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CORONA J

PERFORMANCE EVALUATION REPORT

MISSION 1041-1 and 1041-2

FTV 1634, J-4C

14 December 1967

Declassified and Released by the NRO

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Approved: [REDACTED]

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Manager
Advanced Projects

Approved: [REDACTED]

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Program Manager

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No.

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9 January 1968

TO:

THRU:

FROM:

SUBJECT: MISSION 1041-1 and 1041-2 FINAL REPORT(J-40)

Enclosed is the Final Evaluation Report for
Mission 1041-1 and 1041-2.

[REDACTED]
Manager
Advanced Projects

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FOREWORD

This report details the performance of the payload system during the operational phase of the Program [redacted] Flight Test Vehicle 1634.

Lockheed Missiles and Space Company has the responsibility for evaluating payload performance under the Level of Effort and "J" System contracts.

This document is the final payload test and performance evaluation report for Missions 1041-1 and 1041-2, system J-40 which was launched on 9 May 1967.

TABLE OF CONTENTS

| | Page |
|------------------------------------------------|------|
| TITLE PAGE | |
| FOREWORD | i |
| TABLE OF CONTENTS | ii |
| LIST OF TABLES | iii |
| LIST OF ILLUSTRATIONS | iv |
| INTRODUCTION | 1 |
| SECTION 1 - SYSTEM PERFORMANCE | 2 |
| SECTION 2 - PRE-FLIGHT SYSTEMS TEST | 5 |
| SECTION 3 - FLIGHT OPERATIONS | 9 |
| SECTION 4 - MISSION 1041 RECOVERY SYSTEMS | 13 |
| SECTION 5 - MISSION 1041 PANORAMIC CAMERAS | 15 |
| SECTION 6 - MISSION 1041 STELLAR-INDEX CAMERAS | 18 |
| SECTION 7 - PANORAMIC CAMERA EXPOSURE | 20 |
| SECTION 8 - PERFORMANCE MEASUREMENTS | 31 |
| SECTION 9 - DIFFUSE DENSITY MEASUREMENTS | 32 |
| SECTION 10 - VEHICLE ATTITUDE | 36 |
| SECTION 11 - IMAGE SMEAR ANALYSIS | 49 |
| SECTION 12 - RELIABILITY | 67 |
| SECTION 13 - SUMMARY DATA | 72 |
| SECTION A - APPENDIX | 81 |

LIST OF TABLES

| <u>Table</u> | | <u>Page</u> |
|--------------|------------------------------------------------|-------------|
| 4-1 | Mission 1041 Recovery Sequences | 14 |
| 9-1 | Processing - Exposure Summary | 34 |
| 11-1 | Mission 1041 V/H Ratio and Resolution Limits | 50 |
| 12-1 | Estimated Reliability Summary | 69-71 |
| 13-1 | Mission Summary | 73-74 |
| 13-2 | Performance Summary | 75-77 |
| 13-3 | Exposure - Processing Summary | 78-80 |
| A-1 | Mission 1041-1 FWD Camera Density Distribution | A1-A6 |
| A-2 | Mission 1041-1 AFT Camera Density Distribution | A16-A21 |
| A-3 | Mission 1041-2 FWD Camera Density Distribution | A31-A36 |
| A-4 | Mission 1041-2 AFT Camera Density Distribution | A46-A51 |

LIST OF ILLUSTRATIONS

| <u>Figure</u> | | <u>Page</u> |
|---------------|-----------------------------------------------------------|-------------|
| 1-1 | Mission 1041 Inboard Profile | 4 |
| 7-1 | Mission 1041-1 Solar Elevations | 21 |
| 7-2 | Mission 1041-1 Solar Azimuth | 22 |
| 7-3 | Mission 1041-2 Solar Elevations | 23 |
| 7-4 | Mission 1041-2 Solar Azimuth | 24 |
| 7-5 to 7-10 | Nominal Exposure Points | 25-30 |
| 9-1 | Density Range Charts | 35 |
| 10-1 to 10-6 | Mission 1041-1 Attitude Angle & Rate Error Distributions | 37-42 |
| 10-7 to 10-12 | Mission 1041-2 Attitude Angle & Rate Error Distributions | 43-48 |
| 11-1 to 11-8 | Mission 1041-1 V/H Error & Resolution Limits Distribution | 51-58 |
| 11-9 to 11-16 | Mission 1041-2 V/H Error & Resolution Limits Distribution | 59-66 |
| A-1 to A-9 | Mission 1041-1 FWD Camera Density Distribution Plots | A7-A15 |
| A-10 to A-18 | Mission 1041-1 AFT Camera Density Distribution Plots | A22-A30 |
| A-19 to A-27 | Mission 1041-2 FWD Camera Density Distribution Plots | A37-A45 |
| A-28 to A-36 | Mission 1041-2 AFT Camera Density Distribution Plots | A52-A60 |

INTRODUCTION

This report presents the final performance evaluation of Missions 1041-1 and 1041-2 of the Corona Program. The purpose of this report is to define the performance characteristics of the J-40 payload system and to identify the source of in-flight anomalies.

The performance evaluation was jointly conducted by representatives of Lockheed Missiles and Space Company (LMSC) and AFKK at the facilities of NPIIC and AFSPFF. The off-line evaluation using Corona engineering photography acquired over the United States was performed at the individual contractors plants.

The quantitative data used for this report is obtained from government organizations. The diffuse density data, and MTF/MTV resolution are produced by AFSPFF. The vehicle attitude error values, frame correlation times are made at NPIIC who also supply the Processing Summary reports published by [REDACTED].

Computer programs developed by A/F are utilized to calculate and plot the frequency distribution of the various contributors to image smear to permit analysis and correlation of the conditions of photography to the information content and quality of the acquired pictures. Computer analysis of the exposure, processing and illumination data provides the necessary data to analyze the exposure criteria selected for the mission.

SECTION 1

SYSTEM PERFORMANCE

A. MISSION OBJECTIVES

The payload section of Mission 1041, placed into orbit by Flight Test Vehicle #1634 and THORAD Booster #506, consisted of two panoramic cameras, two Stellar-Index cameras, two Mark 5A recovery capsules and a space structure to enclose the cameras and provide mounting surfaces for all equipment. Figure 1-1 presents an inboard profile of the J-40 payload system. This Corona "J" system is designed to acquire search and reconnaissance photography of selected areas of the earth from orbital altitudes. A seven day -1 mission and a seven day -2 mission was planned.

B. MISSION DESCRIPTION

The payload was launched from Vandenberg Air Force Base (VAFB) at 2152 Z (1452 PDT) on 9 May 1967. Ascent and injection were normal and the achieved orbit was within nominal tolerances. Tracking and command support was effected by the Air Force Satellite Control Facility consisting of tracking and command stations at [REDACTED]

[REDACTED] under central control of the Satellite Test Center at Sunnyvale, California. Mission 1041-1 consisted of a 7 day operation and was completed by air recovery on 16 May 1967. Mission 1041-2 was completed with an air recovery on 23 May 1967 following a 7 day photographic operation.

The comparison of the planned and actual orbit parameters is tabulated as follows:

ORBITAL PARAMETERS

| <u>Parameter</u> | <u>Predicted</u> | <u>Orbit 45 Actuals</u> | <u>Orbit 150 Actuals</u> |
|----------------------------|------------------|-----------------------------|------------------------------|
| Period (Min.) | 91.04 | 94.35 | 94.21 |
| Perigee (N.M.) | 99.8 | 101.1 | 103.2 |
| Apogee (N.M.) | 256 | 430.65 | 430 |
| Inclination (Deg.) | 85 | 85.05 | 85.05 |
| Perigee Latitude (Deg. N.) | 28.6 | 32.9 | 37.9 |
| Eccentricity | 0.0216 | 0.0446 | 0.0441 |

C. PANORAMIC CAMERAS

The photography was rated good by the photo-interpreters. Both cameras operated satisfactorily.

D. STELLAR-INDEX CAMERAS

There were no significant anomalies in the operation of either unit. The base plus fog densities were higher due to radiation in an unusually high apogee. The images were adequate for attitude determinations.

E. RADIATION

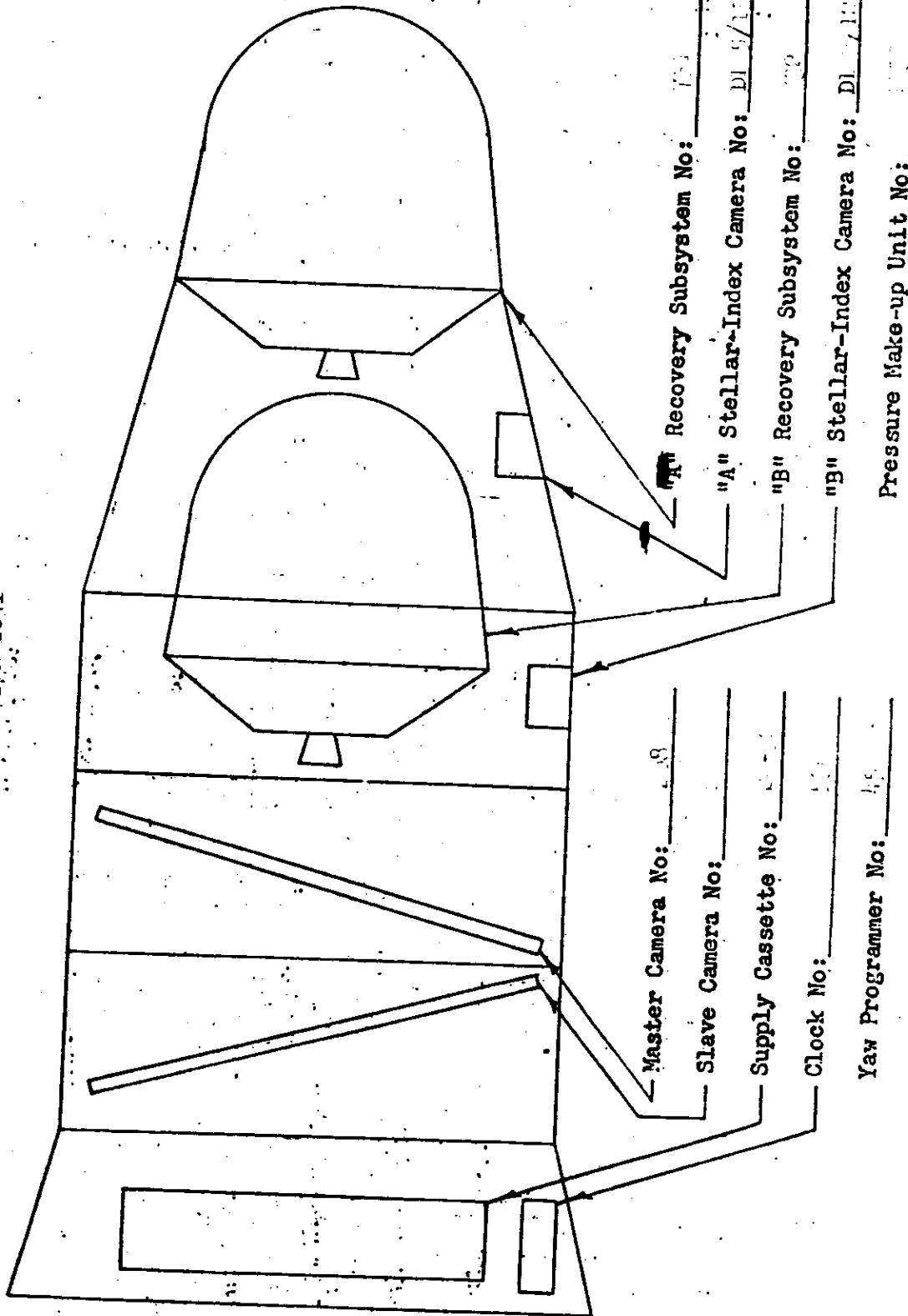
| <u>Emulsion</u> | Mission 1041-1 | | Mission 1041-2 | |
|-----------------|----------------|------------------|----------------|------------------|
| | <u>B + F</u> | <u>Density</u> | <u>B + F</u> | <u>Density</u> |
| | | <u>Radiation</u> | | <u>Radiation</u> |
| Type 3401 | 0.49 | 4.8 R | 0.64 | 7.6 R |
| Royal X Pan | 0.70 | 2.6 R | 0.80 | 3.3 R |

F. OTHER SUBSYSTEMS

The clock instrumentation, command, thermalcontrol, pressure make-up, and recovery subsystems performed satisfactorily.

SCHEMATIC INBOARD PROFILE - CORONA J SYSTEM J-10

MISSION 1041



SECTION 2

PRE-FLIGHT SYSTEMS TESTS

A. ENVIRONMENTAL TESTING

1. Test Objective

As a standard procedure, the J payload systems are subjected to thermal/altitude environmental testing which simulates orbital environment. One of the purposes of this test is to demonstrate the system susceptibility to corona discharge. Such discharge fogs the film thus degrading the operational photography.

2. Test Summary

The J-40 HIVOS test was conducted from 3 August to 10 August 1966. During this time 5638 frames were run into the "A" bucket and 4467 frames into the "B" bucket. The lowest pressure attained was one micron.

The pan films exhibited very slight start-up corona on 4 frames.

The last 200 frames on instrument 209 did not indicate any output H.O. shutter operation. The absence of fogging was probably a bulb failure in the fogging fixture since the TM monitor showed a shutter pulse. To conform to a FEWO #1028 the H.O. units were replaced on this instrument.

The S/I unit #102 did not qualify for flight due to excessive corona, marking and double exposures.

Failsafe occurred in instrument No. 2 in Rev No. 10 of the "E" bucket. Malfunction investigation was inconclusive. Due to failsafe, vehicle deactivate sequence was not performed.

Instrumentation performance was satisfactory.

The cycle rates of the two instruments were one and one-half percent apart during entire test. The Master and Slave cycle counter agreed with actual count.

The -1 Stellar/Index monitor performance was normal.

The -2 Stellar/Index monitor was satisfactory. However, there was one missed meter and two shutter pulse failures in Rev. 10.

Clock accuracy was satisfactory.

The pressure make-up system operated normally. Gas consumption, however, was too high at 9.45 PSI/Min. During PMU operates, internal pressure increased to 40-44 microns.

The command system operated normally. The V/H delay stepper failed to home on one rev. This was due to the command not being held in long enough. In Rev 10 of "A" bucket, the V/H programmer failed to start due to improper number of Br. 27 commands being issued.

Transfer from -1 to -2 was commanded by KZ-38. All transfer functions occurred normally.

The orbital sine function generator (O.S.F.G.) operated normally in both missions.

B. RESOLUTION TEST

Resolution and theodolite tests were performed on 2 September 1966. Results of the thru-focus resolution tests of pan instruments 208 and 209 showed the following characteristics:

Master Pan Instrument No. 208

Maximum high contrast resolution 178 lines/mm at 0.000 focal position.

Maximum low contrast resolution 111 lines/mm at 0.000 focal position.

Slave Instrument No. 209

Maximum high contrast resolution 187 lines/mm at 0.000 focal position.

Maximum low contrast resolution 112 lines/mm at 0.000 focal position.

C/ [REDACTED] NO. [REDACTED]

Both instruments met the system requirements specification.

C. LIGHT LEAK TEST

The J-40 system was tested for light leaks on 7 August 1966. A pin hole was found and repaired on one of the Slave instrument H.O. boots. A light search then proved the system to be acceptable.

D. FLIGHT LOADING AND CERTIFICATION

The first Flight Readiness test of Panoramic Instrument #208 and 209 was completed on 3 May 1967. Excessive emulsion build up was noted in the processed imagery of the platen shrinkage markers and along the format edges of both instruments. Instrument #208 and 209 were cleaned and a second Flight Readiness test was conducted on 2 May 1967. Examination of the processed 3404 type film from both panoramic instruments revealed acceptable camera performance including clean format and shrinkage markers, tracking, normal rail scratches, horizon fiducials and shutter function, time track, serial number, binary index marks, and binary word.

Processed film exhibits from Stellar/Index cameras D-101 and D-102 demonstrated acceptable performance. Both Stellar cameras produced good reseau, fiducial, and correlation lamp imagery on film type 3401. Both Index cameras produced good reseau and correlation lamp imagery on film type 3400.

Flight film spools #24T and 13B (Box 50) were placed in the panoramic camera supply cassette but were removed and returned to [REDACTED] when it was observed that the film wraps were lightly stuck together principally along one film edge. A/P film storage room temperature was 68°F and 38% RH. Box 50 was transferred to the Flight Loading room for a period of 24 hours before opening Box 50 at a room temperature of 79°F and 40% RH.

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The supply cassette was reloaded with flight film from Box 26 without incident.

The system pre-flight acceptance run was initiated and completed without incidence on 4 May 1967.

Customer review and final J-40 system buy-off was concluded on the afternoon of 4 May 1967.

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SECTION 3

FLIGHT OPERATIONS

A. SUMMARY

FTV 1634 was an Agena Vehicle (SG-01B) and a thrust augmented Thor (LV-2A, S/N 503) booster. This vehicle was configured for tail-first in orbit configuration with a dual recovery capability. Launch occurred from VAFB, Pad SLC-3 at 2152 GMT on 09 May 1967.

This payload system was flown with a new main door assembly, which will be standard equipment on systems J-40 and up. There were no problems connected with this new assembly. The J-40 command system was modified to eliminate the capability of real time command (RTC) 15 to reset the intermix sequence and the 4 step counter (operations counter). There were no operational problems encountered with this change. The remainder of the J-40 payload system conformed to the standard J-1 configuration.

The J-40 payload system was prepared for flight utilizing the full Phase III (Factory to Pad) concept.

Launch, ascent, and injection events occurred as programmed. However, a failure of the velocity meter to shut the Agena engine off resulted in burning fuel to depletion with an orbit period longer than predicted. Thus, the orbit achieved was not within 3 sigma dispersions.

Mean camera operational altitudes were approximately five (5) G.M. higher than nominal.

Instrumentation and command systems operated satisfactorily throughout the flight.

The on-orbit sine function generator (OSFG) and clock system functioned normally for the duration of the mission.

Telemetry data indicated a shutter failure on the Index camera during Rev 213. Otherwise the Stellar/Index system functioned normally.

KIK-ZORRO 59 (early -1 to -2 switchover) was performed on Rev 91 by [REDACTED] and all transfer functions were normal.

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B. PANORAMIC CAMERA PERFORMANCE

Both Panoramic Cameras operated normally throughout the mission. Camera system dynamic operation, 20/101 clutch operation, start-up, clear-down, and transport functions were normal for all gasses monitored. The cut and wrap operation and transfer to the -2 system occurred as programmed utilizing the KIK-ZORRO 38 command (early A to S switchover).

