% Range	90% Range	90% Range	90% Range
V/H Ratio Error	"	FWD	14.97	-22.0 to +20.0	8.66	-15.5 to +14.0
		AFT	15.23	-20.0 to +18.0	8.92	-15.5 to +14.5
Along-track Resolution Limit	Foot	FWD	17.80	0.5 to 30.5	10.36	0.5 to 22.5
		AFT	13.55	0.5 to 22.0	8.02	0.5 to 17.5
Cross-track Resolution Limit	Foot	FWD	5.94	0.2 to 7.2	7.10	0.2 to 9.8
		AFT	4.46	0.2 to 5.4	5.31	0.2 to 6.8

TABLE 12-1

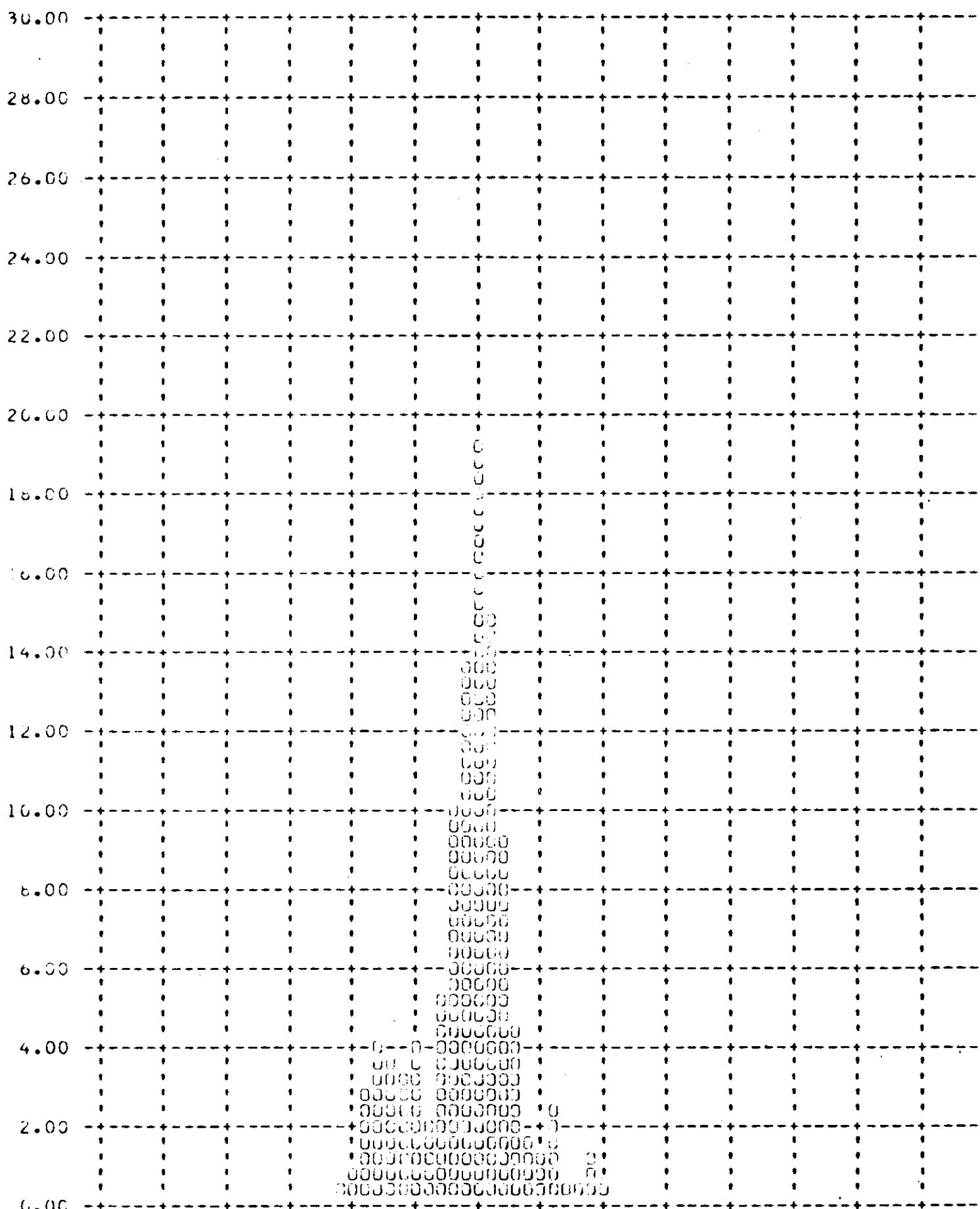
TOP SECRET C

MISSION 1034A1 TOP SECRET

- CONTROL NO.

FRAMES 1-6 OF EACH DP OMITTED 90 PERCENT = 14.

Y V/H RATIO ERROR - PERCENT (X) VERSUS FREQUENCY - PERCENT (Y)

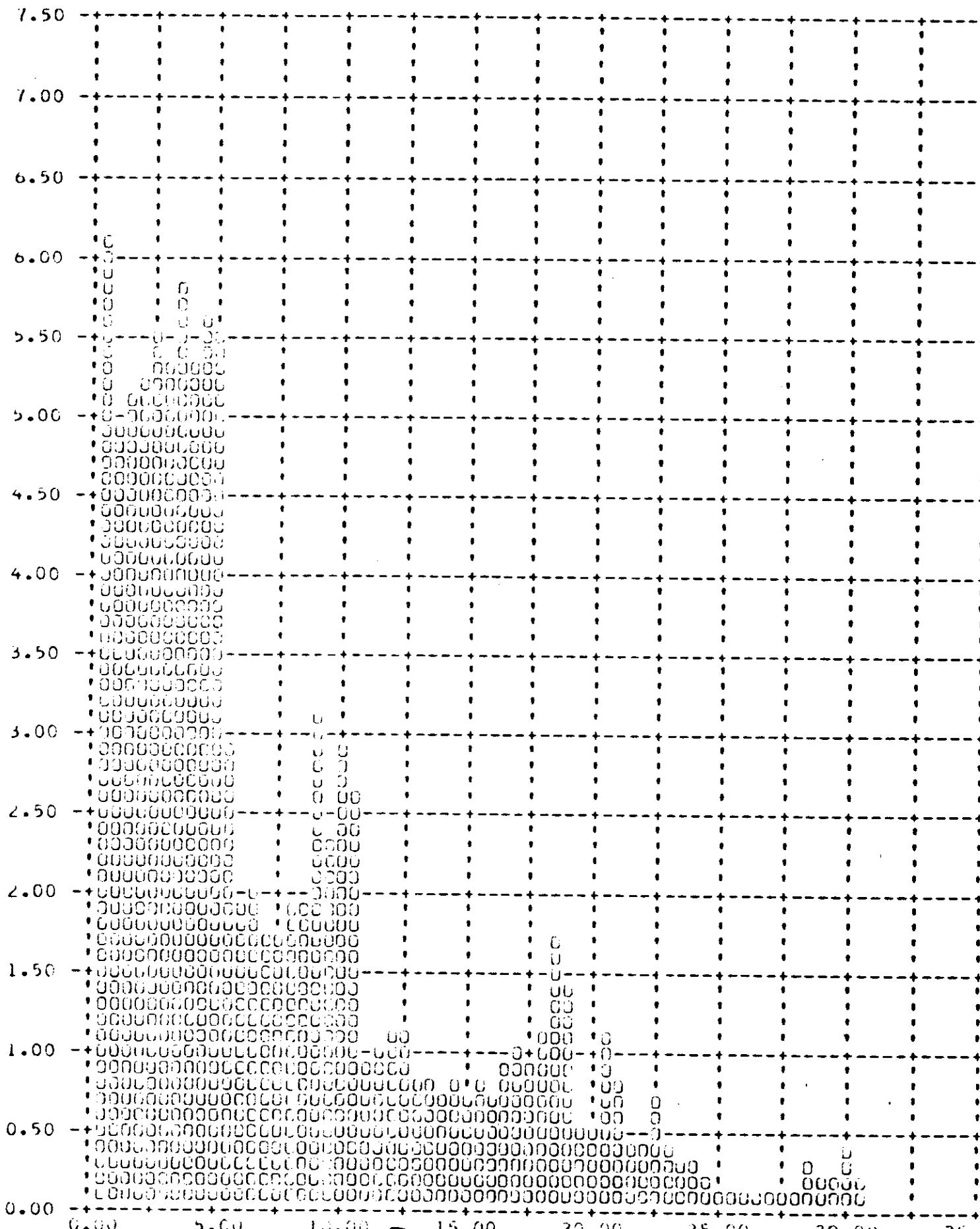


MISSION 1034A1 TOP SECRET

- CONTROL NO.

FRAMES 1-6 OF EACH UP OMITTED 90 PERCENT = 17.

Y ALONG TRACK RESOLUTION LIMIT - FEET (X) VERSUS FREQUENCY - PERCENT (

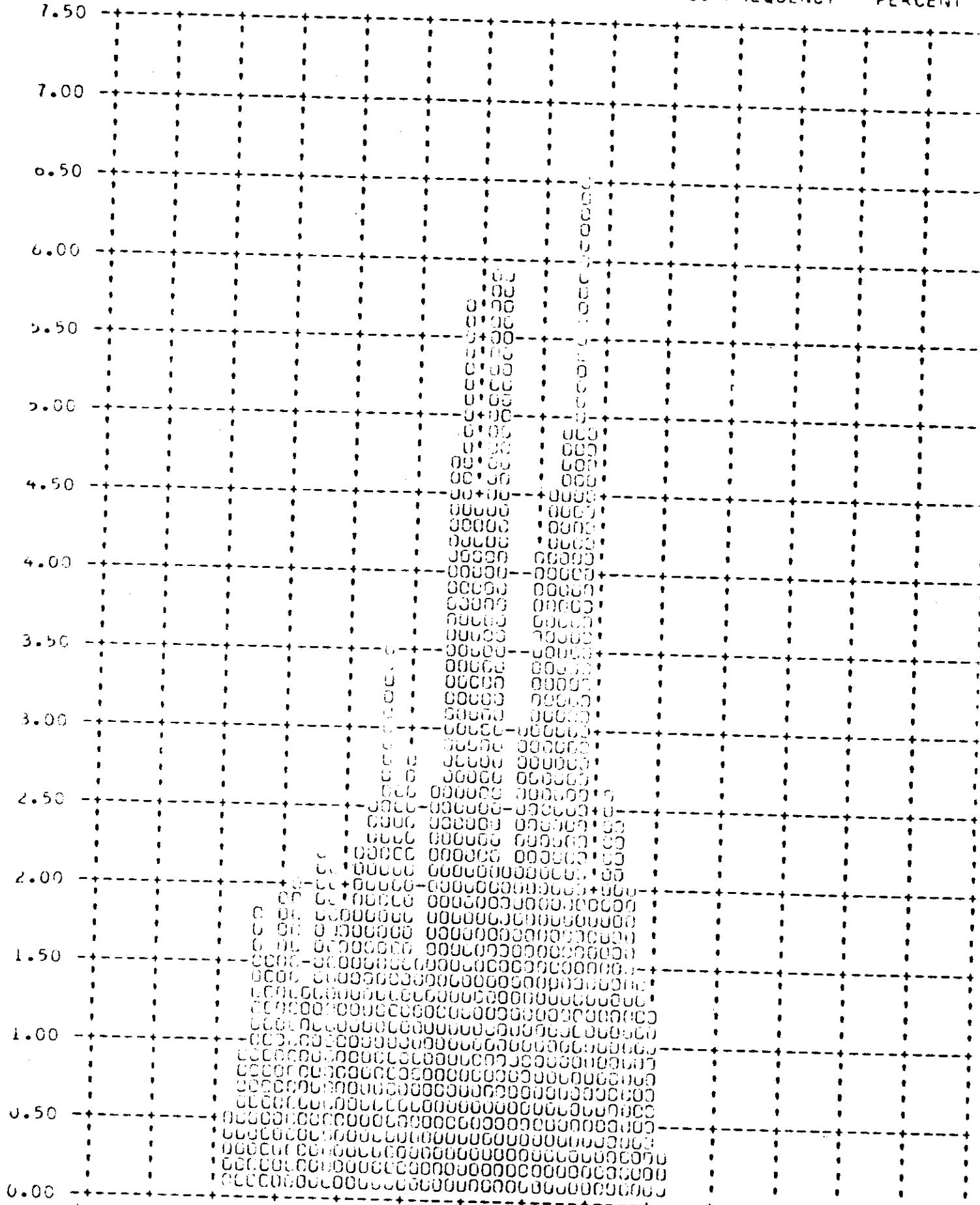


MISSION 1034A1 ~~TOP SECRET~~

- CONTROL NO.

FRAMES 1-6 OF EACH OP OMITTED 90 PERCENT = 5

Y CROSS TRACK RESOLUTION LIMIT - FEET (X) VERSUS FREQUENCY - PERCENT

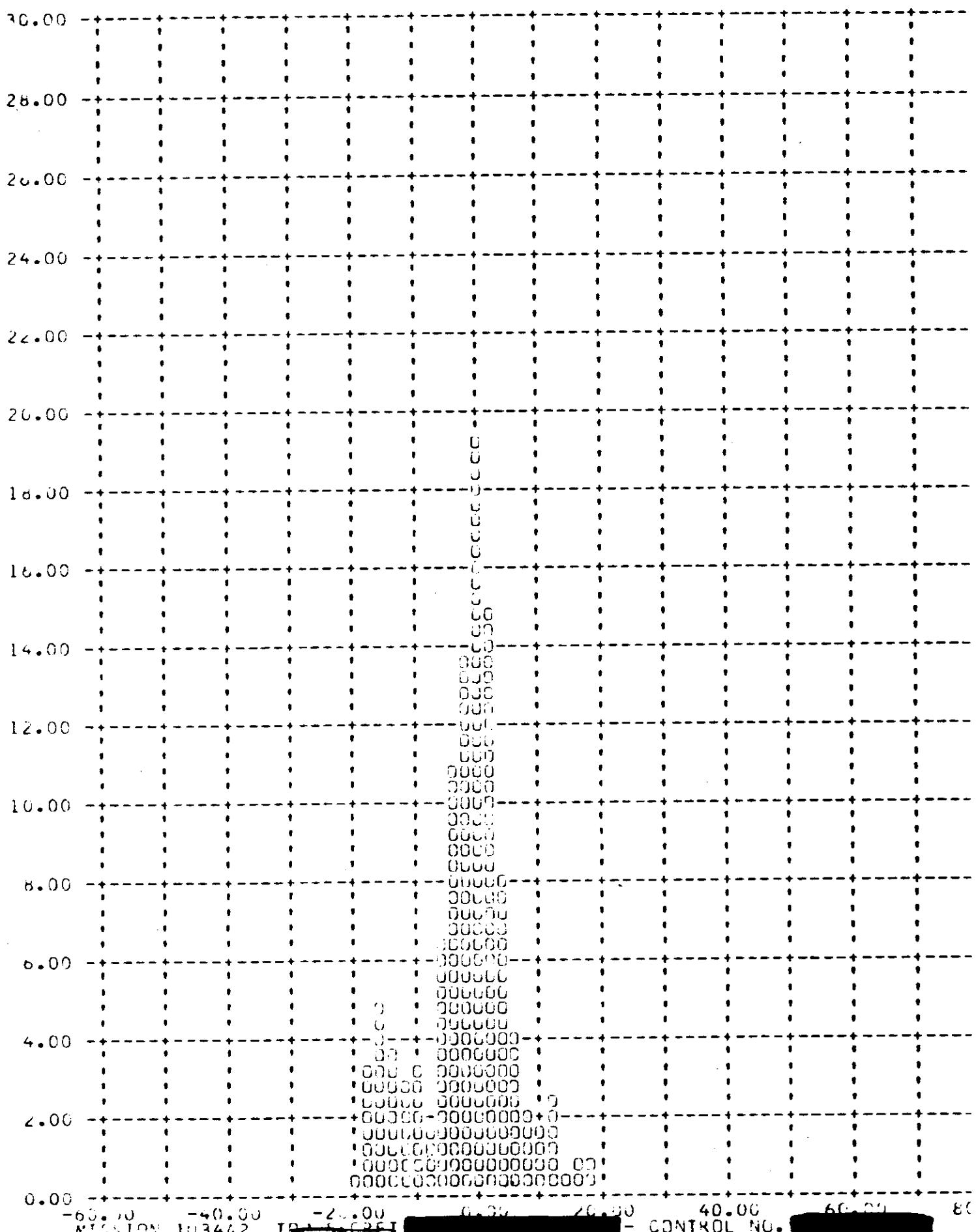
MISSION 1034A1 ~~TOP SECRET~~

MISSION 103442 ~~TOP SECRET~~

- CONTROL NO.

FRAMES 1-6 OF EACH DP OMITTED 90 PERCENT = 15.

Y V/H RATIO ERROR - PERCENT (X) VERSUS FREQUENCY = PERCENT (Y)

MISSION 103442 ~~TOP SECRET~~

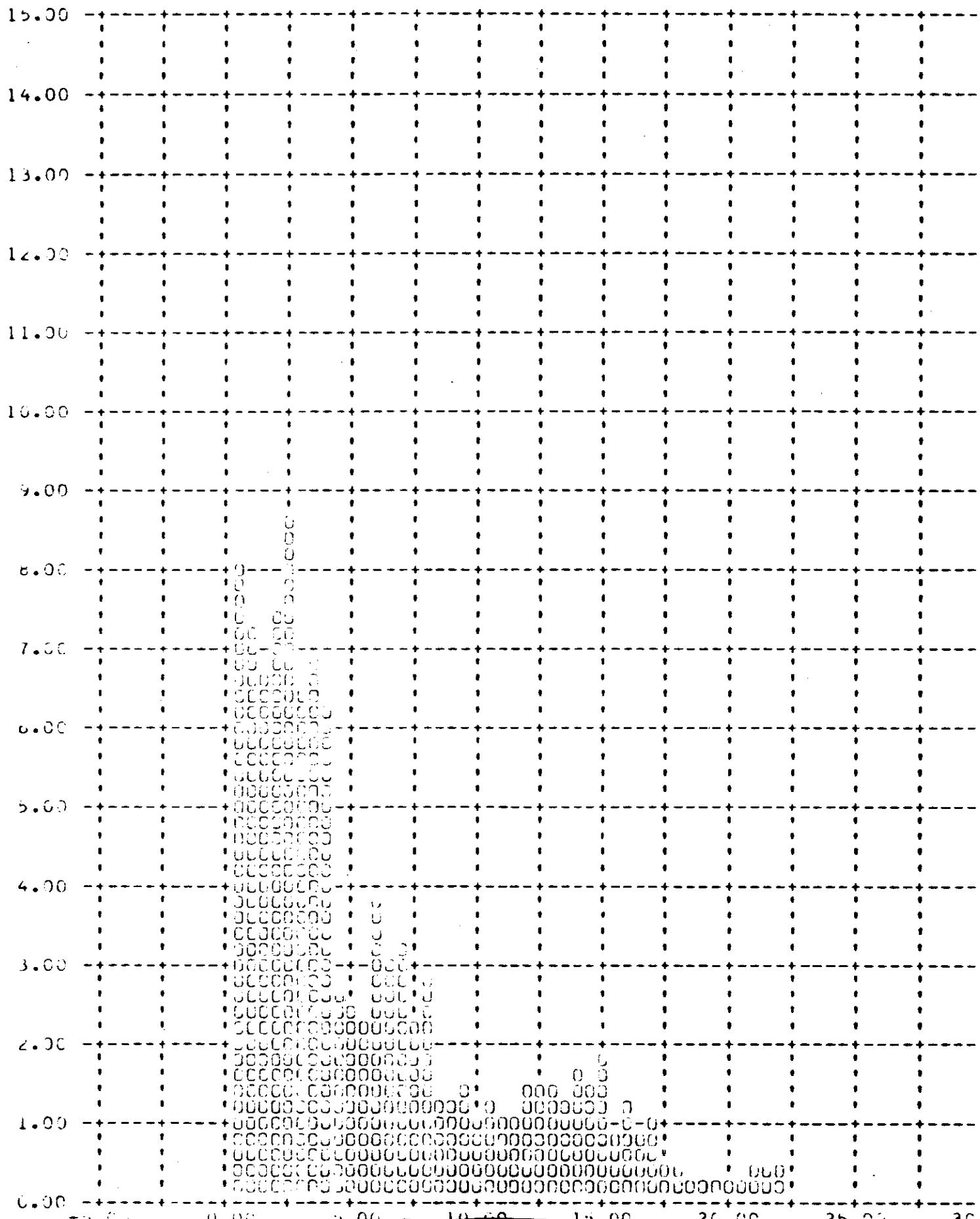
- CONTROL NO.

MISSION 1 34A2 TOP SECRET

- CONTROL NO.

FRAMES 1-6 OF EACH UP OMITTED 90 PERCENT = 13.

Y ALONG TRACK RESOLUTION LIMIT - FEET (X) VERSUS FREQUENCY - PERCENT (

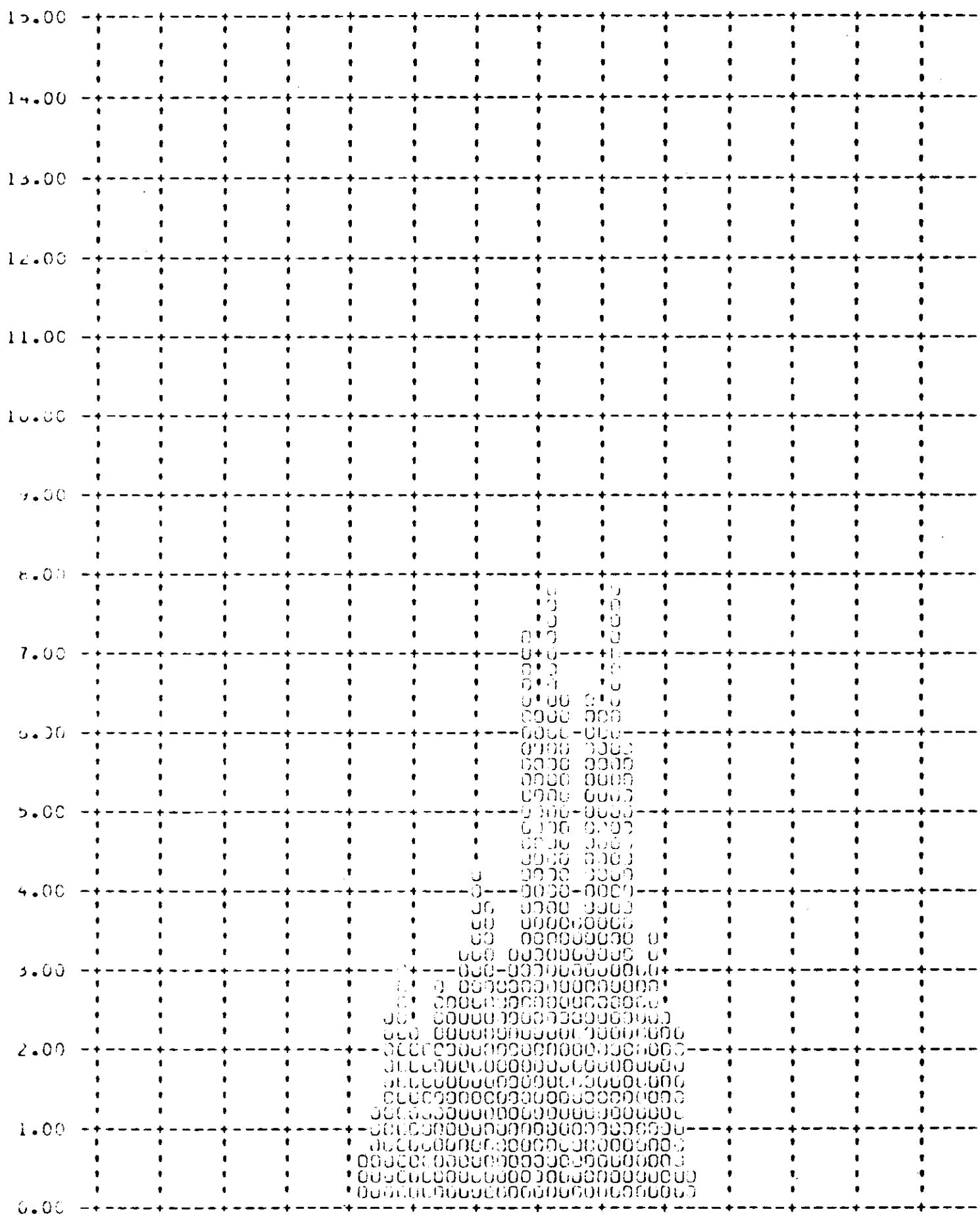


MISSION 1 34A2 TOP SECRET

- CONTROL NO.

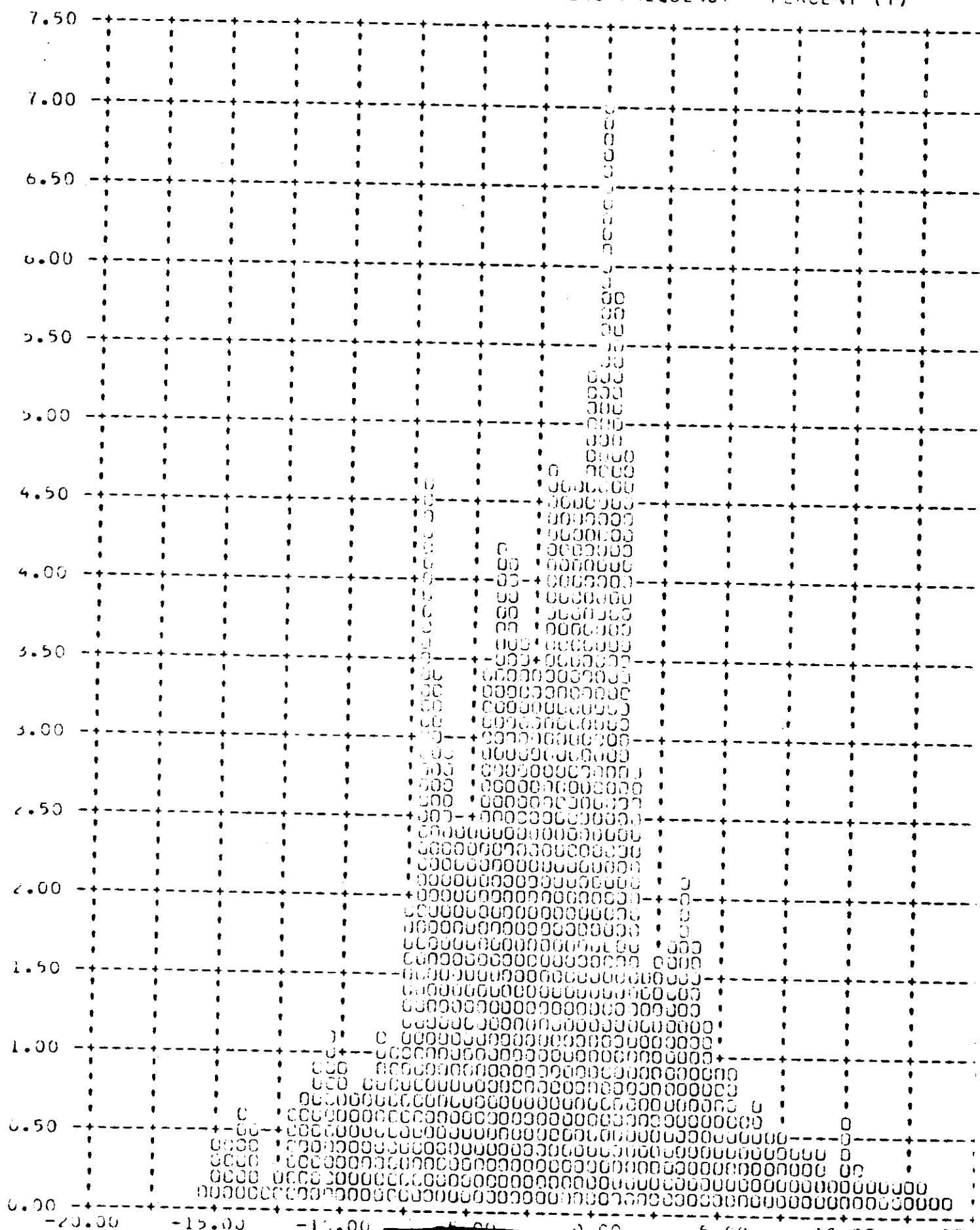
FRAMES 1-6 OF EACH DP OMITTED 90 PERCENT = .4.

Y CROSS TRACK RESOLUTION LIMIT - FEET (Y) VERSUS FREQUENCY - PERCENT (X)



FRAMES 1-6 OF EACH OP OMITTED 90 PERCENT = 6.

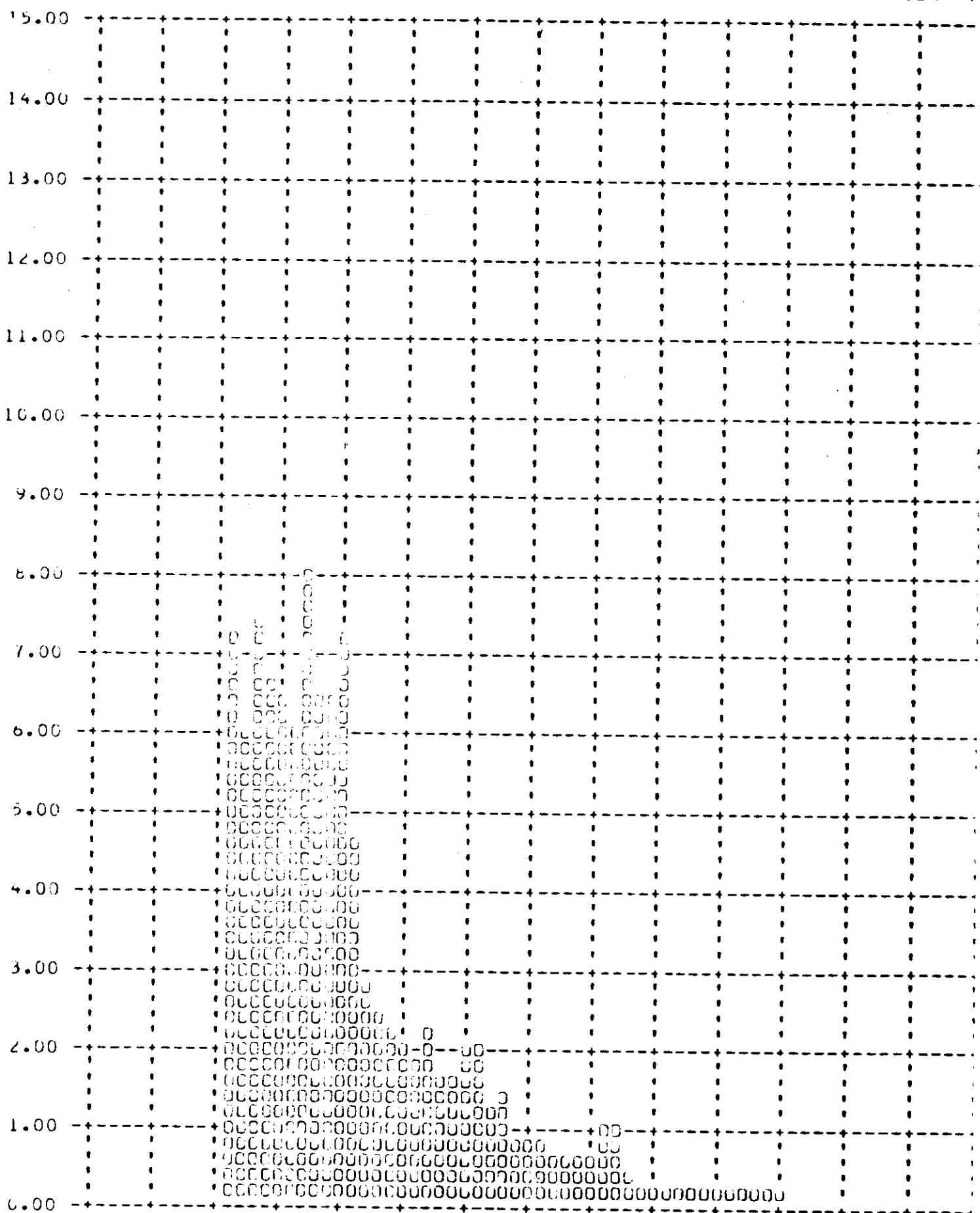
Y V/H RATIO ERROR - PERCENT (X) VERSUS FREQUENCY - PERCENT (Y)



MISSION 1034B1 ~~TOP SECRET~~- CONTROL NO. ~~1034B1~~

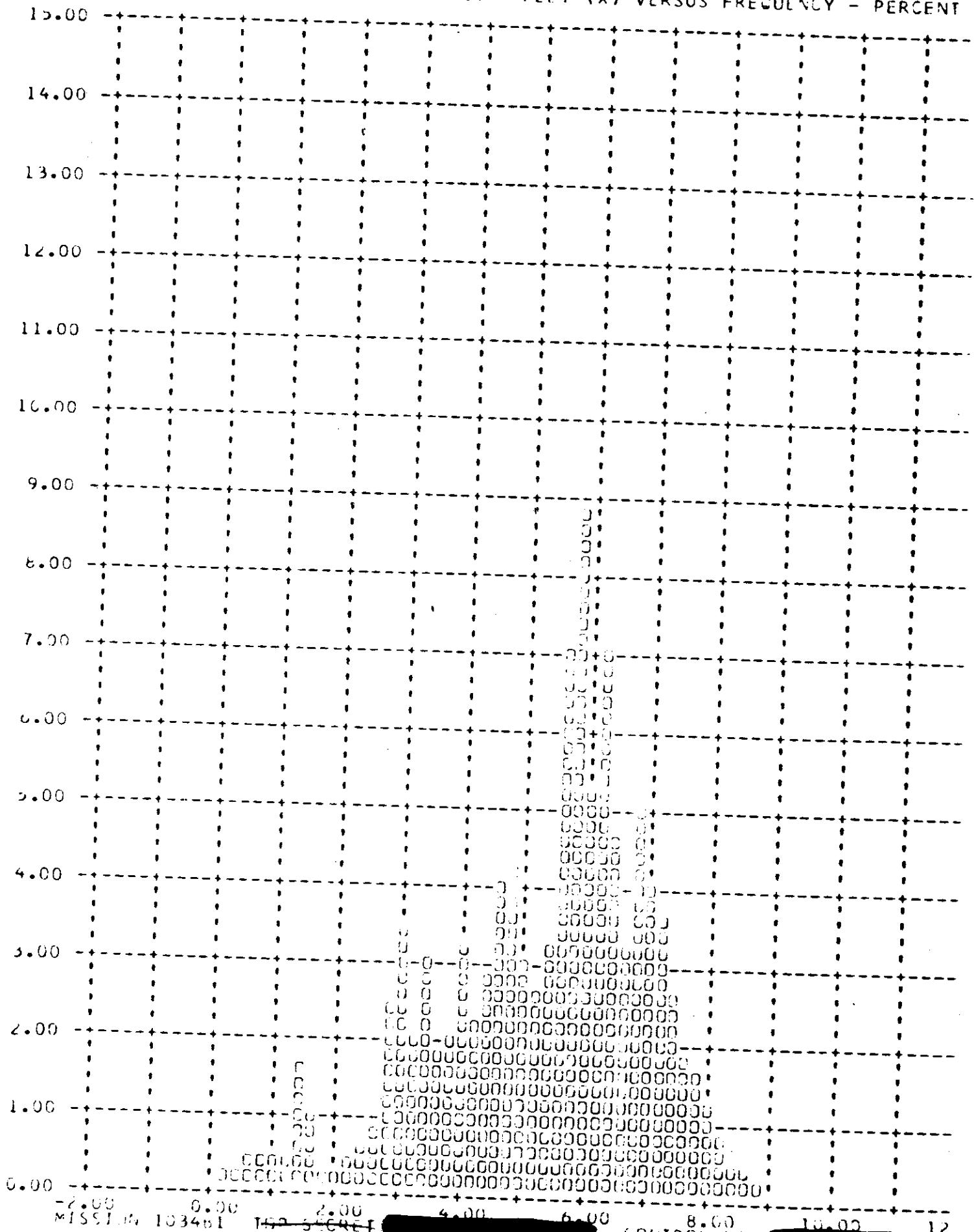
FRAMES 1-6 OF EACH OP OMITTED 90 PERCENT = 10.