The panoramic film was exhausted on Rev 206 frame 101 on the Master and Rev 213 frame 3 on the Slave.

Panoramic Film Consumption (Frames)

| | <u>Actual</u> | |
|------------|---------------|--------------|
| | <u>Master</u> | <u>Slave</u> |
| Pre-Launch | 105 | 114 |
| -1 Mission | 2938 | 2920 |
| -2 Mission | 2995 | 3004 |
| Total | 6038 | 6038 |

FMC Match

The initial orbit dispersion affected instrument operations in several areas. The FMC ramps utilized on this mission were never designed for orbits as eccentric as encountered on this flight. It was also necessary to bias the H-Timer to place the programmed operations over the desired targets.

Operations that were taken on the pre-flight FMC ramp settings prior to adequate orbit determination were at altitudes that were 20 to 30 per cent higher than nominal.

There were some operations taken on the wrong point on the FMC ramp after adequate orbit determination had been accomplished. These operations were on orbits on which the H-Timer was biased after the FMC ramp had started.

The actual ground tracks were moving west from the nominal ground track at a rate of 50 nautical miles (N.M.) per orbit at the equator. It was possible to compensate for this longitudinal misalignment by slewing the H-Timer in 1356 N.M. steps. Longitudinal alignment errors of up to 700 N.M. at the equator were encountered.

Latitudinal mismatch of as much as four (4) degrees were encountered even when the H-Timer was synchronized with the orbit. This resulted in biasing the H-Timer even though no longitudinal misalignment existed.

The mean altitudes of the camera operations were approximately 5 N.M. higher than nominal.

C. INSTRUMENTATION AND COMMAND SYSTEM PERFORMANCE

The command system was satisfactory for both missions. This command system was modified to eliminate the capability of resetting the intermix sequence and the four step counter by RTC 15. There were no operational problems encountered during the flight with this modification. The only instrumentation anomaly encountered during this mission was the No. 2 EMU temperature sensor which became an open T/M point during the pre-flight loading sequence.

D. CLOCK SYSTEM PERFORMANCE

Clock system operation was normal for the duration of the flight. Satisfactory time correlation between the flight clock and [REDACTED] time was obtained.

E. PRESSURE MAKE-UP SYSTEM PERFORMANCE

Pressure make-up system performance was normal throughout the flight. Average gas consumption was approximately 7.9 PSI/min for the 253 minutes of total operate time. The system had a surplus of 550 PSIA at the end of the mission.

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F. THERMAL ENVIRONMENT

The average instrument temperatures ranged from a high of 87°F to a low of 51°F.

The thermal control paint pattern on the payload system was modified prior to launch.

SECTION 4

MISSION 1041 RECOVERY SYSTEMS

-1 MISSION

The -1 recovery capsule was successfully recovered by air catch on Rev. 93 at 0036 GMT on 16 May 1967. All re-entry events appeared normal and occurred within specified tolerances. Capsule impact was within the nominal 3-sigma dispersion.

| | <u>Latitude</u> | <u>Longitude</u> |
|-----------|-----------------|------------------|
| Predicted | 27° 00'N | 163° 35.6'W |
| Actual | 26° 22'N | 163° 17.0'W |

The re-entry sequence of events is contained in Table 4-1.

-2 MISSION

The -2 recovery capsule was successfully recovered by air catch on Rev. 215 at 0008 GMT on 24 May 1967. Capsule impact was approximately 240 miles down range and 17 miles off track. Post recovery exercises indicated recovery timer events were within specifications. An investigation is continuing to determine the cause or causes of this anomaly.

| | <u>Latitude</u> | <u>Longitude</u> |
|-----------|-----------------|------------------|
| Predicted | 28° 00'N | 169° 42.2'W |
| Actual | 24° 10'N | 169° 46.0'W |

MISSION 1041

RECOVERY SEQUENCE OF EVENTS

| <u>Event</u> | <u>Elapsed Time (Seconds)</u> | | <u>Received</u> |
|-------------------------|-------------------------------|------------------|---------------------|
| | <u>Actual</u> | <u>Estimated</u> | |
| *Arm | 76.81 | N/A | 77.0 ± 1.0 |
| *Transfer | 2.00 | N/A | 2.0 ± 0.25 |
| Electrical Disconnect | 0.81 | N/A | 0.900 ± 0.10 |
| Separation | --- | --- | --- |
| **Spin | 3.42 | N/A | 3.4 ± 0.30 |
| Retro | 7.60 | N/A | 7.55 ± 0.45 |
| Despin | 10.64 | N/A | 10.75 ± 0.54 |
| T/C Separation | 1.49 | N/A | 1.5 ± 0.15 |
| ***"G" Switch Open | 530.36 | N/A | 520.7(-1) 533.6(-2) |
| Parachute Cover Off | 31.4 | 33.35 | 31.0 ± 1.5 |
| Drogue Chute Deployed | 0.65 | 0.60 | 0.63 ± 0.13 |
| Main Chute Bag Separate | 11.47 | 10.80 | 10.0 ± 3.0 |
| Main Chute Deployed | 0.65 | 0.65 | 0.52 ± 0.13 |
| Main Chute Disreef | 4.83 | 4.55 | 4.5 ± 0.80 |

* From Separation

** From Electrical Disconnect

*** From Retro

TABLE 4-1

SECTION 5

MISSION 1041 PANORAMIC CAMERAS

A. COMPONENT ASSIGNMENT

| <u>Component</u> | <u>Master (FWD) Serial Number</u> | <u>Slave (AFT) Serial Number</u> |
|-----------------------------|---------------------------------------|--------------------------------------|
| Main Camera | 208 | 209 |
| Main Camera Lens | 2172435 | 2182435 |
| Supply Horizon Camera | 303G6 | 313G6 |
| Supply Horizon Camera Lens | E12861 | E19101 |
| Take-up Horizon Camera | 289G5 | 313G5 |
| Take-up Horizon Camera Lens | E12866 | E19105 |
| Supply Cassette | SC-52 | SC-52 |

B. CAMERA DATA AND FLIGHT SETTINGS

Main Camera:

| | | |
|------|-----------|-----------|
| Lens | 24" f/3.5 | 24" f/3.5 |
|------|-----------|-----------|

| | | |
|------------|--------|--------|
| Slit Width | 0.225" | 0.175" |
|------------|--------|--------|

| | | |
|-------------|-------------|------------|
| Filter Type | Wratten 23A | Wratten 21 |
|-------------|-------------|------------|

| | | |
|---------------------------|------|------|
| Film Type (Eastman Kodak) | 3404 | 3404 |
|---------------------------|------|------|

Supply Horizon Cameras:

| | | |
|------|------|-----------|
| Lens | Port | Starboard |
|------|------|-----------|

| | | |
|------------------|-------------|-------------|
| Aperture Setting | 55 mm f/6.3 | 55 mm f/6.3 |
|------------------|-------------|-------------|

| | | |
|---------------|-------|-------|
| Exposure Time | f/6.3 | f/8.0 |
|---------------|-------|-------|

| | | |
|-------------|--------------|--------------|
| Filter Type | 1/100 second | 1/100 second |
|-------------|--------------|--------------|

| | | |
|--|------------|------------|
| | Wratten 25 | Wratten 25 |
|--|------------|------------|

Take-up Horizon Cameras:

| | | |
|------|-----------|------|
| Lens | Starboard | Port |
|------|-----------|------|

| | | |
|------------------|-------------|-------------|
| Aperture Setting | 55 mm f/6.3 | 55 mm f/6.3 |
|------------------|-------------|-------------|

| | | |
|---------------|-------|-------|
| Exposure Time | f/8.0 | f/6.3 |
|---------------|-------|-------|

| | | |
|-------------|--------------|--------------|
| Filter Type | 1/100 second | 1/100 second |
|-------------|--------------|--------------|

| | | |
|--|------------|------------|
| | Wratten 25 | Wratten 25 |
|--|------------|------------|

MISSION 1041 RAW CAMERAS

C. POST FLIGHT PERFORMANCE EVALUATION

The overall image quality of this mission is generally good. It is considered better than Mission 1038 and comparable to Missions 1039 and 1040. Several factors combined to limit to a moderate degree the value of this mission for current intelligence. The highly eccentric orbit caused some difficulty in obtaining coverage of targets while the high altitude over a small number of targets at the most northern latitudes reduced the ground resolution. Some further degradation resulted from a small area of out-of-focus imagery of the aft-looking camera. Heavy cloud cover and other atmospheric attenuation in some target areas also limited the value of this mission. However, it is noted that the photo-interpreters judged the mission as "fair to good".

The MIP ratings for the -1 and -2 missions were both 85, and the MIP frames for both mission segments were selected from the forward-looking camera material. Usually the aft-looking camera produces the better quality imagery and the MIP frames are selected from that camera. The relatively good performance of the forward camera on this mission may be partly attributed to the relatively high solar elevations encountered (45° and above). Examination of the FNC for each camera shows no significant differences. It is noted that the Performance Evaluation Team stated that "... the information content of the aft camera imagery is equivalent, and in some cases, better".

The only significant anomaly of the forward-looking panoramic camera was an open shutter failure of the starboard (output) H.O. device for one cycle (two panoramic frames). Examination of images from this H.O. both before and after the anomaly showed normal results. Although a continuous open shutter failure of the H.O. device would be catastrophic for the pan camera concerned, the present anomaly is random and no action is indicated.

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On the left-looking pan camera material there was a small out-of-focus area throughout both mission segments. The extent of this anomaly tended to increase through the mission. The cause is believed to be a film tracking bias across the platen resulting from a slight misalignment. Corrective action beyond the extensive alignment precautions presently used is not contemplated.

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SECTION 6

MISSION 104L STELLAR-INDEX CAMERAS

A. COMPONENT ALIGNMENT

| <u>Component</u> | <u>-1 Mission Serial Number</u> | <u>-2 Mission Serial Number</u> |
|------------------|-------------------------------------|-------------------------------------|
| Camera | D-105 | D-102 |
| Index Reseau | 134 | 127 |
| Stellar Reseau | 133 | 127 |

B. CAMERA DATA AND FLIGHT SETTINGS

Stellar Camera:

| | | |
|---------------------|-------------|-------------|
| Lens | 85 mm f/1.8 | 85 mm f/1.8 |
| Exposure Time | 2 seconds | 1 second |
| Filter Type | None | None |
| Film Type (Eastman) | 3401 | 3401 |

Index Camera:

| | | |
|---------------------|--------------|--------------|
| Lens | 38 mm f/4.5 | 38 mm f/4.5 |
| Exposure Time | 1/500 second | 1/500 second |
| Filter Type | Wratten 21 | Wratten 21 |
| Film Type (Eastman) | 3400 | 3400 |

C. POST FLIGHT EVALUATION

Stellar Cameras

Both Stellar cameras were operational throughout their assigned mission segments. Stellar image motion, which was small throughout the mission, was generally in the roll component. The Stellar images were adequate for altitude determination.

The base plus fog densities of the Stellar films was higher than normal with the Mission 1041-2 fog densities significantly higher than those from 1041-1. It has been determined that the cause is increased radiation exposure resulting from the unusually high orbital apogee.

An unidentified image appeared in a five frame sequence of Mission 1041-1, and again in a four frame sequence of Mission 1041-2. It was noted that these sequences occurred on synchronous orbits. However, it was concluded that the object producing the images was external to the vehicle system and thus beyond the scope of engineering investigation.

There were no significant anomalies in the operation of either Stellar camera.

Index Cameras

Both Index cameras were operational throughout their assigned mission segments. The quality of images from both cameras was acceptable.

An increase in base plus fog densities, corresponding to those observed in the Stellar films, was noted on the Index films. The cause was the same: increased radiation exposure, as described in the paragraphs on Stellar Cameras.

There were no significant anomalies in the operation of either Stellar camera.

SECTION 7

PANORAMIC CAMERA EXPOSURE

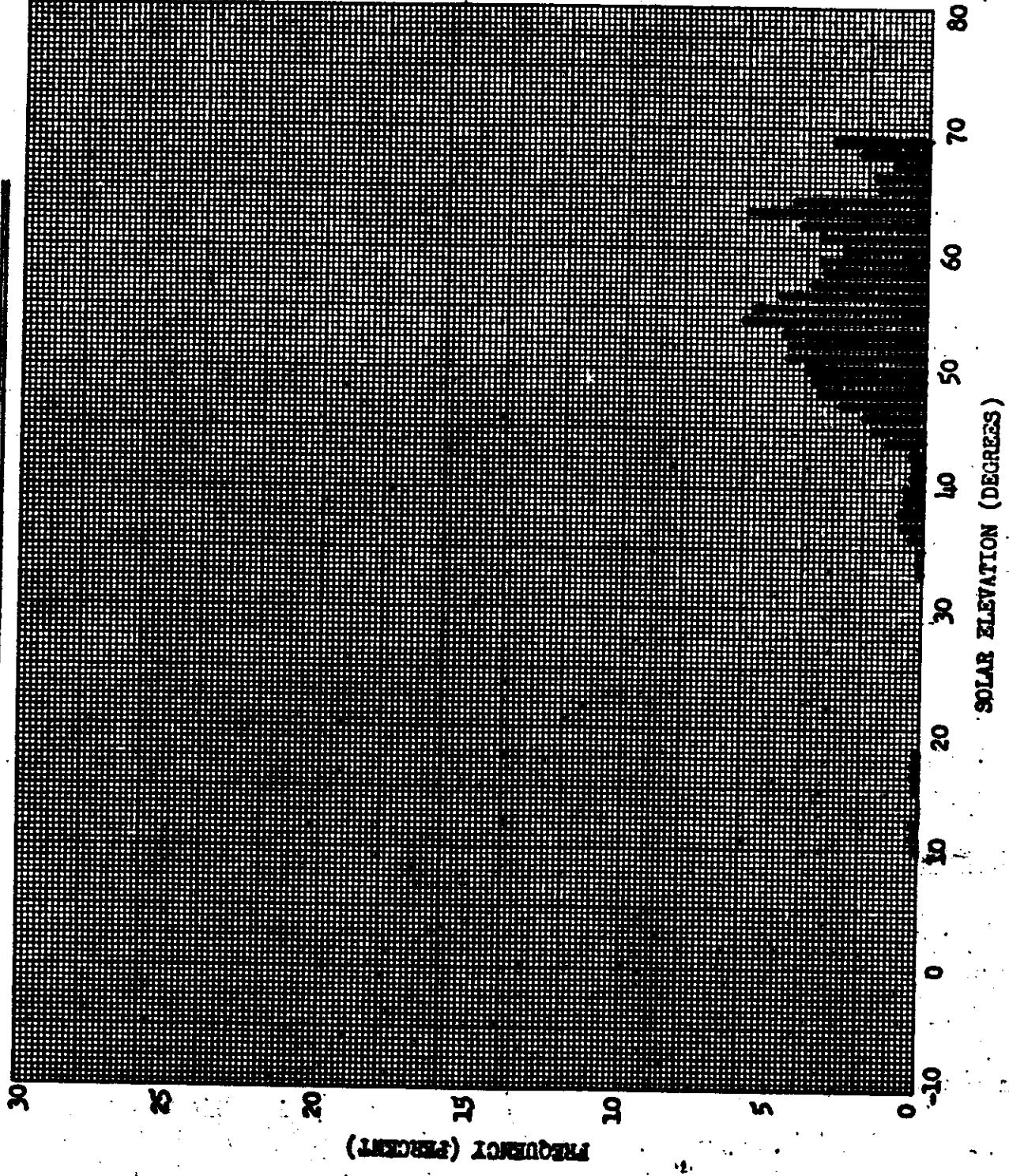
The Master camera contained a 0.225 inch slit and a Wratten 82A filter. The Slave camera had a 0.175 inch slit and a Wratten G1 filter. These conditions placed the nominal exposure near the intermediate processing curve.

The frequency distributions of the solar elevations and solar azimuths encountered during the photographic operations are shown in Figures 7-1 to 7-4.

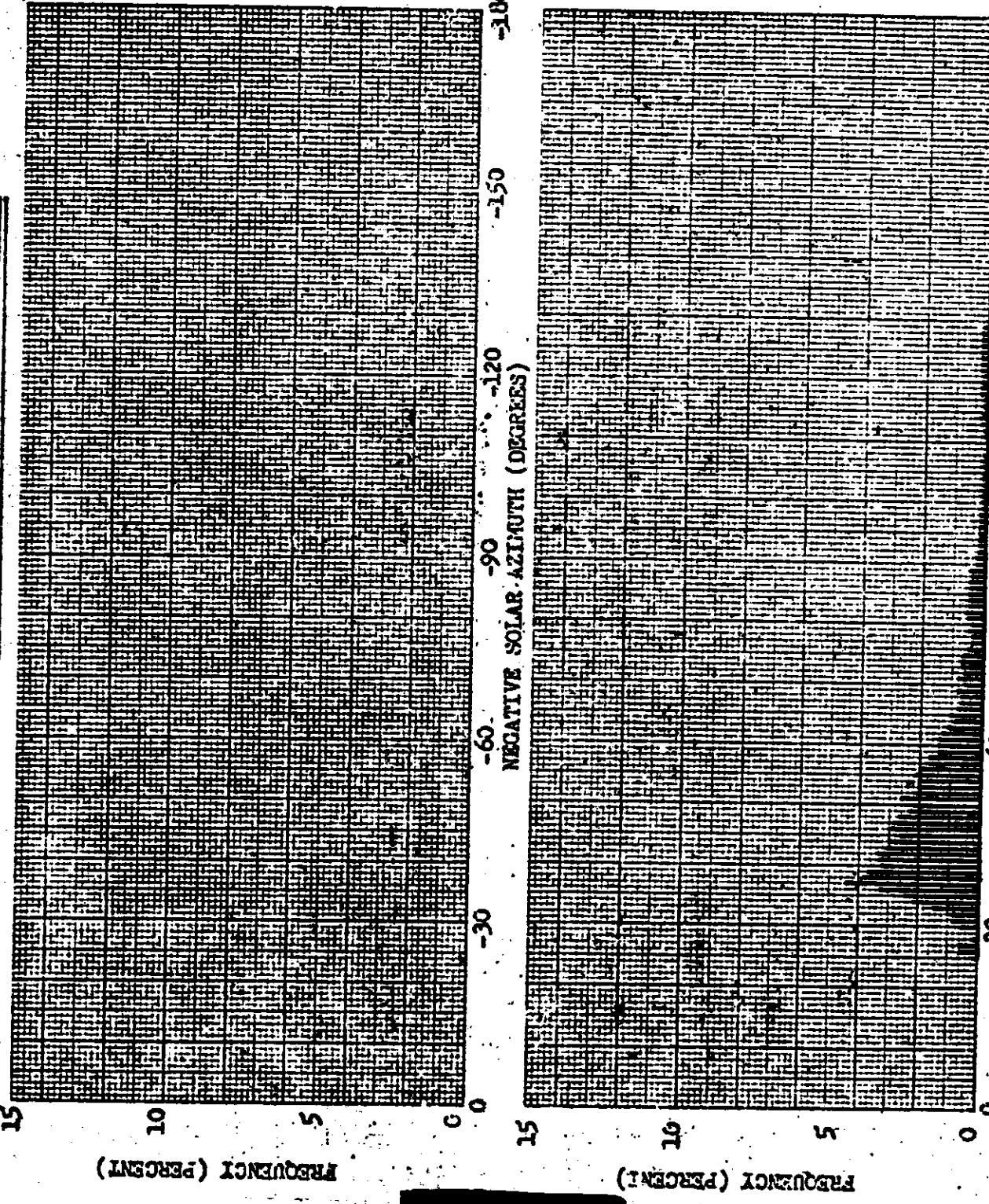
The nominal exposure times of the Master and Slave cameras are shown as a function of latitude for passes D-1, D-93, and D-215 in Figures 7-5 to 7-10. The predicted level of processing for the original negative is based on the in-flight performance estimate and is tabulated below with the processing levels reported by [REDACTED]

| <u>Mission</u> | <u>Camera</u> | | <u>% Primary</u> | <u>% Intermediate</u> | <u>% Full</u> | <u>% Transition</u> |
|----------------|---------------|-----------|------------------|-----------------------|---------------|---------------------|
| 1041-1 | FWD | Predicted | 0 | 100 | 0 | |
| | | Reported | 6 | 31 | 44 | 19 |
| 1041-1 | AFT | Predicted | 0 | 99 | 1 | |
| | | Reported | 8 | 34 | 40 | 18 |
| 1041-2 | FWD | Predicted | 1 | 99 | 0 | |
| | | Reported | 5 | 47 | 58 | 20 |
| 1041-2 | AFT | Predicted | 1 | 99 | 0 | |
| | | Reported | 5 | 20 | 54 | 21 |

SOLAR ELEVATION FREQUENCY DISTRIBUTION



SOLAR AZIMUTH FREQUENCY DISTRIBUTION



Mission No: 1001-1

Payload No: J-10

Camera No: 208

Launch Date: 5/9/67

Launch Time: 2152 Z

Inclination: 85°

SIGN NOTATION

Direction of Flight

POSITIVE SOLAR AZIMUTH (DEGREES)

180

150

120

90

60

30

0

SOLAR ELEVATION FREQUENCY DISTRIBUTION

Mission No: 10U1-2

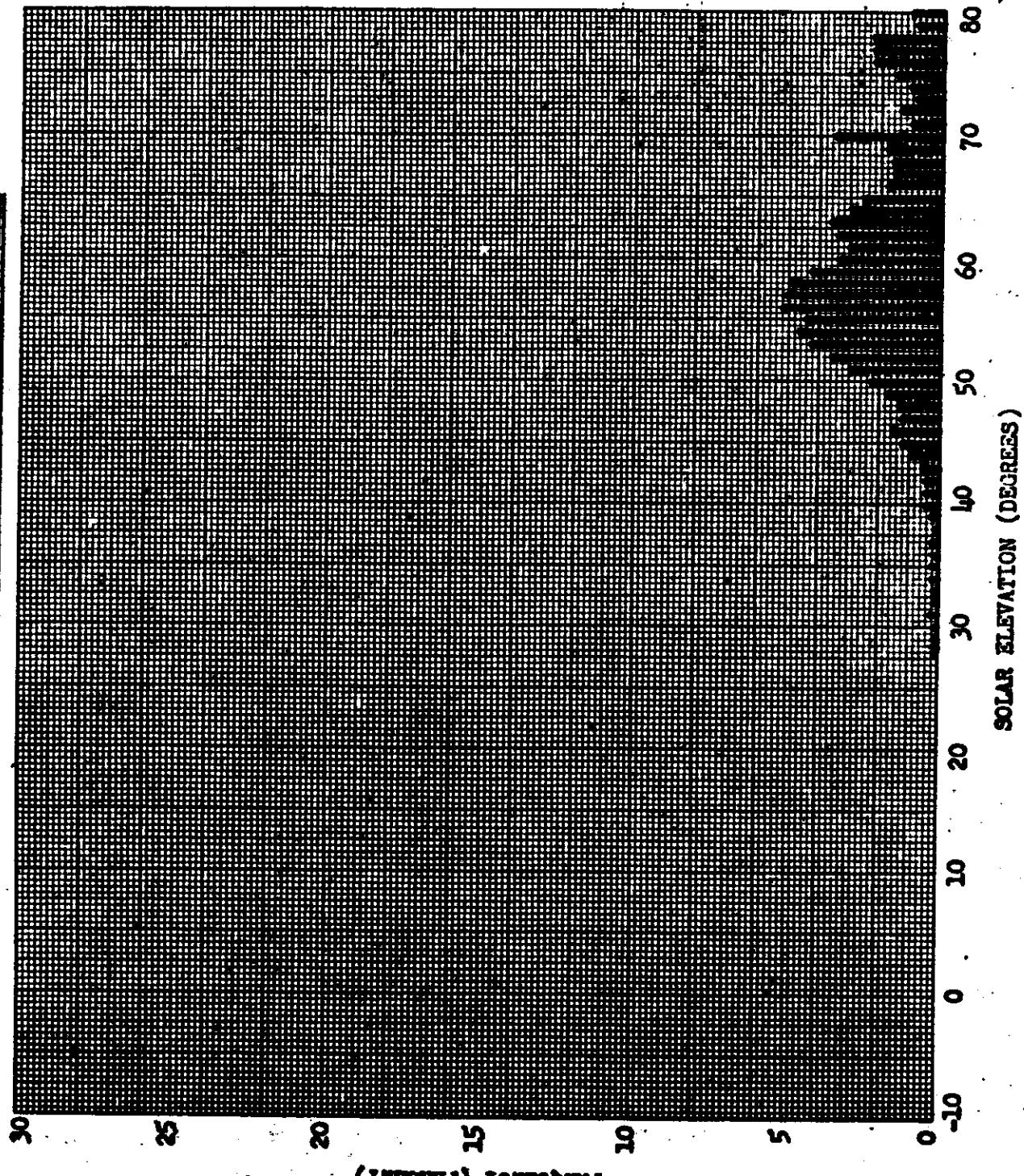
Payload No: J-40

Camera No: 208

Launch Date: 5/9/67

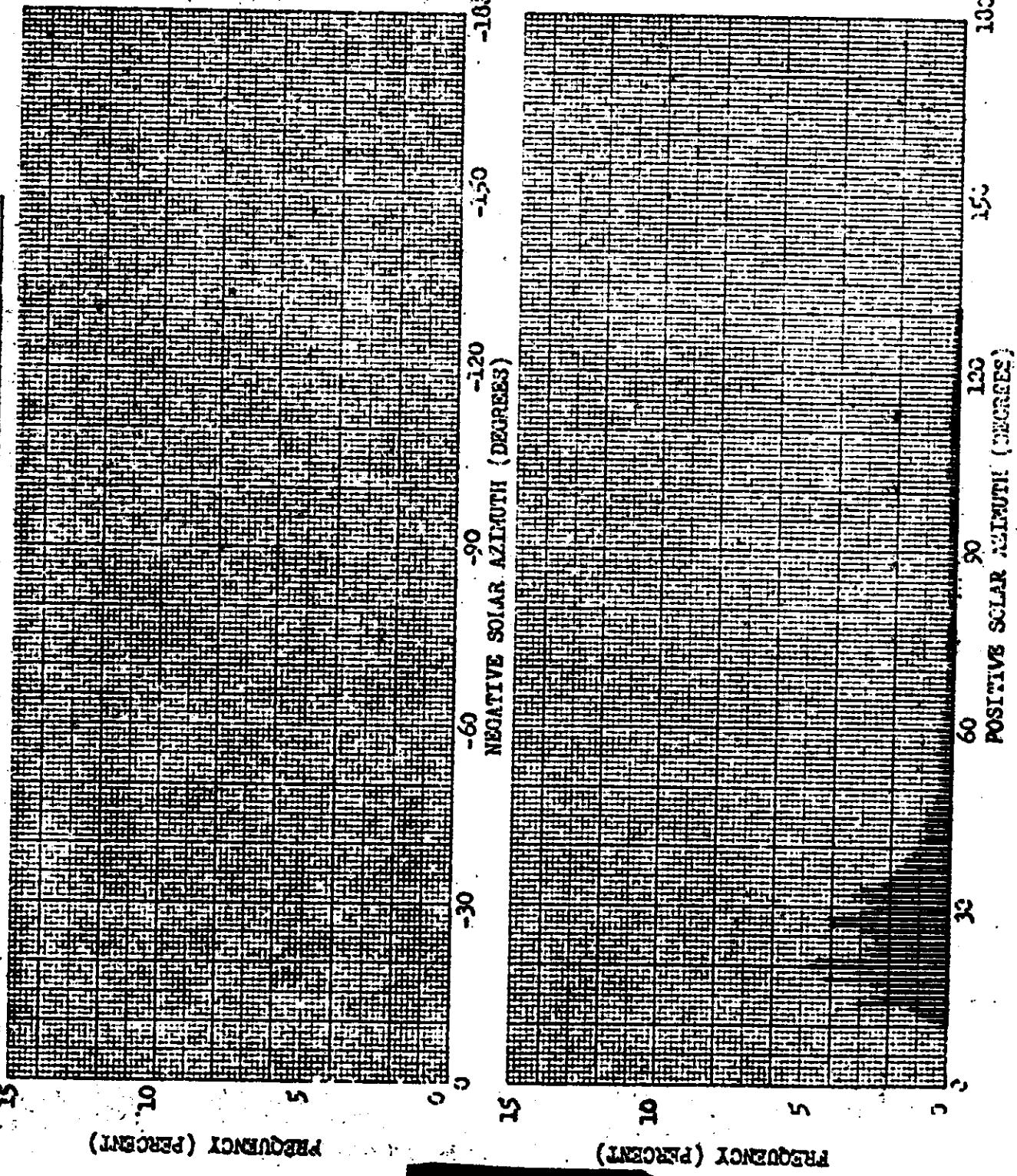
Launch Time: 2152 Z

Inclination: 85°



TOP SECRET

SOLAR AZIMUTH FREQUENCY DISTRIBUTION



Mission No: 1011-2

Payload No: J-40

Camera No: 208

Launch Date: 5/9/67

Launch Time: 2152 Z

Inclination: 85°

SICK NOTATION

Direction of Flight

FREQUENCY (PERCENT)