Y ALONG TRACK RESOLUTION LIMIT - FEET (X) VERSUS FREQUENCY - PERCENT (

MISSION 1034B1 ~~TOP SECRET~~- CONTROL NO. ~~1034B1~~

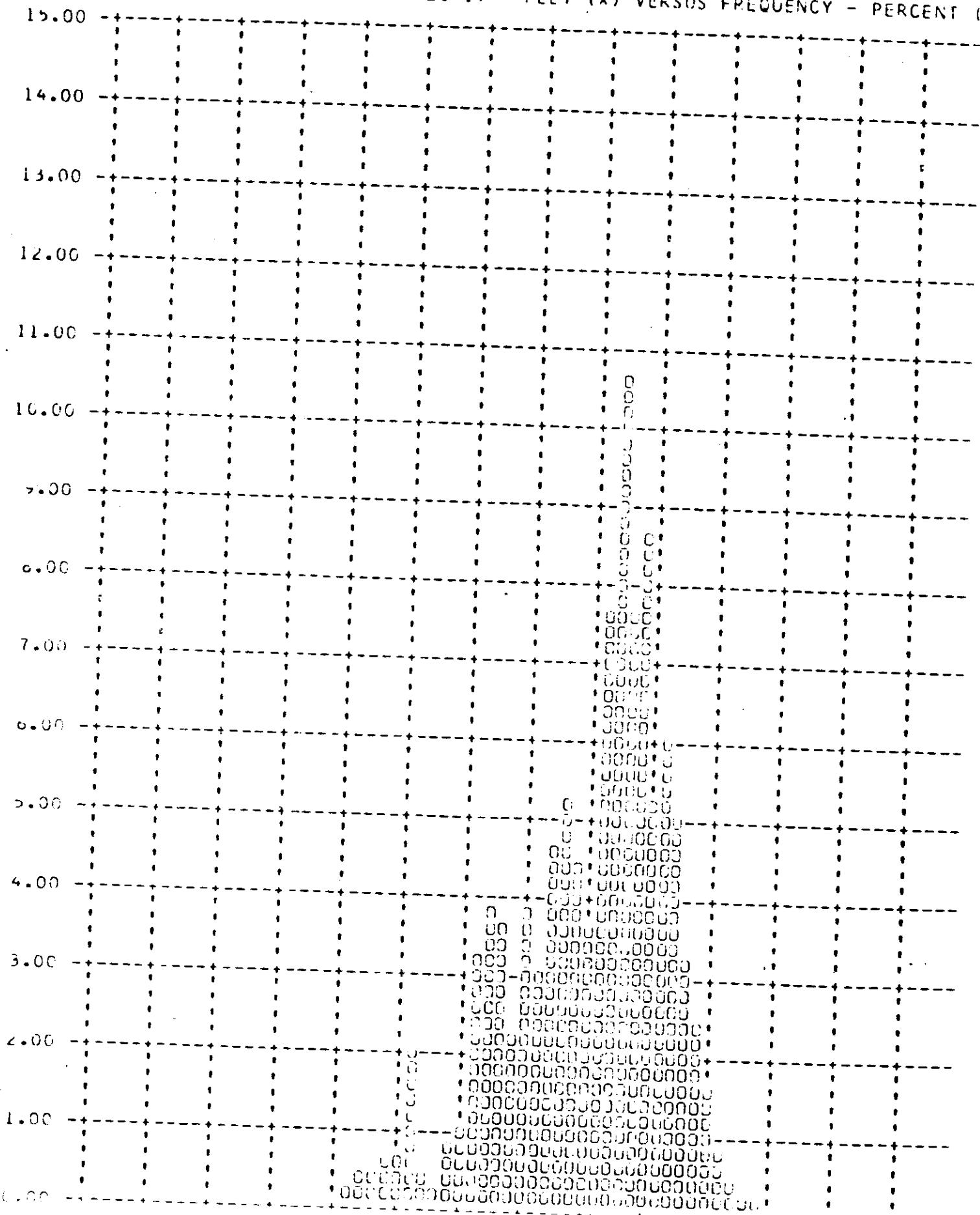
FRAMES 1-6 OF EACH DP OMITTED 90 PERCENT = 7

Y CROSS TRACK RESOLUTION LIMIT - FEET (X) VERSUS FREQUENCY - PERCENT



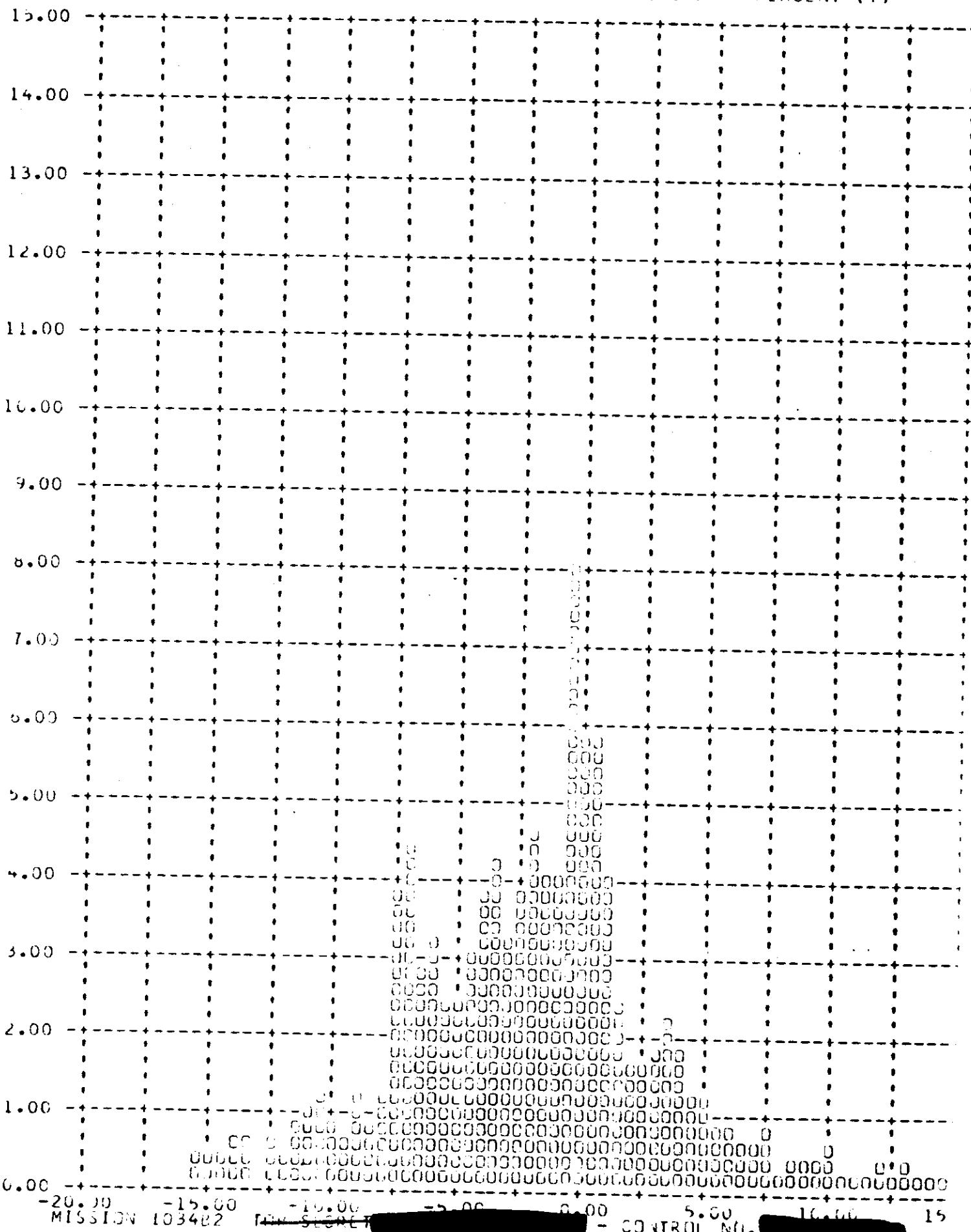
FRAMES 1-6 OF EACH UP DMITTED 90 PERCENT = 5.

Y CROSS TRACK RESOLUTION LIMIT - FEET (X) VERSUS FREQUENCY - PERCENT (



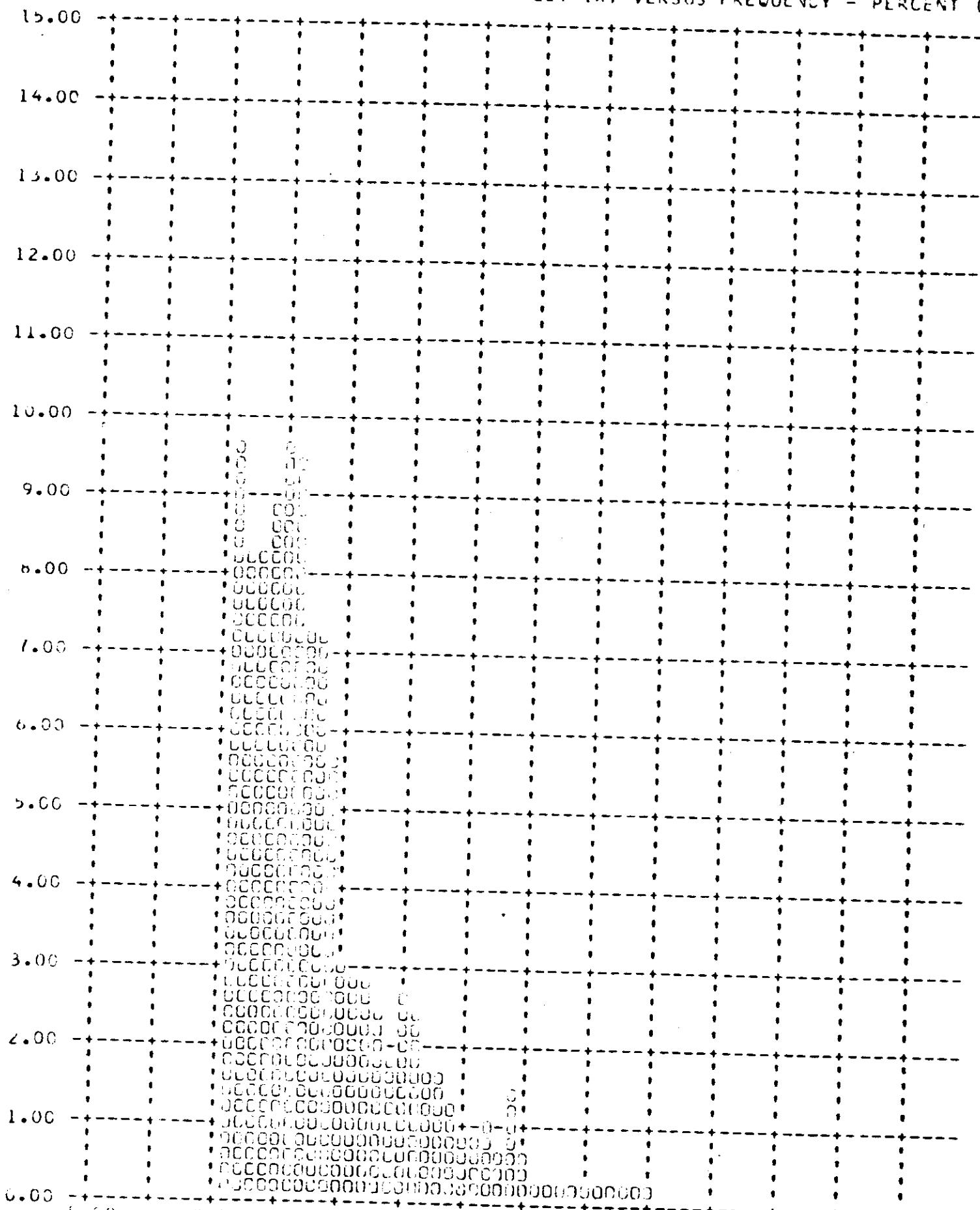
FRAMES 1-6 OF EACH OP OMITTED 90 PERCENT = 8.9

Y V/H RATIO ERROR - PERCLNT (X) VERSUS FREQUENCY - PERCENT (Y)



FRAMES 1-6 OF EACH UP OMITTED 90 PERCENT = 8.

Y ALONG TRACK RESOLUTON LIMIT - FEET (X) VERSUS FREQUENCY - PERCENT (



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SECTION 13

RADIATION DOSAGE

Each recovery system flown on a Corona mission contains a sealed packet of Eastman Type 3401 and Royal X Pan emulsions to determine the total radiation received at the take-up cassette. Both film types have been irradiated by LMSC at various levels and the base plus fog densities recorded after controlled processing.

Following recovery the film dosimeter packets are removed at A/P and processed with a pre-flight sample of the same film type and sensitometric control film. The resulting base plus fog density measurement of the dosimeter strips is used to ascertain the total radiation level. The table below presents the base plus fog readings for the dosimeter strips, and the radiation level equivalents.

<u>Emulsion</u>	Mission 1034-1		Mission 1034-2	
	<u>B + F</u> <u>Density</u>	<u>Radiation</u>	<u>B + F</u> <u>Density</u>	<u>Radiation</u>
Type 3401	0.10	None	0.17	0.5R
Royal X Pan	0.21	0.2 R	0.24	0.4R

These levels are much below that which will degrade the photography. At this level of radiation dosage the graph of the radiation equivalents is rather indeterminate.

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SECTION 14

SYSTEM RELIABILITY

Reliability calculations for the payload are based on a sample beginning with M-7. Hence, both the major part of the Mural Program and the "J" Program are covered in the calculation. For certain auxiliaries, i.e., the stellar-index camera and the horizon cameras, the sample size is changed to recognize incorporation of modified equipment or new designs where reliability was one of the principal reasons for the modification. However, for primary mission function, the sample size is consistent with reliability reporting for the vehicle.

The reliability estimates of this section deal exclusively with the payload. Failures to achieve orbit or vehicle induced failures are thereby excluded. Recoveries before a complete mission has been completed are considered as full missions providing that early termination was caused by reasons not connected with payload operation. Film quality is not considered in the reliability estimate calculation. Hence, only electrical and mechanical functioning are considered. The pressure make-up system, V/h programmer, and flashing light failures are counted against the component reliabilities, but are not included in the estimates given below in that these failures did not compromise or materially degrade the primary mission performance.

The reliability estimate is also divided into primary and secondary functions. The primary functions are operation of the panoramic cameras, main camera door operation, operation of the payload clock, and recovery operations. The secondary mission functions are horizon camera operation excluding catastrophic open shutter failure mode, auxiliary data recording, and stellar-index camera operation. A summary of estimated reliability is shown in Tables 14-1.

Panoramic Camera Reliability

Sample Size - 151 opportunities to operate.

One failure - S/I programmer on System J-19.

Assume - 3000 cycles per camera per mission

Estimated Reliability = 93.9% at 50% confidence level.

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Main Camera Door Reliability

Sample Size - 51 vehicles x 2 doors = 102 opportunities to operate.
Estimated Reliability = 99.3% at 50% confidence level.

Payload Command and Control

Sample Size - 8208 hours operation in sample
Two failures
Estimated reliability = 96.9% at 50% confidence level.

Payload Clock Reliability

Sample Size - 8203 hours operation in sample
No failures
Estimated Reliability = 99.2% at 50% confidence level.

Estimated Reliability of Payload Functioning on orbit = 97.2% at
50% confidence level.

Recovery System Reliability

67 opportunities to recover
1 failure - improper separation due to water seal - cutter failure
Estimated Reliability = 97.5% at 50% confidence level

Stellar-Index Camera Reliability

Sample begins with J5
Sample size = 19,980
Four failures
Estimated Reliability = 90.5 at 50% confidence level

Horizon Camera Reliability

Sample begins with J5 - 82,500 cycles
Estimated Reliability of Single Camera = 98.7% at 50% confidence level
Estimated Reliability of Four Horizon Cameras at a Parallel
Redundant System = 99.9% at 50% confidence level.

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ESTIMATED RELIABILITY SUMMARY

(AT 50% CONFIDENCE LEVEL)

MISSION NUMBER	PRIMARY FUNCTIONS				SECONDARY FUNCTIONS			
	PANORAMIC CAMERA	PANORAMIC DOORS	CAMERA COMMAND & CONTROL SYSTEM	PAYOUT CLOCK	ON - ORBIT FUNCTIONS	RECOVERY SYSTEM	STELLAR - INDEX	HORIZON CAMERAS
	SAMPLE FAILURES	SAMPLE FAILURES	RELIABILITY	FAILURES	RELIABILITY	SAMPLE FAILURES	SAMPLE FAILURES	SAMPLE FAILURES
9038 to 1008	52	60348	98.6	0	96.0	96.1	90.7	93.1
1009	54	3216	98.6	0	96.0	96.2	92.5	93.7
1010	56	3432	98.7	0	96.0	96.4	92.5	93.4
1011	58	3600	98.8	0	96.1	96.4	92.5	93.7
1012	60	3720	98.9	0	96.1	96.5	93.0	94.7
1013	62	3940	98.9	0	96.2	96.6	93.5	94.7
1014	64	4056	99.0	1	96.3	96.7	93.5	94.8
1015	66	4320	99.0	1	96.3	96.8	93.5	94.8
1016	68	4560	99.0	1	96.4	96.9	93.5	94.8
1017	70	4760	99.0	1	96.5	96.9	93.6	94.9
1018	72	4920	99.1	1	96.5	97.0	93.7	95.0
1019	74	5136	99.1	1	96.6	97.1	93.8	95.1

* RETURN FIX MEASURED PREVIOUS FAILURE CONSIDERATIONS

** 100% SAMPLE OUT OF WARRANTY

ESTIMATED RELIABILITY SUMMARY

(AT 50% CONFIDENCE LEVEL)

MISSION NUMBER	PRIMARY FUNCTIONS				SECONDARY FUNCTIONS				FUNCTIONS			
	PANORAMIC CAMERA		COMMAND & CONTROL SYSTEM		ON-ORBIT FUNCTIONS		RECOVERY SYSTEM		STELLAR - INDEX CAMERAS		HORIZON CAMERAS	
	SAMPLE	DOORS	SAMPLE	CLOCK	SAMPLE	FUNCS	SAMPLE	SYSTEM	SAMPLE	CAMERAS	SAMPLE	CAMERAS
1020	106	78	5	98	0	99	0	96	9	43	10,680	48,000
1021	104	76	5	97	1	97	1	96	1	961	2	69,9
1022	112	80	0	93	1	97	0	96	9	980	2	46,500
1023	114	82	0	98	5	97	4	96	9	11,550	2	51,000
1024	114	84	0	99	2	97	3	96	9	963	2	90,7
1025	122	86	0	99	2	95	8	96	9	12,190	2	54,000
1026	126	88	0	99	2	96	0	96	2	965	2	57,000
1027	128	90	0	99	2	96	1	96	3	13,040	2	98,1
1028	132	92	0	99	2	96	0	96	3	966	2	98,1
1029	136	94	0	99	2	96	1	96	0	13,890	2	60,000
1030	140	96	0	99	3	96	5	96	0	967	2	92,1
1031	143	98	0	99	3	96	6	96	0	14,740	2	63,000
										53		
										968		
										967		
										965		
										15,165		
										970		
										16,015		
										971		
										16,580		
										972		
										17,430		
										61		
										973		
										974		
										975		
										976		
										977		
										978		
										979		

ESTIMATED RELIABILITY SUMMARY

(AT 50% CONFIDENCE LEVEL)

MISSION NUMBER	PRIMARY FUNCTIONS				SECONDARY FUNCTIONS			
	PANORAMIC CAMERA	PANORAMIC CAMERA DOORS	COMMAND & CONTROL SYSTEM	PAYOUT CLOCK	ON - ORBIT FUNCTIONS	RECOVERY SYSTEM	STELLAR - INDEX CAMERAS	HORIZON CAMERAS
	SAMPLE	SAMPLE	SAMPLE	SAMPLE	SAMPLE	SAMPLE	SAMPLE	SAMPLE
	FAILURES	FAILURES	FAILURES	FAILURES	FAILURES	FAILURES	FAILURES	FAILURES
	RELIABILITY	RELIABILITY	RELIABILITY	RELIABILITY	RELIABILITY	RELIABILITY	RELIABILITY	RELIABILITY
1033	100	7968	7968	0	97 1	65	9,130	78,500
	0	2	96 8	0	99 2	1	4	0
	98 9	99 3	8208	8208		97 4	90 2	98 7
151	102	0	2	0	97 2	67	19,980	82,500
	1	98 9	99 3	96 9	99 2	1	4	0
1034	98 9	99 3	99 3	99 3		97 5	90 5	98 7

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NO. [REDACTED]

SECTION 15

SUMMARY DATA

The comparison of the operating parameters and the performance achieved by previous missions has been difficult due to the large volume of data that results from each mission. Some of the pertinent characteristics from prior missions have been summarized in Tables 15-1 through 15-3.

The summary data was started with Mission 1004 as the J-05 camera system was the first to incorporate the major modifications of the titanium drum and scan arm, four roller scan head and Corona J capabilities. Only those missions that culminated in the recovery of some photography have been listed, therefore Missions 1003, 1005 and 1032 are deleted.

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MISSION SUMMARY

MISSION NUMBER	PAYLOAD NUMBER	VEHICLE NUMBER	LAUNCH DATE	LAUNCH TIME	ORBIT NUMBER	ALTITUDE (NM)	REF. VELOCITY (NM/H)	REF. DISTANCE (NM)	REF. DURATION (NM)	WIFIEE	CAMERA	SATELLITE FILTER	CAMERA NUMBER	STELLAR	AMPA	AMPA	AMPA	AMPA
														NUMBER	NUMBER	NUMBER	NUMBER	
1004	J-05	1174	2/15/64	2159 2	74.9	99.9	29.0	49	112	124	0.250	W-21	125	0.250	W-21	029/29/29	042/42/37	
1006	J-09	1175	6/4/64	2259 2	79.9	84.0	63.2	65	128	148	0.200	W-21	149	0.200	W-21	045/47/45	049/53/42	
1007	J-07	1609	6/19/64	2316 2	85.0	99.2	41.5	65	128	144	0.250	W-25	145	0.200	W-21	043/43/43	054/56/51	
1008	J-10	1177	7/10/64	2314 2	85.0	99.4	40.8	49	112	150	0.200	W-21	151	0.200	W-21	048/45/48	053/58/53	
1009	J-12	1605	8/5/64	2316 2	80.1	99.6	39.5	49	128	154	0.200	W-21	155	0.200	W-21	056/39/56	058/38/34	
1010	J-11	1178	9/14/64	2254 2	84.9	97.4	42.5	65	144	152	0.175	W-21	153	0.175	W-21	030/30/30	044/46/44	
1011	J-3X	1170	10/5/64	2150 2	79.9	99.3	20.9	65	—	160	0.175	W-21	161	0.175	W-21	057/57/57	057/57/57	
1012	J-13	1179	10/17/64	2202 2	75.0	96.2	32.4	49	91	156	0.200	W-21	157	0.200	W-21	046/52/51	046/52/51	
1013	J-15	1173	11/12/64	2150 2	80.0	100.0	25.0	65	61	159	0.225	W-21	159	0.225	W-21	052/49/55	047/48/54	
1014	J-16	1180	11/18/64	2036 2	70.0	103.2	65.6	61	145	162	0.250	W-25	139	0.175	W-21	053/59/49	050/44/46	
1015	J-17	1607	12/19/64	2110 2	74.9	95.7	21.5	61	175	138	0.250	W-25	141	0.175	W-21	061/61/61	058/58/58	
1016	J-18	1608	1/15/65	2151 2	74.9	99.4	30.2	81	159	132	0.250	W-25	133	0.175	W-21	059/50/59	059/50/59	
1017	J-14	1611	2/25/65	2144 2	75.0	97.2	25.9	61	145	140	0.250	W-25	165	0.175	W-21	021/21/21	060/81/81	
1018	J-19	1612	3/25/65	2111 2	96.0	100.2	40.3	66	99	122	0.250	W-25	123	0.175	W-21	020/20/20	022/22/22	
1019	J-04	1614	4/29/65	2144 2	85.0	99.1	27.1	80	118	0.250	W-25	119	0.175	W-21	039/39/35	019/18/19		
1020	J-20	1613	6/9/65	2158 2	75.1	97.1	40.6	97	113	136	0.250	W-25	137	0.175	W-21	067/85/80	062/65/65	
1021	J-21	1615	5/18/65	1803 2	75.0	109.2	24.3	81	161	166	0.175	W-21	167	0.250	W-25	063/69/69	025/27/25	
1022	J-22	1617	7/19/65	2201 2	85.0	99.7	30.3	65	144	168	0.250	W-25	169	0.175	W-21	017/19/82	024/24/24	
1023	J-23	1618	8/17/65	2100 2	70.0	97.8	29.0	81	144	170	0.225	W-25	171	0.150	W-21	059/72/84	064/82/85	
1024	J-24	1619	9/22/65	2131 2	80.0	95.9	18.4	81	161	172	0.225	W-25	173	0.150	W-21	071/87/87	066/74/83	
1025	JX-28	1616	10/5/65	1746 2	75.0	112.9	44.3	81	161	142	0.175	W-21	127	0.175	W-21	077/97/97	078/76/95	
1026	J-25	1620	10/28/65	2117 2	75.0	93.0	17.0	81	160	174	0.225	W-25	175	0.150	W-21	072/89/85	072/89/85	
1027	JX-27	1621	12/9/65	2110 2	80.0	97.4	17.3	17	33	164	0.250	W-25	163	0.175	W-21	070/88/91	077/97/97	
1028	J-26	1610	12/24/65	2106 2	80.0	97.6	28.4	81	144	176	0.250	W-25	177	0.175	W-21	078/76/95	078/76/95	

MISSION SUMMARY

PERFORMANCE SUMMARY

MISSION NUMBER	Aircraft	Type	S.A. Ref.	Performance																	
				Altitude ft	Speed ft/min																
1004-1	FWD	AFT	124	84	78	97	109	121	121	124	124	128	128	128	128	128	128	128	128	128	128
1004-2	FWD	AFT	125	85	76	86	96	113	113	84	92	92	92	92	92	92	92	92	92	92	92
1005-1	FWD	AFT	148	90	78	65	88	97	97	97	97	97	97	97	97	97	97	97	97	97	97
1006-2	FWD	AFT	149	90	85	74	150	91	91	97	97	97	97	97	97	97	97	97	97	97	97
1007-1	FWD	AFT	144	85	80	60	60	87	82	91	95	95	95	95	95	95	95	95	95	95	95
1007-2	FWD	AFT	145	85	79	79	350	43	81	320	110	69	74	81	110	69	74	81	110	69	74
1008-1	FWD	AFT	150	85	80	80	95	81	83	95	95	95	95	95	95	95	95	95	95	95	95
1008-2	FWD	AFT	151	85	82	84	96	96	91	92	92	92	92	92	92	92	92	92	92	92	92
1009-1	FWD	AFT	154	85	92	80	80	75	88	88	88	88	88	88	88	88	88	88	88	88	88
1009-2	FWD	AFT	155	85	94	85	350	85	83	83	83	83	83	83	83	83	83	83	83	83	83
1010-1	FWD	AFT	152	85	90	90	90	88	88	90	90	90	90	90	90	90	90	90	90	90	90
1010-2	FWD	AFT	153	85	92	88	350	86	86	86	86	86	86	86	86	86	86	86	86	86	86
1011-1	FWD	AFT	160	90	84	350	76	80	91	87	87	87	87	87	87	87	87	87	87	87	87
1011-2	FWD	AFT	161	90	84	77	80	86	91	80	80	80	80	80	80	80	80	80	80	80	80
1012-1	FWD	AFT	156	85	92	80	80	87	80	89	89	89	89	89	89	89	89	89	89	89	89
1012-2	FWD	AFT	157	85	91	—	80	89	91	80	84	84	84	84	84	84	84	84	84	84	84
1013-1	FWD	AFT	158	85	89	—	80	94	80	85	93	93	93	93	93	93	93	93	93	93	93
1014-1	FWD	AFT	162	80	87	—	80	78	78	74	86	86	86	86	86	86	86	86	86	86	86
1014-2	FWD	AFT	159	85	83	—	80	75	80	80	95	107	107	107	107	107	107	107	107	107	107
1015-1	FWD	AFT	138	85	87	—	80	73	80	80	89	89	89	89	89	89	89	89	89	89	89
1015-2	FWD	AFT	141	85	83	—	80	72	72	72	90	90	90	90	90	90	90	90	90	90	90
1016-1	FWD	AFT	140	85	85	—	80	61	80	90	94	94	94	94	94	94	94	94	94	94	94
1016-2	FWD	AFT	165	85	85	—	80	55	80	92	91	91	91	91	91	91	91	91	91	91	91
1017-1	FWD	AFT	122	85	79	—	80	74	80	82	92	92	92	92	92	92	92	92	92	92	92
1017-2	FWD	AFT	123	85	84	—	80	75	80	96	103	103	103	103	103	103	103	103	103	103	103
1018-1	FWD	AFT	122	85	77	—	80	74	80	96	103	103	103	103	103	103	103	103	103	103	103
1018-2	FWD	AFT	123	85	84	—	80	75	80	97	103	103	103	103	103	103	103	103	103	103	103