25

20

15

10

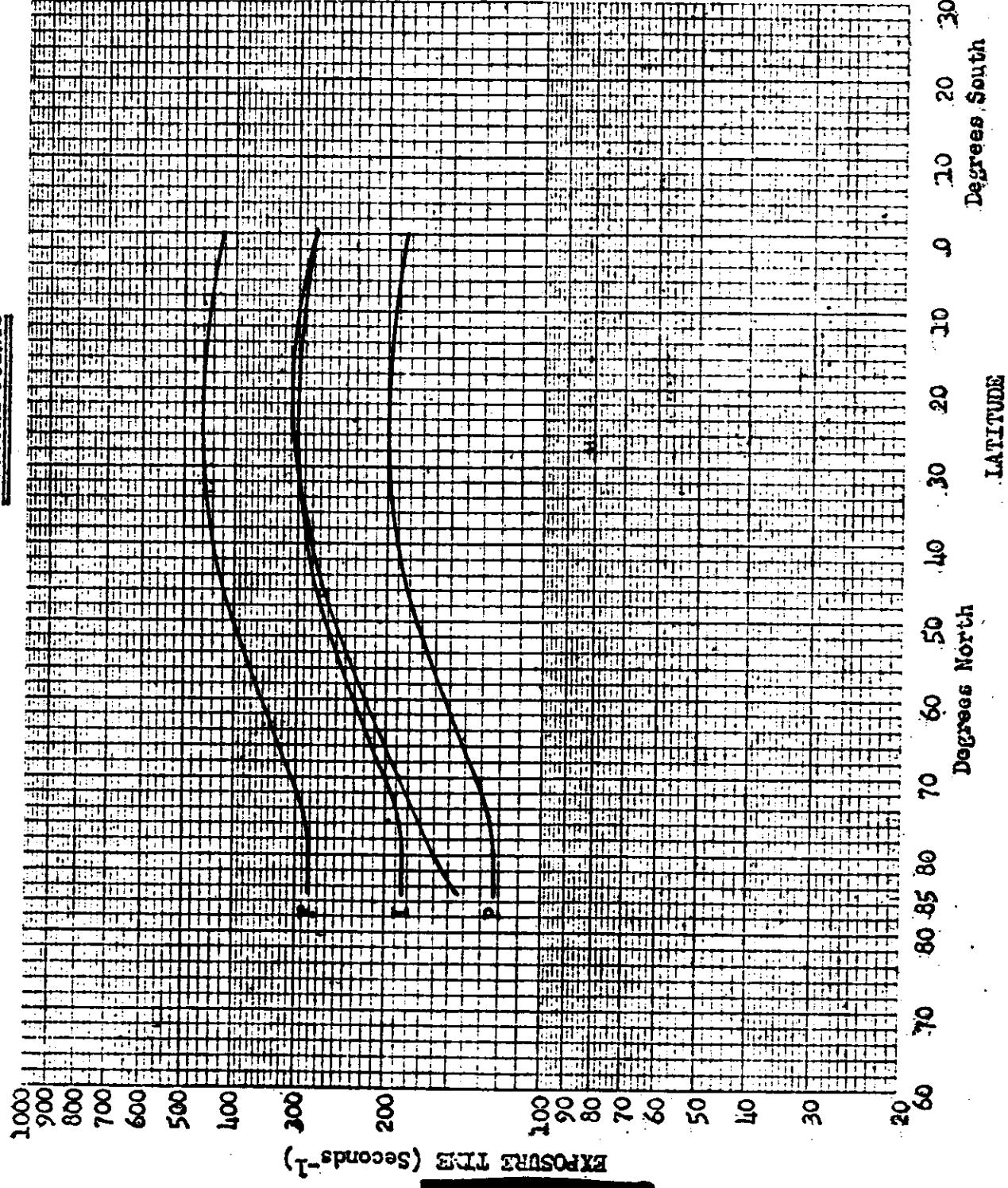
5

0

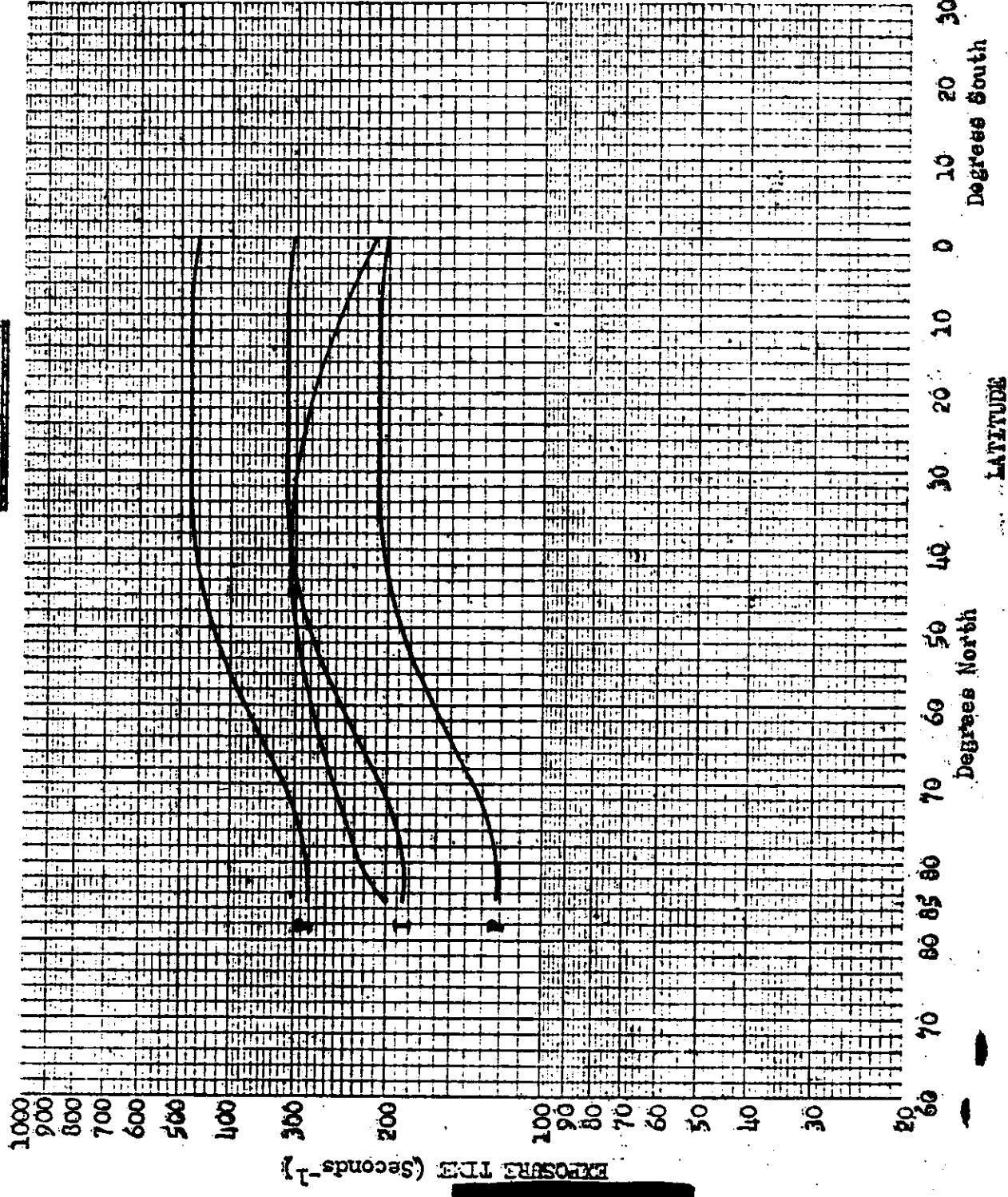
5

10

EXPOSURE POINTS



EXPOSURE POINTS



Mission No: 1041

Payload No: J-40

Camera No: 208

Pass No: 93

Launch Date: 5/9/67

Launch Time: 2152 Z

Slit Width: .225

Filter Type: Wratten 23A

Film Type: 3401

Degrees South

LATITUDE

100
90
80
70
60
50
40
30
20
10
0

Degrees North

નાના

ପରିବେଶ କାନ୍ତିକାଳୀନ
ମହାଦେଶକାନ୍ତିକାଳୀନ

નોટેશન્સ

Filter Type: Watten 2A

Slit Width: .225

Launch Time: 2152 Z

Launch Date: 5/9/67

Pass No. 215

Ganerex No.: 208

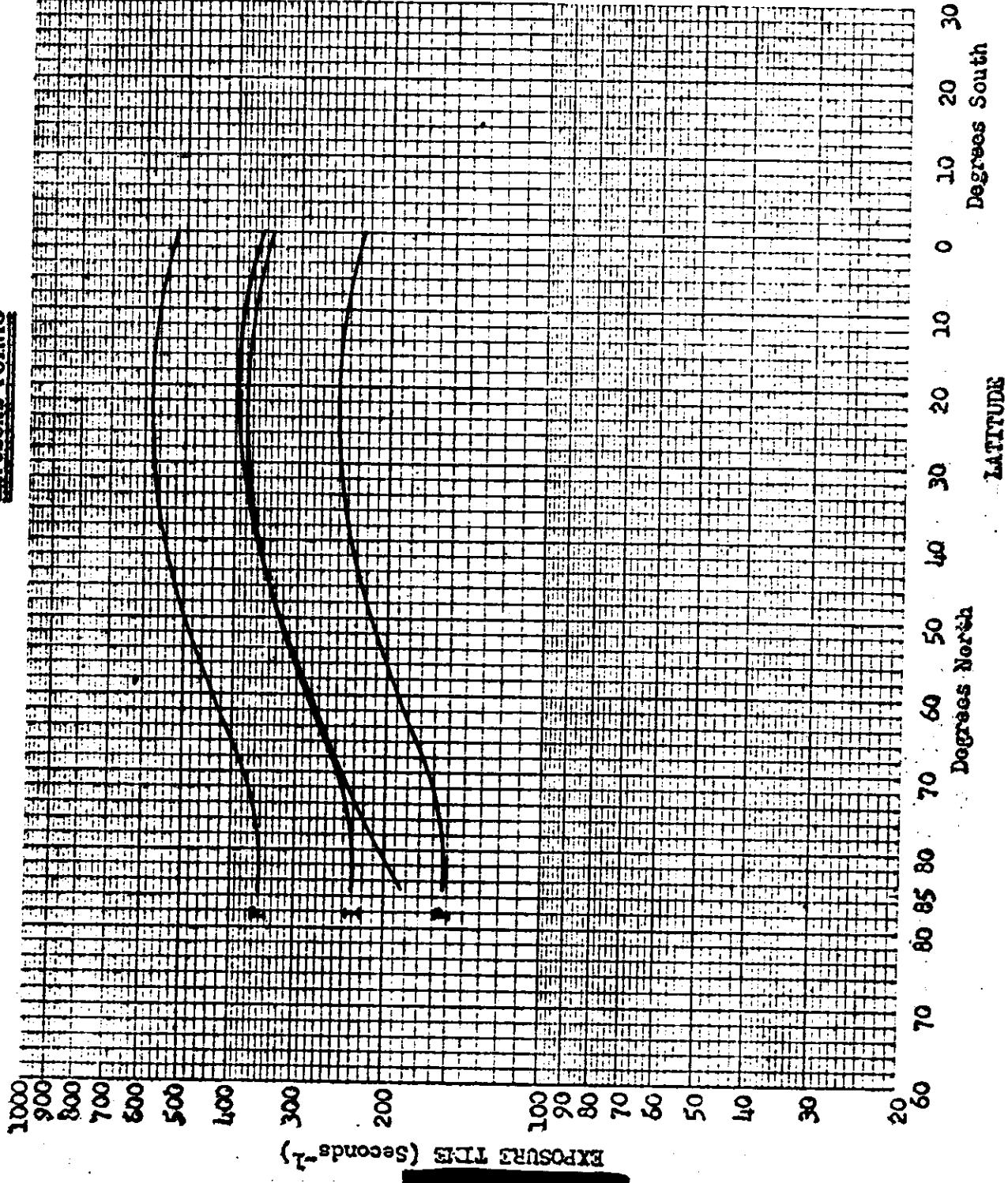
Payload No: J-ho

Mise au Nom

A scatter plot on a grid showing a positive linear trend. The x-axis ranges from 20 to 900 with major ticks every 10 units. The y-axis ranges from 20 to 90 with major ticks every 10 units. A series of points forms a line starting at approximately (200, 20) and ending at approximately (800, 90), with a slight downward curve towards the right end.

EXPOSURE TIME (seconds)

EXPOSURE POINTS



Mission No: 1041

Payload No: J-40

Camera No: 209

Pass No: 93

Launch Date: 5/9/67

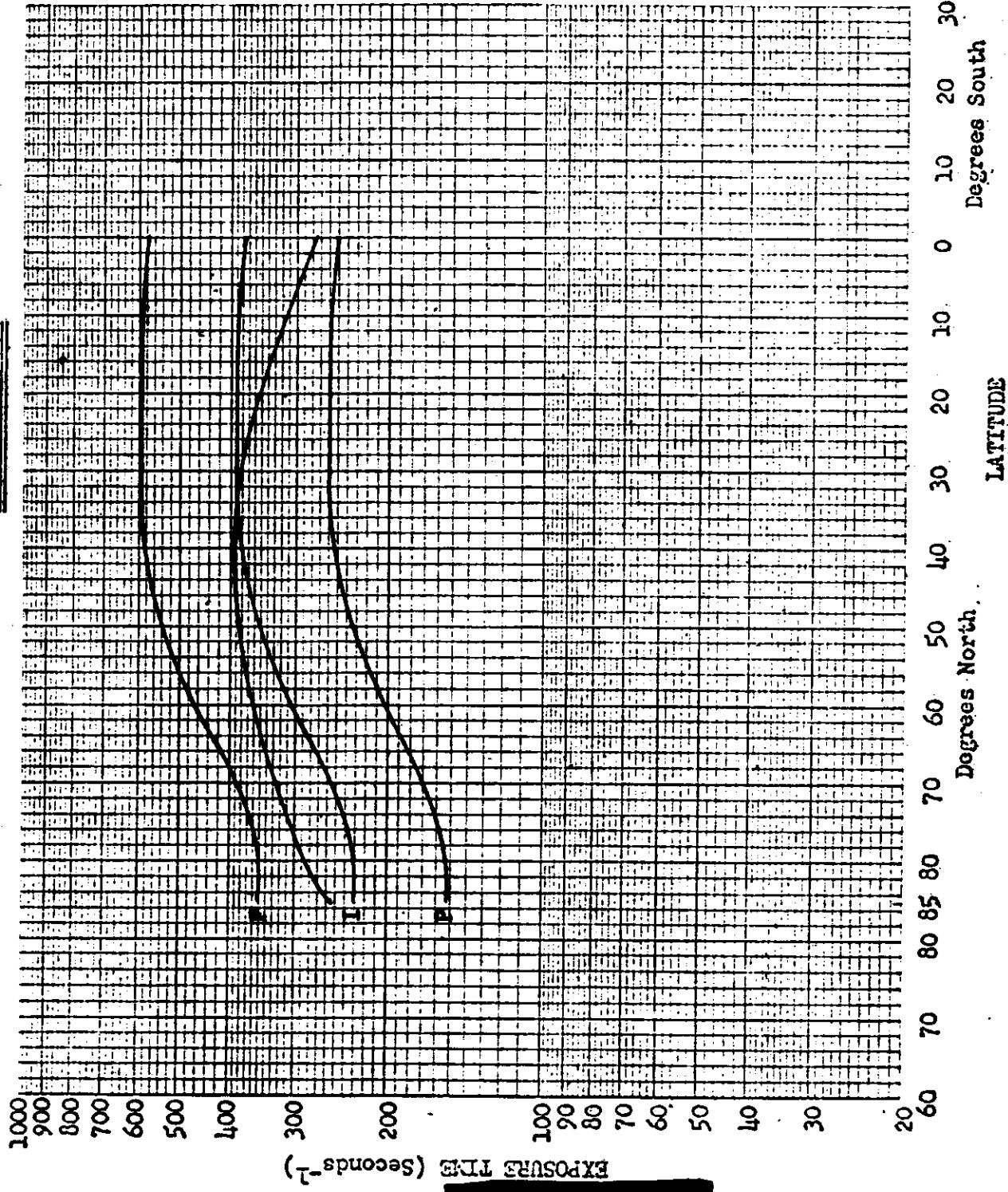
Launch Time: 2152 Z

•175

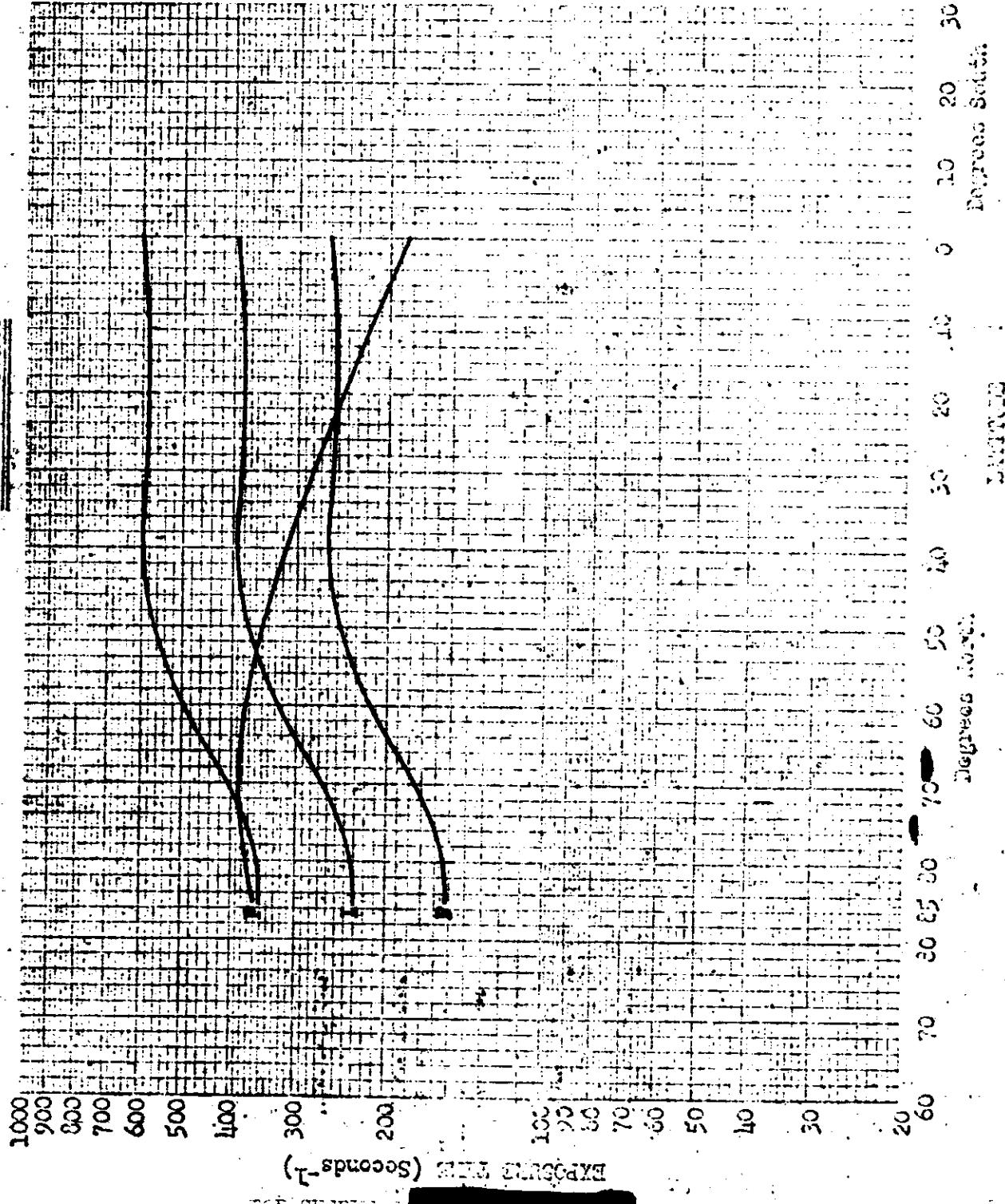
Främling Two: Watten 21

3404

EXPOSURE POINTS



EXPOSURE POINTS



Mission No: 101

Payload No: J-40

Camera No: 209

Pass No: 215

Launch Date: 5/9/67

Launch Phase: 2152 Z

Sat. Weight: .175

Flight Layer: Watten 21

File Type: 3401

Degrees Sats.

2152 Z

SECTION 8

PERFORMANCE MEASUREMENTS

The photography acquired by both panoramic cameras during Missions 1041-1 and 1041-2 received an MIP rating of 85. A summary is tabulated below of the MTF/MTM resolution values measured by AFSPFF and reported in cycles/mm. The microdensitometer slit used was 1 micron by 80 microns.

| <u>Mission</u> | <u>Camera</u> | <u>Cycles/mm</u> | <u>Avg.</u> | <u>Ground Resolution</u> |
|----------------|---------------|------------------|-------------|--------------------------|
| 1041-1 | FWD | 72 | | |
| | | | 73 | 23.1' |
| 1041-2 | FWD | 73 | | |
| 1041-1 | AFT | 82 | | |
| | | | 80 | 15.0' |
| 1041-2 | AFT | 78 | | |

The details of the measurement and computing techniques, targets measured and target locations are fully reported in the Evaluation report published by AFSPFF and are not included in this report. These values were determined by using the "Interim MTF/MTM Program" technique.

SECTION 9

DIFFUSE DENSITY MEASUREMENTS

The diffuse density measurements made by AFCEPPF were computer sorted at A/P to permit analysis of the density ranges encountered at the three processing levels. A study of sorting techniques showed that no absolute method was available to separate the density values as the accuracy of the Processing History published by [REDACTED] appears rather low and processing transition phases are not accounted for. The sorting technique selected uses the base plus fog density values where measurements up to 0.09 density are considered as having received Primary processing 0.10 to 0.17 as Intermediate and above 0.17 density as Full. The percentage of original negative that was processed at each level, based on the computer sort, is tabulated below with the predicted and reported processing percentages.

| <u>Mission</u> | <u>Camera</u> | | <u>%</u> | <u>%</u> | <u>%</u> | <u>%</u> |
|----------------|---------------|-----------|----------------|---------------------|-------------|-------------------|
| | | | <u>Primary</u> | <u>Intermediate</u> | <u>Full</u> | <u>Transition</u> |
| 1041-1 | FWD | Predicted | 0 | 100 | 0 | |
| | | Reported | 6 | 31 | 44 | 49 |
| | | Computed | 0 | 46 | 54 | |
| 1041-1 | AFT | Predicted | 0 | 99 | 1 | |
| | | Reported | 8 | 34 | 40 | 13 |
| | | Computed | 0 | 47 | 53 | |
| 1041-2 | FWD | Predicted | 1 | 99 | 0 | |
| | | Reported | 5 | 17 | 53 | 20 |
| | | Computed | 0 | 23 | 77 | |
| 1041-2 | AFT | Predicted | 1 | 99 | 0 | |
| | | Reported | 5 | 20 | 54 | 21 |
| | | Computed | 0 | 30 | 70 | |

The tabulations of density frequency distributions for Missions 1041-1 and 1041-2 are included in Appendix A, Table A-1 thru A-4. The graphical presentation of the density distribution have been plotted in Appendix A, Figures A-1 thru A-36.

A summary of the processing and exposure analysis is shown in Table 9-1. The terrain D-Min criteria, (image) for pre-processing and processing is 0.40 to 0.50 density units. The area measured for D-Min is selected subjectively and is not necessarily the absolute D-Min in the photography.

A density range chart Figure 9-1 is included in this report. This type of chart for Missions 1004 thru 1031 is included in the AF/AF report for Mission 1031.

These charts are produced from the same density measurements previously mentioned in this section. The computer produced the mean, median and range figures for the various processing levels used. The chart includes the number of frames (samples) in which the density measurements were made. These measurements are made approximately every tenth frame throughout the mission.

~~TOP SECRET C~~

| MISSION 1041-1 | | INSTR - FWD | | 6/27/67 | | PROCESSING AND EXPOSURE ANALYSIS | | | |
|----------------|-------------|---------------|-----------------|------------------|----------------|----------------------------------|----------------|--------------|--------------|
| PROCESS LEVEL | SAMPLE SIZE | UNDER EXPOSED | UNDER PROCESSED | CORRECT EXP/PROC | OVER PROCESSED | CORRECT EXP/PROC | OVER PROCESSED | OVER EXPOSED | OVER EXPOSED |
| PRIMARY | 0 | 0 PC | 0 PC | 0 PC | 68 PC | 54 PC | 7 PC | 54 PC | 54 PC |
| INTERMEDIATE | 107 | 0 PC | 22 PC | 68 PC | 7 PC | 7 PC | 2 PC | 2 PC | 2 PC |
| FULL | 126 | 10 PC | 10 PC | 88 PC | 2 PC | 79 PC | 4 PC | 0 PC | 0 PC |
| ALL LEVELS | 233 | 6 PC | 10 PC | 79 PC | 4 PC | 79 PC | 4 PC | 1 PC | 1 PC |
| MISSION 1041-1 | | INSTR - AFT | | 6/27/67 | | PROCESSING AND EXPOSURE ANALYSIS | | | |
| PROCESS LEVEL | SAMPLE SIZE | UNDER EXPOSED | UNDER PROCESSED | CORRECT EXP/PROC | OVER PROCESSED | CORRECT EXP/PROC | OVER PROCESSED | OVER EXPOSED | OVER EXPOSED |
| PRIMARY | 0 | 0 PC | 0 PC | 0 PC | 78 PC | 54 PC | 10 PC | 52 PC | 52 PC |
| INTERMEDIATE | 102 | 0 PC | 10 PC | 92 PC | 6 PC | 92 PC | 6 PC | 2 PC | 2 PC |
| FULL | 113 | 2 PC | 9 PC | 86 PC | 8 PC | 86 PC | 8 PC | 0 PC | 0 PC |
| ALL LEVELS | 215 | 1 PC | 5 PC | 86 PC | 8 PC | 86 PC | 8 PC | 1 PC | 1 PC |
| MISSION 1041-2 | | INSTR - FWD | | 6/27/67 | | PROCESSING AND EXPOSURE ANALYSIS | | | |
| PROCESS LEVEL | SAMPLE SIZE | UNDER EXPOSED | UNDER PROCESSED | CORRECT EXP/PROC | OVER PROCESSED | CORRECT EXP/PROC | OVER PROCESSED | OVER EXPOSED | OVER EXPOSED |
| PRIMARY | 0 | 0 PC | 0 PC | 0 PC | 66 PC | 27 PC | 21 PC | 27 PC | 27 PC |
| INTERMEDIATE | 53 | 0 PC | 9 PC | 85 PC | 10 PC | 85 PC | 10 PC | 4 PC | 4 PC |
| FULL | 177 | 5 PC | 0 PC | 80 PC | 13 PC | 80 PC | 13 PC | 0 PC | 0 PC |
| ALL LEVELS | 230 | 4 PC | 2 PC | 80 PC | 13 PC | 80 PC | 13 PC | 1 PC | 1 PC |
| MISSION 1041-2 | | INSTR - AFT | | 6/27/67 | | PROCESSING AND EXPOSURE ANALYSIS | | | |
| PROCESS LEVEL | SAMPLE SIZE | UNDER EXPOSED | UNDER PROCESSED | CORRECT EXP/PROC | OVER PROCESSED | CORRECT EXP/PROC | OVER PROCESSED | OVER EXPOSED | OVER EXPOSED |
| PRIMARY | 0 | 0 PC | 0 PC | 0 PC | 85 PC | 38 PC | 5 PC | 37 PC | 37 PC |
| INTERMEDIATE | 73 | 0 PC | 10 PC | 82 PC | 5 PC | 82 PC | 5 PC | 0 PC | 0 PC |
| FULL | 170 | 12 PC | 9 PC | 83 PC | 5 PC | 83 PC | 5 PC | 0 PC | 0 PC |
| ALL LEVELS | 243 | 9 PC | 3 PC | 83 PC | 5 PC | 83 PC | 5 PC | 0 PC | 0 PC |
| MISSION 1041-2 | | INSTR - AFT | | 6/27/67 | | PROCESSING AND EXPOSURE ANALYSIS | | | |
| PROCESS LEVEL | BASE FOG | UNDER EXPOSED | UNDER PROCESSED | CORRECT EXP/PROC | OVER PROCESSED | CORRECT EXP/PROC | OVER PROCESSED | OVER EXPOSED | OVER EXPOSED |
| PRIMARY | 0.01-0.09 | 0.01-0.13 | 0.14-0.39 | 0.40-0.90 | ---- | 0.91-1.34 | 0.91-1.34 | 0.91 AND UP | 0.91 AND UP |
| INTERMEDIATE | 0.10-0.17 | 0.01-0.20 | 0.21-0.39 | 0.40-0.90 | ---- | 0.40-0.90 | 0.40-0.90 | 1.35 AND UP | 1.35 AND UP |
| FULL | 0.18 AND UP | 0.01-0.39 | ---- | 0.40-0.90 | ---- | 0.91-1.69 | 0.91-1.69 | 1.70 AND UP | 1.70 AND UP |

~~TOP SECRET C~~

J MISSION DENSITY RANGES

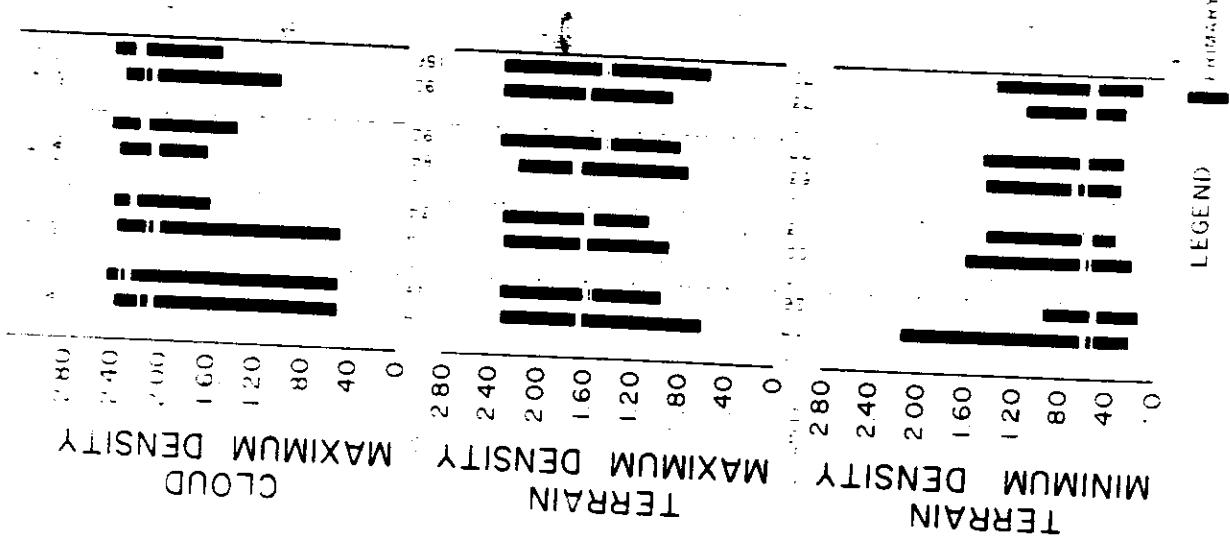


FIGURE C

SECTION 10

VEHICLE ATTITUDE

The vehicle attitude errors for both Mission 1041-1 and 1041-2 were derived from the reduction of the Stellar camera photography. This attitude data is supplied to A/P by MPIC.

The attitude errors for each frame and the attitude control rates are calculated at the A/P computer facility. The computer also plots the frequency distribution of the rates and errors. Figures 10-1 through 10-6 show these distributions for Mission 1041-1 and Figures 10-7 through 10-12 for Mission 1041-2.

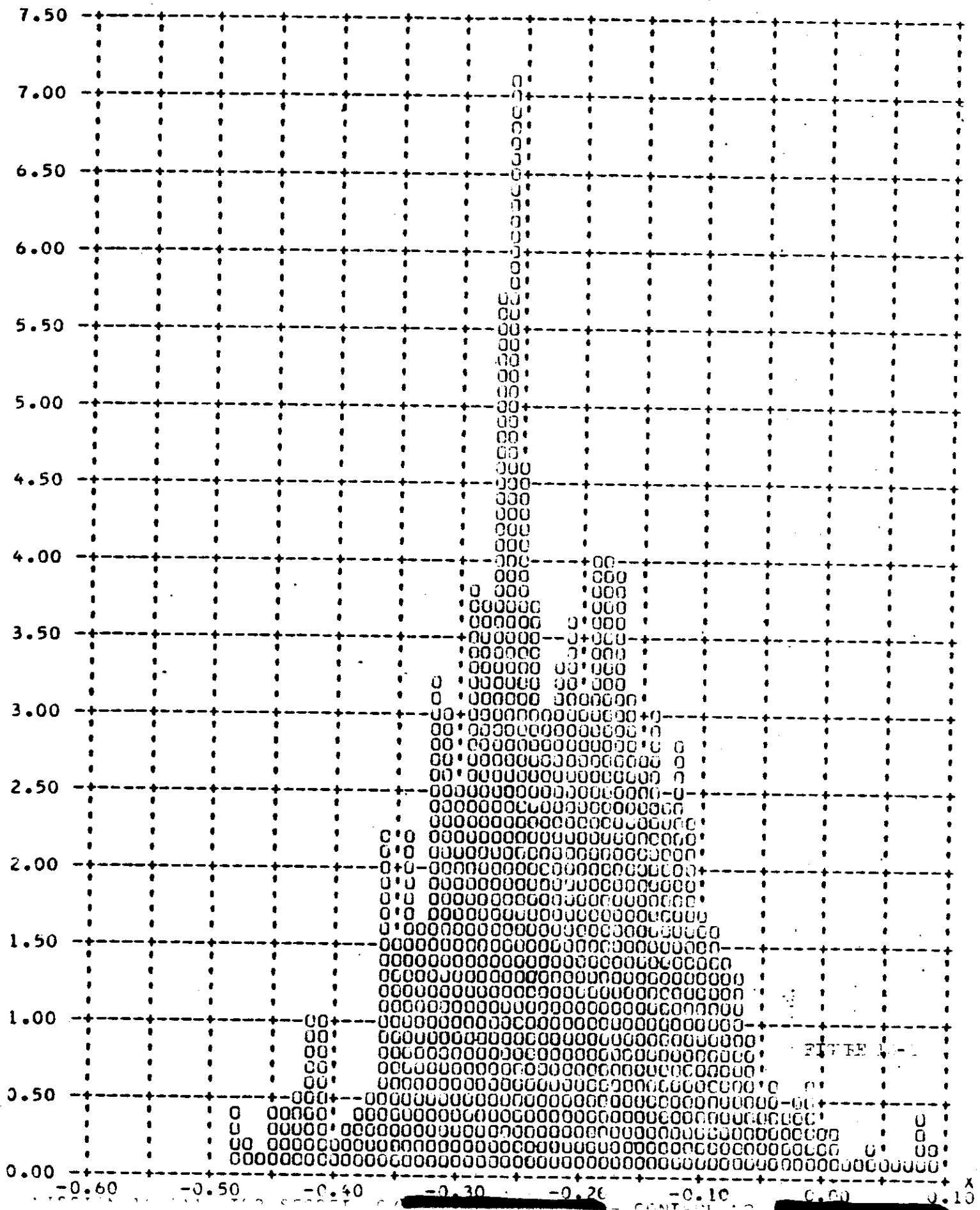
The summary table below lists the maximum attitude errors and rates that were experienced during 90% of the FWD camera photographic operations, excluding the first six frames of each operation, and the total range of the errors and rates.

| | Mission 1041-1 | Mission 1041-2 |
|--------------------------------------|---------------------|---------------------|
| | 90% Range | 90% Range |
| Pitch Error ($^{\circ}$) | 0.34 -0.48 to +0.08 | 0.26 -0.44 to +0.32 |
| Roll Error ($^{\circ}$) | 0.16 -0.26 to -0.25 | 0.23 -0.36 to +0.18 |
| Yaw Error ($^{\circ}$) | 3.05 -3.35 to -0.10 | 2.94 -3.4 to -0.05 |
| Pitch Rate ($^{\circ}/\text{hr.}$) | 14.73 -38 to +34 | 22.94 -60 to +50 |
| Roll Rate ($^{\circ}/\text{hr.}$) | 13.97 -30 to +50 | 15.70 -46 to +38 |
| Yaw Rate ($^{\circ}/\text{hr.}$) | 12.71 -52 to +34 | 18.83 -50 to +34 |

The performance of the attitude control system is comparable to the control systems used on recent missions. The panoramic photography was not degraded by the attitude control system.

MISSION 1041A1 - TOP SECRET C - CONTROL NO. [REDACTED]
FRAMES 1-6 OF EACH UP OMITTED 90 PERCENT = 0.34

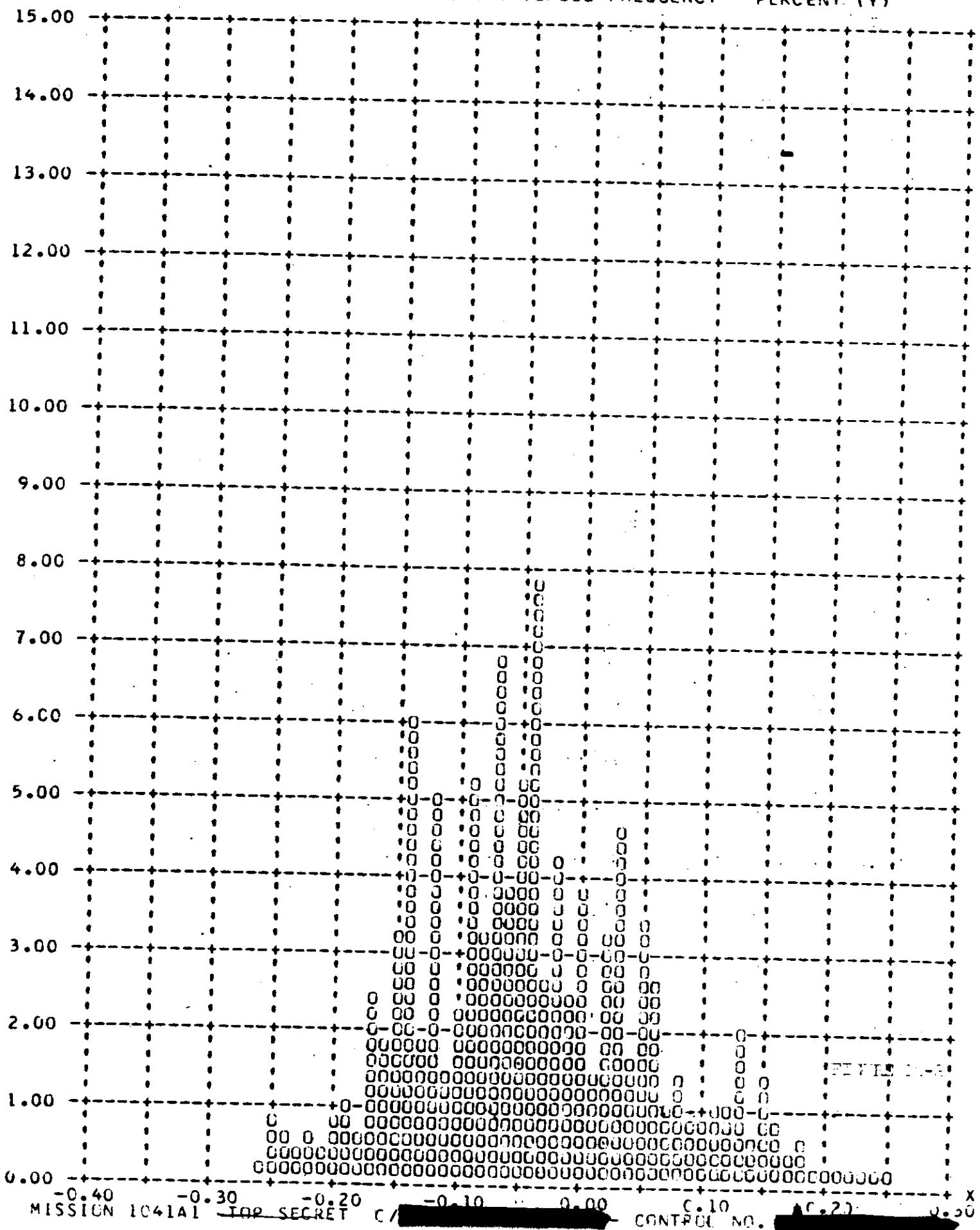
Y PITCH ANGLE ERROR - DEGREES (X) VERSUS FREQUENCY - PERCENT (Y)



MISSION 1041A1 ~~TOP SECRET~~

- CONTROL NO. [REDACTED]
FRAMES 1-6 OF EACH UP OMITTED 90 PERCENT = 0.10

Y ROLL ANGLE ERROR - DEGREES (X) VERSUS FREQUENCY - PERCENT (Y)



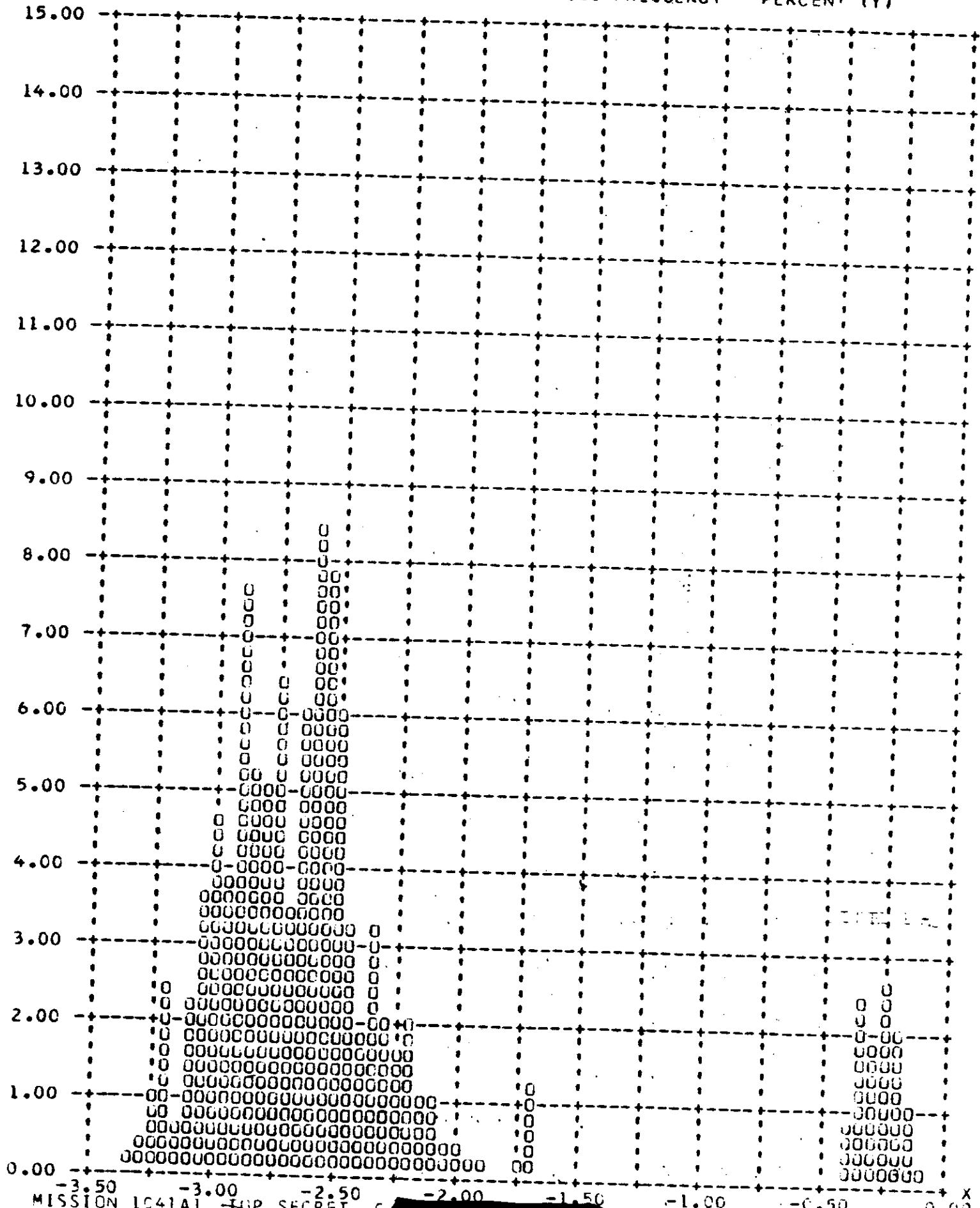
MISSION 1041A1 ~~TOP SECRET~~ C/ [REDACTED]