PERFORMANCE SUMMARY

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1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99	100
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99	100
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99	100
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99	100

EXPOSURE - PROCESSING SUMMARY

EXPOSURE - PROCESSING SUMMARY

TESTS

TEST NUMBER	TEST DATE	TEST TIME	TESTER	TESTER COMMENTS	
1019-1	FWD	24-70	24-152	0-21	79-57
	AFT	25-70	21-152	0-24	46-42
1020-1	FWD	30-75	19-156	0-19	81-59
	AFT	29-75	17-156	0-15	46-39
1020-2	FWD	47-63	18-35	0-15	66-36
	AFT	46-69	17-33	0-15	66-36
1021-1	FWD	15-66	14-88	0-25	69-32
	AFT	14-66	-17-41	0-29	99-53
1021-2	FWD	13-52	-13-3	0-100	53-25
	AFT	13-52	-13-3	0-100	53-25
1022-1	FWD	28-67	26-150	0-36	56-36
	AFT	27-67	26-150	0-36	56-36
1022-2	FWD	29-74	21-152	0-89	92-17
	AFT	28-74	19-152	0-100	92-17
1023-1	FWD	22-82	8-164	0-5	95-9
	AFT	20-81	5-163	0-11	89-9
1023-2	FWD	29-80	13-177	0-7	93-9
	AFT	28-80	13-178	0-3	97-9
1024-1	FWD	0-61	2-4	137-0	0-100
	AFT	9-61	2-4	136-0	0-100
1024-2	FWD	9-79	1-151	0-0	0-100
	AFT	8-79	9-151	0-0	0-100
1025-1	FWD	1-70	-123-18	0-72	8-32
	AFT	0-70	-121-19	0-72	8-49
1025-2	FWD	0-56	-124-31	0-71	29-342
	AFT	0-55	-122-33	0-73	27-345
1026-1	FWD	0-57	2-355	0-4	36-36
	AFT	0-57	2-135	0-5	95-0
1026-2	FWD	0-72	8-84	0-0	0-100
	AFT	0-57	1-13	78-0	0-100
1027-1	FWD	3-63	2-6	110-0	0-0
	AFT	2-63	2-6	108-0	0-0
1028-1	FWD	3-73	1-155	0-4	96-0
	AFT	0-73	1-14	133-0	0-100
1028-2	FWD	2-61	5-48	0-3	97-0
	AFT	-80	80-5	43-0	10-90
1029-1	FWD	3-63	1-18	130-0	0-8
	AFT	4-63	2-22	129-0	0-53
1029-2	FWD	3-62	1-16	158-0	0-42
	AFT	2-78	7-157	-1	23-76
1030-1	FWD	5-63	2-7	130-0	0-8
	AFT	1-70	18-140	0-99	1-18
1031-1	FWD	1-70	18-140	0-99	1-18
	AFT	1-70	18-140	0-99	1-18
1031-2	FWD	1-70	18-140	0-99	1-18
	AFT	1-70	18-140	0-99	1-18
1033-1	FWD	1-70	4-16	155-0	0-89
	AFT	1-70	4-15	135-0	0-100
1033-2	FWD	0-54	3-34	131-0	0-84
	AFT	0-54	3-34	131-0	0-86

INSUFFICIENT DATA

TEST NUMBER	TEST DATE	TEST TIME	TESTER	TESTER COMMENTS	TEST DATE	TEST TIME	TESTER	TESTER COMMENTS	TEST DATE	TEST TIME	TESTER	TESTER COMMENTS
1019-1	FWD	24-70	24-152	0-21	79-57	4-42	3-41	6-61	5-60	2-14	4-45	1-50-1-50
	AFT	25-70	21-152	0-24	46-42	5-47	4-43	6-61	5-60	2-26	4-45	1-50-1-50
1020-1	FWD	30-75	19-156	0-19	81-59	1-54	1-53	2-60	0-50	2-26	2-45	1-54-1-54
	AFT	29-75	17-156	0-17	156-0	1-54	1-53	2-60	0-50	2-26	2-45	1-54-1-54
1020-2	FWD	47-63	18-35	0-14	33-25	1-54	1-53	2-60	0-50	2-26	2-45	1-54-1-54
	AFT	46-69	17-33	0-14	33-25	1-54	1-53	2-60	0-50	2-26	2-45	1-54-1-54
1021-1	FWD	15-66	14-88	0-25	69-32	0-53	0-52	0-51	0-50	0-35	0-42	0-50-0-50
	AFT	14-66	-17-41	0-100	53-25	0-53	0-52	0-51	0-50	0-35	0-42	0-50-0-50
1021-2	FWD	13-52	-13-3	0-100	53-25	0-53	0-52	0-51	0-50	0-35	0-42	0-50-0-50
	AFT	13-52	-13-3	0-100	53-25	0-53	0-52	0-51	0-50	0-35	0-42	0-50-0-50
1022-1	FWD	28-67	26-150	0-36	56-36	0-42	0-41	0-40	0-39	0-38	0-47	0-42-0-42
	AFT	27-67	26-150	0-36	56-36	0-42	0-41	0-40	0-39	0-38	0-47	0-42-0-42
1022-2	FWD	29-74	21-152	0-89	92-17	0-47	0-46	0-45	0-44	0-43	0-52	0-43-0-43
	AFT	28-74	19-152	0-100	92-17	0-47	0-46	0-45	0-44	0-43	0-52	0-43-0-43
1023-1	FWD	2-82	8-164	0-5	95-9	1-54	1-53	2-60	1-51	2-61	2-60	1-51-1-51
	AFT	20-81	5-163	0-11	89-9	0-19	0-18	0-18	0-18	0-18	0-18	0-18-0-18
1023-2	FWD	2-9	1-151	0-0	0-100	1-73	0-19	0-18	0-18	0-18	0-18	0-18-0-18
	AFT	2-8	9-151	0-0	0-100	1-72	0-19	0-18	0-18	0-18	0-18	0-18-0-18
1024-1	FWD	0-61	2-4	137-0	0-100	0-57	0-53	0-52	0-51	0-50	0-50	0-50-0-50
	AFT	9-61	2-4	136-0	0-100	0-57	0-53	0-52	0-51	0-50	0-50	0-50-0-50
1024-2	FWD	9-79	1-151	0-0	0-100	1-21	0-19	0-18	0-18	0-18	0-18	0-18-0-18
	AFT	8-79	9-151	0-0	0-100	1-22	0-19	0-18	0-18	0-18	0-18	0-18-0-18
1025-1	FWD	1-70	-123-18	0-72	8-32	0-41	0-41	0-40	0-39	0-38	0-38	0-38-0-38
	AFT	0-70	-121-19	0-72	8-49	0-43	0-43	0-42	0-41	0-40	0-40	0-40-0-40
1025-2	FWD	0-56	-124-31	0-71	29-342	0-42	0-42	0-41	0-40	0-39	0-39	0-39-0-39
	AFT	0-55	-122-33	0-73	27-345	0-42	0-42	0-41	0-40	0-39	0-39	0-39-0-39
1026-1	FWD	0-57	2-355	0-4	36-36	0-34	0-34	0-33	0-32	0-31	0-31	0-31-0-31
	AFT	0-57	2-135	0-5	95-0	0-4	96-0	0-4	96-0	0-4	96-0	0-45-0-45
1026-2	FWD	0-72	8-84	0-0	0-100	1-5	94-0	0-5	95-0	0-5	95-0	0-45-0-45
	AFT	0-57	1-13	78-0	0-100	1-5	93-0	0-5	94-0	0-5	94-0	0-45-0-45
1027-1	FWD	3-63	2-6	110-0	0-0	0-100	0-100	0-100	0-100	0-100	0-100	0-100-0-100
	AFT	2-63	2-6	108-0	0-0	0-100	0-100	0-100	0-100	0-100	0-100	0-100-0-100
1028-1	FWD	3-73	1-15	135-0	0-4	96-0	0-4	96-0	0-4	96-0	0-4	96-0-96-0
	AFT	2-73	1-14	133-0	0-5	95-0	0-5	95-0	0-5	95-0	0-5	95-0-95-0
1028-2	FWD	2-61	5-48	0-100	97-0	1-9	90-0	1-9	90-0	1-9	90-0	1-90-1-90
	AFT	-80	5	43-0	10-90	0-6	94-0	0-6	94-0	0-6	94-0	0-94-0-94
1029-1	FWD	3-63	1-18	130-0	0-8	92-0	1-16	83-0	1-14	86-0	1-14	86-0-86-0
	AFT	4-63	2-22	129-0	0-53	47-0	0-46	54-0	0-52	57-0	0-54	57-0-57-0
1029-2	FWD	3-62	1-16	128-0	0-20	80-0	0-21	79-0	0-25	75-0	0-25	75-0-75-0
	AFT	2-78	7-157	-1	23-76	0-28	72-0	0-30	70-0	0-34	94-0	0-82-0-82-0
1030-1	FWD	5-63	2-7	130-0	0-58	42-0	3-32	65-0	-5	57-0	0-57	57-0-57-0
	AFT	1-70	18-140	0-140	0-14	46-0	0-46	54-0	0-52	57-0	0-54	57-0-57-0
1031-1	FWD	1-70	18-140	0-140	0-14	46-0	0-46	54-0	0-52	57-0	0-54	57-0-57-0
	AFT	1-70	18-140	0-140	0-14	46-0	0-46	54-0	0-52	57-0	0-54	57-0-57-0
1031-2	FWD	1-70	18-140	0-140	0-14	46-0	0-46	54-0	0-52	57-0	0-54	57-0-57-0
	AFT	1-70	18-140	0-140	0-14	46-0	0-46	54-0	0-52	57-0	0-54	57-0-57-0
1033-1	FWD	1-70	4-16	155-0	0-89	11-0	3-97	0-97	0-98	0-28	35-0	30-0-30-0
	AFT	1-70	4-15	135-0	0-100	90-0	3-88	0-90	0-90	0-28	35-0	30-0-30-0
1033-2	FWD	0-54	3-34	131-0	0-84	16-1	4-95	0-95	0-95	0-28	35-0	30-0-30-0
	AFT	0-54	3-34	131-0	0-86	14-0	5-95	0-95	0-95	0-28	35-0	30-0-30-0

EXPOSURE - PROCESSING SUMMARY

MISSION NUMBER	CAMERA	SOLAR ELEVATION RANGE (°)	AZIMUTH RANGE (°)	PROTECTED PROCESSING (%)	OPENING (%)	COMPUTED			TERRAIN P. MIN			TERRAIN P. MAX			CLIMATE			CLOUD COVER (%)						
						LOW	HIGH	F	B	I	F	B	I	LOW	HIGH	MEAN	LOW	HIGH	MEAN					
1034-1	FWD	23	77	16	65	0	96	4	1	21	76	0	20	80	0.57	0.55	2.42	1.58	1.61	0.88	2.22	2.26	2.26	
	AFT	25	77	10	65	0	55	45	2	34	67	0	16	84	0.29	1.63	0.41	2.35	1.55	1.60	0.97	2.44	2.19	2.25
1034-2	FWD	29	86	0	178	0	86	12	9	26	65	0	27	73	0.19	1.52	0.52	2.40	1.63	1.60	1.21	2.47	2.25	2.31
	AFT	30	86	0	178	0	86	12	0	34	57	0	34	66	0.26	1.60	0.54	2.48	1.59	1.62	1.08	2.48	2.22	2.29

~~TOP SECRET C~~

NO.

SECTION A

APPENDIX

~~TOP SECRET C~~

+ PRE-SEAL

- CONTROL NO. [REDACTED]

MISSION # 1034-1 * INSTRUMENT # FRWD * 8/25/66 - DENSITY FREQ-DISTR

DENSITY VALUE	PRIMARY MIN MAX LIM	INTERMEDIATE MIN MAX LIM	FULL MIN MAX LIM		ALL LEVELS MIN MAX LIM	
			FULL MIN	FULL MAX	ALL LEVELS MIN	ALL LEVELS MAX
0.01	0.01	0.01	0.01	0.01	0.01	0.01
0.02	0.02	0.02	0.02	0.02	0.02	0.02
0.03	0.03	0.03	0.03	0.03	0.03	0.03
0.04	0.04	0.04	0.04	0.04	0.04	0.04
0.05	0.05	0.05	0.05	0.05	0.05	0.05
0.06	0.06	0.06	0.06	0.06	0.06	0.06
0.07	0.07	0.07	0.07	0.07	0.07	0.07
0.08	0.08	0.08	0.08	0.08	0.08	0.08
0.09	0.09	0.09	0.09	0.09	0.09	0.09
0.10	0.10	0.10	0.10	0.10	0.10	0.10
0.11	0.11	0.11	0.11	0.11	0.11	0.11
0.12	0.12	0.12	0.12	0.12	0.12	0.12
0.13	0.13	0.13	0.13	0.13	0.13	0.13
0.14	0.14	0.14	0.14	0.14	0.14	0.14
0.15	0.15	0.15	0.15	0.15	0.15	0.15
0.16	0.16	0.16	0.16	0.16	0.16	0.16
0.17	0.17	0.17	0.17	0.17	0.17	0.17
0.18	0.18	0.18	0.18	0.18	0.18	0.18
0.19	0.19	0.19	0.19	0.19	0.19	0.19
0.20	0.20	0.20	0.20	0.20	0.20	0.20
0.21	0.21	0.21	0.21	0.21	0.21	0.21
0.22	0.22	0.22	0.22	0.22	0.22	0.22
0.23	0.23	0.23	0.23	0.23	0.23	0.23
0.24	0.24	0.24	0.24	0.24	0.24	0.24
0.25	0.25	0.25	0.25	0.25	0.25	0.25
0.26	0.26	0.26	0.26	0.26	0.26	0.26
0.27	0.27	0.27	0.27	0.27	0.27	0.27
0.28	0.28	0.28	0.28	0.28	0.28	0.28
0.29	0.29	0.29	0.29	0.29	0.29	0.29
0.30	0.30	0.30	0.30	0.30	0.30	0.30
0.31	0.31	0.31	0.31	0.31	0.31	0.31
0.32	0.32	0.32	0.32	0.32	0.32	0.32
0.33	0.33	0.33	0.33	0.33	0.33	0.33
0.34	0.34	0.34	0.34	0.34	0.34	0.34
0.35	0.35	0.35	0.35	0.35	0.35	0.35
0.36	0.36	0.36	0.36	0.36	0.36	0.36
0.37	0.37	0.37	0.37	0.37	0.37	0.37
0.38	0.38	0.38	0.38	0.38	0.38	0.38
0.39	0.39	0.39	0.39	0.39	0.39	0.39
0.40	0.40	0.40	0.40	0.40	0.40	0.40
0.41	0.41	0.41	0.41	0.41	0.41	0.41
0.42	0.42	0.42	0.42	0.42	0.42	0.42
0.43	0.43	0.43	0.43	0.43	0.43	0.43
0.44	0.44	0.44	0.44	0.44	0.44	0.44
0.45	0.45	0.45	0.45	0.45	0.45	0.45
0.46	0.46	0.46	0.46	0.46	0.46	0.46
0.47	0.47	0.47	0.47	0.47	0.47	0.47
0.48	0.48	0.48	0.48	0.48	0.48	0.48
0.49	0.49	0.49	0.49	0.49	0.49	0.49
0.50	0.50	0.50	0.50	0.50	0.50	0.50
0.51	0.51	0.51	0.51	0.51	0.51	0.51
0.52	0.52	0.52	0.52	0.52	0.52	0.52
0.53	0.53	0.53	0.53	0.53	0.53	0.53
0.54	0.54	0.54	0.54	0.54	0.54	0.54
0.55	0.55	0.55	0.55	0.55	0.55	0.55
0.56	0.56	0.56	0.56	0.56	0.56	0.56
0.57	0.57	0.57	0.57	0.57	0.57	0.57
0.58	0.58	0.58	0.58	0.58	0.58	0.58
0.59	0.59	0.59	0.59	0.59	0.59	0.59
0.60	0.60	0.60	0.60	0.60	0.60	0.60
0.61	0.61	0.61	0.61	0.61	0.61	0.61
0.62	0.62	0.62	0.62	0.62	0.62	0.62
0.63	0.63	0.63	0.63	0.63	0.63	0.63
0.64	0.64	0.64	0.64	0.64	0.64	0.64
0.65	0.65	0.65	0.65	0.65	0.65	0.65
0.66	0.66	0.66	0.66	0.66	0.66	0.66
0.67	0.67	0.67	0.67	0.67	0.67	0.67
0.68	0.68	0.68	0.68	0.68	0.68	0.68
0.69	0.69	0.69	0.69	0.69	0.69	0.69
0.70	0.70	0.70	0.70	0.70	0.70	0.70
0.71	0.71	0.71	0.71	0.71	0.71	0.71
0.72	0.72	0.72	0.72	0.72	0.72	0.72
0.73	0.73	0.73	0.73	0.73	0.73	0.73
0.74	0.74	0.74	0.74	0.74	0.74	0.74
0.75	0.75	0.75	0.75	0.75	0.75	0.75
0.76	0.76	0.76	0.76	0.76	0.76	0.76
0.77	0.77	0.77	0.77	0.77	0.77	0.77
0.78	0.78	0.78	0.78	0.78	0.78	0.78
0.79	0.79	0.79	0.79	0.79	0.79	0.79
0.80	0.80	0.80	0.80	0.80	0.80	0.80
0.81	0.81	0.81	0.81	0.81	0.81	0.81
0.82	0.82	0.82	0.82	0.82	0.82	0.82
0.83	0.83	0.83	0.83	0.83	0.83	0.83
0.84	0.84	0.84	0.84	0.84	0.84	0.84
0.85	0.85	0.85	0.85	0.85	0.85	0.85
0.86	0.86	0.86	0.86	0.86	0.86	0.86
0.87	0.87	0.87	0.87	0.87	0.87	0.87
0.88	0.88	0.88	0.88	0.88	0.88	0.88
0.89	0.89	0.89	0.89	0.89	0.89	0.89
0.90	0.90	0.90	0.90	0.90	0.90	0.90
0.91	0.91	0.91	0.91	0.91	0.91	0.91
0.92	0.92	0.92	0.92	0.92	0.92	0.92
0.93	0.93	0.93	0.93	0.93	0.93	0.93
0.94	0.94	0.94	0.94	0.94	0.94	0.94
0.95	0.95	0.95	0.95	0.95	0.95	0.95
0.96	0.96	0.96	0.96	0.96	0.96	0.96
0.97	0.97	0.97	0.97	0.97	0.97	0.97
0.98	0.98	0.98	0.98	0.98	0.98	0.98
0.99	0.99	0.99	0.99	0.99	0.99	0.99
1.00	1.00	1.00	1.00	1.00	1.00	1.00

+ PRE-SEAL

- CONTROL NO. [REDACTED]

SIGHT AT

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- CONTROL NO.

MISSION # 1034-1 * INSTRUMENT # FRWD

8/25/66 DENSITY FREQ DISTR

DENSITY VALUE	PRIMARY MIN MAX LIM	INTERMEDIATE MIN MAX LIM	FULL MIN MAX LIM	ALL LEVELS MIN MAX LIM
------------------	------------------------	-----------------------------	---------------------	---------------------------

- CONTROL NO.

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CONTACT NO.

MISSING * 1034-1 * INSTRUMENT * FRWD

8/25/66 DENSITY FREQ DISTR

DEENSITY	PRIMARY	INTERMEDIATE	FULL	ALL LEVELS
VALVE	MIN MAX LIM	MIN MAX LIM	MIN MAX LIM	MIN MAX LIM

- CITA 1801 NO.

Table 3-1

HYPERTEXT

- CONTROL NO.

MISSION # 1014-1 * INSTRUMENT # FWD 8/25/66 DENSITY FREQ DISTR

DENSITY NAME	PRIMARY MIN MAX LIM	INTERMEDIATE MIN MAX LIM	FULL MIN MAX LIM	ALL LEVELS MIN MAX LIM
-----------------	------------------------	-----------------------------	---------------------	---------------------------

- CONTROL NO.

Table 1 (continued)

~~TOP SECRET~~

- CONTROL NO. [REDACTED]

MISSION # 1034-1 INSTRUMENT # FRWD

8/25/66 DENSITY FREQ DISTR

DENSITY VALUE	PRIMARY		INTERMEDIATE		FULL	ALL LEVELS	
	MIN	MAX LIM	MIN	MAX LIM	MIN MAX LIM	MIN	MAX LIM
2.01					0	0	0
2.02					0	0	0
2.03					0	0	0
2.04					0	0	0
2.05					0	0	0
2.06					0	0	0
2.07					0	0	0
2.08					0	0	0
2.09					0	0	0
2.10					0	0	0
2.11					0	0	0
2.12					0	0	0
2.13					0	0	0
2.14					0	0	0
2.15					0	0	0
2.16					0	0	0
2.17					0	0	0
2.18					0	0	0
2.19					0	0	0
2.20					0	0	0
2.21					0	0	0
2.22					0	0	0
2.23					0	0	0
2.24					0	0	0
2.25					0	0	0
2.26					0	0	0
2.27					0	0	0
2.28					0	0	0
2.29					0	0	0
2.30					0	0	0
2.31					0	0	0
2.32					0	0	0
2.33					0	0	0
2.34					0	0	0
2.35					0	0	0
2.36					0	0	0
2.37					0	0	0
2.38					0	0	0
2.39					0	0	0
2.40					0	0	0
2.41					0	0	0
2.42					0	0	0
2.43					0	0	0
2.44					0	0	0
2.45					0	0	0
2.46					0	0	0
2.47					0	0	0
2.48					0	0	0
2.49					0	0	0
2.50					0	0	0
2.51					0	0	0
2.52					0	0	0
2.53					0	0	0
2.54					0	0	0
2.55					0	0	0
2.56					0	0	0
2.57					0	0	0
2.58					0	0	0
2.59					0	0	0
2.60					0	0	0
2.61					0	0	0
2.62					0	0	0
2.63					0	0	0
2.64					0	0	0
2.65					0	0	0
2.66					0	0	0
2.67					0	0	0
2.68					0	0	0
2.69					0	0	0
2.70					0	0	0
2.71					0	0	0
2.72					0	0	0
2.73					0	0	0
2.74					0	0	0
2.75					0	0	0
2.76					0	0	0
2.77					0	0	0
2.78					0	0	0
2.79					0	0	0
2.80					0	0	0
2.81					0	0	0
2.82					0	0	0
2.83					0	0	0
2.84					0	0	0
2.85					0	0	0
2.86					0	0	0
2.87					0	0	0
2.88					0	0	0
2.89					0	0	0
2.90					0	0	0
2.91					0	0	0
2.92					0	0	0
2.93					0	0	0
2.94					0	0	0
2.95					0	0	0
2.96					0	0	0
2.97					0	0	0
2.98					0	0	0
2.99					0	0	0
2.00					0	0	0
2.01					0	0	0
2.02					0	0	0
2.03					0	0	0
2.04					0	0	0
2.05					0	0	0
2.06					0	0	0
2.07					0	0	0
2.08					0	0	0
2.09					0	0	0
2.10					0	0	0
2.11					0	0	0
2.12					0	0	0
2.13					0	0	0
2.14					0	0	0
2.15					0	0	0
2.16					0	0	0
2.17					0	0	0
2.18					0	0	0
2.19					0	0	0
2.20					0	0	0
2.21					0	0	0
2.22					0	0	0
2.23					0	0	0
2.24					0	0	0
2.25					0	0	0
2.26					0	0	0
2.27					0	0	0
2.28					0	0	0
2.29					0	0	0
2.30					0	0	0
2.31					0	0	0
2.32					0	0	0
2.33					0	0	0
2.34					0	0	0
2.35					0	0	0
2.36					0	0	0
2.37					0	0	0
2.38					0	0	0
2.39					0	0	0
2.40					0	0	0
2.41					0	0	0
2.42					0	0	0
2.43					0	0	0
2.44					0	0	0
2.45					0	0	0
2.46					0	0	0
2.47					0	0	0
2.48					0	0	0
2.49					0	0	0
2.50					0	0	0
2.51					0	0	0
2.52					0	0	0
2.53					0	0	0
2.54					0	0	0
2.55					0	0	0
2.56					0	0	0
2.57					0	0	0
2.58					0	0	0
2.59					0	0	0
2.60					0	0	0
2.61					0	0	0
2.62					0	0	0
2.63					0	0	0
2.64					0	0	0
2.65					0	0	0
2.66					0	0	0
2.67					0	0	0
2.68					0	0	0
2.69					0	0	0
2.70					0	0	0
2.71					0	0	0
2.72					0	0	0
2.73					0	0	0
2.74					0	0	0
2.75					0	0	0
2.76					0	0	0
2.77					0	0	0
2.78					0	0	0
2.79					0	0	0
2.80					0	0	0
2.81					0	0	0
2.82					0	0	0
2.83					0	0	0
2.84					0	0	0
2.85					0	0	0
2.86					0	0	0
2.87					0	0	0
2.88					0	0	0
2.89					0	0	0
2.90					0	0	0
2.91					0	0	0
2.92					0	0	0
2.93					0	0	0
2.94					0	0	0
2.95					0	0	0
2.96					0	0	0
2.97					0	0	0
2.98					0	0	0
2.99					0	0	0
2.00					0	0	0
2.01					0	0	0
2.02					0	0	0
2.03					0	0	0
2.04					0	0	0
2.05					0	0	0
2.06					0	0	0
2.07					0	0	0
2.08					0	0	0
2.09					0	0	0
2.10					0	0	0
2.11					0	0	0
2.12					0	0	0
2.13					0	0	0
2.14					0	0	0
2.15					0	0	0
2.16					0	0	0
2.17					0	0	0
2.18					0	0	0
2.19					0	0	0
2.20					0	0	0
2.21					0	0	0
2.22					0	0	0
2.23					0	0	0
2.24					0	0	0
2.25					0	0	0
2.26					0	0	0
2.27					0	0	0
2.28					0	0	0
2.29					0	0	0
2.30					0	0	0
2.31					0	0	0
2.32					0	0	0
2.33					0	0	0
2.34					0	0	0
2.35					0	0	0
2.36					0	0</	

~~TOP SECRET~~

- CONTROL NO.

MISSION # 1034-1 * INSTRUMENT # FRWD 8/25/66 DENSITY FREQ DISTR

DENSITY VALUE	PRIMARY MIN MAX LIM	INTERMEDIATE MIN MAX LIM	FULL MIN MAX LIM	ALL LEVELS MIN MAX LIM
2.51	0 0	0 0	0 0	0 0
2.52	0 0	0 0	0 0	0 0
2.53	0 0	0 0	0 0	0 0
2.54	0 0	0 0	0 0	0 0
2.55	0 0	0 0	0 0	0 0
2.56	0 0	0 0	0 0	0 0
2.57	0 0	0 0	0 0	0 0
2.58	0 0	0 0	0 0	0 0
2.59	0 0	0 0	0 0	0 0
2.60	0 0	0 0	0 0	0 0
2.61	0 0	0 0	0 0	0 0
2.62	0 0	0 0	0 0	0 0
2.63	0 0	0 0	0 0	0 0
2.64	0 0	0 0	0 0	0 0
2.65	0 0	0 0	0 0	0 0
2.66	0 0	0 0	0 0	0 0
2.67	0 0	0 0	0 0	0 0
2.68	0 0	0 0	0 0	0 0
2.69	0 0	0 0	0 0	0 0
2.70	0 0	0 0	0 0	0 0
SUBTOTAL	0 0	0 0	0 0	0 0
TOTAL	0 0	50 47	203 203	253 253 250

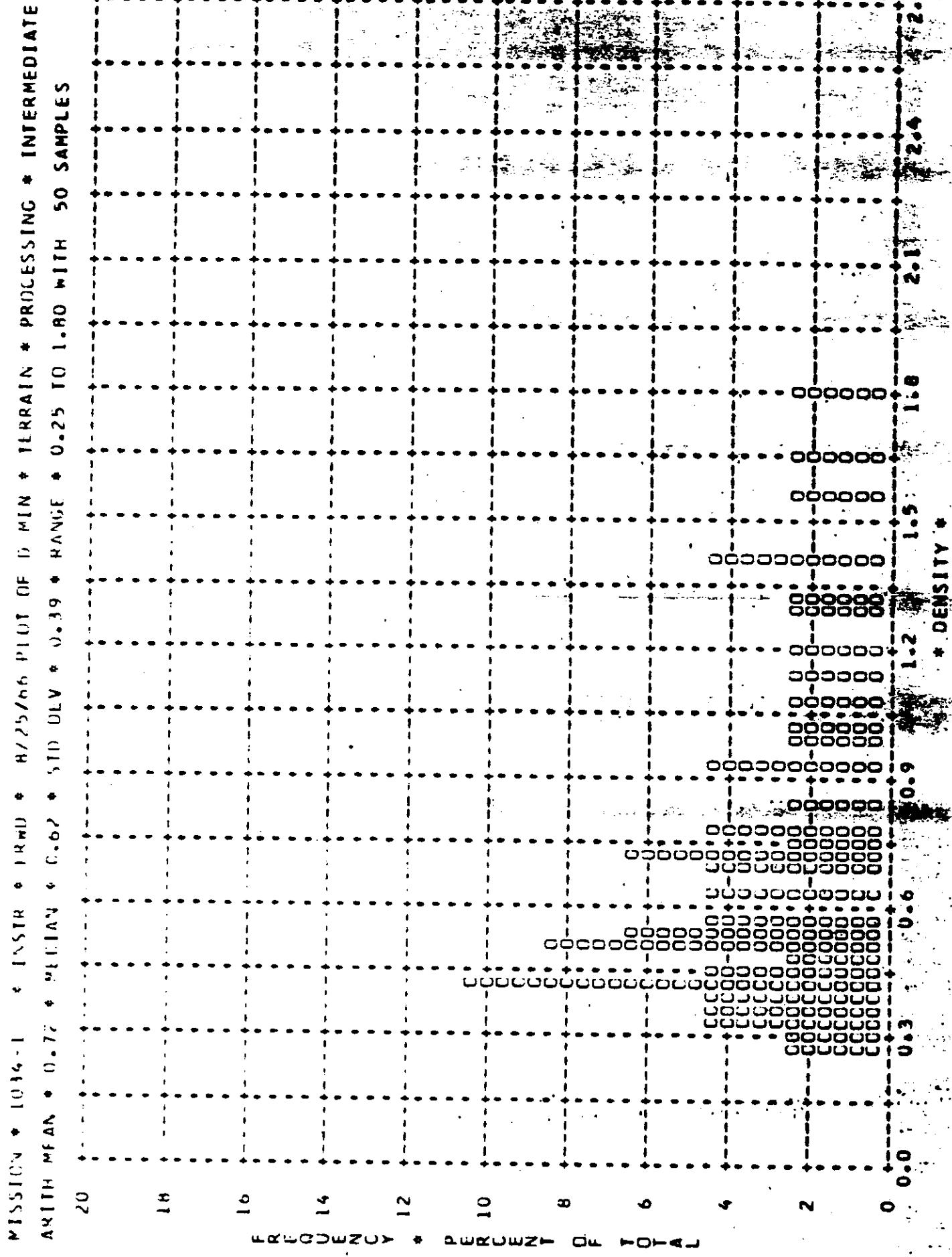
MISSION 1034-1 INSTR - FRWD 8/25/66 PROCESSING AND EXPOSURE ANAL

PROCESS LEVEL	SAMPLE SIZE	UNDER EXPPOSED	UNDER PROCESSED	CORRECT EXP+PROC	OVER PROCESSED	OVE EXPPOSED
PRIMARY	0	0 PC	0 PC	0 PC	0 PC	0 PC
INTERMEDIATE	50	0 PC	16 PC	56 PC	18 PC	10 PC
FULL	203	23 PC	0 PC	73 PC	4 PC	0 PC
ALL LEVELS	253	18 PC	3 PC	70 PC	7 PC	2 PC
PROCESS LEVEL	BASE + FCG	UNDER EXPPOSED	UNDER PROCESSED	CORRECT EXP+PROC	OVER PROCESSED	OVE EXPPOSED
PRIMARY	0.01-0.09	0.01-0.13	0.14-0.39	0.40-0.90	-----	0.91 AND
INTERMED	0.10-0.17	0.01-0.20	0.21-0.39	0.40-0.90	0.91-1.34	1.35 AND
FULL	0.18 AND UP	0.01-0.39	-----	0.40-0.90	0.91-1.69	1.70 AND

~~TOP SECRET~~

- CONTROL NO.

Table A-1



TRIP SUMMARY

- CONVIRI NO.