- CONTROL NO. [REDACTED]

MISSION 1041A1 ~~TOP SECRET~~

C/ CONTROL NO. FRAMES 1-6 OF EACH UP OMITTED 90 PERCENT = 3.05

Y YAW ANGLE ERROR - DEGREES (X) VERSUS FREQUENCY - PERCENT (Y)

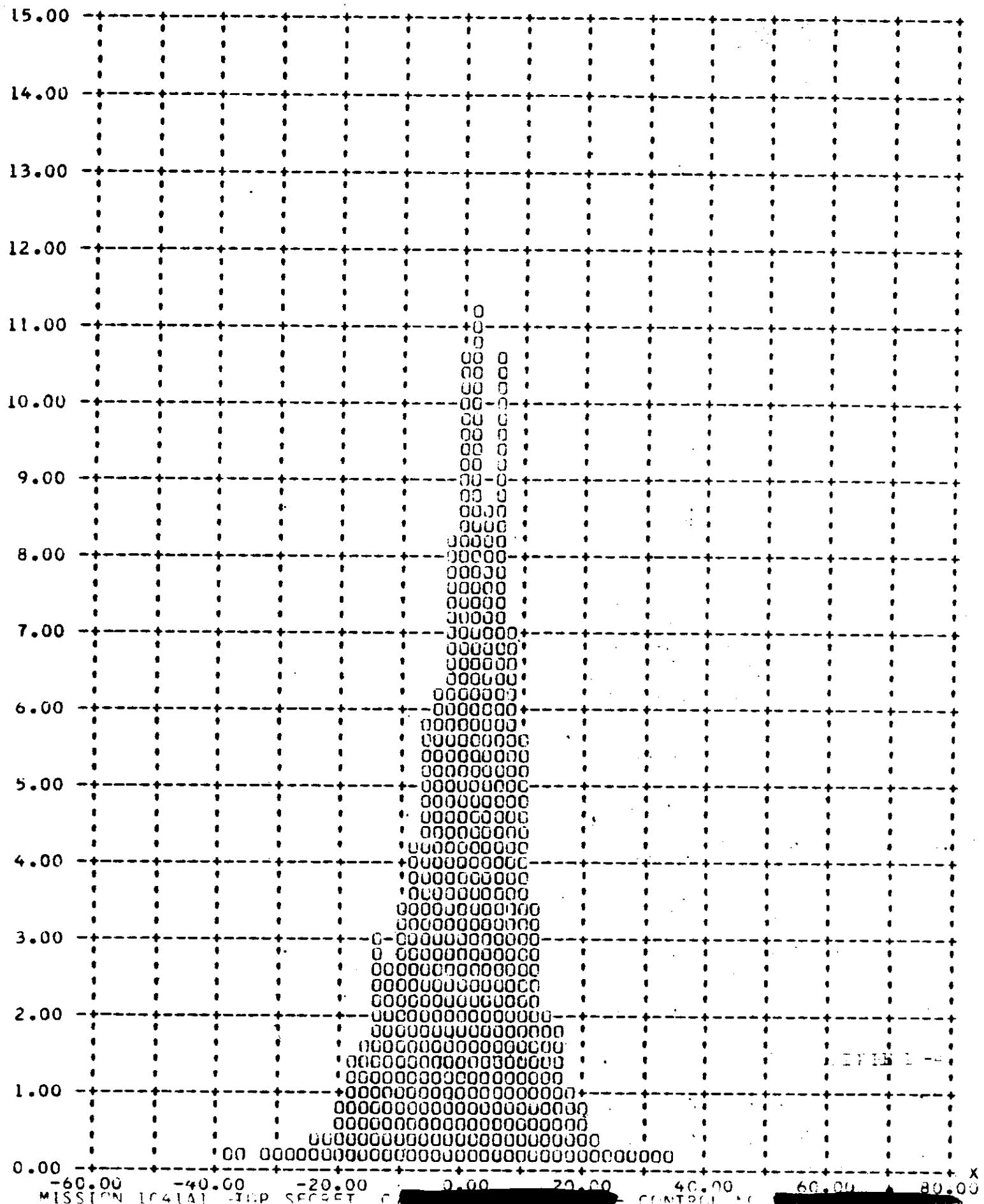
MISSION 1041A1 ~~TOP SECRET~~ C/

CONTROL NO.

X

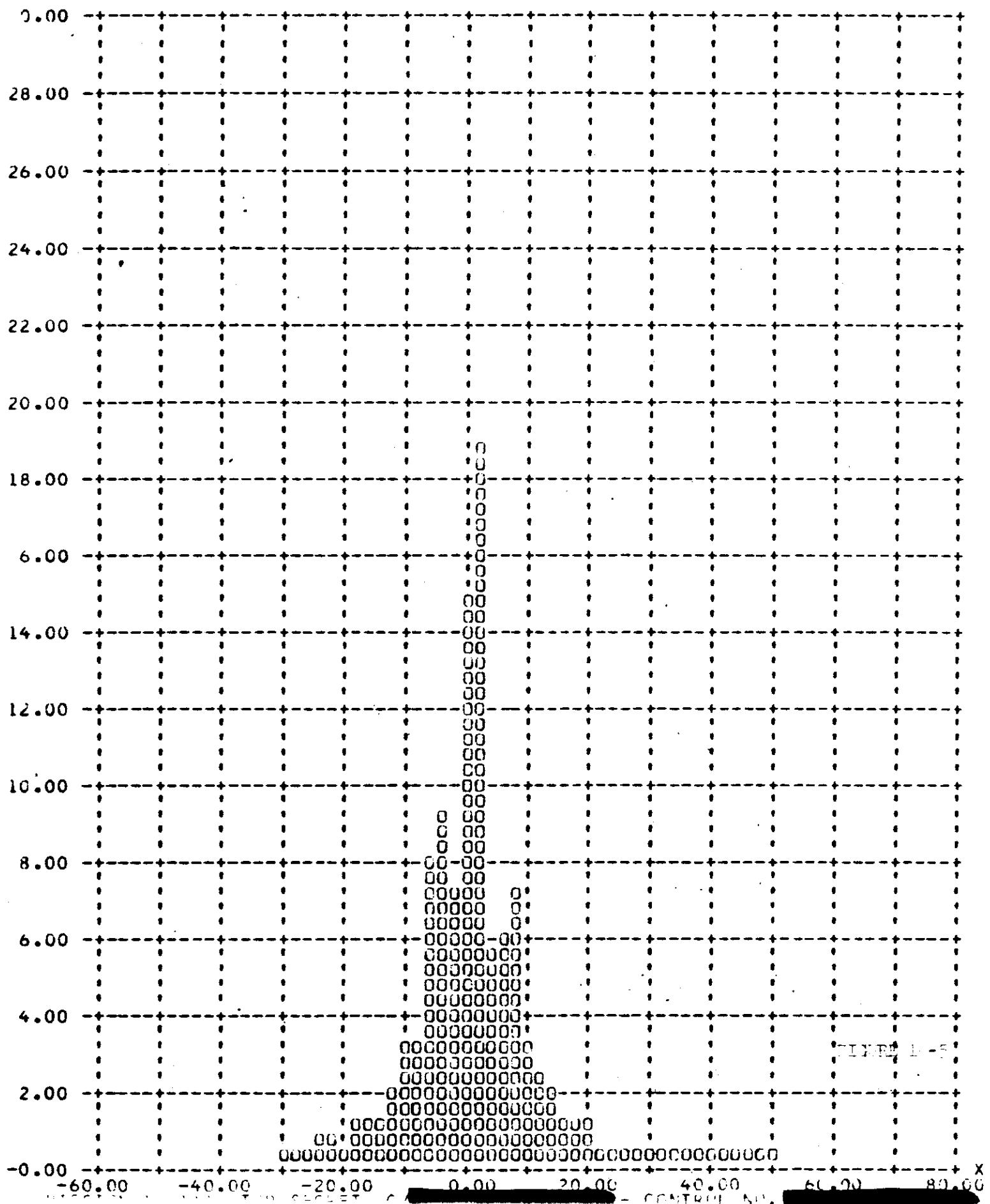
MISSION 1041A1 ~~TOP SECRET~~ C - CONTROL NO. [REDACTED]
FRAMES 1-6 OF EACH UP UMITTED 90 PERCENT = 14.73

Y PITCH RATE ERROR - DEG/HOUR (X) VERSUS FREQUENCY - PERCENT (Y)

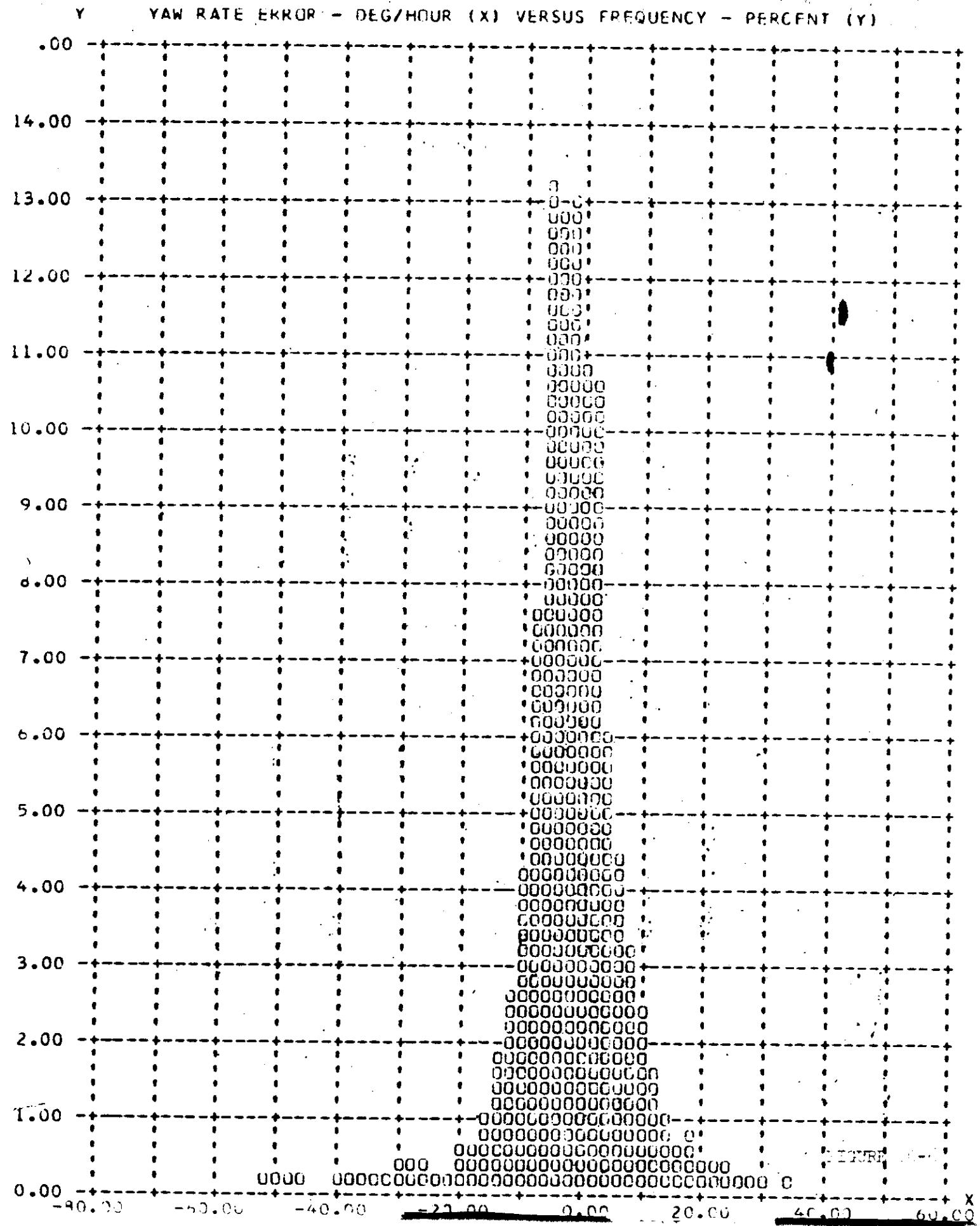


MISSION 1041A1 TOP SECRET C - CONTROL NO. [REDACTED] -
FRAMES 1-6 OF EACH UP OMITTED 90 PERCENT = 13.97

Y ROLL RATE ERROR - DEG/HOUR (X) VERSUS FREQUENCY - PERCENT (Y)

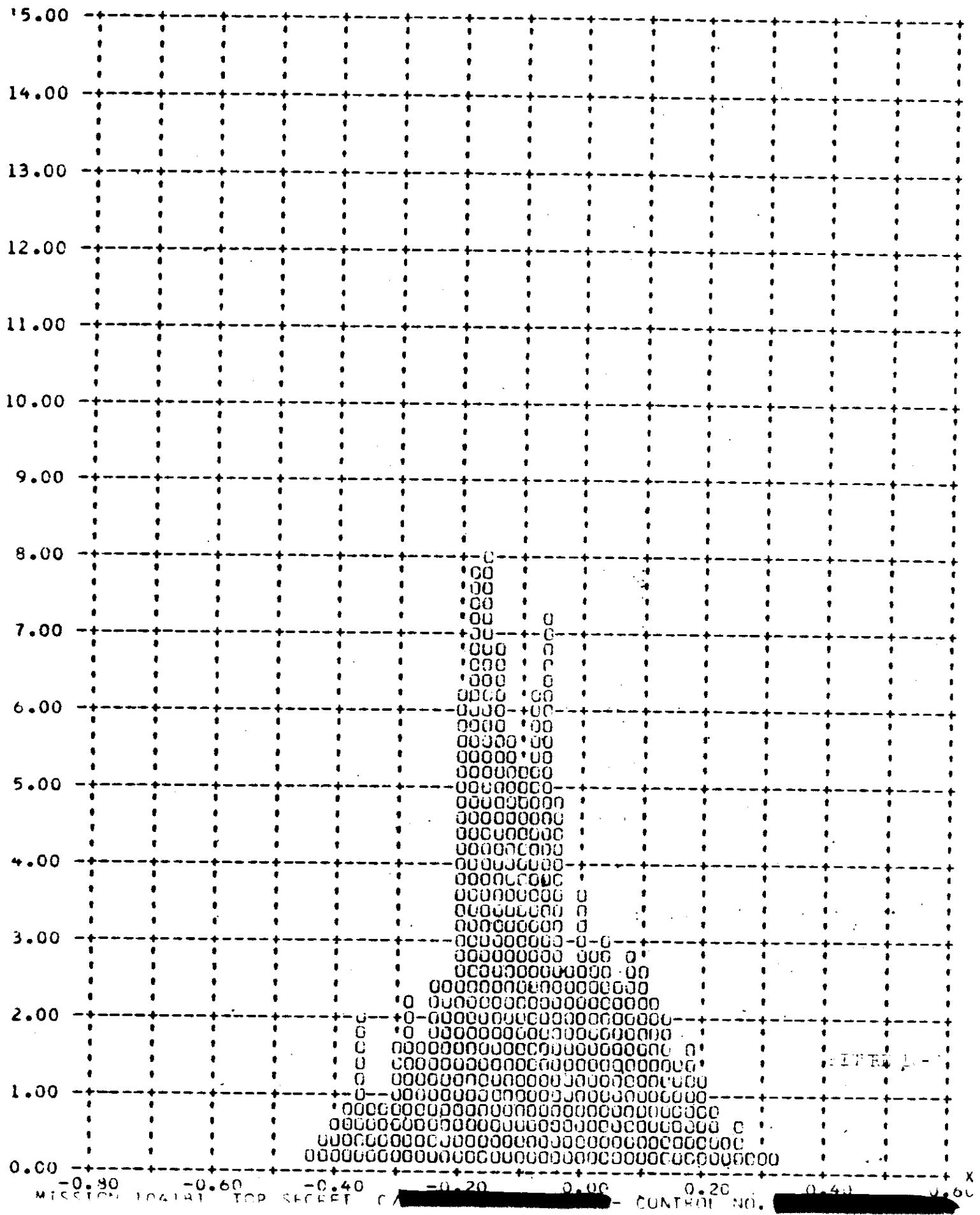


MISSION 1041A1 ~~TOP SECRET~~ C - CONTROL NO. [REDACTED] -
FRAMES 1-5 OF EACH UP OMITTED .90 PERCENT ± 12.71



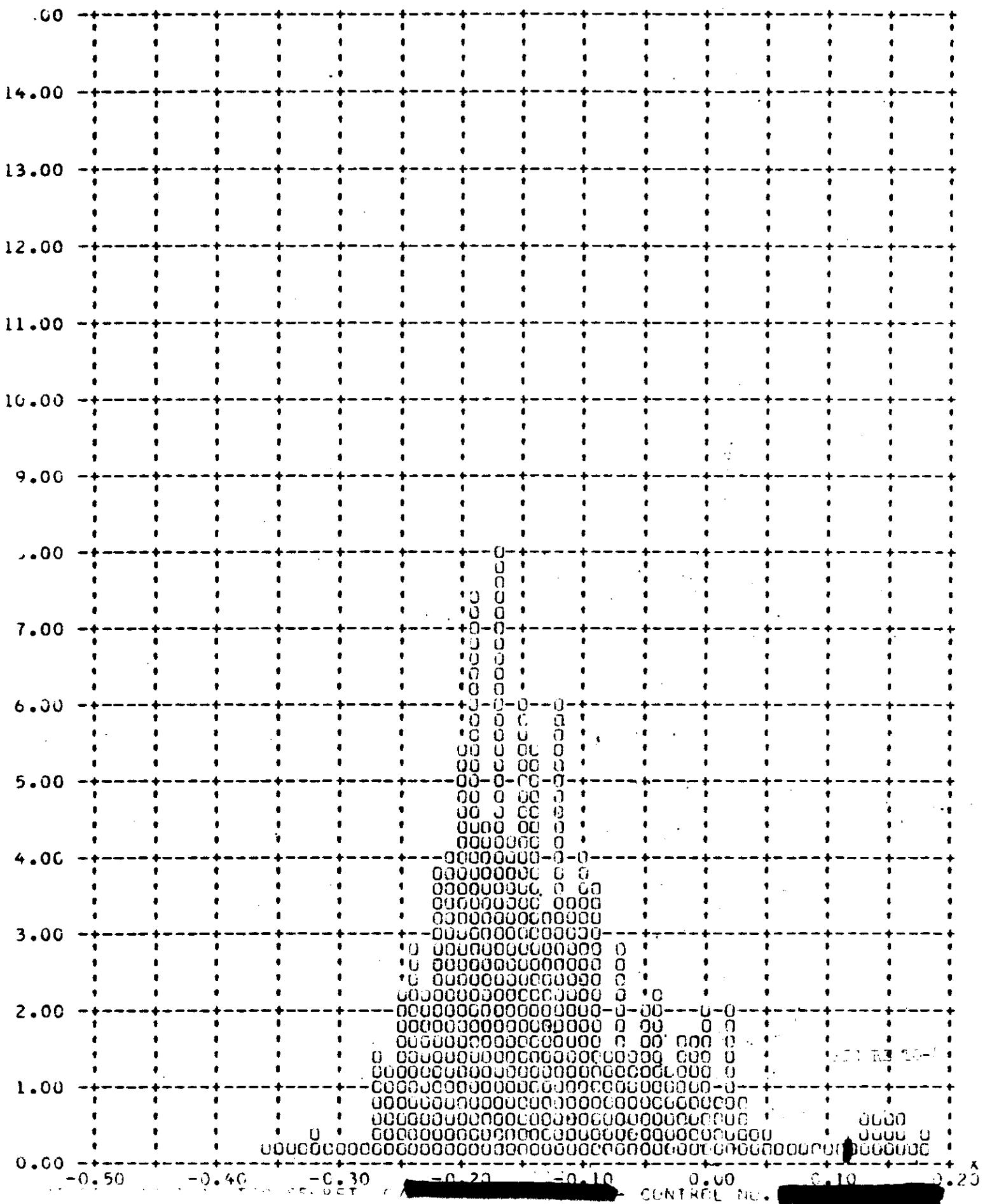
MISSION 1041B1 ~~TOP SECRET~~ C CONTROL NO.
FRAMES 1-6 OF EACH OP OMITTED 90 PERCENT = 0.20