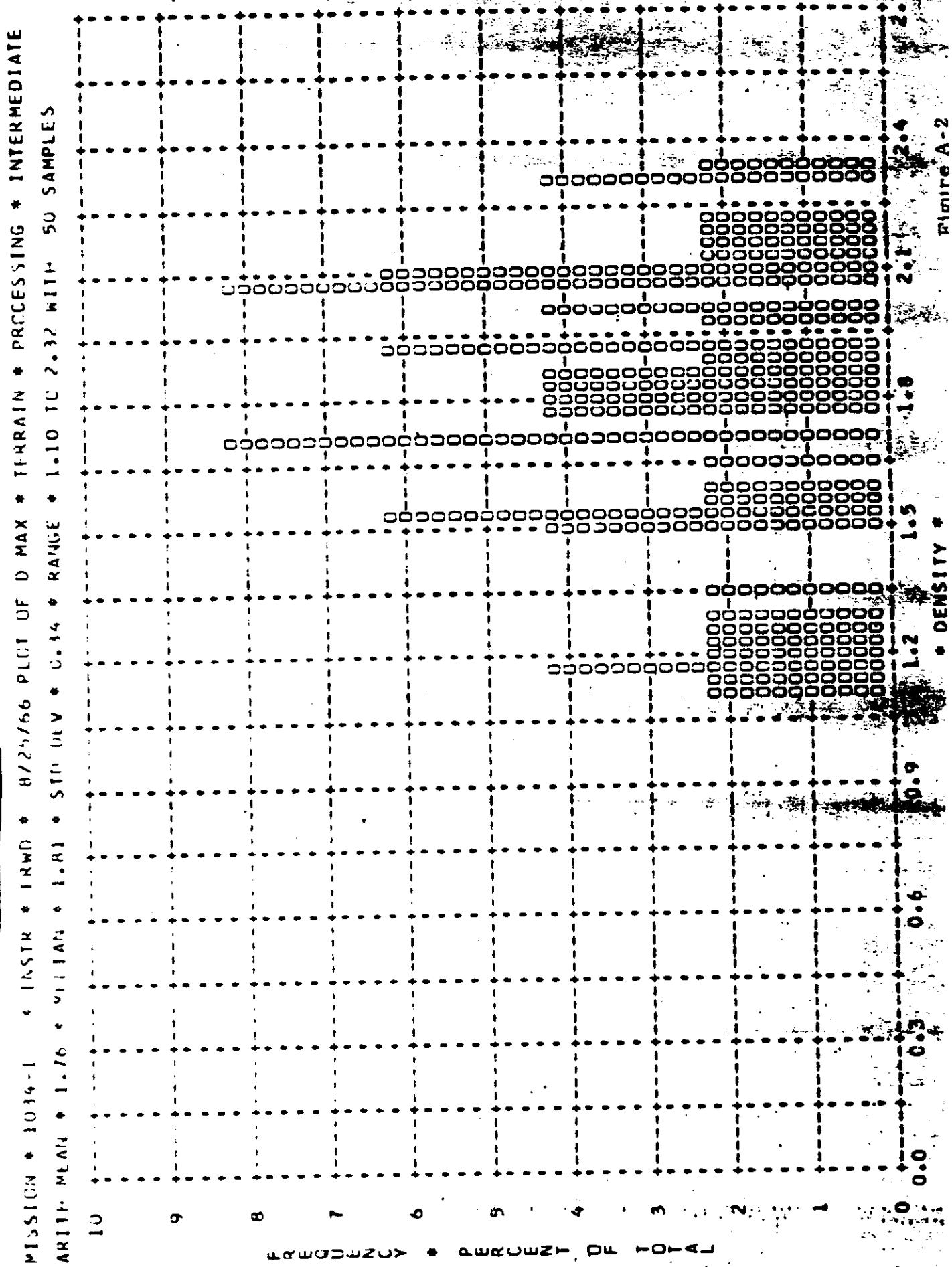
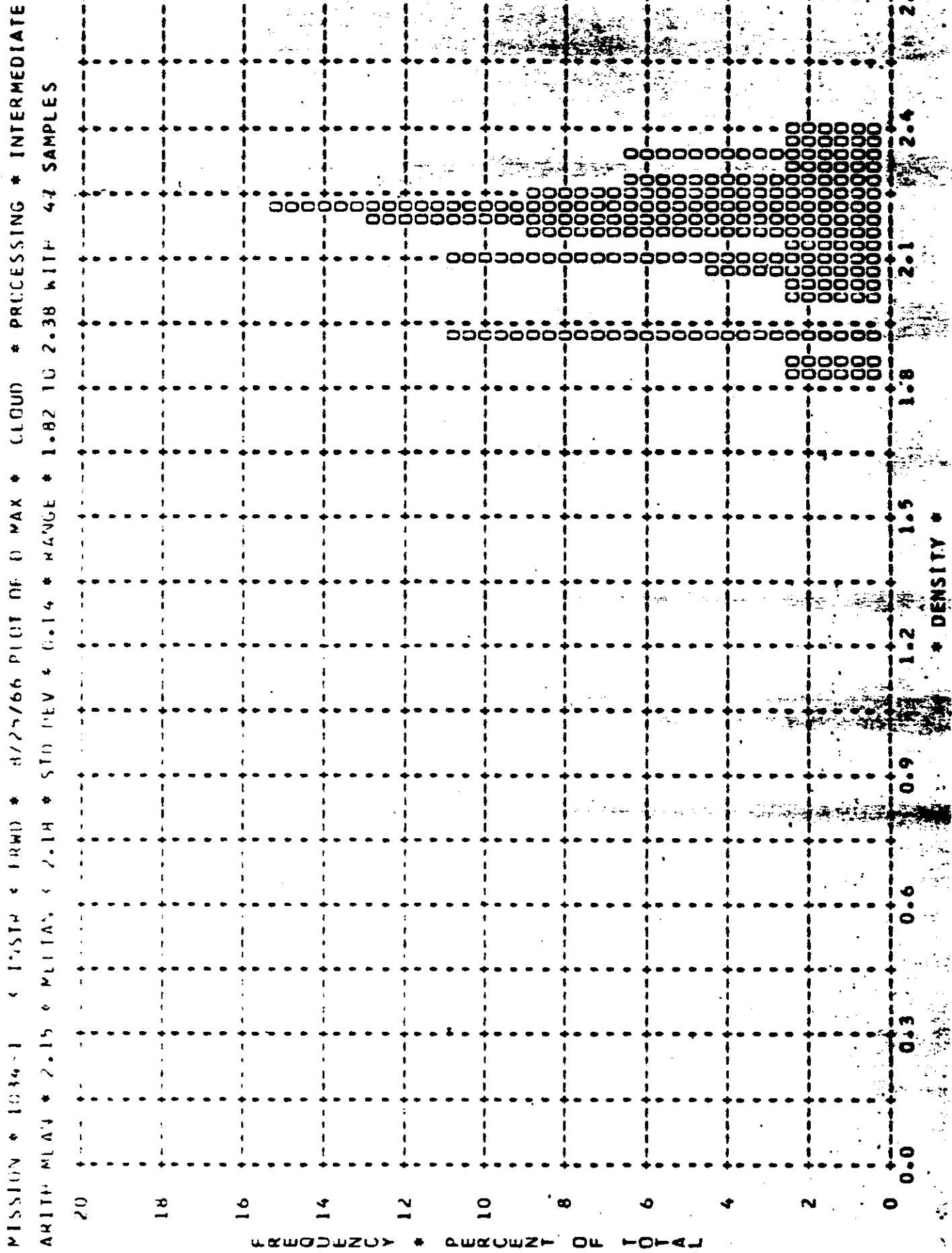


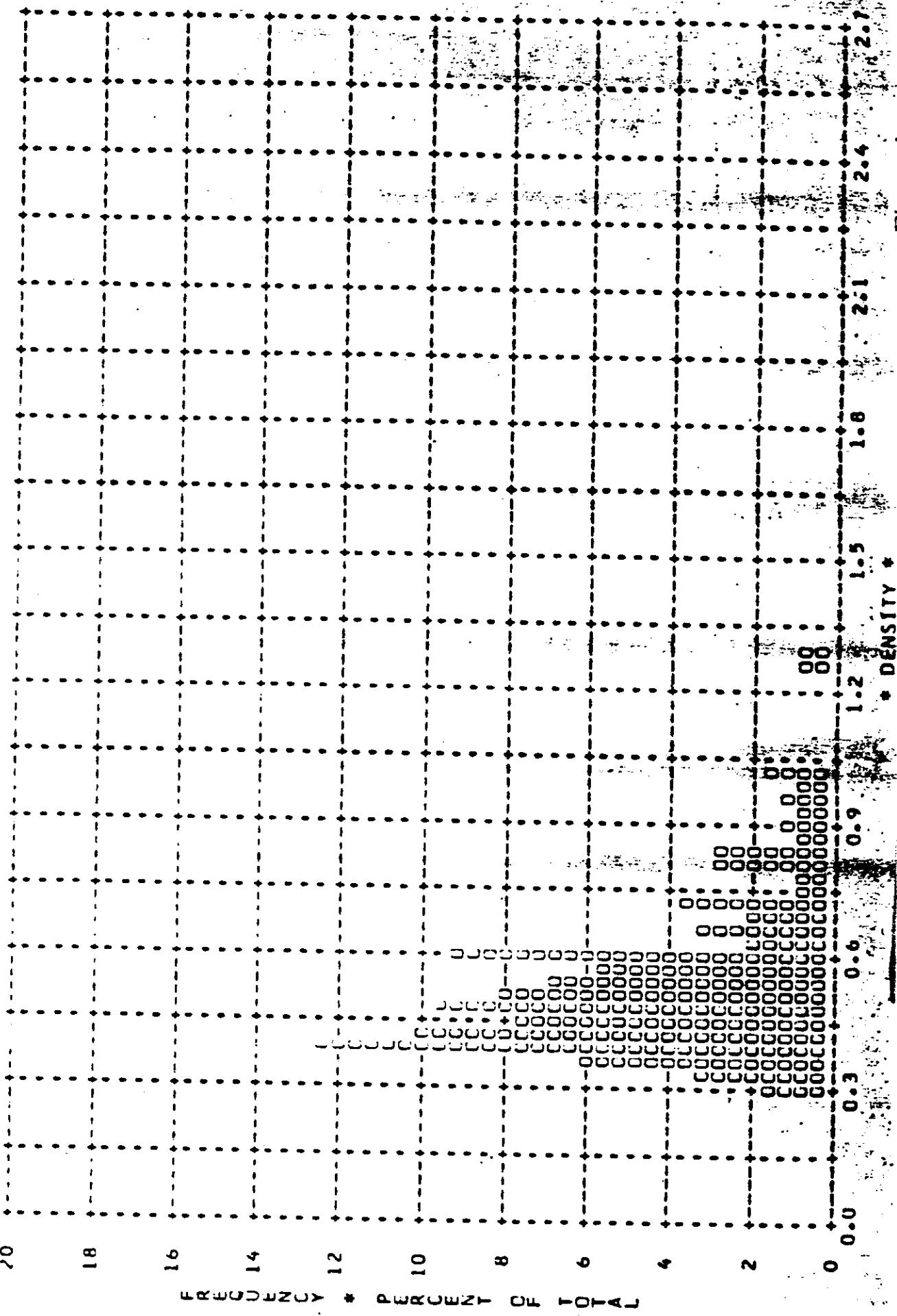
Figure A-2

- CONTROL NO.



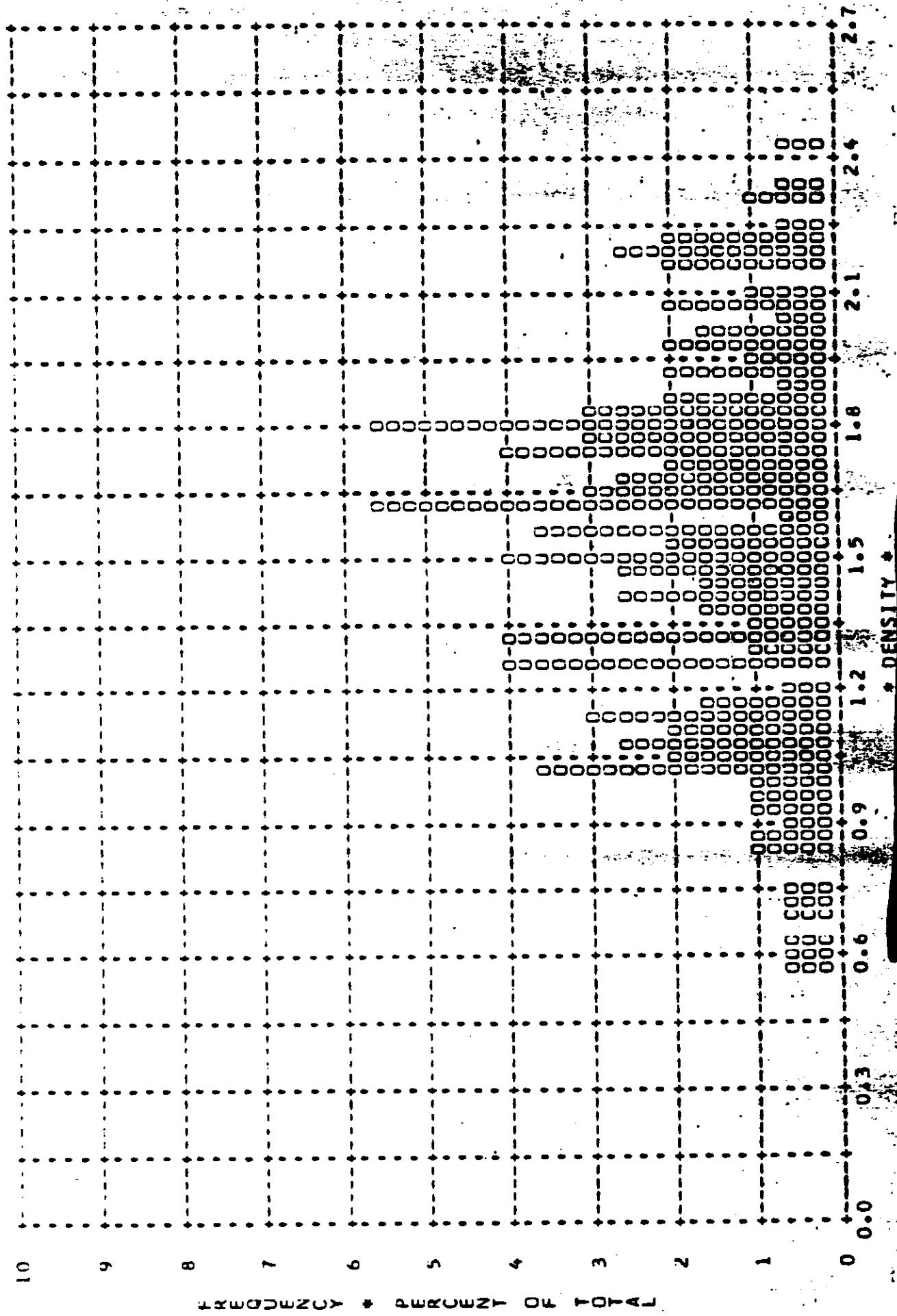
MISSION * 1034-1 * INSTR * IRAD * 8/25/66 PLOT OF D MIN * TERRAIN * PROCESSING * FULL
ARITH MEAN * 0.53 * MEDIAN * 0.49 * STD DEV * 0.17 * RANGE * 0.29 TO 1.28 WITH 203 SAMPLES

LINE SECT # - CONTROL NO. [REDACTED]



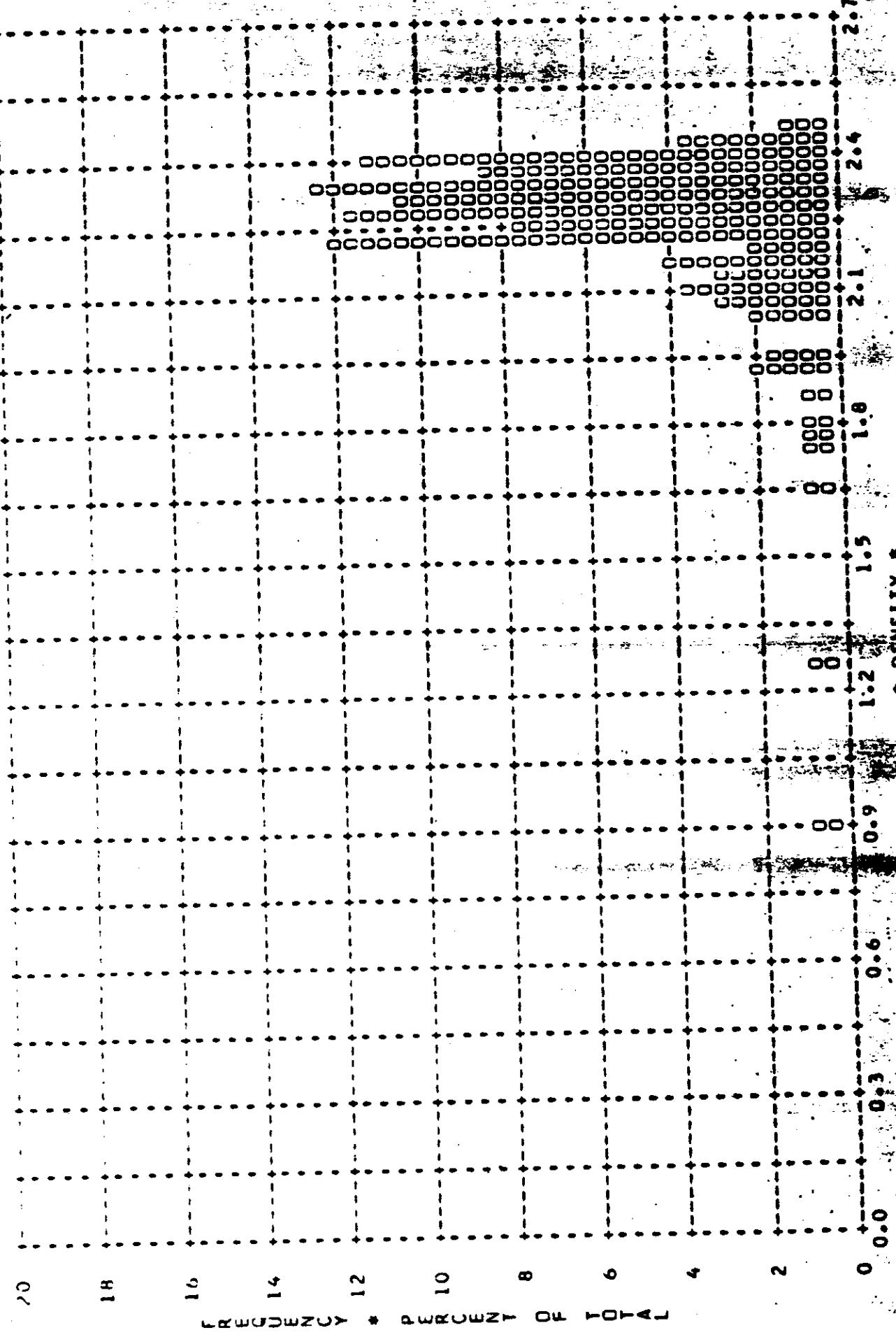
- CONTROL NO. [REDACTED]

MISSION # 1034-1 * PLSR + PRWU * H/15/66 PLOT UF D MAX * TERRAIN * PROCESSING * FULL
ARITH MEAN = 1.74 * MEDIAN = 1.56 * STD DLV = 0.46 * RANGE = 0.55 TO 2.42 WITH 203 SAMPLES



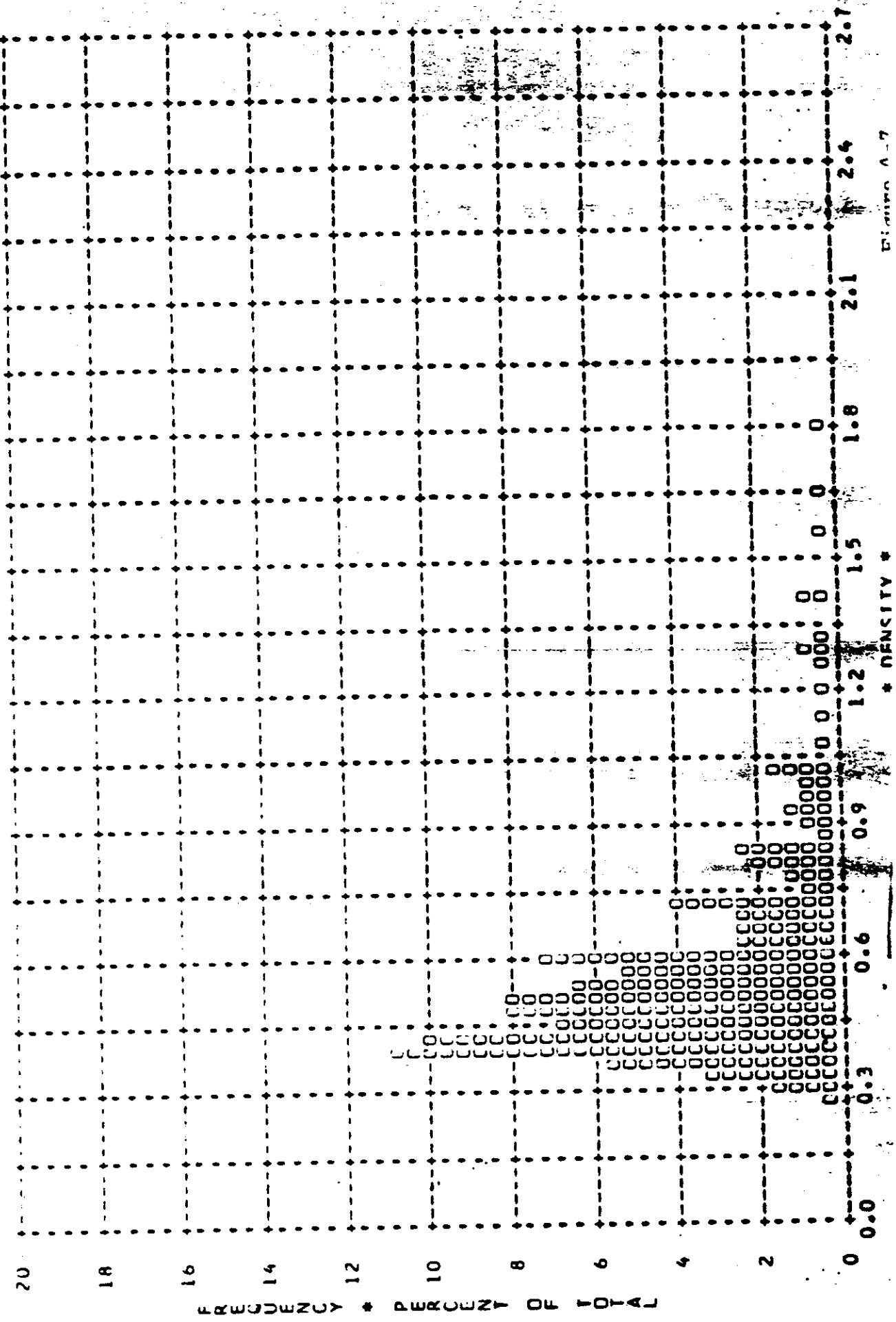
- CONTROL NO.

MISSION # 1916.1 * LISTER & THOM * H/25/66 PLOT OF MAX * CLOUD * PROCESSING * FULL
ARITH MEAN = 2.024 * STDEV = 0.224 * SDEV = 0.18 * RANG = 0.08 TO 2.45 WITH 203 SAMPLES



CONTINUOUS

MISSION # 1016-1 * 1.5TH * FWD & RWD * PILOT OF 0 MIN * TERRAIN * PROCESSING * ALL LEVELS
 ARITH MEAN # 0.57 * MEAN # 0.50 * STD DEV # 0.24 * RANGE # 0.25 TO 1.00 WITH 253 SAMPLES



CONTROL NO. [REDACTED]

MISSION # 10341 * L1STR + IRWD * R/23/66 PLOT OF D MAX * TERRAIN * PROCESSING * ALL LEVELS
AWLTH VENY + 1.48 * MILLAR, C 1.61 * S1D DIV * C.4C * RANGE * 0.55 TC 2.42 WITH 253 SAMPLES

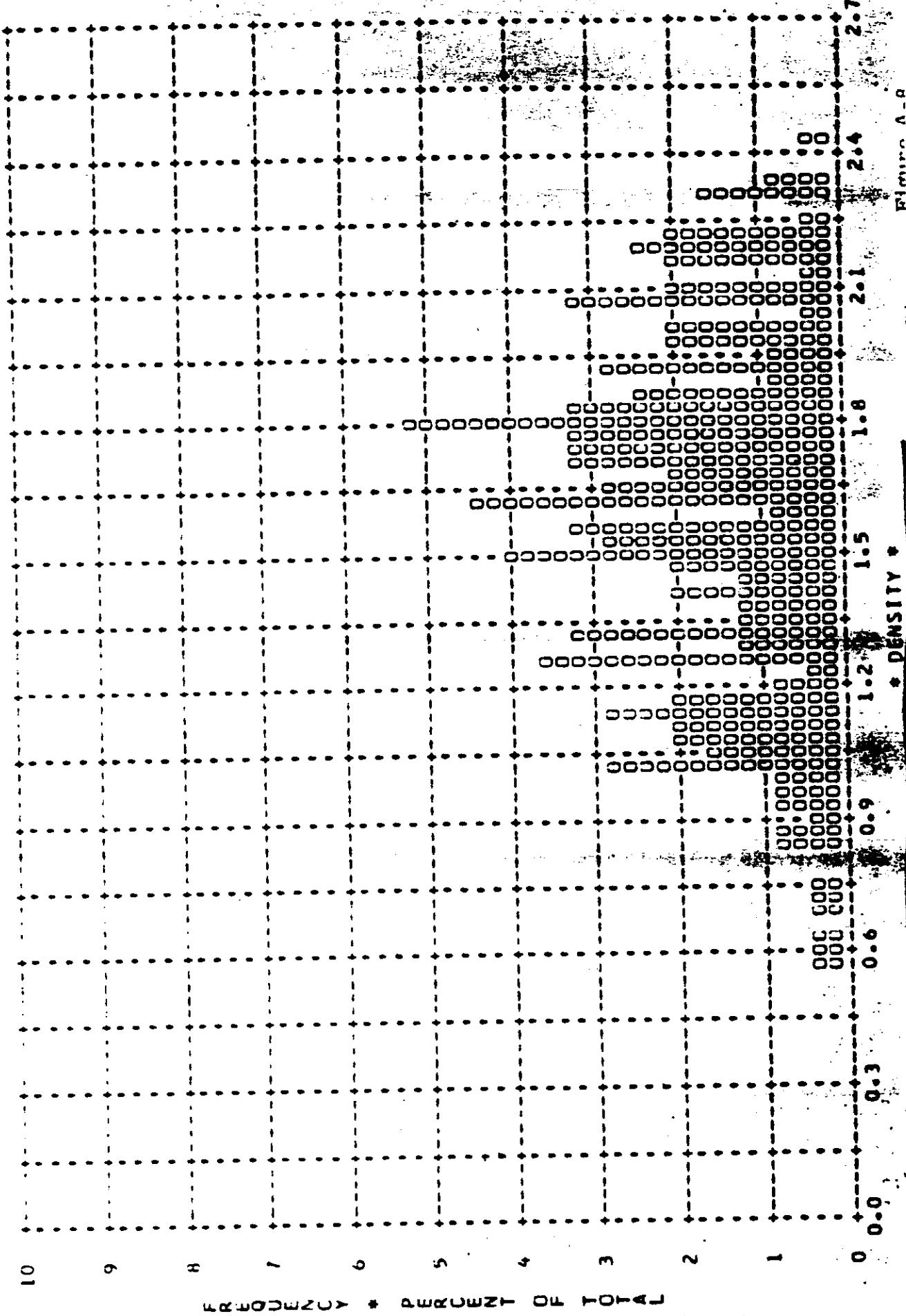


Figure A-14

- CONTROL NO. [REDACTED]

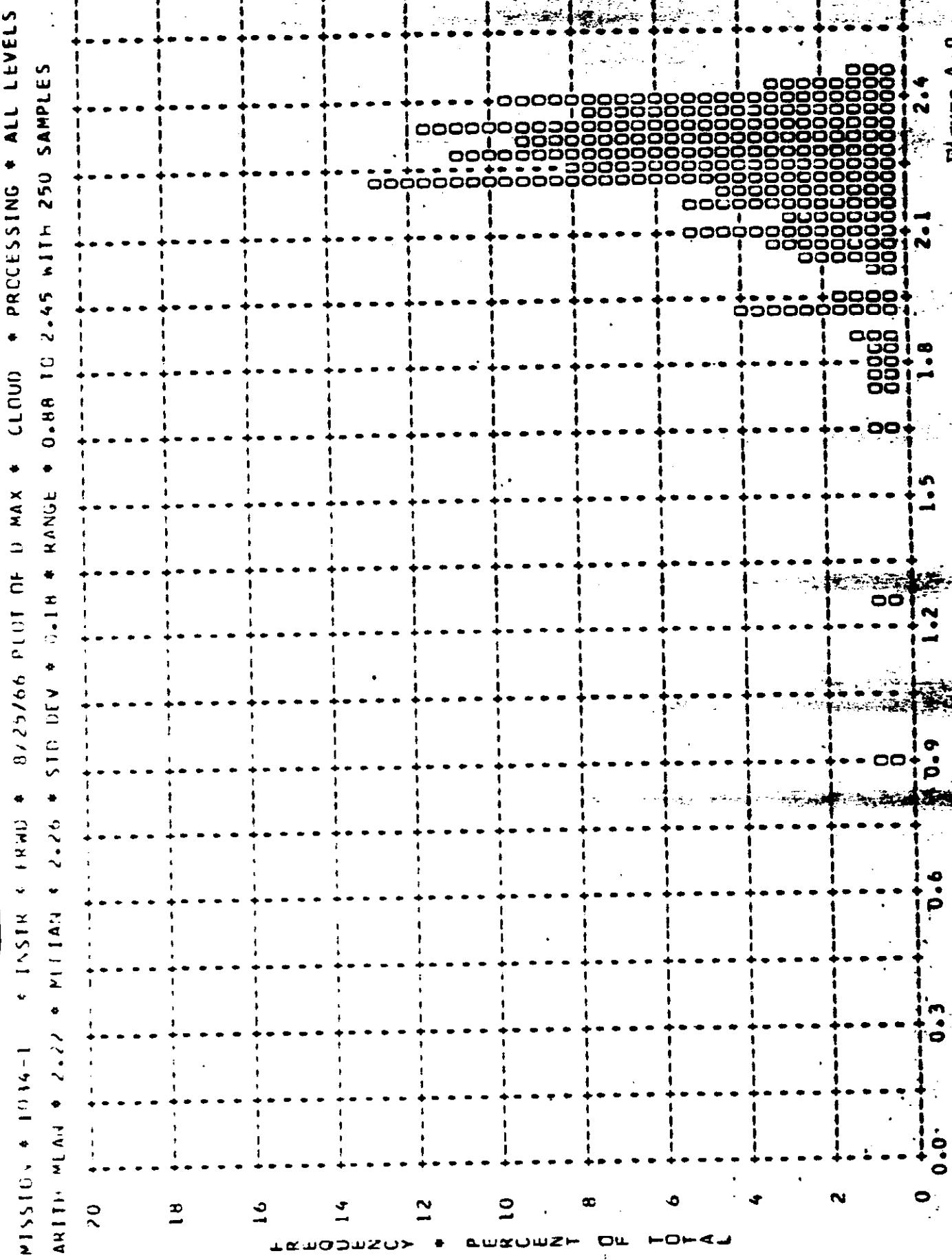


Figure A-8

~~TOP SECRET~~

- CONTROL NO.