Y PITCH ANGLE ERROR - DEGREES (X) VERSUS FREQUENCY - PERCENT (Y)



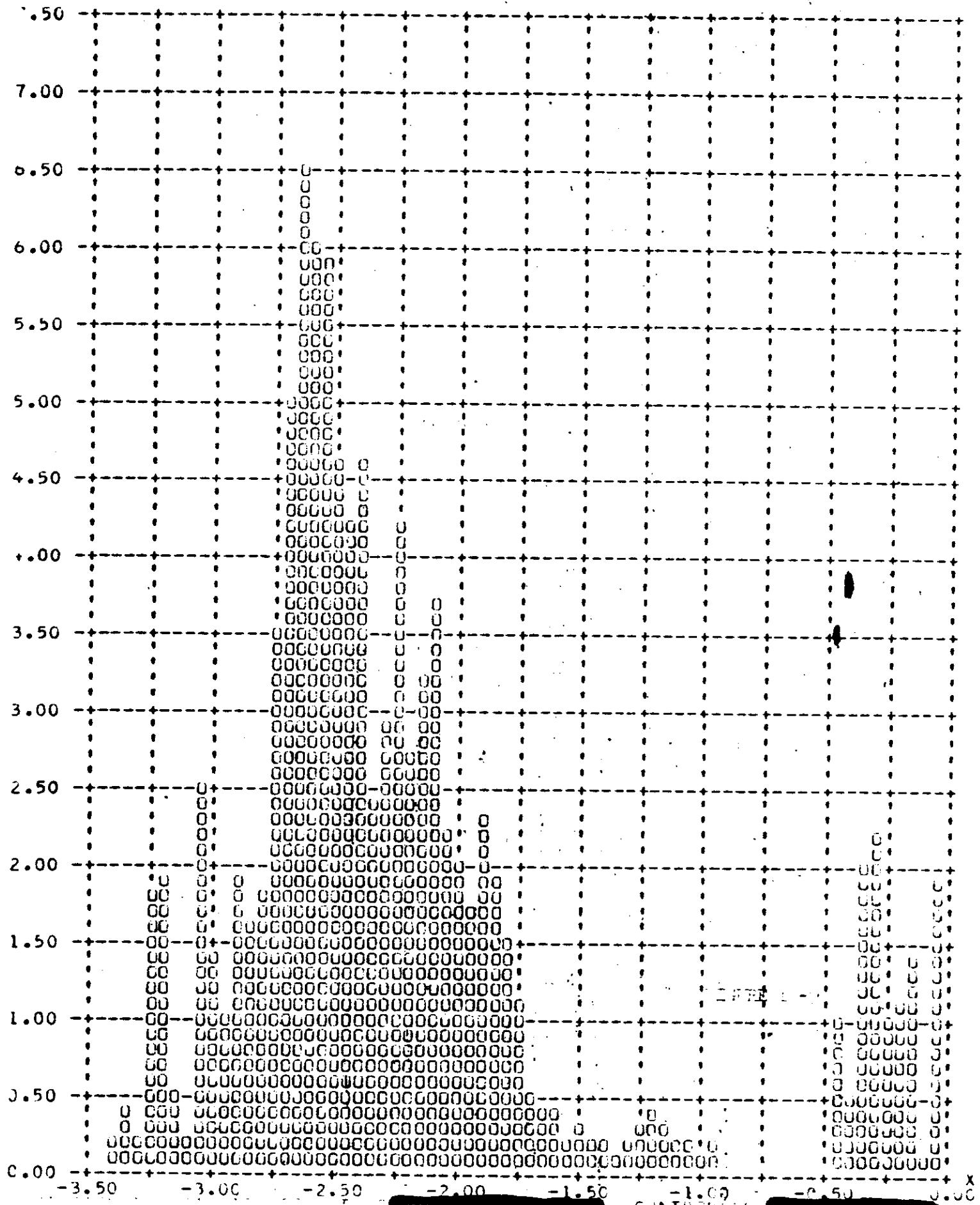
MISSION 1041B1 ~~TOP SECRET~~ C - CONTROL NO. [REDACTED]
FRAMES 1-6 OF EACH UP OMITTED 90 PERCENT = 0.23

Y ROLL ANGLE ERROR - DEGREES (X) VERSUS FREQUENCY - PERCENT (Y)



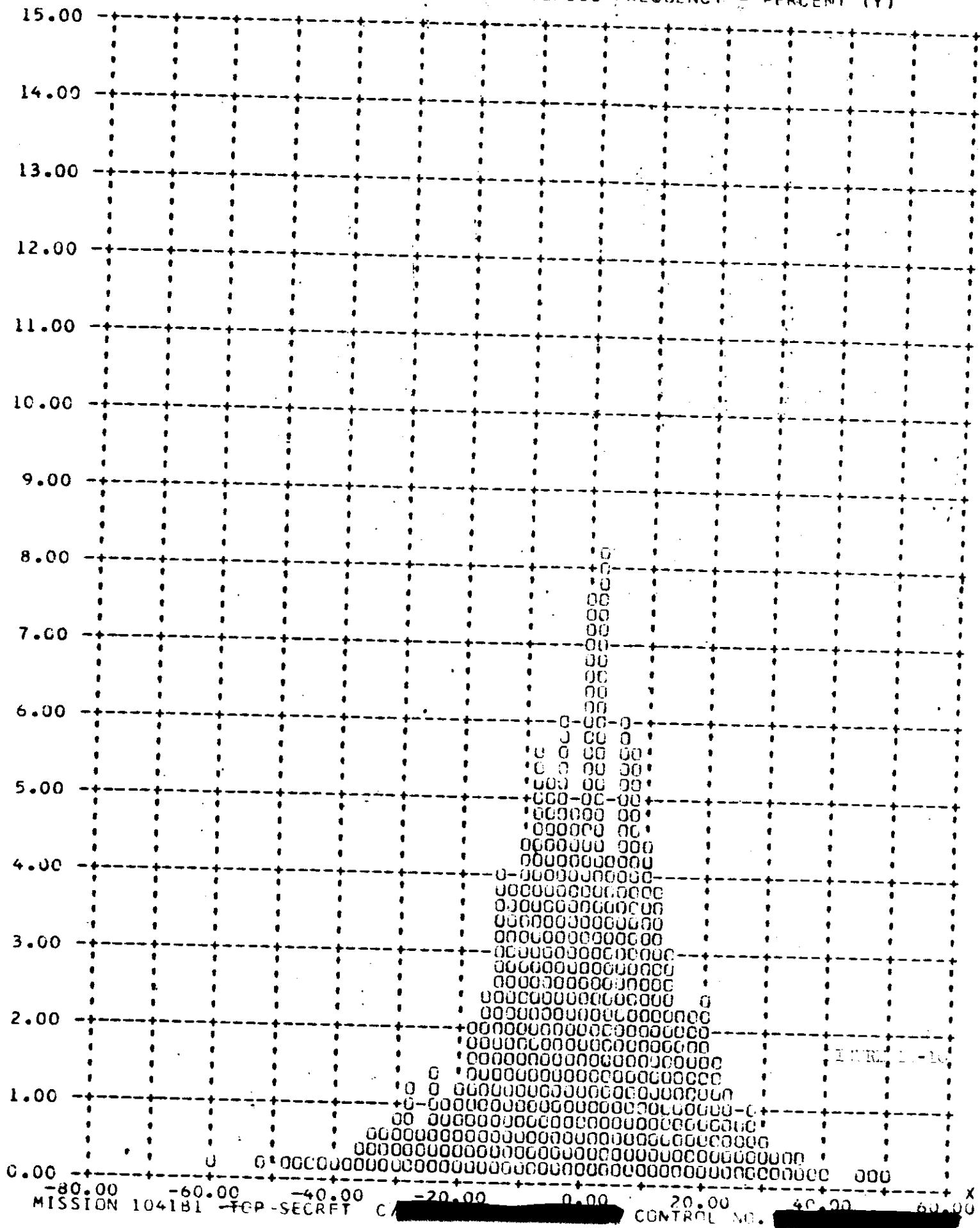
MISSION 104181 ~~TOP SECRET~~ C - CONTROL NO. [REDACTED]
FRAMES 1-6 OF EACH JP OMITTED 9C PERCENT = 2.94

Y YAW ANGLE ERROR - DEGREES (X) VERSUS FREQUENCY - PERCENT (Y)



MISSION 1041B1 ~~TOP SECRET~~ C CONTROL NO. FRAMES 1-6 OF EACH CP OMITTED 90 PERCENT = 22.94

Y PITCH RATE ERROR - DEG/HOUR (X) VERSUS FREQUENCY - PERCENT (Y)

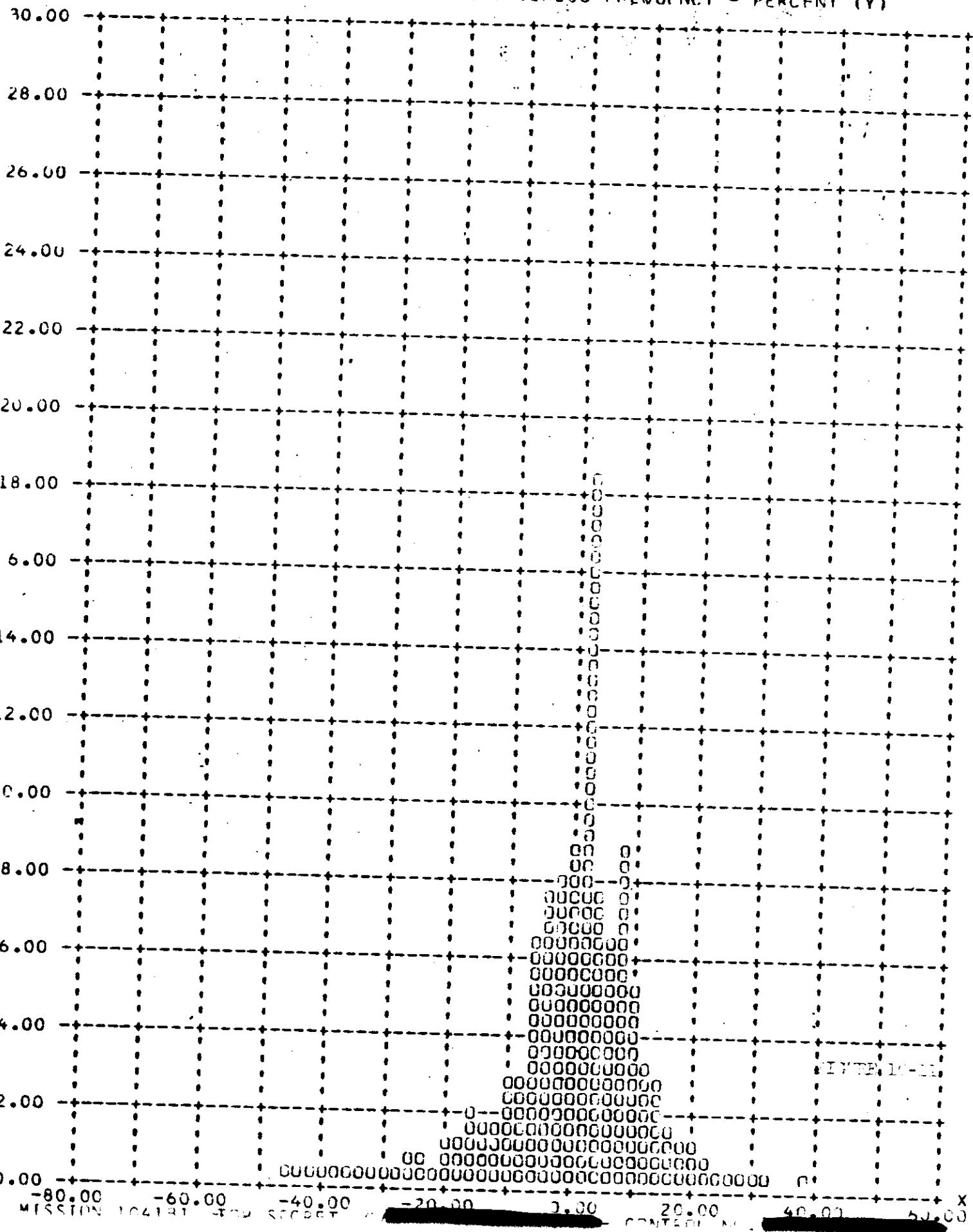


MISSION 1041B1 ~~TOP SECRET~~ C

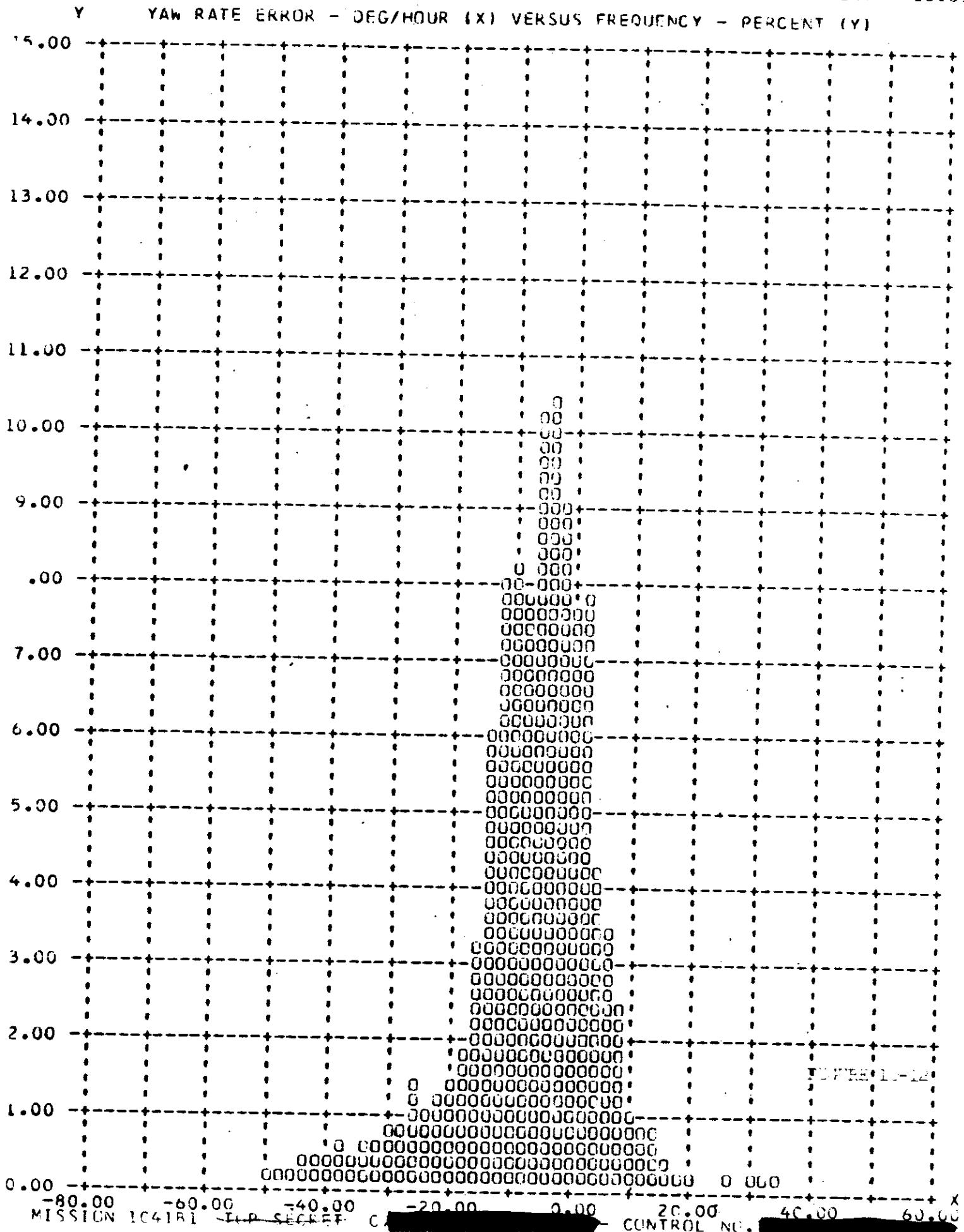
CONTROL NO.

MISSION 1041BI ~~TOP SECRET~~ C - CONTROL NO. [REDACTED] -
FRAMES 1-6 OF EACH UP OMITTED 90 PERCENT = 15.76

Y ROLL RATE ERROR - DEG/HOUR (X) VERSUS FREQUENCY - PERCENT (Y)



MISSION 104181 ~~TOP SECRET~~ C - CONTROL NO. [REDACTED]
FRAMES 1-6 OF EACH CP OMITTED 90 PERCENT = 18.83.