MISSION * 1034-1 * INSTRUMENT * AFT

8/25/66 DENSITY FREQ DISTR

DENSITY VALUE	PRIMARY MIN MAX LIM	INTERMEDIATE MIN MAX LIM	FULL MIN MAX LIM	ALL LEVELS MIN MAX LIM
0.01	C	C	0	0
0.02	CCCC	CCCC	00	00
0.03	CCCC	CCCC	00	00
0.04	CCCC	CCCC	00	00
0.05	CCCC	CCCC	00	00
0.06	CCCC	CCCC	00	00
0.07	CCCC	CCCC	00	00
0.08	CCCC	CCCC	00	00
0.09	CCCC	CCCC	00	00
0.10	CCCC	CCCC	00	00
0.11	CCCC	CCCC	00	00
0.12	CCCC	CCCC	00	00
0.13	CCCC	CCCC	00	00
0.14	CCCC	CCCC	00	00
0.15	CCCC	CCCC	00	00
0.16	CCCC	CCCC	00	00
0.17	CCCC	CCCC	00	00
0.18	CCCC	CCCC	00	00
0.19	CCCC	CCCC	00	00
0.20	CCCC	CCCC	00	00
0.21	CCCC	CCCC	00	00
0.22	CCCC	CCCC	00	00
0.23	CCCC	CCCC	00	00
0.24	CCCC	CCCC	00	00
0.25	CCCC	CCCC	00	00
0.26	CCCC	CCCC	00	00
0.27	CCCC	CCCC	00	00
0.28	CCCC	CCCC	00	00
0.29	CCCC	CCCC	00	00
0.30	CCCC	CCCC	00	00
0.31	CCCC	CCCC	00	00
0.32	CCCC	CCCC	00	00
0.33	CCCC	CCCC	00	00
0.34	CCCC	CCCC	00	00
0.35	CCCC	CCCC	00	00
0.36	CCCC	CCCC	00	00
0.37	CCCC	CCCC	00	00
0.38	CCCC	CCCC	00	00
0.39	CCCC	CCCC	00	00
0.40	CCCC	CCCC	00	00
0.41	CCCC	CCCC	00	00
0.42	CCCC	CCCC	00	00
0.43	CCCC	CCCC	00	00
0.44	CCCC	CCCC	00	00
0.45	CCCC	CCCC	00	00
0.46	CCCC	CCCC	00	00
0.47	CCCC	CCCC	00	00
0.48	CCCC	CCCC	00	00
0.49	CCCC	CCCC	00	00
0.50	CCCC	CCCC	00	00
SUBTOTAL	CCCC	CCCC	1909	117
				136

~~TOP SECRET~~

- CONTROL NO.

Table A-2

~~TOP SECRET~~

- CONTROL NO.

MISSION * 1034-1 * * INSTRUMENT * AFT

8/25/66 DENSITY-FREQ DISTR.

~~-TOP SECRET~~

- CONTROL NO.

Table A-2

~~-TOP SECRET-~~

CONTROL NO.

MISSION * 1034-1 * INSTRUMENT * AFT 8/25/66 DENSITY FREQ DISTR

DENSITY VALUE	PRIMARY MIN MAX LIM	INTERMEDIATE MIN MAX LIM	FULL MIN MAX LIM	ALL LEVELS MIN MAX LIM
1.01				0
1.02				0
1.03				0
1.04				0
1.05				0
1.06				0
1.07				0
1.08				0
1.09				0
1.10				0
1.11				0
1.12				0
1.13				0
1.14				0
1.15				0
1.16				0
1.17				0
1.18				0
1.19				0
1.20				0
1.21				0
1.22				0
1.23				0
1.24				0
1.25				0
1.26				0
1.27				0
1.28				0
1.29				0
1.30				0
1.31				0
1.32				0
1.33				0
1.34				0
1.35				0
1.36				0
1.37				0
1.38				0
1.39				0
1.40				0
1.41				0
1.42				0
1.43				0
1.44				0
1.45				0
1.46				0
1.47				0
1.48				0
1.49				0
1.50				0
SUBTOTAL				0

— 200 —

- CONTROL NO. 1

Table A-2

~~TOP SECRET~~

- CONTROL NO. [REDACTED]

MISSION * 1034-1 * INSTRUMENT * AFT 8/25/66 DENSITY FREQ DISTR

DENSITY VALUE	PRIMARY MIN MAX LIM	INTERMEDIATE MIN MAX LIM	FULL MIN MAX LIM	ALL LEVELS MIN MAX LIM
1.51	0 00000000	0 00000000	0 00000000	0 00000000
1.52	0 00000000	0 00000000	1 0140511161204062503232131110302231214240211100201	101506121840504620423213221040224141427022200201
1.53	0 00000000	0 00000000	0 00000000	0 00000000
1.54	0 00000000	0 00000000	0 00000000	0 00000000
1.55	0 00000000	0 00000000	0 00000000	0 00000000
1.56	0 00000000	0 00000000	0 00000000	0 00000000
1.57	0 00000000	0 00000000	0 00000000	0 00000000
1.58	0 00000000	0 00000000	0 00000000	0 00000000
1.59	0 00000000	0 00000000	0 00000000	0 00000000
1.60	0 00000000	0 00000000	0 00000000	0 00000000
1.61	0 00000000	0 00000000	0 00000000	0 00000000
1.62	0 00000000	0 00000000	0 00000000	0 00000000
1.63	0 00000000	0 00000000	0 00000000	0 00000000
1.64	0 00000000	0 00000000	0 00000000	0 00000000
1.65	0 00000000	0 00000000	0 00000000	0 00000000
1.66	0 00000000	0 00000000	0 00000000	0 00000000
1.67	0 00000000	0 00000000	0 00000000	0 00000000
1.68	0 00000000	0 00000000	0 00000000	0 00000000
1.69	0 00000000	0 00000000	0 00000000	0 00000000
1.70	0 00000000	0 00000000	0 00000000	0 00000000
1.71	0 00000000	0 00000000	0 00000000	0 00000000
1.72	0 00000000	0 00000000	0 00000000	0 00000000
1.73	0 00000000	0 00000000	0 00000000	0 00000000
1.74	0 00000000	0 00000000	0 00000000	0 00000000
1.75	0 00000000	0 00000000	0 00000000	0 00000000
1.76	0 00000000	0 00000000	0 00000000	0 00000000
1.77	0 00000000	0 00000000	0 00000000	0 00000000
1.78	0 00000000	0 00000000	0 00000000	0 00000000
1.79	0 00000000	0 00000000	0 00000000	0 00000000
1.80	0 00000000	0 00000000	0 00000000	0 00000000
1.81	0 00000000	0 00000000	0 00000000	0 00000000
1.82	0 00000000	0 00000000	0 00000000	0 00000000
1.83	0 00000000	0 00000000	0 00000000	0 00000000
1.84	0 00000000	0 00000000	0 00000000	0 00000000
1.85	0 00000000	0 00000000	0 00000000	0 00000000
1.86	0 00000000	0 00000000	0 00000000	0 00000000
1.87	0 00000000	0 00000000	0 00000000	0 00000000
1.88	0 00000000	0 00000000	0 00000000	0 00000000
1.89	0 00000000	0 00000000	0 00000000	0 00000000
1.90	0 00000000	0 00000000	0 00000000	0 00000000
1.91	0 00000000	0 00000000	0 00000000	0 00000000
1.92	0 00000000	0 00000000	0 00000000	0 00000000
1.93	0 00000000	0 00000000	0 00000000	0 00000000
1.94	0 00000000	0 00000000	0 00000000	0 00000000
1.95	0 00000000	0 00000000	0 00000000	0 00000000
1.96	0 00000000	0 00000000	0 00000000	0 00000000
1.97	0 00000000	0 00000000	0 00000000	0 00000000
1.98	0 00000000	0 00000000	0 00000000	0 00000000
1.99	0 00000000	0 00000000	0 00000000	0 00000000
2.00	0 00000000	0 00000000	0 00000000	0 00000000
SUBTOTAL	0 00000000	0 00000000	0 00000000	0 00000000

~~TOP SECRET~~

- CONTROL NO. [REDACTED]

Table A-2

-TOP SECRET-

CONTROL NO.

MISSION * 1034-1 * INSTRUMENT * AFT

8/25/66

DENSITY FREQ DISTR

~~ICP SECRET~~

CONTROL NO.

Table A-2

~~TOP SECRET~~

CONTROL NO.

MISSION * 1034-1 * INSTRUMENT * AFT 8/25/66 DENSITY FREQ DISTR

DENSITY VALUE	PRIMARY			INTERMEDIATE			FULL			ALL LEVELS		
	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM
2.51	0	0	0	0	0	0	0	0	0	0	0	0
2.52	0	0	0	0	0	0	0	0	0	0	0	0
2.53	0	0	0	0	0	0	0	0	0	0	0	0
2.54	0	0	0	0	0	0	0	0	0	0	0	0
2.55	0	0	0	0	0	0	0	0	0	0	0	0
2.56	0	0	0	0	0	0	0	0	0	0	0	0
2.57	0	0	0	0	0	0	0	0	0	0	0	0
2.58	0	0	0	0	0	0	0	0	0	0	0	0
2.59	0	0	0	0	0	0	0	0	0	0	0	0
2.60	0	0	0	0	0	0	0	0	0	0	0	0
2.61	0	0	0	0	0	0	0	0	0	0	0	0
2.62	0	0	0	0	0	0	0	0	0	0	0	0
2.63	0	0	0	0	0	0	0	0	0	0	0	0
2.64	0	0	0	0	0	0	0	0	0	0	0	0
2.65	0	0	0	0	0	0	0	0	0	0	0	0
2.66	0	0	0	0	0	0	0	0	0	0	0	0
2.67	0	0	0	0	0	0	0	0	0	0	0	0
2.68	0	0	0	0	0	0	0	0	0	0	0	0
2.69	0	0	0	0	0	0	0	0	0	0	0	0
2.70	0	0	0	0	0	0	0	0	0	0	0	0
SUBTOTAL	C	C	0	0	0	0	0	0	0	0	0	0
TOTAL	C	C	0	42	42	45	220	220	208	262	262	253

MISSION 1034-1 INSTR - AFT 8/25/66 PROCESSING AND EXPOSURE ANALY

PROCESS LEVEL	SAMPLE SIZE	UNDER EXPOSED		UNDER PROCESSED		CORRECT EXP+PROC		OVER PROCESSED		OVER EXPOSED	
		0	PC	0	PC	0	PC	0	PC	0	PC
PRIMARY	0	0	PC	0	PC	0	PC	0	PC	0	PC
INTERMEDIATE	42	0	PC	24	PC	60	PC	17	PC	0	PC
FULL	220	22	PC	0	PC	73	PC	5	PC	0	PC
ALL LEVELS	262	18	PC	4	PC	71	PC	7	PC	0	PC
PROCESS LEVEL	BASE + FCG	UNDER EXPOSED		UNDER PROCESSED		CORRECT EXP+PROC		OVER PROCESSED		OVER EXPOSED	
		0.01-0.09	0.01-0.13	0.14-0.39	0.40-0.90	-----	-----	0.91	AND	0.91	AND
		INTERMED	0.16-0.17	0.01-0.20	0.21-0.39	0.40-0.90	0.91-1.34	1.35	AND	0.91	1.70 AND
FULL	0.18 AND UP	0.01-0.39	-----	0.40-0.90	0.91-1.69	1.70	AND	0.91	1.70 AND		

~~TOP SECRET~~

CONTROL NO.

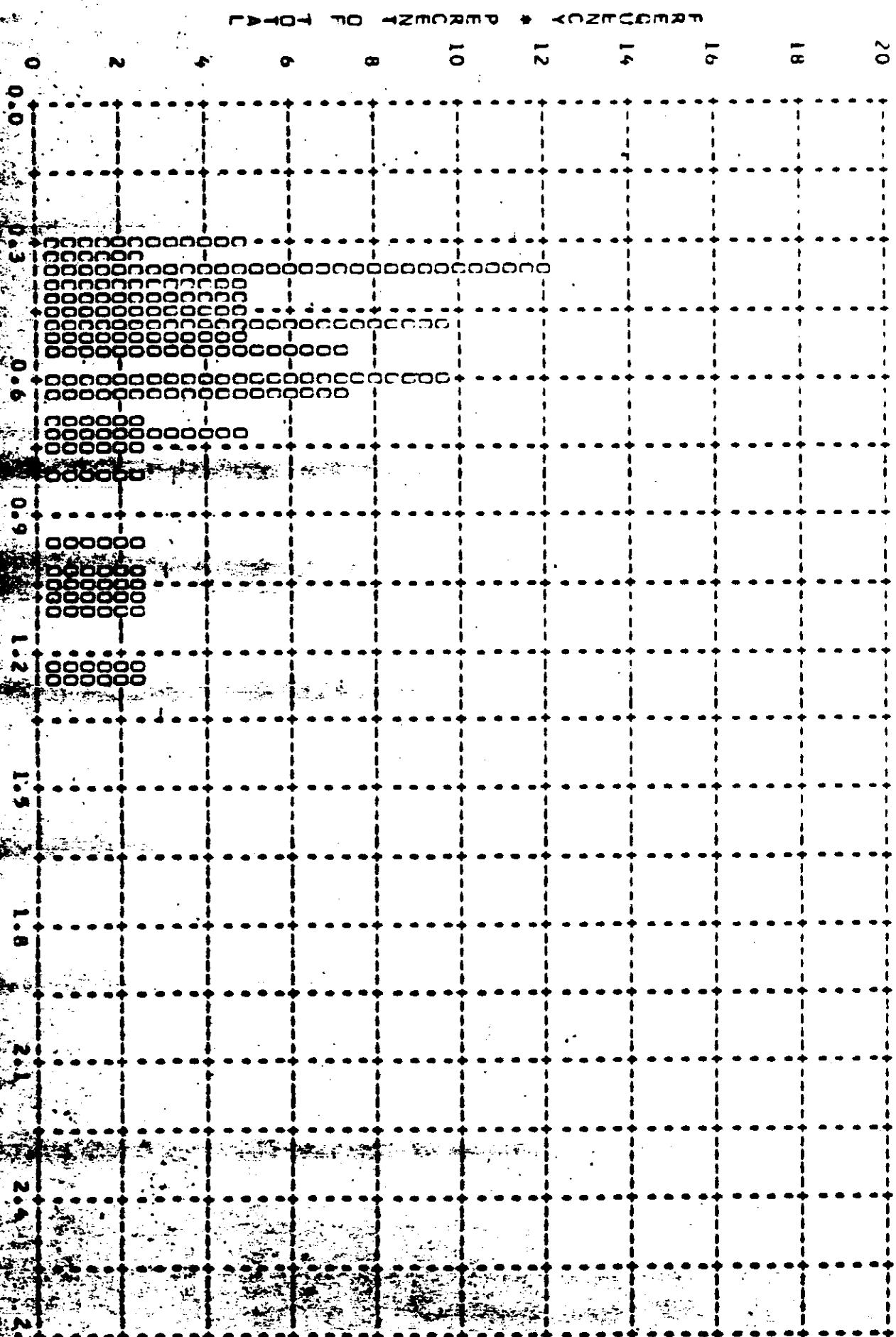
Table A-2

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CUNN. NO.

MISSION # 1034-1 * INSTR # AFT * 8/25/66 PILOT OF 0 MIN * TERRAIN * PROCESSING * INTERMEDIATE
ARITH MEAN * 0.60 * MEDIAN * 0.54 * STD DEV * 0.26 * RANGE * 0.29 TO 1.26 WITH 42 SAMPLES

A-22



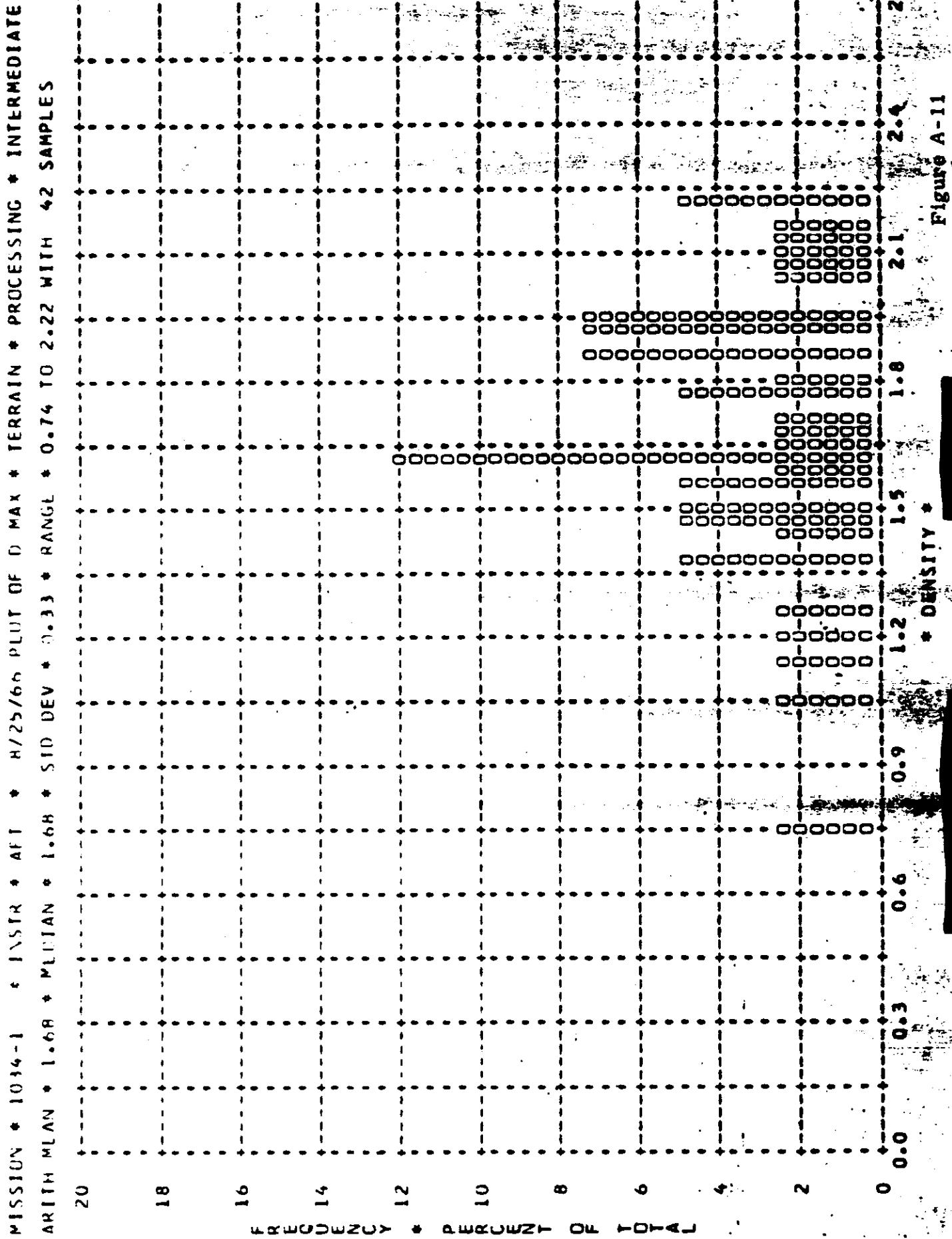


Figure A-11

MISSION * 1034-1 * INSTR * AFT * R/25/66 PLOT OF D MAX * CLOUD * PROCESSING * INTERMEDIATE

ARITH MEAN * 2.17 * MEDIAN * 2.15 * STD DEV * C.13 * RANGE * 1.84 TO 2.31 WITH 45 SAMPLES

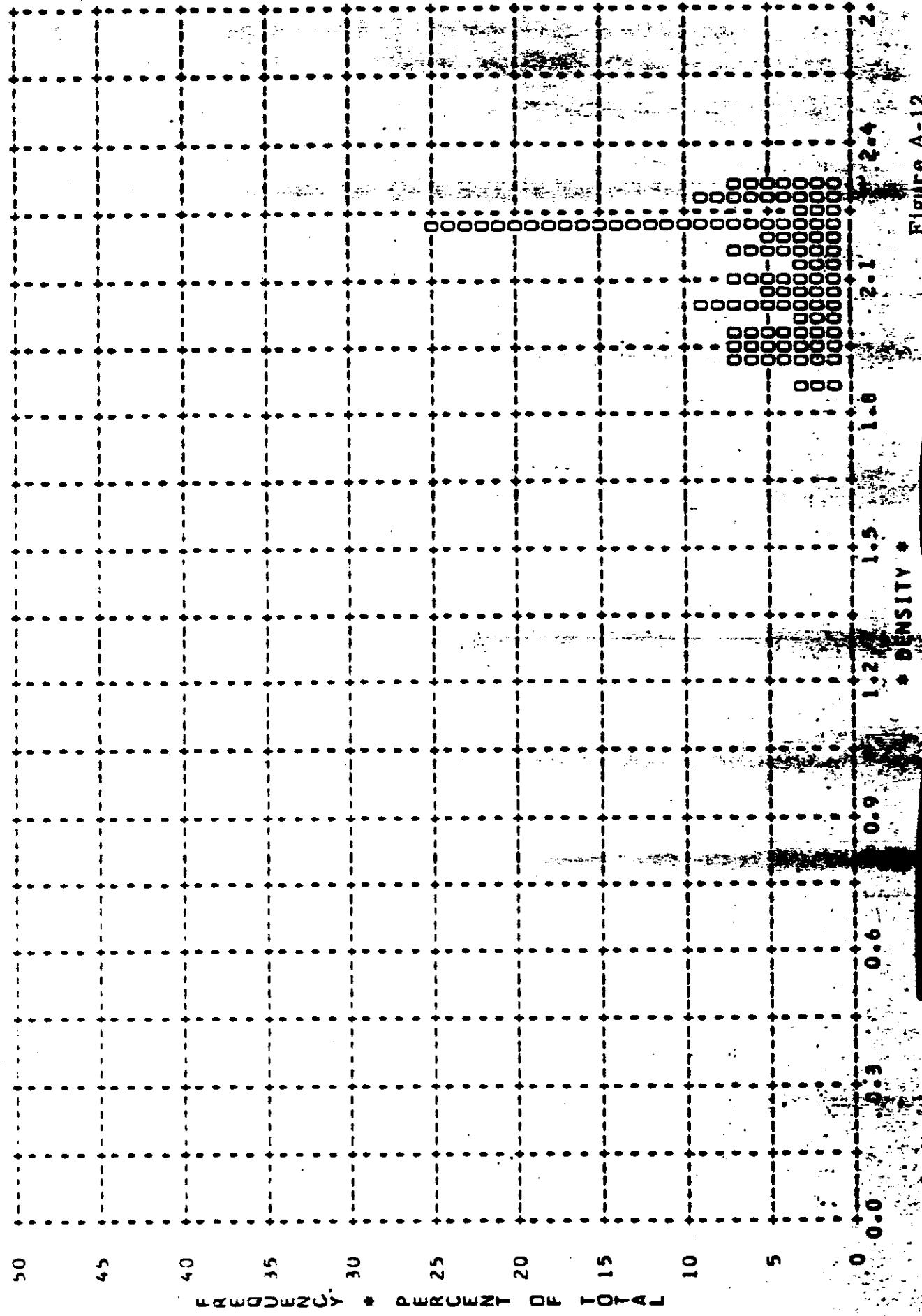
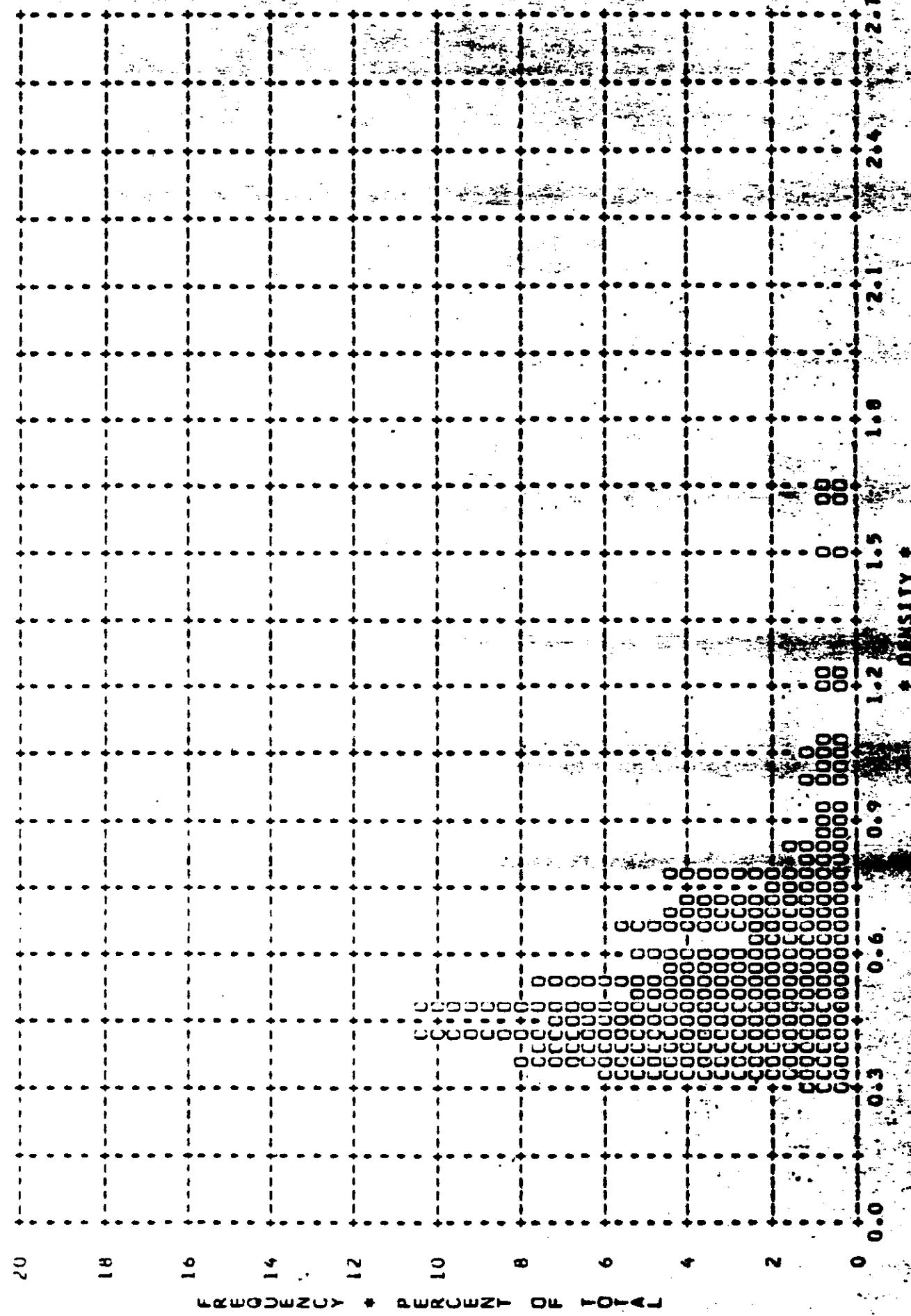


Figure A-12

CON. VOL NO.

STEP-STERE

MISSION * 1014-1 * INSTN * AFT * 8/25/66 PLOT UF D MIN * TERRAIN * PROCESSING * FULL
ARITH MEAN * 0.55 * MEDIAN * 0.50 * STD DEV * 0.21 * RANGE * 0.30 TO 1.63 WITH 220 SAMPLES



CUN...JL NO.

MISSION * 1034-1 * INSTR * AII * 8/25/66 PILOT OF D MAX * TERRAIN * PROCESSING * FULL
ARITH. MEAN * 1.53 * MEDIAN * 1.56 * STD DEV * 0.44 * RANGE * 0.41 TO 2.35 WITH 220 SAMPLES

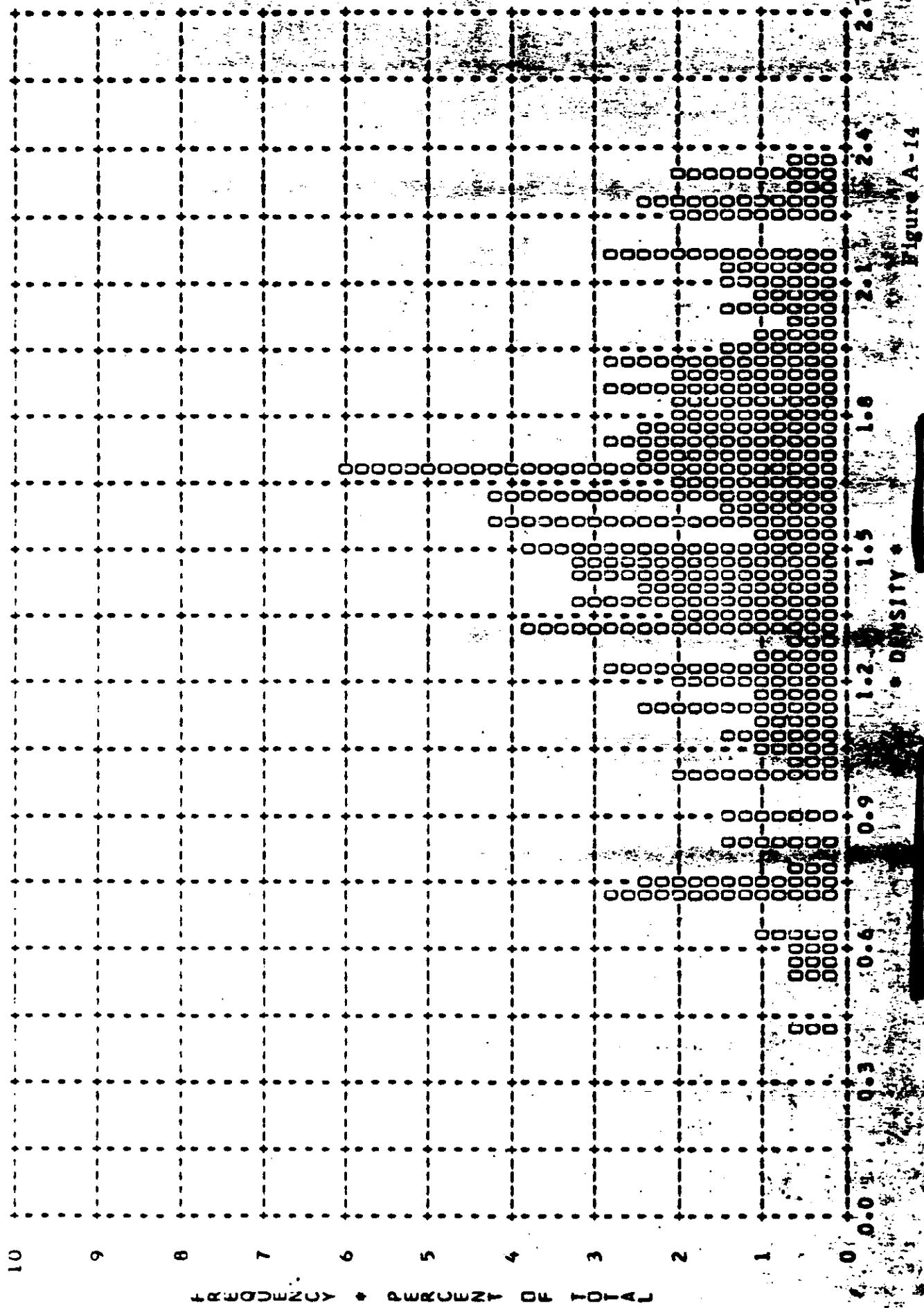
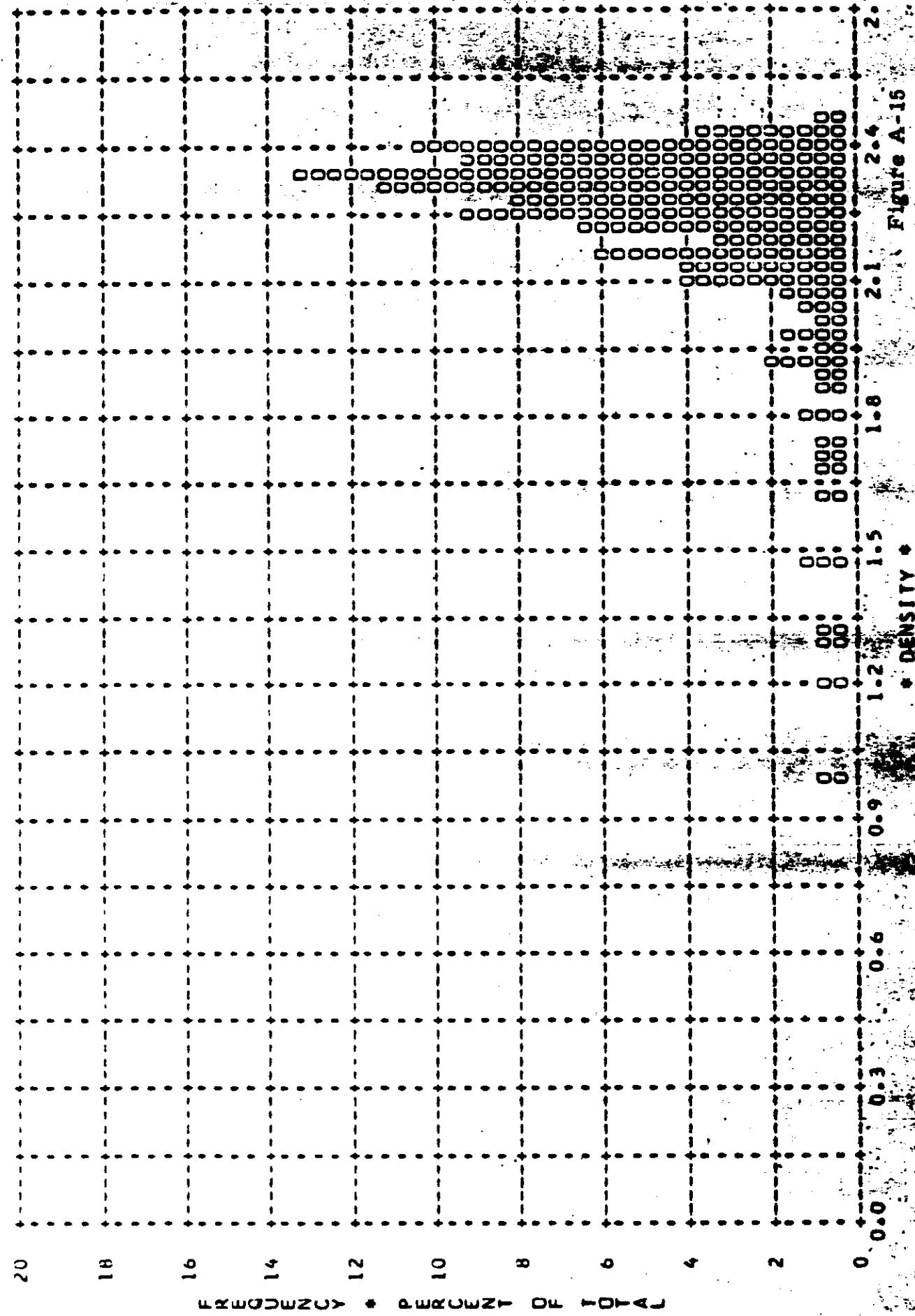


Figure A-14

-TOP-SETTHT-

- CUN. .0L N).

MISSION * 1034-1 * INSTR * AFT * 8/25/66 PLCT OF U MAX * CLOUD * PROCESSING * FULL
ARITH MEAN * 2.21 * MEDIAN * 2.28 * STD DEV * 0.22 * RANGE * 0.97 TO 2.44 WITH 208 SAMPLES

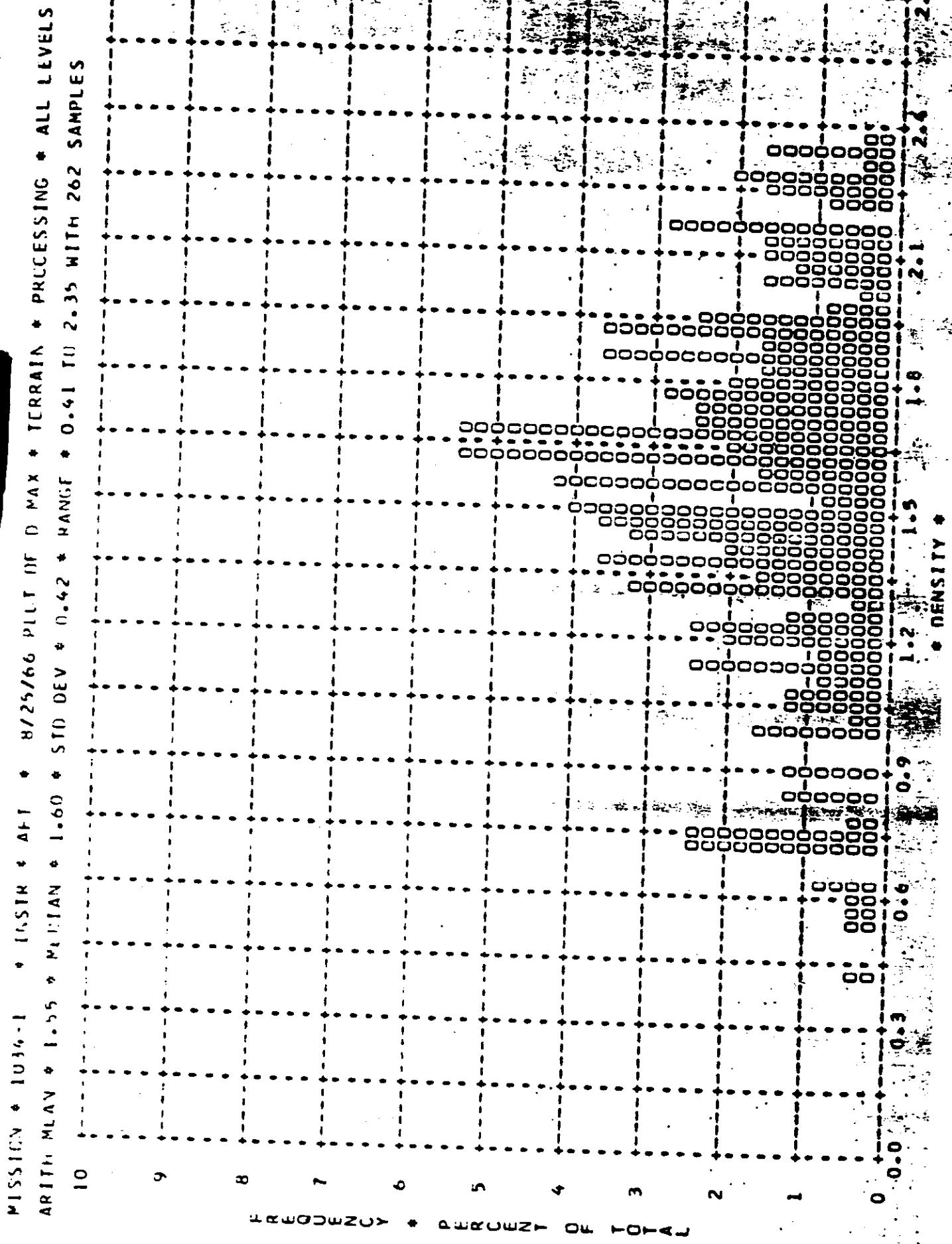


- CONTROL NO. [REDACTED]

MISSILE * 1034-1 * INSTN * API * A/25/66 PILOT OF D MIN * TERRAIN * PROCESSING * ALL LEVELS
ARITH MEAN * 0.56 * MILLIAN * 0.50 * SIN DFV * 0.22 * RANGE * 0.29 TO 1.63 WITH 262 SAMPLES



FIGURE A-14



MISSION * 1034-1 * INSTR * AFT * 8/25/66 PILOT OF D MAX * CLOUD * PROCESSING * ALL LEVELS
ARITH MTAN * 2.13 * MILLAN * 2.25 * SIG DEV * 0.21 * RANGE * 0.97 TU 2.64 WITH 263 SAMPLES



Figure A-18

~~TOP SECRET~~

- CONTROL NO.

MISSION * 1034-2 * INSTRUMENT * FWD * 8/25/66 DENSITY EREQ DISTR

DENSITY	PRIMARY	INTERMEDIATE	FULL	ALL LEVELS
VALUE	MIN MAX LIM	MIN MAX LIM	MIN MAX LIM	MIN MAX LIM

0.01	0	0	0	0
0.02	0	0	0	0
0.03	0	0	0	0
0.04	0	0	0	0
0.05	0	0	0	0
0.06	0	0	0	0
0.07	0	0	0	0
0.08	0	0	0	0
0.09	0	0	0	0
0.10	0	0	0	0
0.11	0	0	0	0
0.12	0	0	0	0
0.13	0	0	0	0
0.14	0	0	0	0
0.15	0	0	0	0
0.16	0	0	0	0
0.17	0	0	0	0
0.18	0	0	0	0
0.19	0	0	0	0
0.20	0	0	0	0
0.21	0	0	0	0
0.22	0	0	0	0
0.23	0	0	0	0
0.24	0	0	0	0
0.25	0	0	0	0
0.26	0	0	0	0
0.27	0	0	0	0
0.28	0	0	0	0
0.29	0	0	0	0
0.30	0	0	0	0
0.31	0	0	0	0
0.32	0	0	0	0
0.33	0	0	0	0
0.34	0	0	0	0
0.35	0	0	0	0
0.36	0	0	0	0
0.37	0	0	0	0
0.38	0	0	0	0
0.39	0	0	0	0
0.40	0	0	0	0
0.41	0	0	0	0
0.42	0	0	0	0
0.43	0	0	0	0
0.44	0	0	0	0
0.45	0	0	0	0
0.46	0	0	0	0
0.47	0	0	0	0
0.48	0	0	0	0
0.49	0	0	0	0
0.50	0	0	0	0
SUBTOTAL	0	0	0	0

28

~~TOP SECRET~~

- CONTROL NO.

Table A-3

~~TOP SECRET~~

CONTROL NO.

MISSION * 1034-2 * INSTRUMENT * FWD 8/25/66 DENSITY FREQ DISTR

DENSITY VALUE	PRIMARY MIN MAX LIM	INTERMEDIATE MIN MAX LIM	FULL MIN MAX LIM	ALL LEVELS MIN MAX LIM
0.51	0 0	0 0	0 0	0 0
0.52	0 0	0 0	0 0	0 0
0.53	0 0	0 0	0 0	0 0
0.54	0 0	0 0	0 0	0 0
0.55	0 0	0 0	0 0	0 0
0.56	0 0	0 0	0 0	0 0
0.57	0 0	0 0	0 0	0 0
0.58	0 0	0 0	0 0	0 0
0.59	0 0	0 0	0 0	0 0
0.60	0 0	0 0	0 0	0 0
0.61	0 0	0 0	0 0	0 0
0.62	0 0	0 0	0 0	0 0
0.63	0 0	0 0	0 0	0 0
0.64	0 0	0 0	0 0	0 0
0.65	0 0	0 0	0 0	0 0
0.66	0 0	0 0	0 0	0 0
0.67	0 0	0 0	0 0	0 0
0.68	0 0	0 0	0 0	0 0
0.69	0 0	0 0	0 0	0 0
0.70	0 0	0 0	0 0	0 0
0.71	0 0	0 0	0 0	0 0
0.72	0 0	0 0	0 0	0 0
0.73	0 0	0 0	0 0	0 0
0.74	0 0	0 0	0 0	0 0
0.75	0 0	0 0	0 0	0 0
0.76	0 0	0 0	0 0	0 0
0.77	0 0	0 0	0 0	0 0
0.78	0 0	0 0	0 0	0 0
0.79	0 0	0 0	0 0	0 0
0.80	0 0	0 0	0 0	0 0
0.81	0 0	0 0	0 0	0 0
0.82	0 0	0 0	0 0	0 0
0.83	0 0	0 0	0 0	0 0
0.84	0 0	0 0	0 0	0 0
0.85	0 0	0 0	0 0	0 0
0.86	0 0	0 0	0 0	0 0
0.87	0 0	0 0	0 0	0 0
0.88	0 0	0 0	0 0	0 0
0.89	0 0	0 0	0 0	0 0
0.90	0 0	0 0	0 0	0 0
0.91	0 0	0 0	0 0	0 0
0.92	0 0	0 0	0 0	0 0
0.93	0 0	0 0	0 0	0 0
0.94	0 0	0 0	0 0	0 0
0.95	0 0	0 0	0 0	0 0
0.96	0 0	0 0	0 0	0 0
0.97	0 0	0 0	0 0	0 0
0.98	0 0	0 0	0 0	0 0
0.99	0 0	0 0	0 0	0 0
1.00	0 0	0 0	0 0	0 0
SUBTOTAL		34	11	88

~~TOP SECRET~~

CONTROL NO.

Table A-3

~~TOP SECRET~~

CONTROL NO.

MISSION * 1034-2 * INSTRUMENT * FWD 8/25/66 . DENSITY FREQ DISTR

-10- 61684

- CONTROL NO.

Table A-3

~~TOP SECRET~~

- CONTROL NO.

MISSION * 1034-2 * INSTRUMENT * FWD

8/25/66 DENSITY FREQ DESTR

DENSITY VALUE	PRIMARY MIN MAX LIM	INTERMEDIATE MIN MAX LIM	FULL MIN MAX LIM	ALL LEVELS MIN MAX LIM
1.51	0	0	0	0
1.52	0	0	2	2
1.53	0	0	4	6
1.54	0	0	4	7
1.55	0	0	1	4
1.56	0	0	0	0
1.57	0	0	0	0
1.58	0	0	0	0
1.59	0	0	0	0
1.60	0	0	0	0
1.61	0	0	0	0
1.62	0	0	0	0
1.63	0	0	0	0
1.64	0	0	0	0
1.65	0	0	0	0
1.66	0	0	0	0
1.67	0	0	0	0
1.68	0	0	0	0
1.69	0	0	0	0
1.70	0	0	0	0
1.71	0	0	0	0
1.72	0	0	0	0
1.73	0	0	0	0
1.74	0	0	0	0
1.75	0	0	0	0
1.76	0	0	0	0
1.77	0	0	0	0
1.78	0	0	0	0
1.81	0	0	0	0
1.82	0	0	0	0
1.83	0	0	0	0
1.84	0	0	0	0
1.85	0	0	0	0
1.86	0	0	0	0
1.87	0	0	0	0
1.88	0	0	0	0
1.89	0	0	0	0
1.91	0	0	0	0
1.92	0	0	0	0
1.93	0	0	0	0
1.94	0	0	0	0
1.95	0	0	0	0
1.96	0	0	0	0
1.97	0	0	0	0
1.98	0	0	0	0
1.99	0	0	0	0
2.00	0	0	0	0
SUBTOTAL		48	81	129

~~TOP SECRET~~

- CONTROL NO.

Table A-3

~~TOP SECRET~~

CONTROL NO.

MISSION * 1034-2 * INSTRUMENT * FWD

8/25/66 DENSITY FREQ DISTR

DENSITY VALUE	PRIMARY MIN MAX LIM	INTERMEDIATE MIN MAX LIM	FULL MIN MAX LIM	ALL LEVELS MIN MAX LIM
2.01	0	0	0	0
2.02	0	0	0	0
2.03	0	0	0	0
2.04	0	0	0	0
2.05	0	0	0	0
2.06	0	0	0	0
2.07	0	0	0	0
2.08	0	0	0	0
2.09	0	0	0	0
2.10	0	0	0	0
2.11	0	0	0	0
2.12	0	0	0	0
2.13	0	0	0	0
2.14	0	0	0	0
2.15	0	0	0	0
2.16	0	0	0	0
2.17	0	0	0	0
2.18	0	0	0	0
2.19	0	0	0	0
2.20	0	0	0	0
2.21	0	0	0	0
2.22	0	0	0	0
2.23	0	0	0	0
2.24	0	0	0	0
2.25	0	0	0	0
2.26	0	0	0	0
2.27	0	0	0	0
2.28	0	0	0	0
2.29	0	0	0	0
2.30	0	0	0	0
2.31	0	0	0	0
2.32	0	0	0	0
2.33	0	0	0	0
2.34	0	0	0	0
2.35	0	0	0	0
2.36	0	0	0	0
2.37	0	0	0	0
2.38	0	0	0	0
2.39	0	0	0	0
2.40	0	0	0	0
2.41	0	0	0	0
2.42	0	0	0	0
2.43	0	0	0	0
2.44	0	0	0	0
2.45	0	0	0	0
2.46	0	0	0	0
2.47	0	0	0	0
2.48	0	0	0	0
2.49	0	0	0	0
2.50	0	0	0	0
SLBTOTAL	0	0	42	38 233

~~TOP SECRET~~

CONTROL NO.

Table A-3

~~TOP SECRET~~

CONTROL NO.

MISSION * 1034-2 * INSTRUMENT * FWD 8/25/66 DENSITY FREQ DISTR.

DENSITY VALUE	PRIMARY MIN MAX LIM	INTERMEDIATE MIN MAX LIM	FULL MIN MAX LIM	ALL LEVELS MIN MAX LIM
2.51	C C	C 0	0 0 0	0 0 0 0
2.52	CC C	CC 0	0 0 0	0 0 0 0
2.53	CCC C	CC 0	0 0 0	0 0 0 0
2.54	CCCC C	CC 0	0 0 0	0 0 0 0
2.55	CCCCC C	CC 0	0 0 0	0 0 0 0
2.56	CCCCC C	CC 0	0 0 0	0 0 0 0
2.57	CCCCC C	CC 0	0 0 0	0 0 0 0
2.58	CCCCC C	CC 0	0 0 0	0 0 0 0
2.59	CCCCC C	CC 0	0 0 0	0 0 0 0
2.60	CCCCC C	CC 0	0 0 0	0 0 0 0
2.61	CCCCC C	CC 0	0 0 0	0 0 0 0
2.62	CCCCC C	CC 0	0 0 0	0 0 0 0
2.63	CCCCC C	CC 0	0 0 0	0 0 0 0
2.64	CCCCC C	CC 0	0 0 0	0 0 0 0
2.65	CCCCC C	CC 0	0 0 0	0 0 0 0
2.66	CCCCC C	CC 0	0 0 0	0 0 0 0
2.67	CCCCC C	CC 0	0 0 0	0 0 0 0
2.68	CCCCC C	CC 0	0 0 0	0 0 0 0
2.69	CCCCC C	CC 0	0 0 0	0 0 0 0
2.70	CCCCC C	CC 0	0 0 0	0 0 0 0
SUBTOTAL	C C	0 0	0 0 0	0 0 0 0
TOTAL	C C	0 69	69 51 190	259 259 256

MISSION 1034-2 INSTR - AFT 8/25/66 PROCESSING AND EXPOSURE ANALY

PROCESS LEVEL	SAMPLE SIZE	UNDER EXPOSED	UNDER PROCESSED	CORRECT EXP+PROC	OVER PROCESSED	OVER EXPOSED
PRIMARY	0	0 PC	0 PC	0 PC	0 PC	0 PC
INTERMEDIATE	69	1 PC	16 PC	67 PC	14 PC	14 PC
FULL	190	15 PC	0 PC	79 PC	5 PC	0 PC
ALL LEVELS	259	12 PC	4 PC	76 PC	8 PC	0 PC
PROCESS LEVEL	BASE + FCG	UNDER EXPOSED	UNDER PROCESSED	CORRECT EXP+PROC	OVER PROCESSED	OVER EXPOSED
PRIMARY	0.01-0.09	0.01-0.13	0.14-0.39	0.40-0.90	-----	0.91 AND
INTERMED	0.10-0.17	0.01-0.20	0.21-0.39	0.40-0.90	0.91-1.34	1.35 AND
FULL	C.1B AND LP	0.01-0.39	-----	0.40-0.90	0.91-1.69	1.70 AND

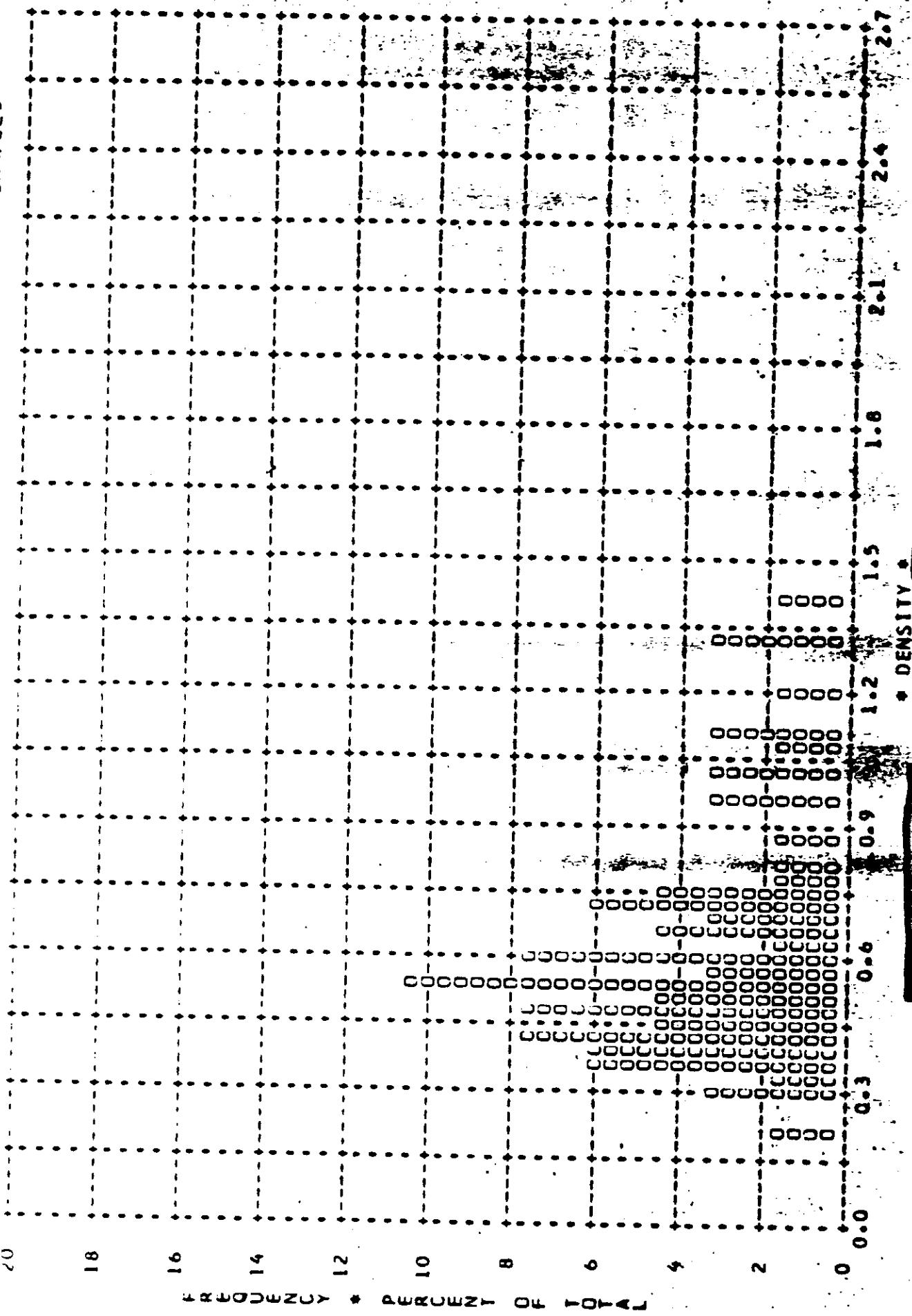
~~TOP SECRET~~

CONTROL NO.

Table A-3

[REDACTED] - CONTROL NO.

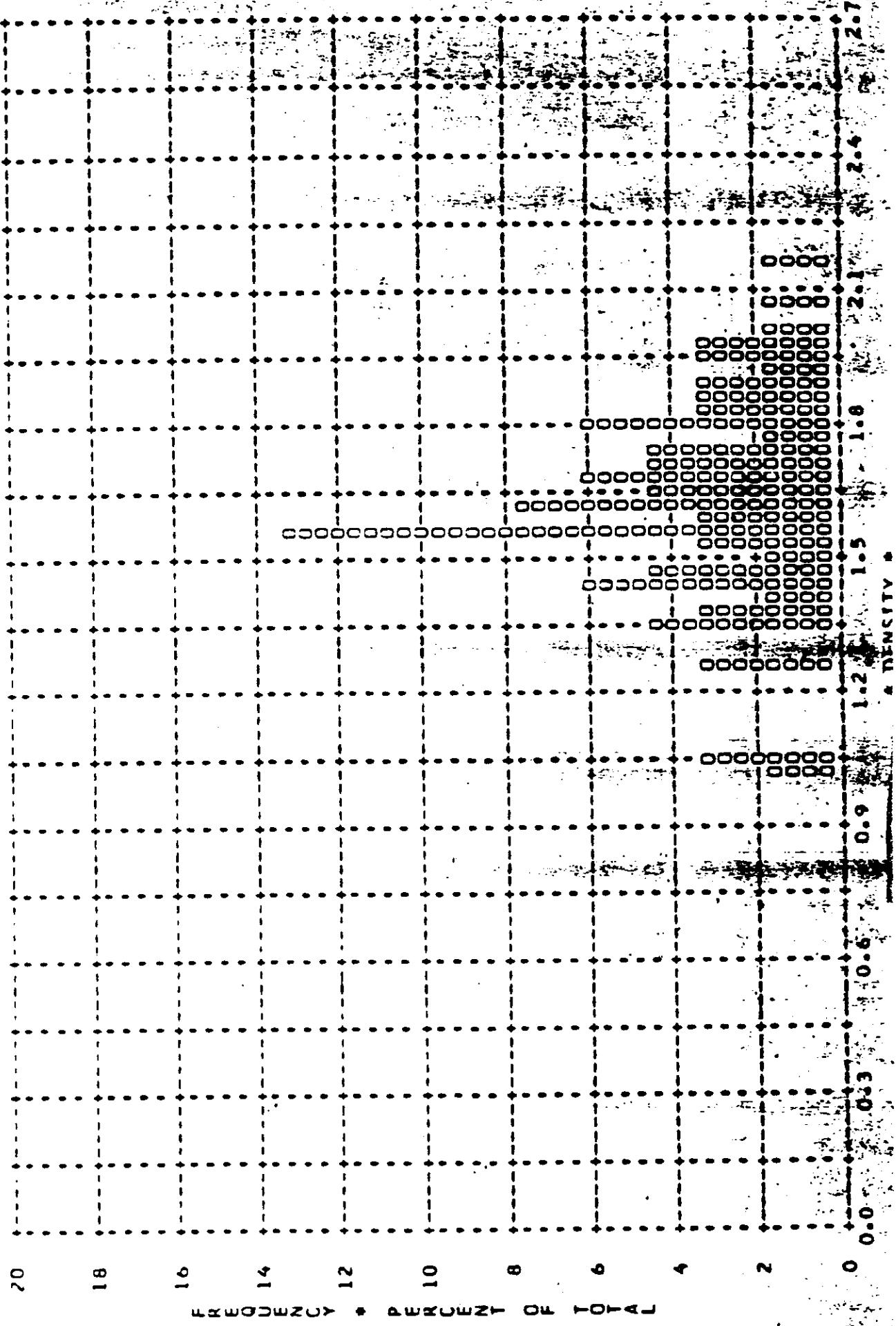
MISSION * 1034-2 * TEST * FWD * R/25/66 PLUT OF D MIN * TERRAIN * PROCESSING * INTERMEDIATE
ARITH MEAN * 0.12 * MILITIA * 0.54 * STD DEV * 0.21 * RANGE * 0.19 TO 1.40 WITH 69 SAMPLES



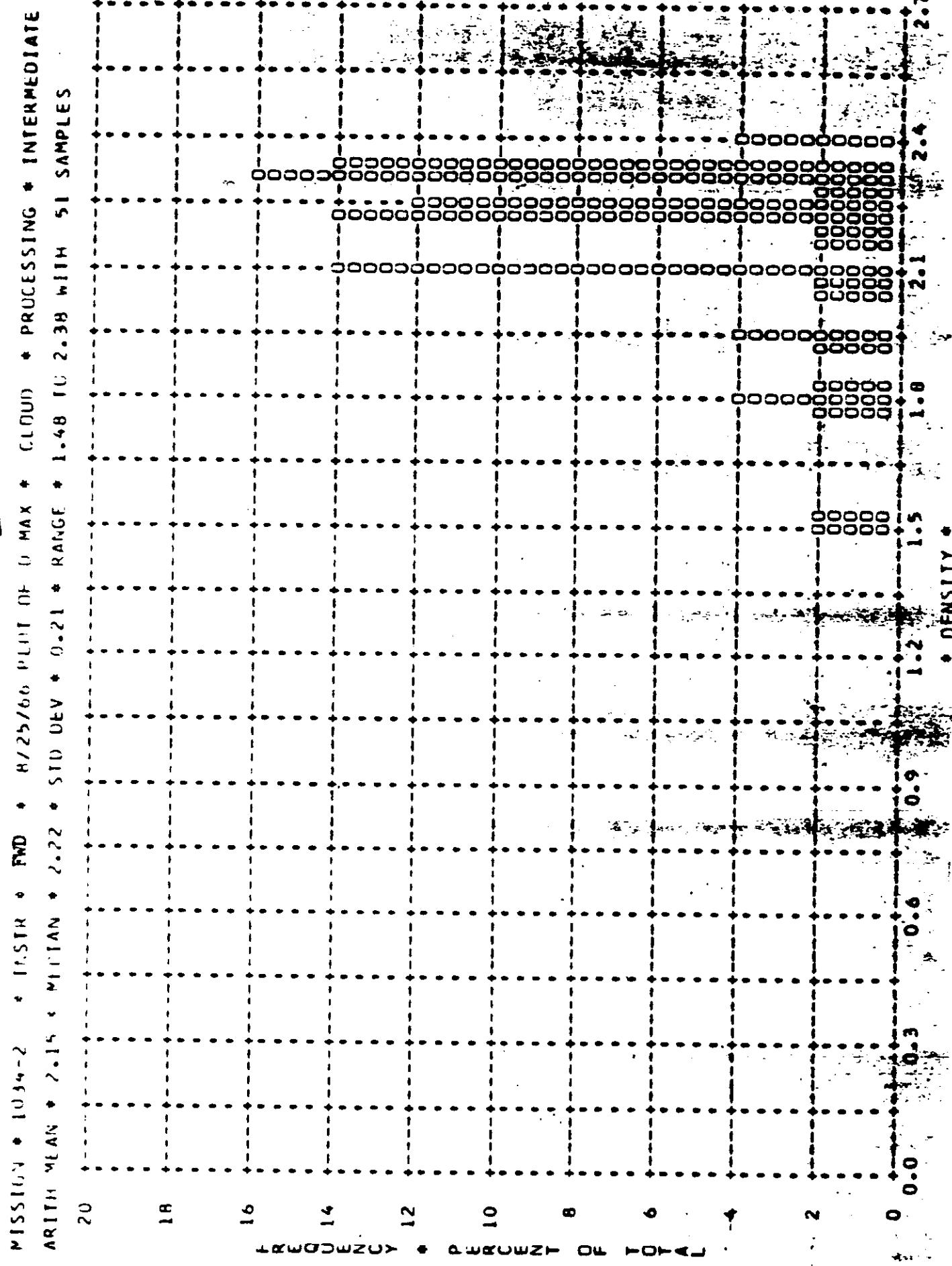
- CONTROL NO.

MISSION # 1034-2 • INSTN • FWD • H/75/66 PLOT OF 0 MAX • TERRAIN • PROCESSING • INTERMEDIATE

ARITH. MEAN • 1.61 • MEDIAN • 1.60 • STD DEV • 0.23 • RANGE • 1.00 TO 2.14 WITH 69 SAMPLES

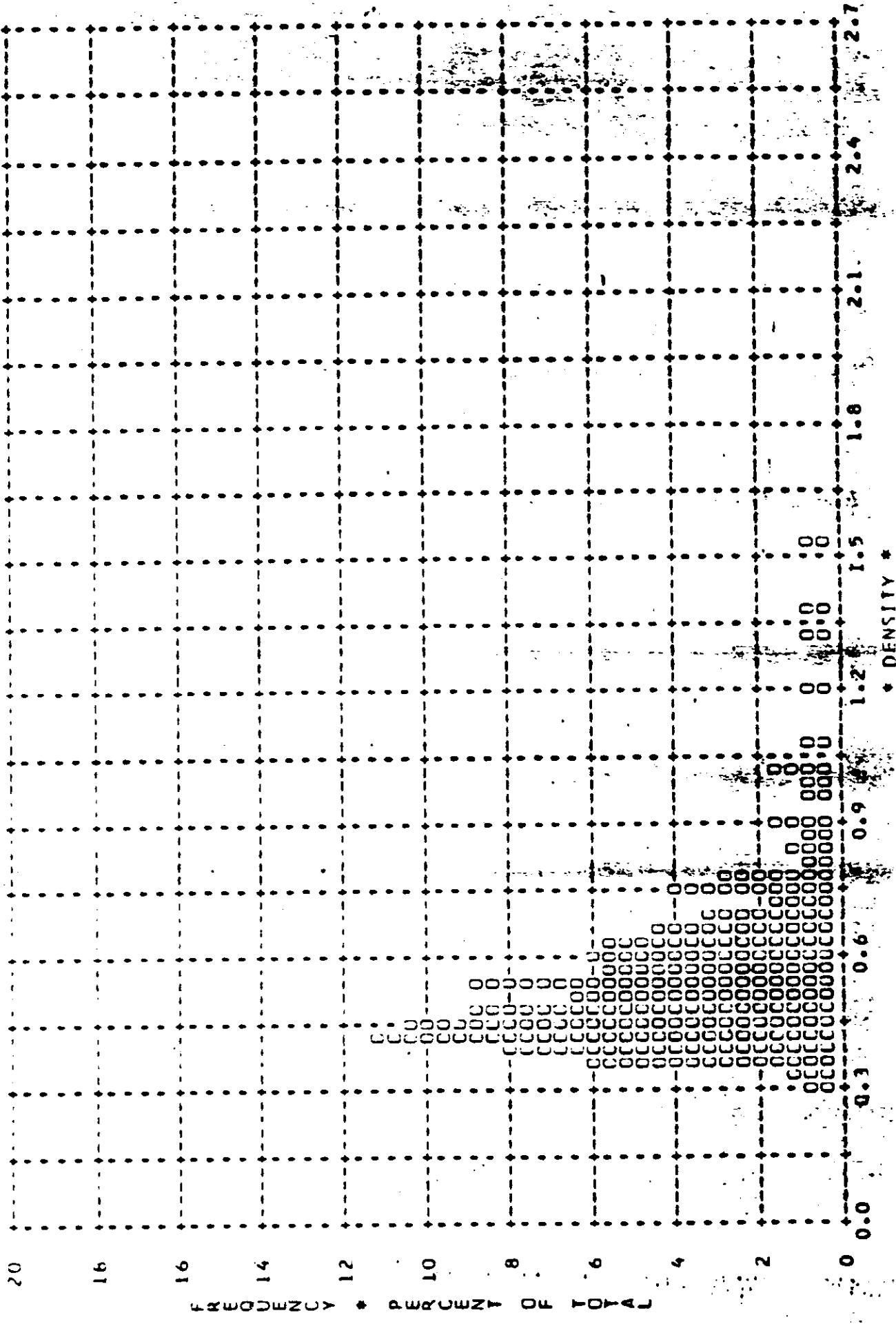


----- CONTROL NO.



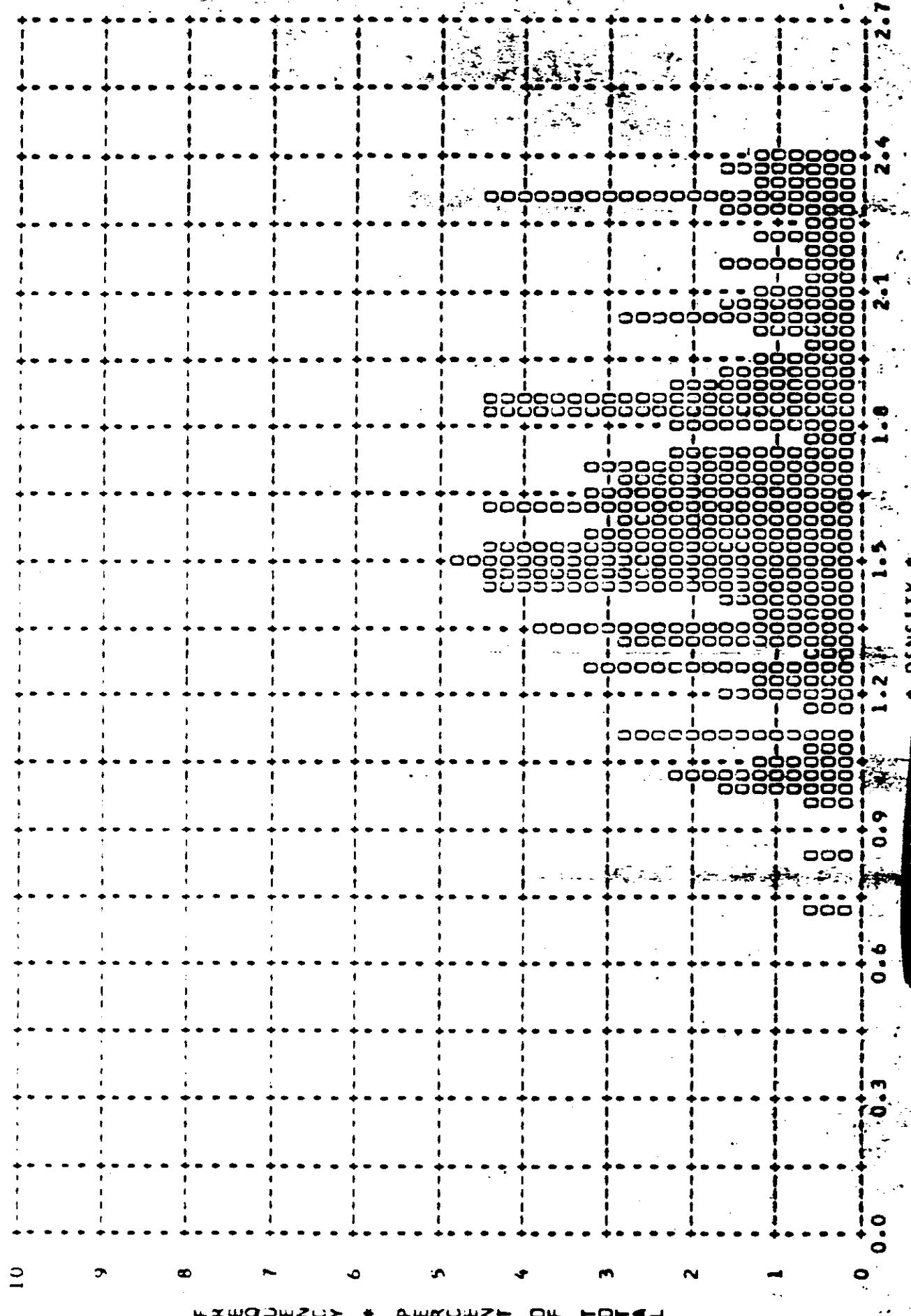
- CONTROL NO. [REDACTED]

MISSION # 1034-2 CLOUDS & FWD * 1/25/66 PLUT OF D MINE * TERRAIN * PROCESSING * FULL
ARITH MEAN = 0.54 * STDEV = 0.50 * STD DEV = 0.19 * RANGE = 0.30 TO 1.52 WITH 190 SAMPLES



- CONTROL NO.

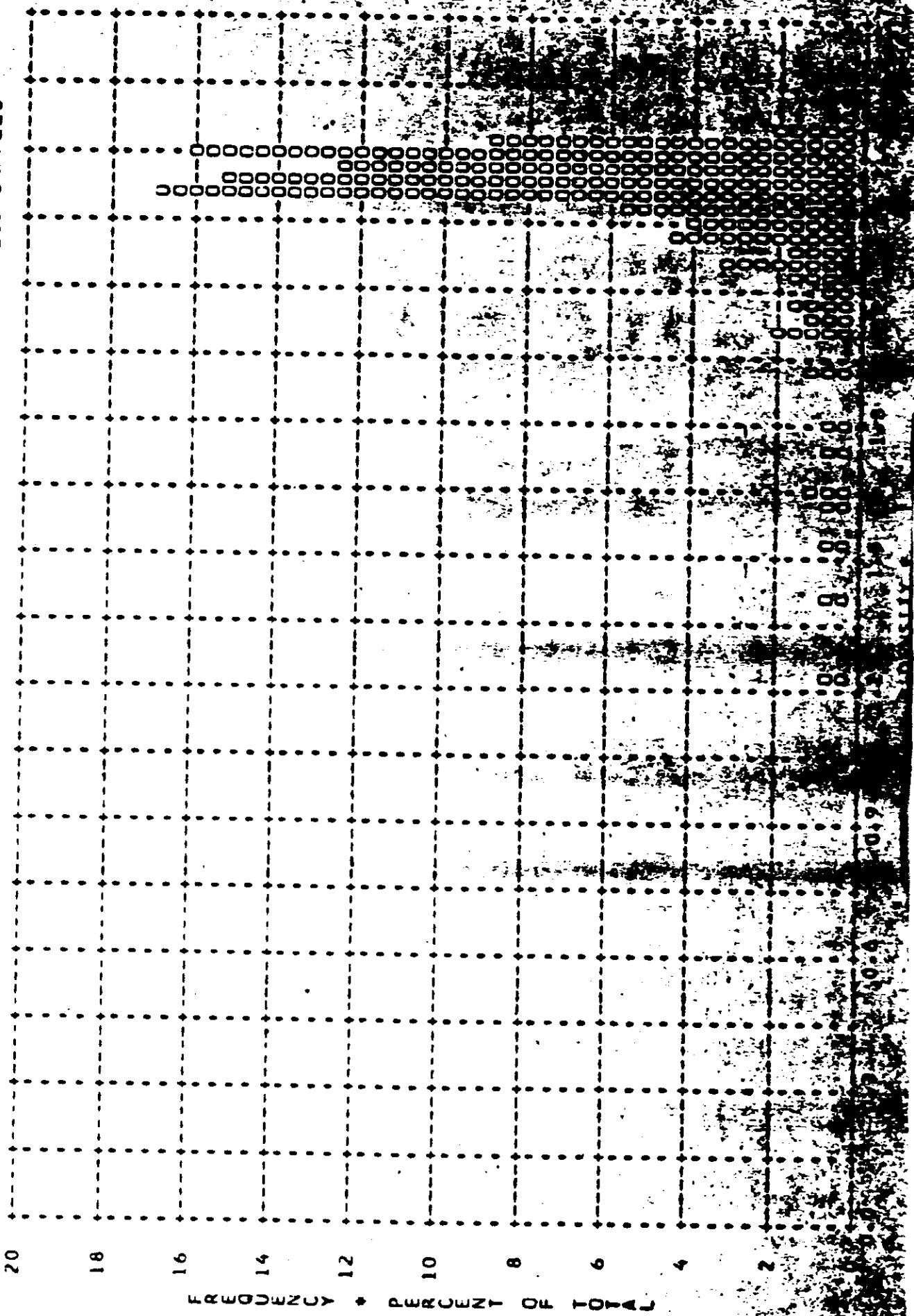
MISSION * 1034-2 * FWD * 4/25/66 RT-T OF 10 MAX * TERRAIN * PROCESSING * FULL
ARITH: MEAN * 1.64 & MEDIAN * 1.60 * STD DEV * 0.37 * RANGE * 0.12 TO 2.40 with 190 SAMPLES



TOP SECRET

- CONTROL NO.

MISSION # 1034-2 * INSTR # FWD * 8/25/66 PLOT OF D MAX * CLOUD * PROCESSING * FULL
ARITH. MEAN * 2.048 * MEDIAN * 2.32 * STD DEV * 0.1H * RANGE * 1.21 10 2.47 WITH 205 SAMPLES

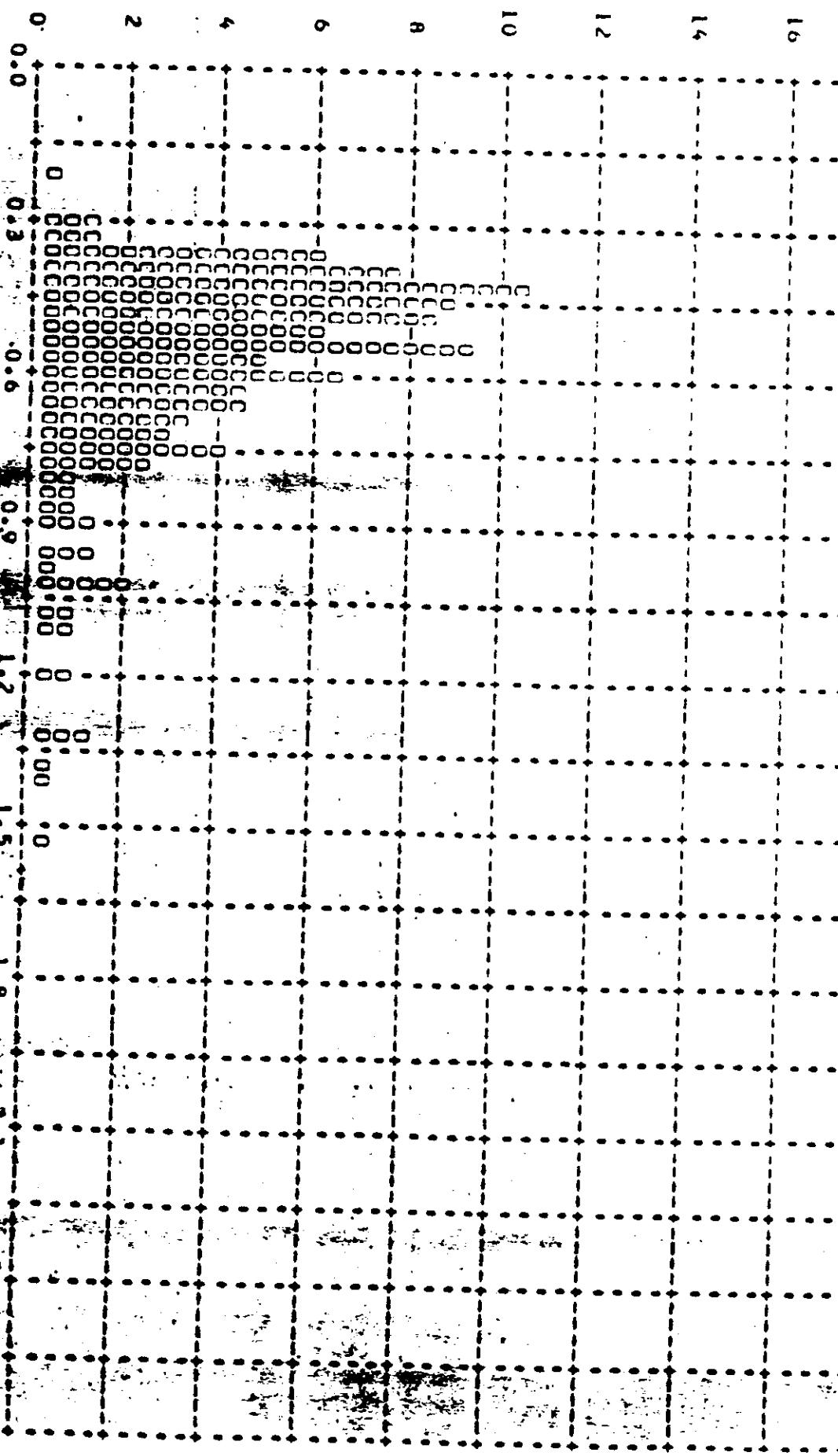


CONTROL NO. [REDACTED]

MISSION • IUS4-2 • USIN • PWD • R/25/66 PLOT OF D MIN • TERRAIN • PROCESSING • ALL LEVELS
ARITH MEAN • 0.07 • MEDIAN • 0.52 • STD DEV • 0.22 • RANGE • 0.19 TO 1.52 WITH 259 SAMPLES

A-43

DATAFILE # 404-1044



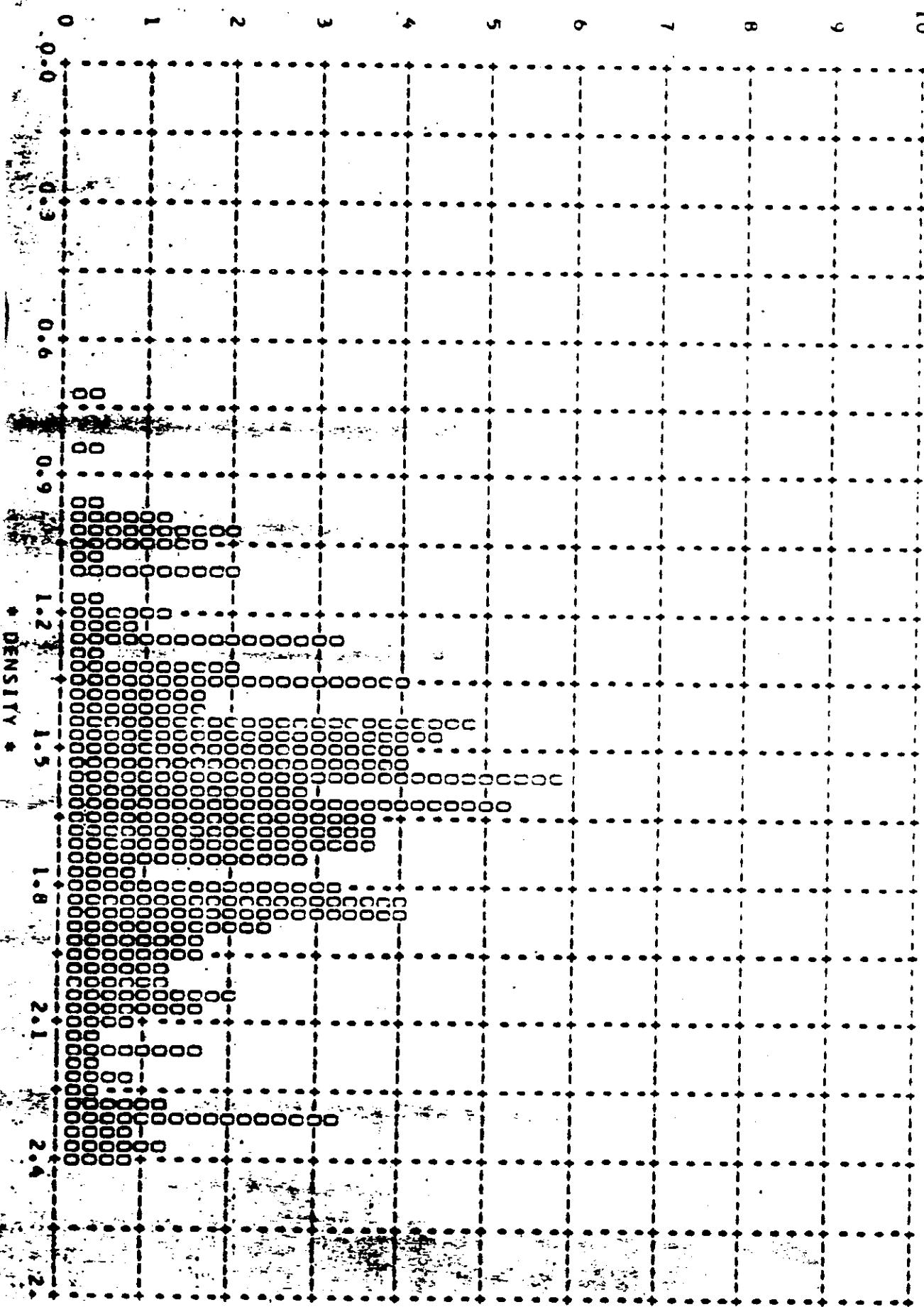
RECORDED

CONTINUO.

MISSION # 1034-2 * INSTR # PWD * 8/25/66 PLUT OR 0 MAX * IRRAIN * PROCESSING * ALL LEVELS
ARITH. MEAN # 1.03 * MEDIAN # 1.60 * STD DEV # 0.34 * RANGE # 0.17 TO 2.40 WITH 259 SAMPLES

A-44

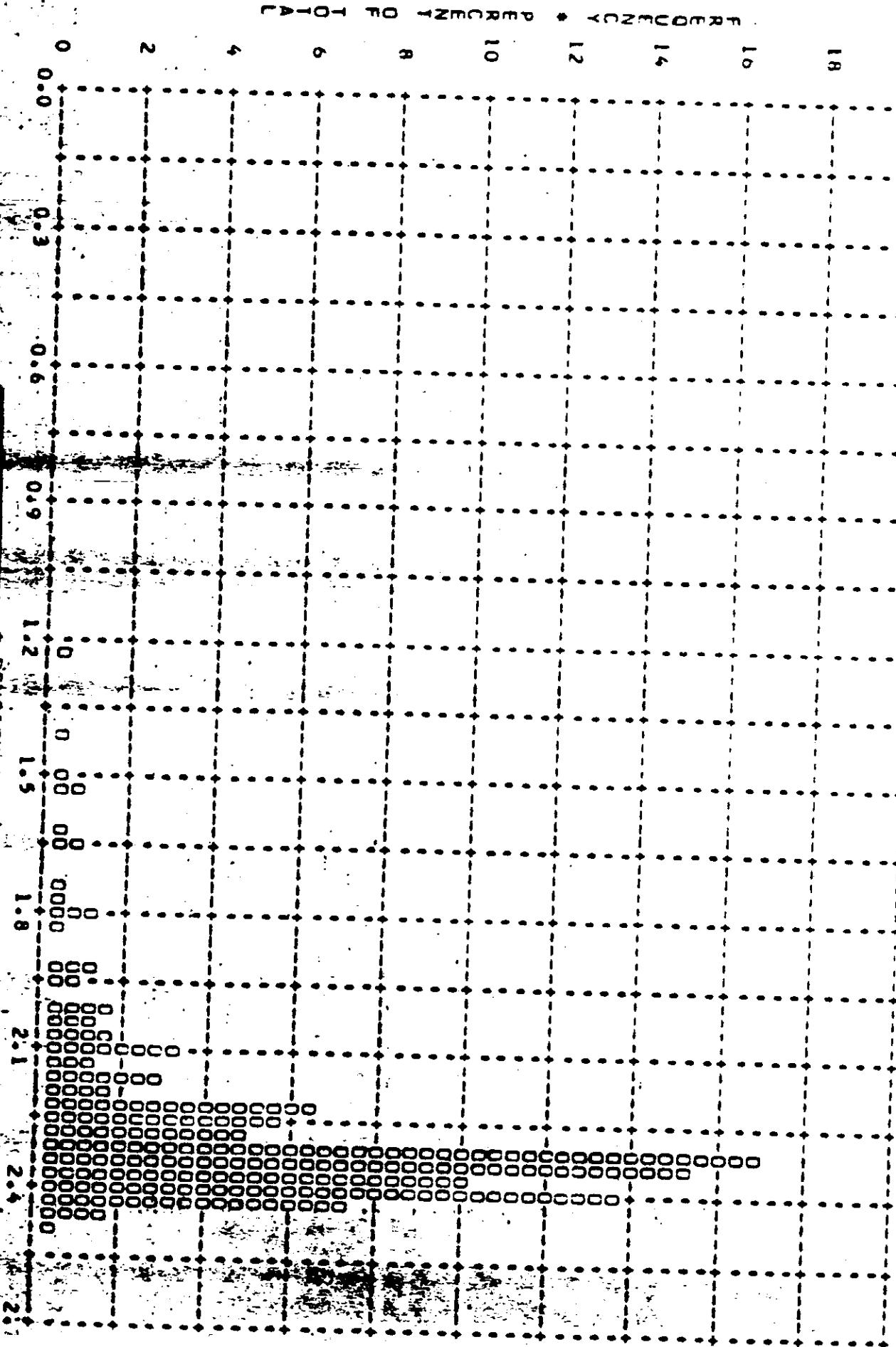
DATA SOURCE * AVERAGE OF 10443



A-45

MISSION # 1034-2 * LASH * FWD * 8/25/66 PLOT OF D MAX * CLOUD * PROCESSING * ALL LEVELS
AERIE MEAN * 2.25 * MEDIAN * 2.11 * STD DEV * 0.13 * RANGE * 1.21 TO 2.47 WITH 256 SAMPLES

- CONTROL NO. [REDACTED]



~~-TOP SECRET~~

CONTROL NO.

MISSION * 1034-2 * INSTRUMENT * ATT

8/25/66

8/25/66 DENSITY FREQ DISTR

~~TOP SECRET~~

- CONTROL NO.

Table A-4

~~TOP SECRET~~

CONTROL NO.

MISSION * 1034-2 * INSTRUMENT * AFT

8/25/66 DENSITY FREQ DISTR

100 SECRET

- CONTROL NO.

Table A-4

~~TOP SECRET~~

CONTROL NO.

MISSION * 1034-2 * INSTRUMENT * AFT 8/25/66 DENSITY FREQ.DISTR.

~~TOP SECRET~~

CONTROL NO.

Table A-4

~~TOP SECRET~~

- CONTROL NO.

MISSION * 1034-2 * INSTRUMENT * AFT 8/25/66 DENSITY FREQ DISTR

DENSITY VALUE	PRIMARY MIN MAX LIM	INTERMEDIATE MIN MAX LIM	FULL MIN MAX LIM	ALL LEVELS MIN MAX LIM
1.51	0 0	0 0	0 0	0 0
1.52	0 0	0 0	0 0	0 0
1.53	0 0	0 0	0 0	0 0
1.54	0 0	0 0	0 0	0 0
1.55	0 0	0 0	0 0	0 0
1.56	0 0	0 0	0 0	0 0
1.57	0 0	0 0	0 0	0 0
1.58	0 0	0 0	0 0	0 0
1.59	0 0	0 0	0 0	0 0
1.60	0 0	0 0	0 0	0 0
1.61	0 0	0 0	0 0	0 0
1.62	0 0	0 0	0 0	0 0
1.63	0 0	0 0	0 0	0 0
1.64	0 0	0 0	0 0	0 0
1.65	0 0	0 0	0 0	0 0
1.66	0 0	0 0	0 0	0 0
1.67	0 0	0 0	0 0	0 0
1.68	0 0	0 0	0 0	0 0
1.69	0 0	0 0	0 0	0 0
1.70	0 0	0 0	0 0	0 0
1.71	0 0	0 0	0 0	0 0
1.72	0 0	0 0	0 0	0 0
1.73	0 0	0 0	0 0	0 0
1.74	0 0	0 0	0 0	0 0
1.75	0 0	0 0	0 0	0 0
1.76	0 0	0 0	0 0	0 0
1.77	0 0	0 0	0 0	0 0
1.78	0 0	0 0	0 0	0 0
1.79	0 0	0 0	0 0	0 0
1.80	0 0	0 0	0 0	0 0
1.81	0 0	0 0	0 0	0 0
1.82	0 0	0 0	0 0	0 0
1.83	0 0	0 0	0 0	0 0
1.84	0 0	0 0	0 0	0 0
1.85	0 0	0 0	0 0	0 0
1.86	0 0	0 0	0 0	0 0
1.87	0 0	0 0	0 0	0 0
1.88	0 0	0 0	0 0	0 0
1.89	0 0	0 0	0 0	0 0
1.90	0 0	0 0	0 0	0 0
1.91	0 0	0 0	0 0	0 0
1.92	0 0	0 0	0 0	0 0
1.93	0 0	0 0	0 0	0 0
1.94	0 0	0 0	0 0	0 0
1.95	0 0	0 0	0 0	0 0
1.96	0 0	0 0	0 0	0 0
1.97	0 0	0 0	0 0	0 0
1.98	0 0	0 0	0 0	0 0
1.99	0 0	0 0	0 0	0 0
2.00	0 0	0 0	0 0	0 0
SUBTOTAL	0 0	0 0	0 0	0 0

~~TOP SECRET~~

- CONTROL NO.

Table A-4

~~TOP SECRET~~

CONTROL NO.

MISSION * 1034-2 * INSTRUMENT * AFT

8/25/66 DENSITY FREQ DISTR

DENSITY VALUE	PRIMARY MIN MAX LIM	INTERMEDIATE MIN MAX LIM	FULL MIN MAX LIM	ALL LEVELS MIN MAX LIM
2.01	0	0	0	0 0
2.02	0	0	0	0 0
2.03	0	0	0	0 0
2.04	0	0	0	0 0
2.05	0	0	0	0 0
2.06	0	0	0	0 0
2.07	0	0	0	0 0
2.08	0	0	0	0 0
2.09	0	0	0	0 0
2.10	0	0	0	0 0
2.11	0	0	0	0 0
2.12	0	0	0	0 0
2.13	0	0	0	0 0
2.14	0	0	0	0 0
2.15	0	0	0	0 0
2.16	0	0	0	0 0
2.17	0	0	0	0 0
2.18	0	0	0	0 0
2.19	0	0	0	0 0
2.20	0	0	0	0 0
2.21	0	0	0	0 0
2.22	0	0	0	0 0
2.23	0	0	0	0 0
2.24	0	0	0	0 0
2.25	0	0	0	0 0
2.26	0	0	0	0 0
2.27	0	0	0	0 0
2.28	0	0	0	0 0
2.29	0	0	0	0 0
2.30	0	0	0	0 0
2.31	0	0	0	0 0
2.32	0	0	0	0 0
2.33	0	0	0	0 0
2.34	0	0	0	0 0
2.35	0	0	0	0 0
2.36	0	0	0	0 0
2.37	0	0	0	0 0
2.38	0	0	0	0 0
2.39	0	0	0	0 0
2.40	0	0	0	0 0
2.41	0	0	0	0 0
2.42	0	0	0	0 0
2.43	0	0	0	0 0
2.44	0	0	0	0 0
2.45	0	0	0	0 0
2.46	0	0	0	0 0
2.47	0	0	0	0 0
2.48	0	0	0	0 0
2.49	0	0	0	0 0
2.50	0	0	0	0 0
SUM TOTAL	0	0	148	16 210

~~TOP SECRET~~

CONTROL NO.

Table A-4

~~TOP SECRET~~

CONTROL NO.

MISSION * 1034-2 * INSTRUMENT * APT 8/25/66 DENSITY FREQ DISTR

DENSITY VALUE	PRIMARY			INTERMEDIATE			FULL			ALL LEVELS		
	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM
2.51	0	C	0	0	0	0	0	0	0	0	0	0
2.52	00	C	00	00	00	00	00	00	00	00	00	00
2.53	000	C	000	000	000	000	000	000	000	000	000	000
2.54	0000	C	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000
2.55	00000	C	00000	00000	00000	00000	00000	00000	00000	00000	00000	00000
2.56	000000	C	000000	000000	000000	000000	000000	000000	000000	000000	000000	000000
2.57	0000000	C	0000000	0000000	0000000	0000000	0000000	0000000	0000000	0000000	0000000	0000000
2.58	00000000	C	00000000	00000000	00000000	00000000	00000000	00000000	00000000	00000000	00000000	00000000
2.59	000000000	C	000000000	000000000	000000000	000000000	000000000	000000000	000000000	000000000	000000000	000000000
2.60	0000000000	C	0000000000	0000000000	0000000000	0000000000	0000000000	0000000000	0000000000	0000000000	0000000000	0000000000
2.61	00000000000	C	00000000000	00000000000	00000000000	00000000000	00000000000	00000000000	00000000000	00000000000	00000000000	00000000000
2.62	000000000000	C	000000000000	000000000000	000000000000	000000000000	000000000000	000000000000	000000000000	000000000000	000000000000	000000000000
2.63	0000000000000	C	0000000000000	0000000000000	0000000000000	0000000000000	0000000000000	0000000000000	0000000000000	0000000000000	0000000000000	0000000000000
2.64	00000000000000	C	00000000000000	00000000000000	00000000000000	00000000000000	00000000000000	00000000000000	00000000000000	00000000000000	00000000000000	00000000000000
2.65	000000000000000	C	000000000000000	000000000000000	000000000000000	000000000000000	000000000000000	000000000000000	000000000000000	000000000000000	000000000000000	000000000000000
2.66	0000000000000000	C	0000000000000000	0000000000000000	0000000000000000	0000000000000000	0000000000000000	0000000000000000	0000000000000000	0000000000000000	0000000000000000	0000000000000000
2.67	00000000000000000	C	00000000000000000	00000000000000000	00000000000000000	00000000000000000	00000000000000000	00000000000000000	00000000000000000	00000000000000000	00000000000000000	00000000000000000
2.68	000000000000000000	C	000000000000000000	000000000000000000	000000000000000000	000000000000000000	000000000000000000	000000000000000000	000000000000000000	000000000000000000	000000000000000000	000000000000000000
2.69	0000000000000000000	C	0000000000000000000	0000000000000000000	0000000000000000000	0000000000000000000	0000000000000000000	0000000000000000000	0000000000000000000	0000000000000000000	0000000000000000000	0000000000000000000
2.70	00000000000000000000	C	00000000000000000000	00000000000000000000	00000000000000000000	00000000000000000000	00000000000000000000	00000000000000000000	00000000000000000000	00000000000000000000	00000000000000000000	00000000000000000000
SUBTOTAL	C	C	0	0	0	0	0	0	0	0	0	0
TOTAL	C	C	0	.88	88	80	167	167	165	255	255	245

MISSION 1034-2 INSTR - FRWD 8/25/66 PROCESSING AND EXPOSURE ANALY

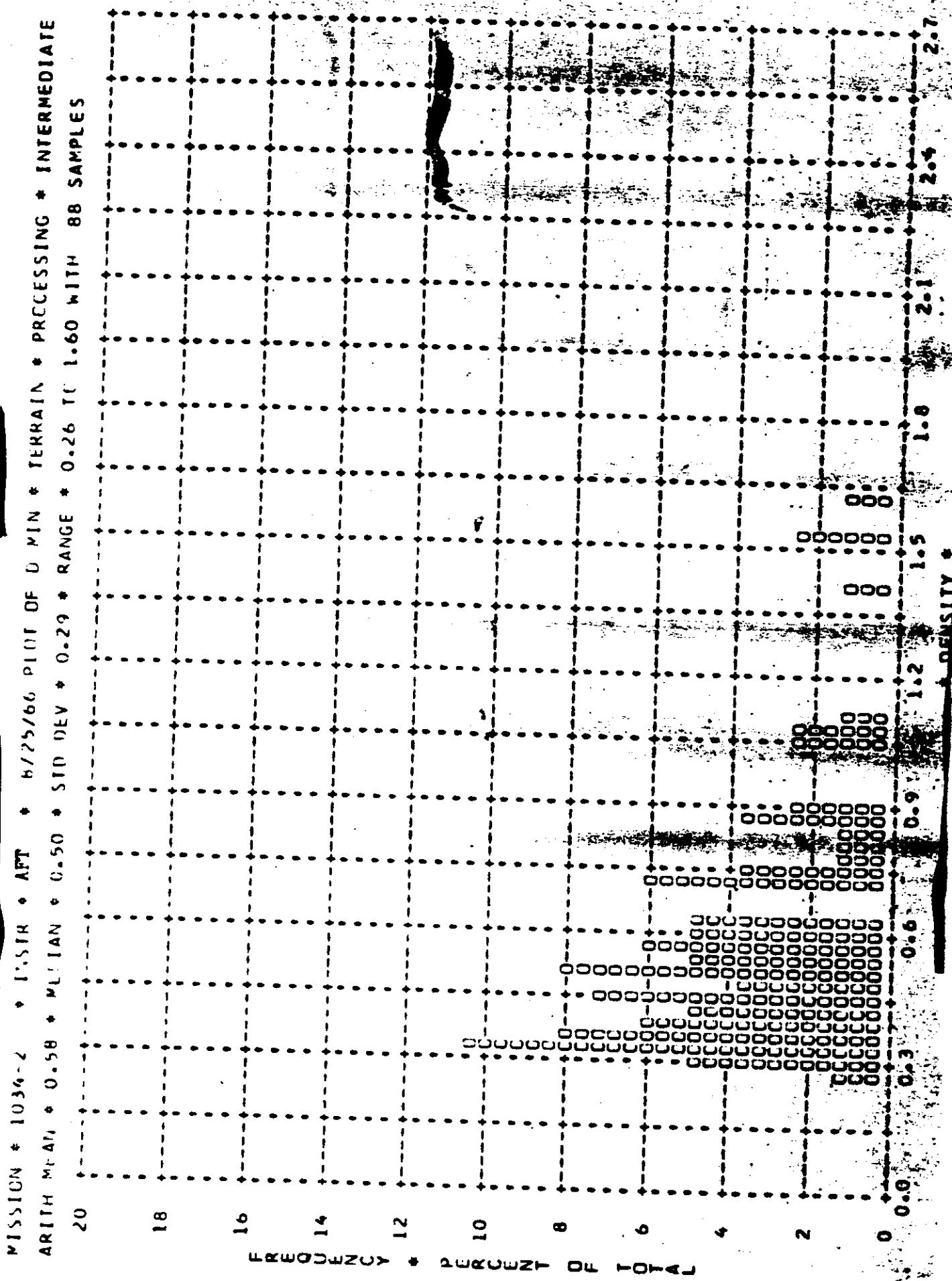
PROCESS LEVEL	SAMPLE SIZE	UNDER EXPOSED		UNDER PROCESSED		CORRECT EXP+PROC		OVER PROCESSED		OVER EXPOSED	
		PC	PC	PC	PC	PC	PC	PC	PC	PC	PC
PRIMARY	0	0	0	0	0	0	0	0	0	0	0
INTERMEDIATE	88	0	0	30	30	0	0	0	0	0	0
FULL	167	18	18	0	0	60	60	6	6	3	3
ALL LEVELS	255	12	12	10	10	80	80	2	2	0	0
PROCESS LEVEL	EASE + FCG	UNDER EXPOSED	UNDER PROCESSED	CORRECT EXP+PROC	OVER PROCESSED	OVER EXPOSED	OVER EXPOSED	OVER EXPOSED	OVER EXPOSED	OVER EXPOSED	OVER EXPOSED
PRIMARY	0.01-0.09	0.01-0.13	0.14-0.39	0.40-0.90	-----	-----	-----	-----	-----	0.91	AND
INTERMED	0.10-0.17	0.01-0.20	0.21-0.39	0.40-0.90	0.91-1.34	1.35	1.35	1.35	1.35	1.70	AND
FULL	0.18 AND UP	0.01-0.39	-----	0.40-0.90	0.91-1.69	1.70	1.70	1.70	1.70	1.70	AND

~~TOP SECRET~~

CONTROL NO.

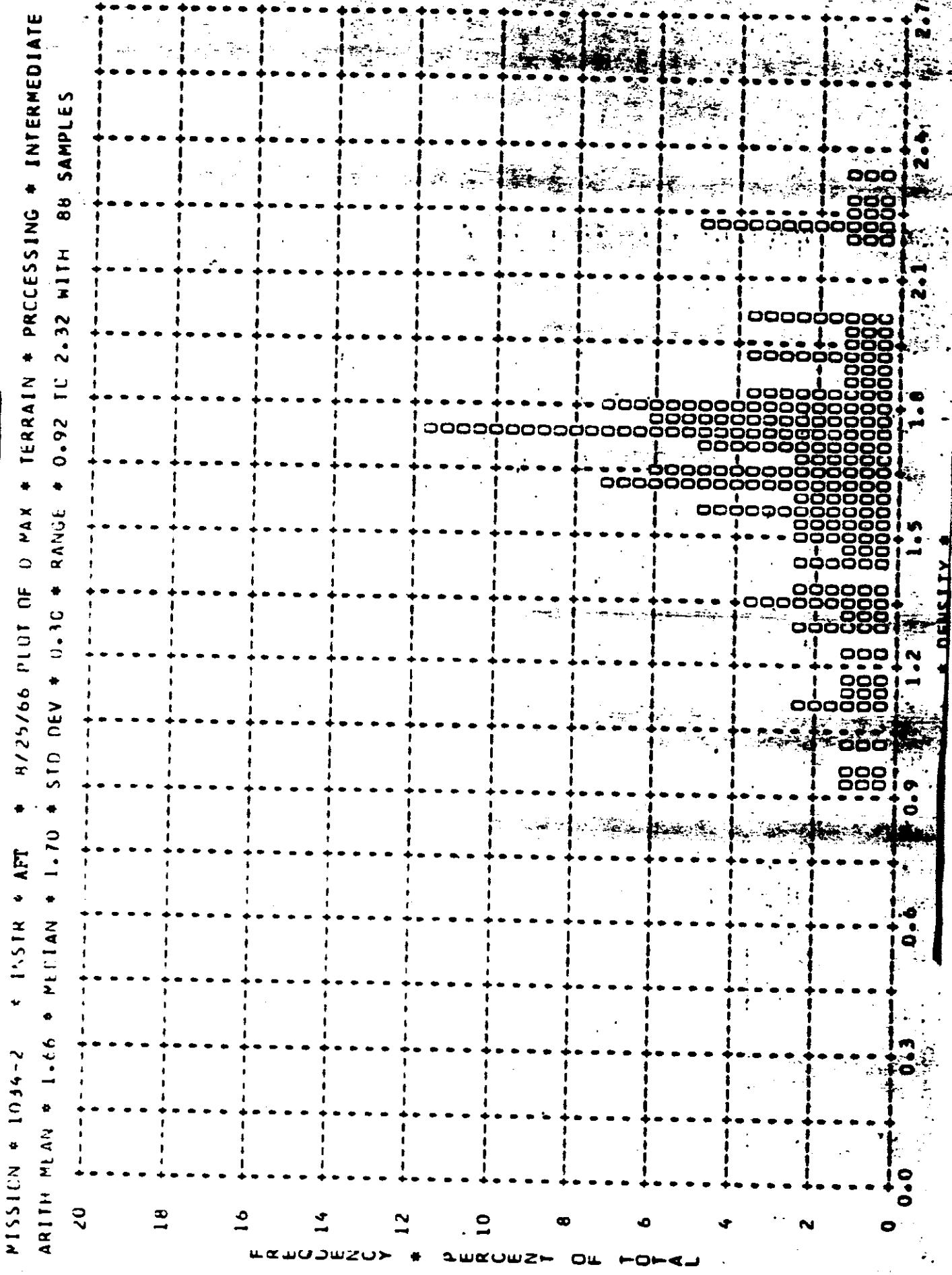
Table A-4

CONTROL NO.



TRANSMITTER

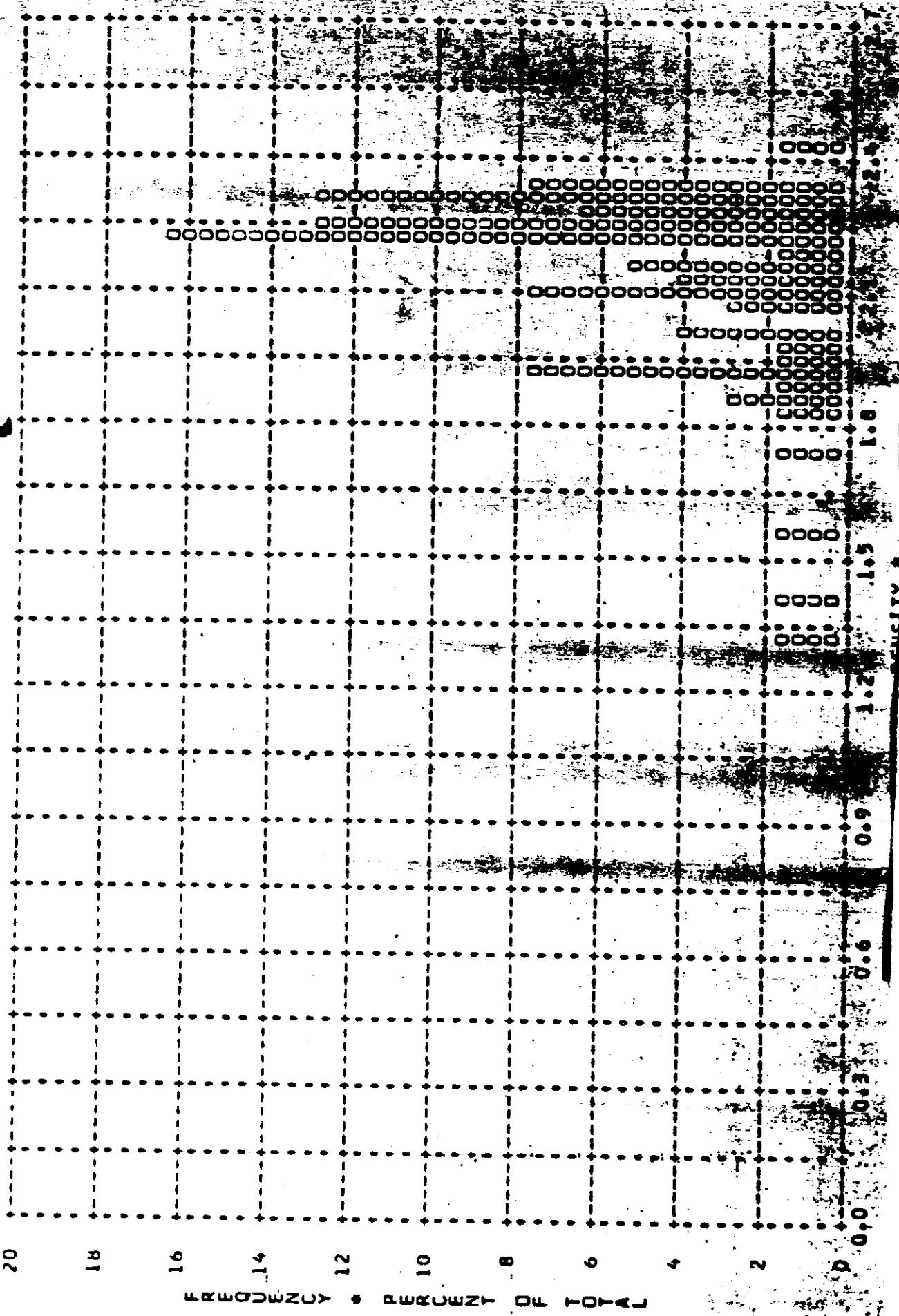
- CONTROL NO.



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- CONTROL NO.

MISSION * 1034-2 * LASTR * AFT * 8/25/66 PILOT OF D MAX * CLOUD * PROCESSING * INTERMEDIATE
ARITH MFLY * 2.13 * MILLIAN * 2.20 * STD DEV * 0.21 * RANGE * 1.32 TC 2.41 WITH 80 SAMPLES



- CONTROL NO.

MISSION * 1044 * INSTR * APT * A/25/66 PLOT OF 0 MIN * TERRAIN * PROCESSING * FULL
ARITH MEAN * 0.51 * MEDIAN * 0.49 * STD DEV * 0.15 * RANGE * 0.29 TO 1.48 WITH 167 SAMPLES

18

16

14

12

10

8

6

4

2

0

0.0

0.3

0.6

0.9

1.2

1.5

1.8

2.1

2.4

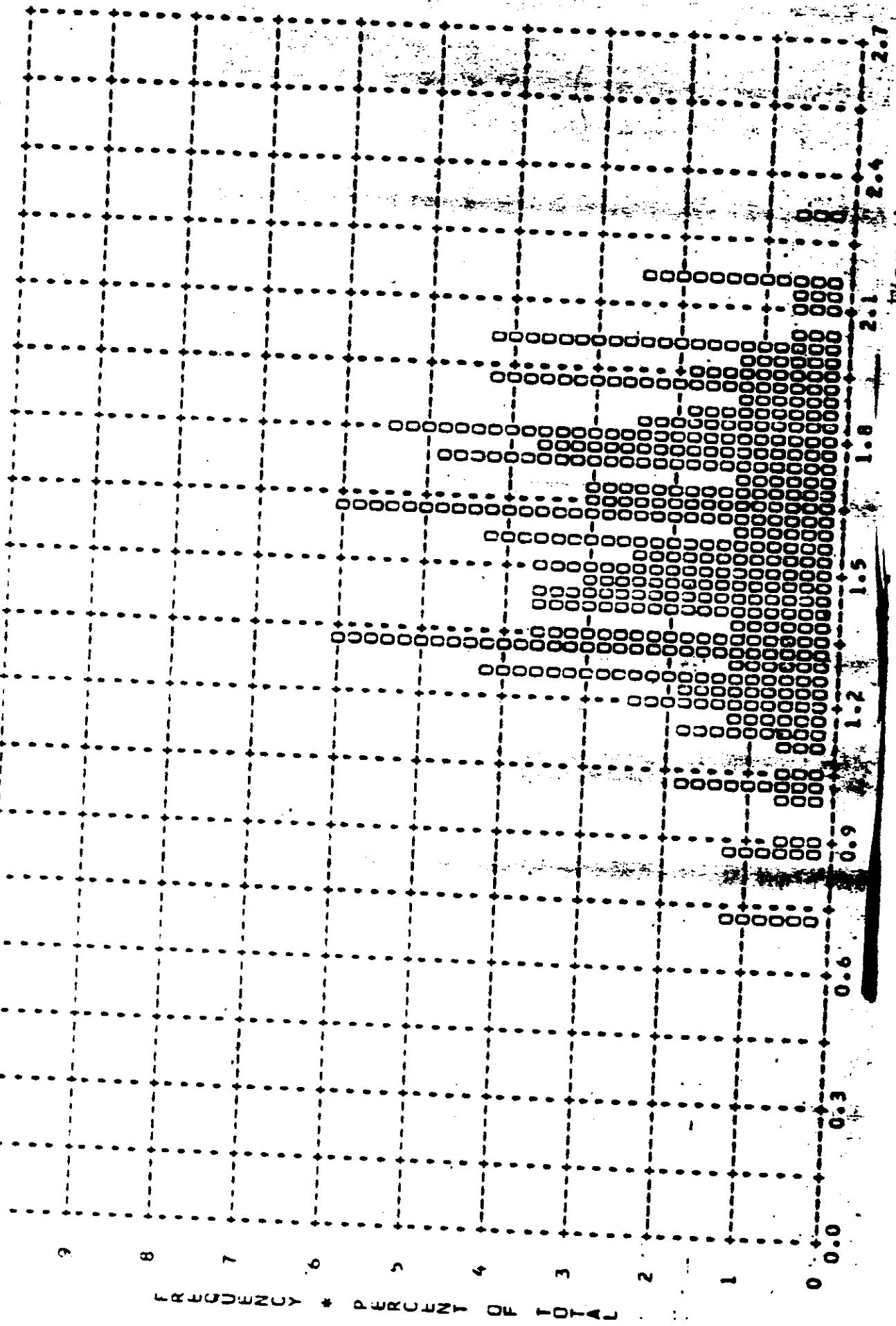
2.7

FREQUENCY * PERCENT OF TOTAL

~~TRANSMITTER~~

- CONTROL NO.

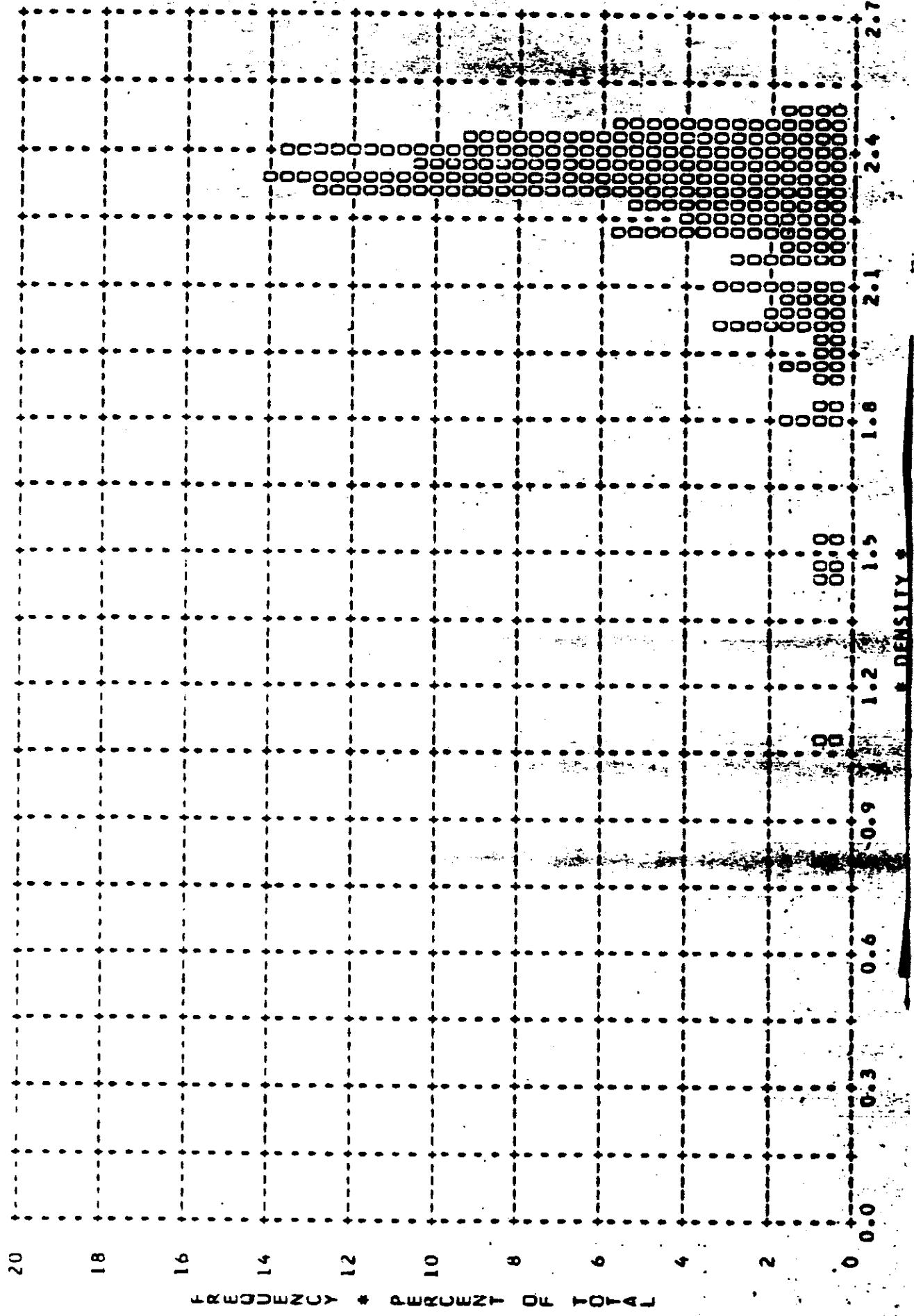
MISSION # 1014-2 * LAST * AFT * 8/25/66 PLUT UF 0 MAX * TERRAIN * PROCESSING * FULL
ARLIN STAN * 1.56 * MILLIAN * 1.56 * FID DFV * 0.31 * RANGE * 0.70 TO 2.30 WITH 167 SAMPLES



- CONTROL NO.

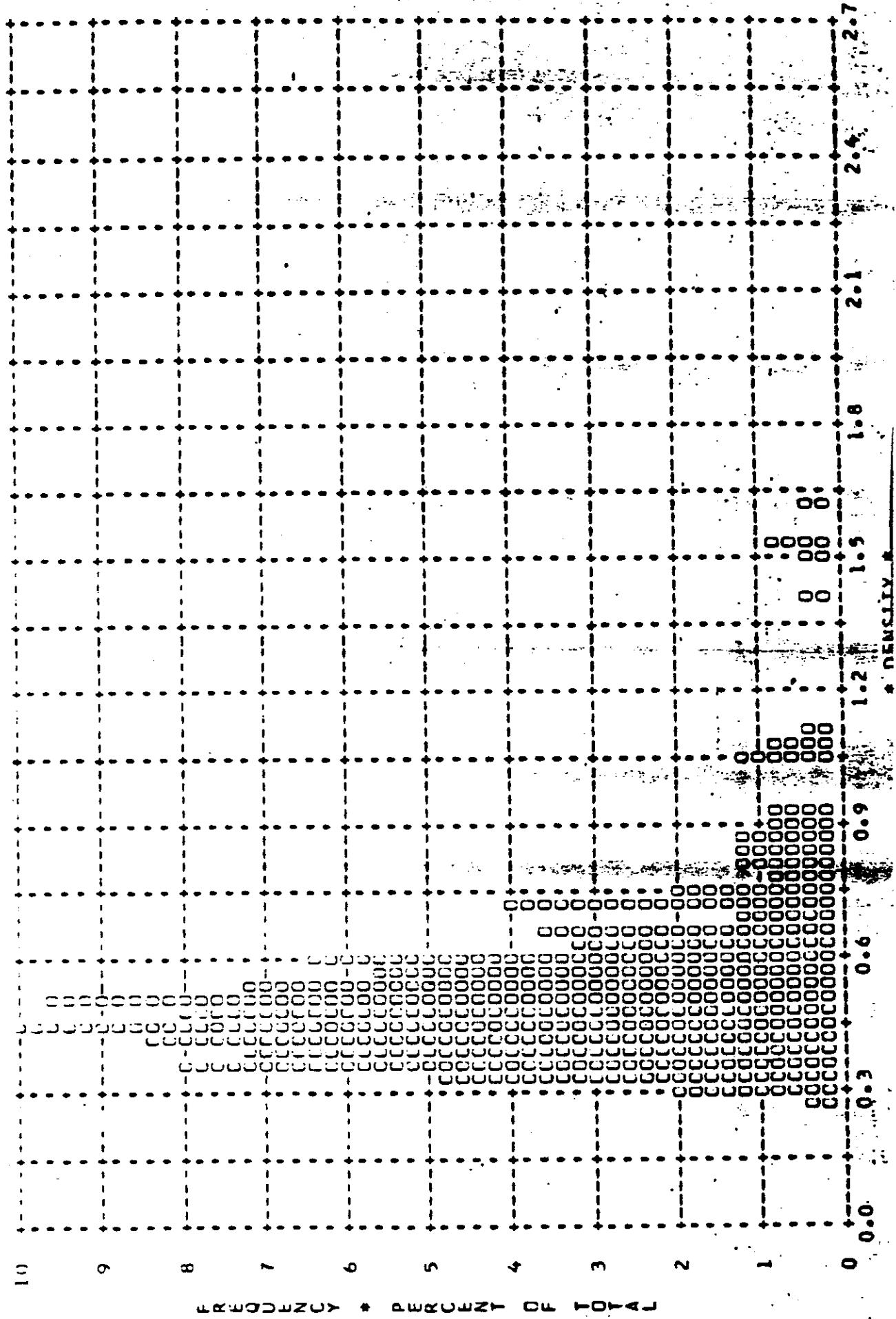
- TEST NO.

MISSION * 1034-2 * INSTR * AFT * H75/66 PLOT OF U MAX * CLOUD * PROCESSING * FULL
ARITH MEAN * 2.26 * MEDIAN * 2.32 * STD DEV * 0.20 * RANGE * 1.08 TU 2.48 WITH 165 SAMPLES

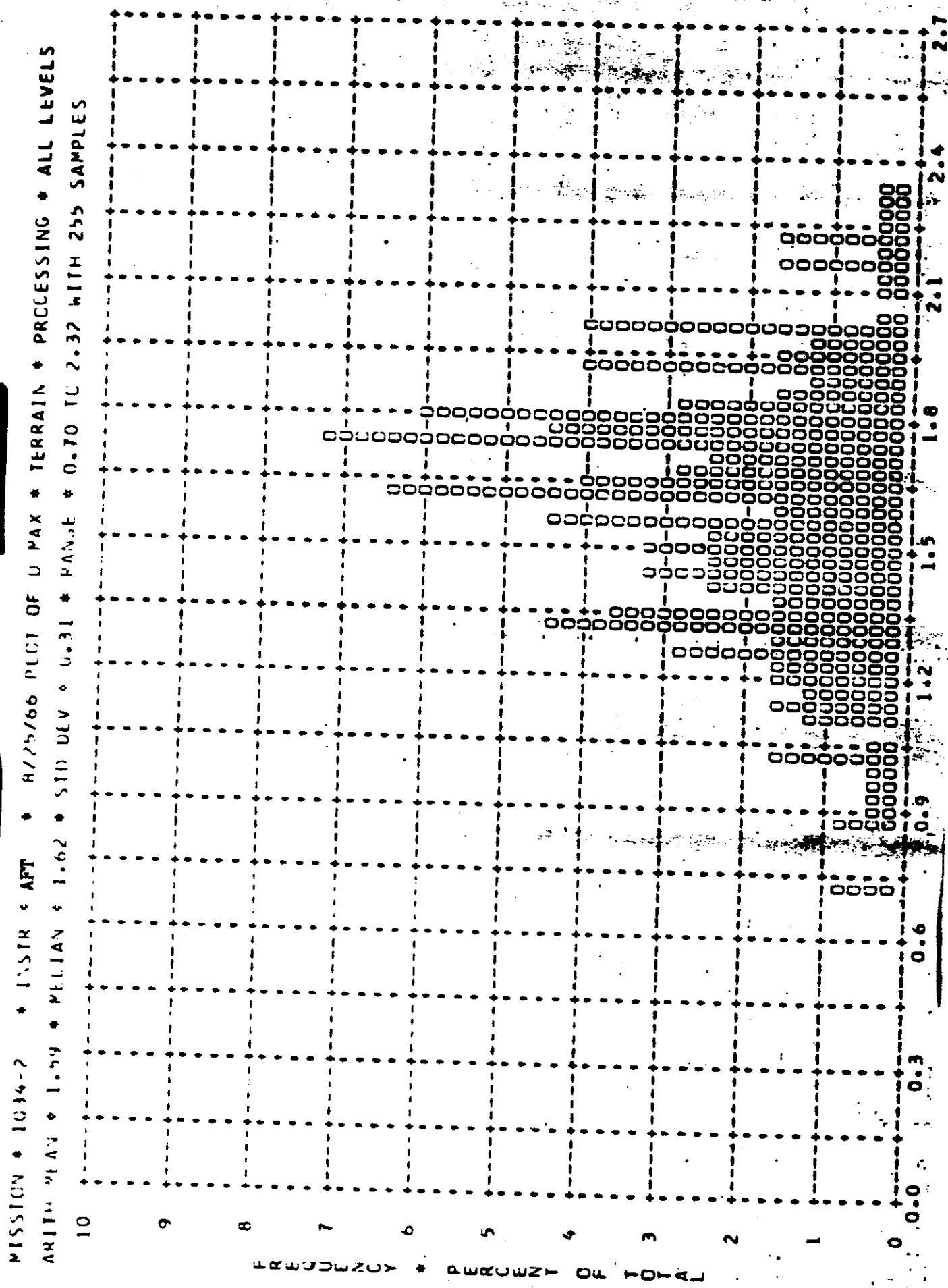


- CONTROL NO.

MISSION # 1014-2 * INSTR * AFT * 6/25/66 PLOT OF WIN * TERRAIN * PROCESSING * ALL LEVELS
ARITH. MEAN * 0.54 * MEDIAN * 0.49 * STD DEV * 0.21 * RANG * 0.26 TO 1.60 WITH 255 SAMPLES

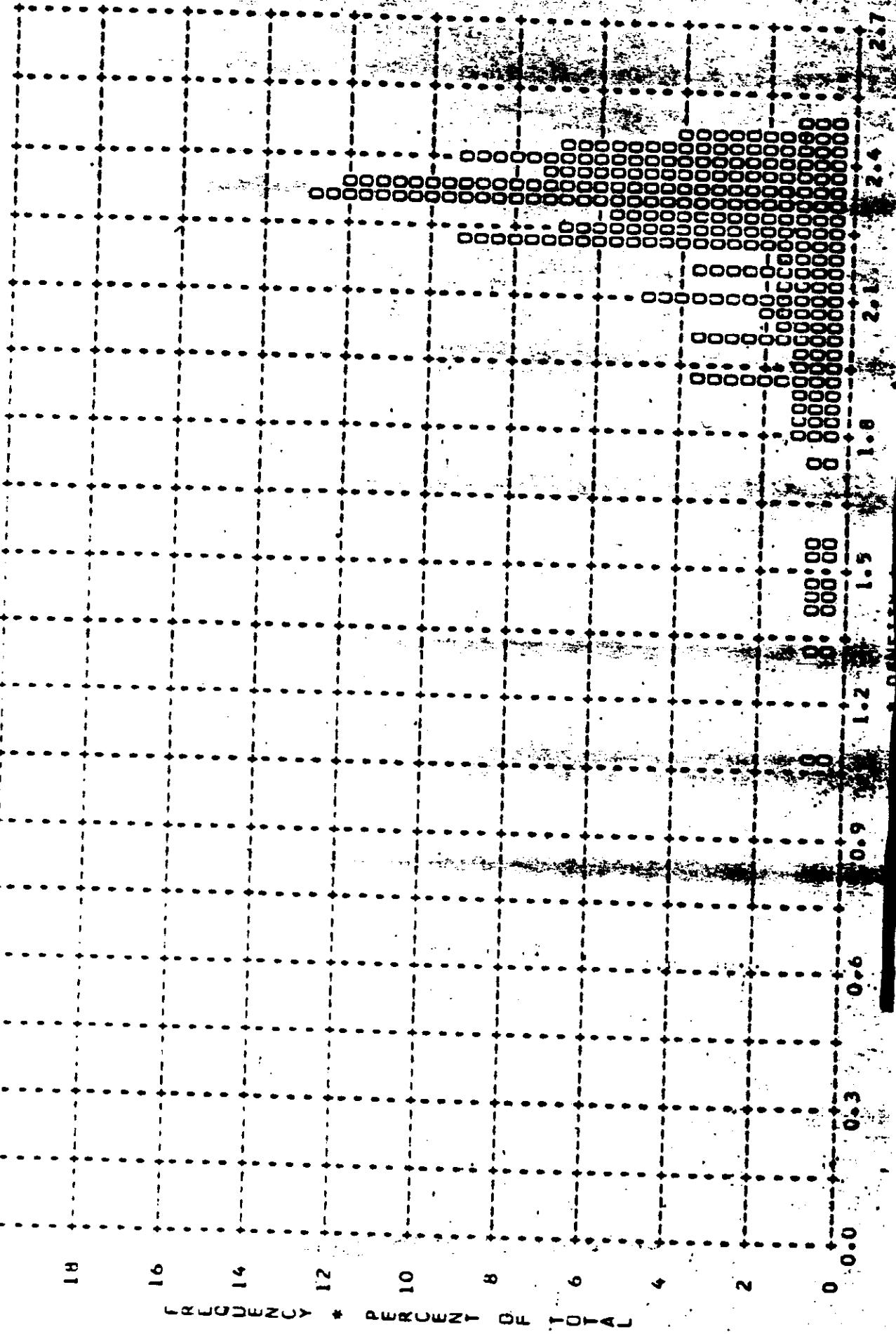


- CONTROL NO.



CONTROL N.U.

MISSION # 1049 * INSTR * AFT * H/25/66 PLINT OF D MAX * CLOUU * PROCESSING * ALL LEVELS
AUXILIARY STAN # 2.22 * MILITAN # 2.29 * STD DEV # 0.21 * KANGI # 1.08 TO 2.48 WITH 245 SAMPLES



TOP SECRET C [REDACTED]

Distribution:

Copy No.

To

[REDACTED]
[REDACTED]
[REDACTED]
[REDACTED]
[REDACTED]
[REDACTED]
[REDACTED]
[REDACTED]
[REDACTED]
[REDACTED]

TOP SECRET C [REDACTED]