~~TOP SECRET~~

C/ NO. [REDACTED]

SECTION II

IMAGE SMEAR ANALYSIS

The frame correlation tape supplied to A/P by NPIC contains the binary time word of each frame of photography. A computer program has been assembled at A/P which calculates the exposure time of each frame and compares the camera cycle rate with the ephemeris to calculate the V/H mismatch. This data is combined with the vehicle attitude error and rate values of each frame and the crab error caused by earth rotation at the latitude of each frame. The program outputs the total along track and cross track IMC error and the limit of ground resolution that can be acquired by a camera regardless of focal length and system capabilities.

The computer rejects the first six frames of all operations as the large V/H error induced by camera start-up is not representative of the overall system operations. The frequency distribution of the V/H errors and resolution limits are computer plotted and are shown in Figure 11-1 through 11-16.

The summary table 11-1 presents the maximum V/H ratio errors and resolution limits that existed during 90% of the photographic operations and the total range of values during all operations that were computed.

MISSION 1041

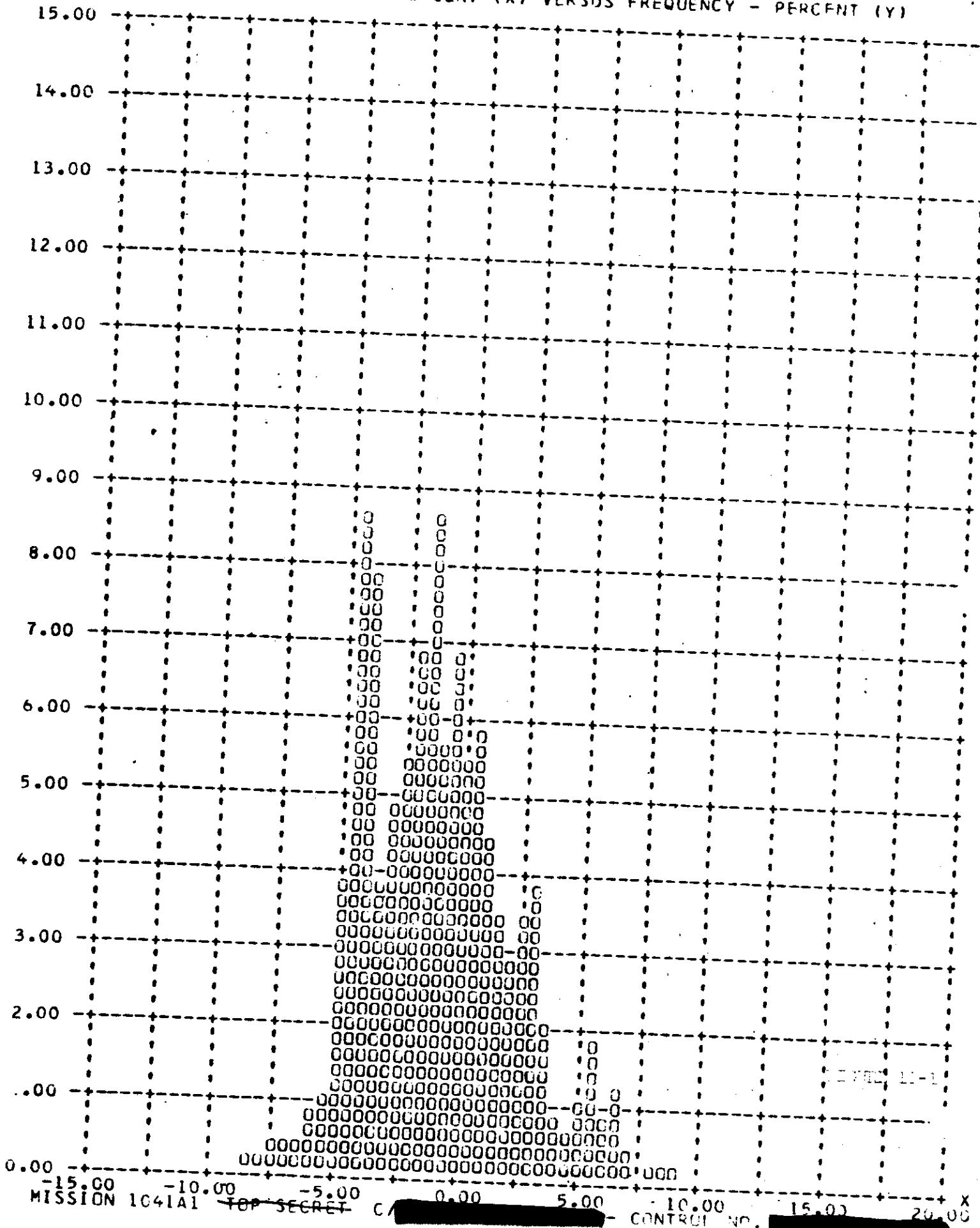
V/H RATIO AND RESOLUTION LIMITS

| <u>VALUE</u> | <u>UNITS</u> | <u>CAMERA</u> | MISSION 1041-1 | | MISSION 1041-2 | |
|------------------------------|--------------|---------------|----------------|--------------|----------------|---------------|
| | | | <u>20°</u> | <u>Range</u> | <u>20°</u> | <u>Range</u> |
| V/H Ratio Error | % | | 5.05 | -8.0 to +9.0 | 4.36 | -8.5 to +10.0 |
| | | FWD | 5.84 | -8.5 to +9.0 | 5.55 | -8.5 to +9.5 |
| Along Track Resolution Limit | Feet | | 6.12 | 0.2 to 12.2 | 6.36 | 0.2 to 23.2 |
| | | AFT | 5.72 | 0.2 to 15.4 | 5.46 | 0.2 to 10.0 |
| Cross Track Resolution Limit | Feet | | 3.43 | 0.2 to 6.6 | 2.14 | 0.2 to 6.0 |
| | | AFT | 2.98 | 0.2 to 5.4 | 2.04 | 0.2 to 4.6 |

TABLE II-1

MISSION 1041A1 TOP SECRET C - CONTROL NO. [REDACTED] - FRAMES 1-6 OF EACH UP OMITTED 90 PERCENT = 5.05

Y V/H RATIO ERROR - PERCENT (X) VERSUS FREQUENCY - PERCENT (Y)

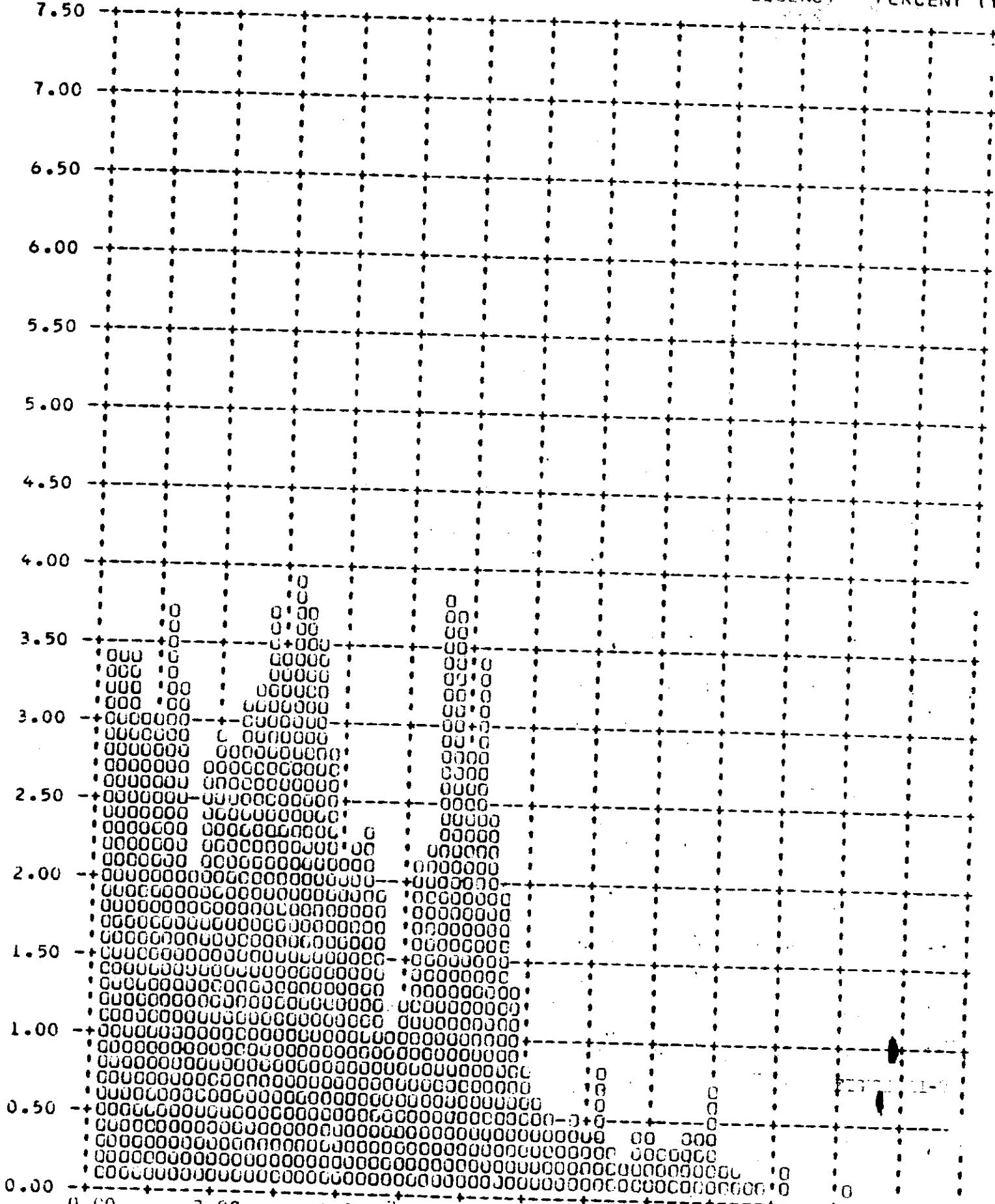


MISSION 1041A1 TOP SECRET C

CONTROL NO. [REDACTED]

MISSION 1041A1 ~~TOP SECRET~~ C - CONTROL NO. ~~SECRET~~ 6.42
FRAMES 1-6 OF EACH UP OMITTED 90 PERCENT = 6.42

Y ALONG TRACK RESOLUTION LIMIT - FEET (X) VERSUS FREQUENCY - PERCENT (Y)

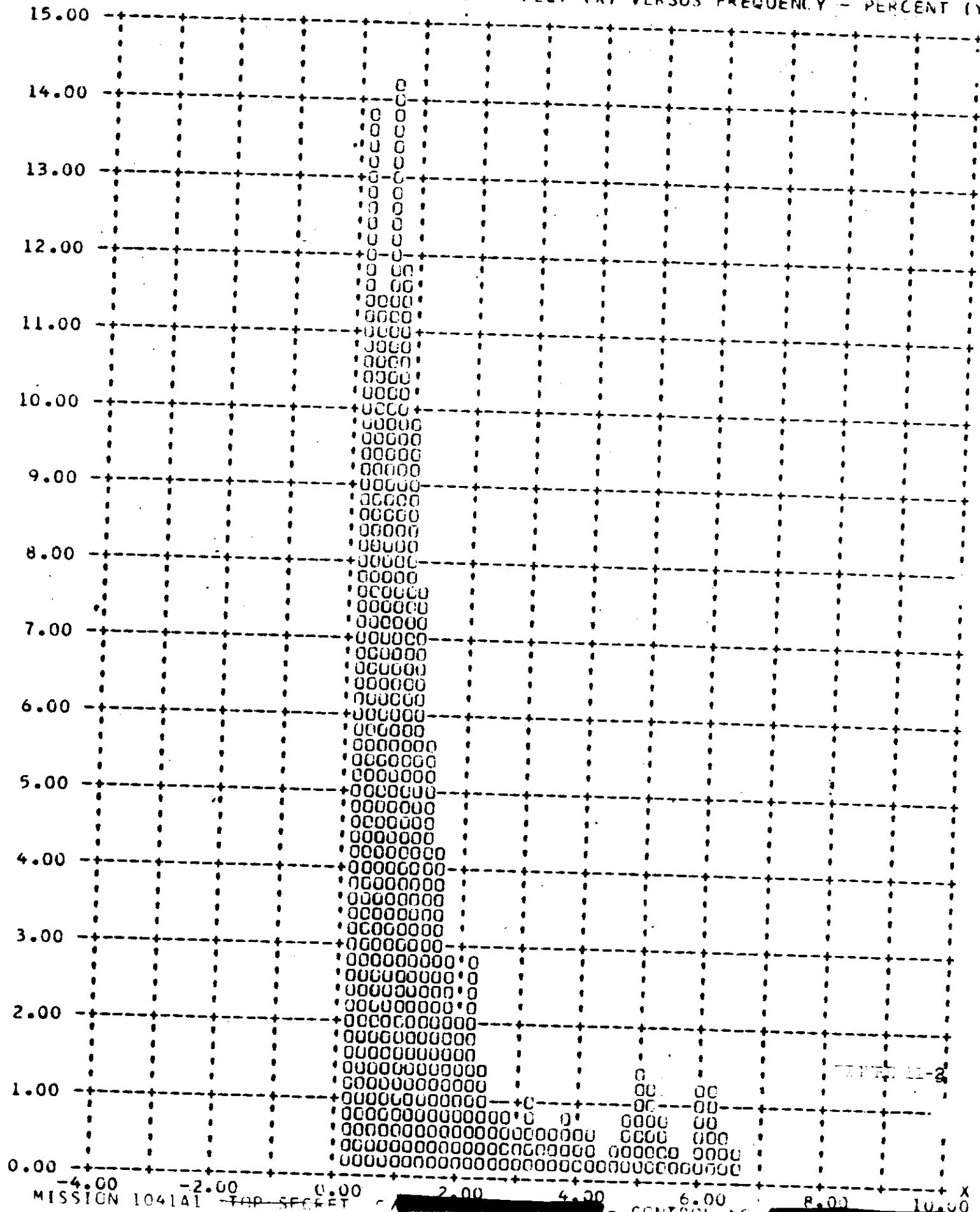


MISSION 1041A1 ~~TOP SECRET~~ 6.42

MISSION 1041A1 -TOP SECRET C

- CONTROL NO. [REDACTED] -
FRAMES 1-6 OF EACH OP OMITTED 90 PERCENT = 5.43

Y CROSS TRACK RESOLUTION LIMIT - FEET (X) VERSUS FREQUENCY - PERCENT (Y)

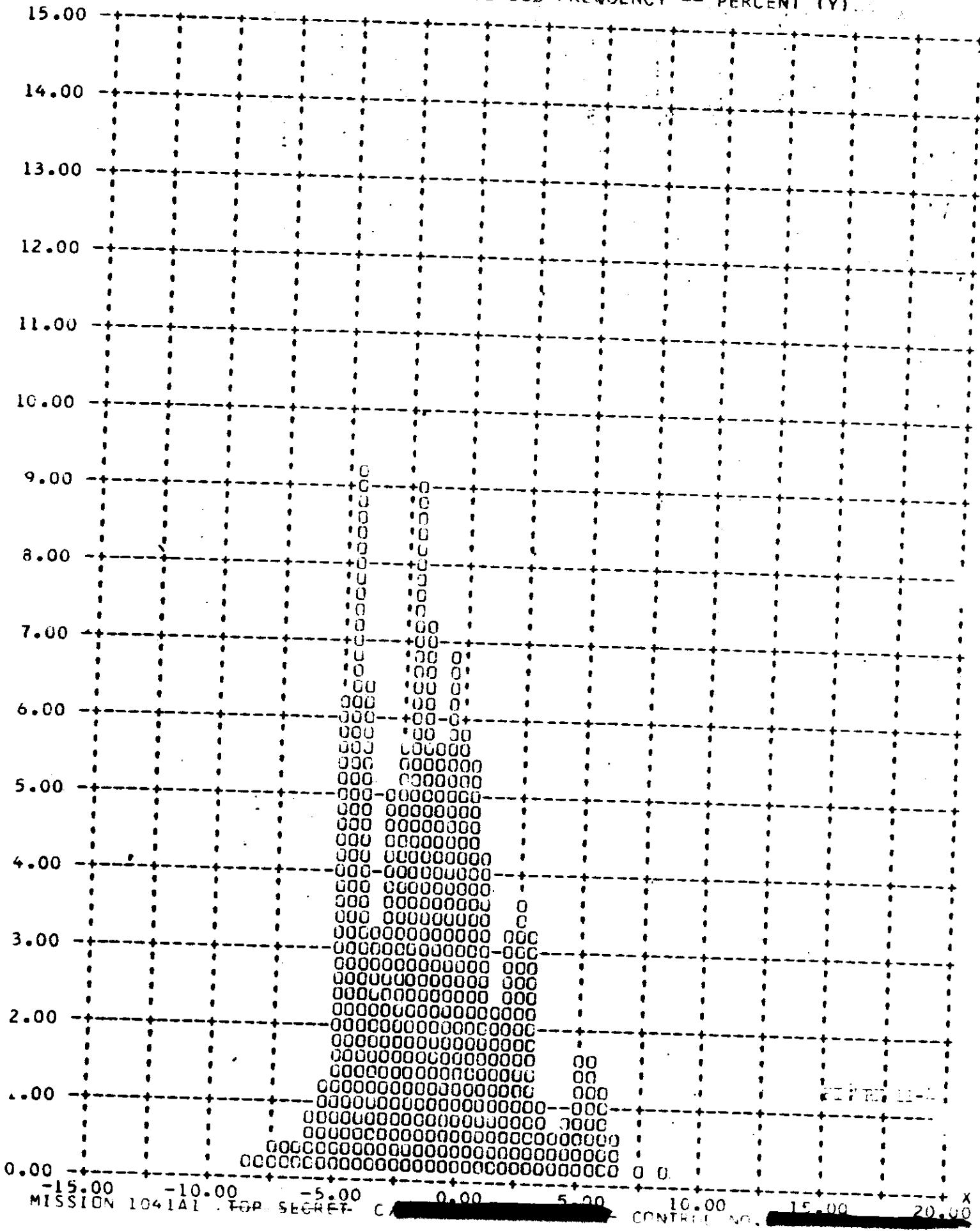


MISSION 1041A1 -TOP SECRET C

MISSION 1041A1 TOP SECRET C

CONTROL NO. [REDACTED] FRAMES 1-6 OF EACH UP OMITTED 90 PERCENT = 5.15

Y IMC ERROR -- PERCENT (X) VERSUS FREQUENCY -- PERCENT (Y)

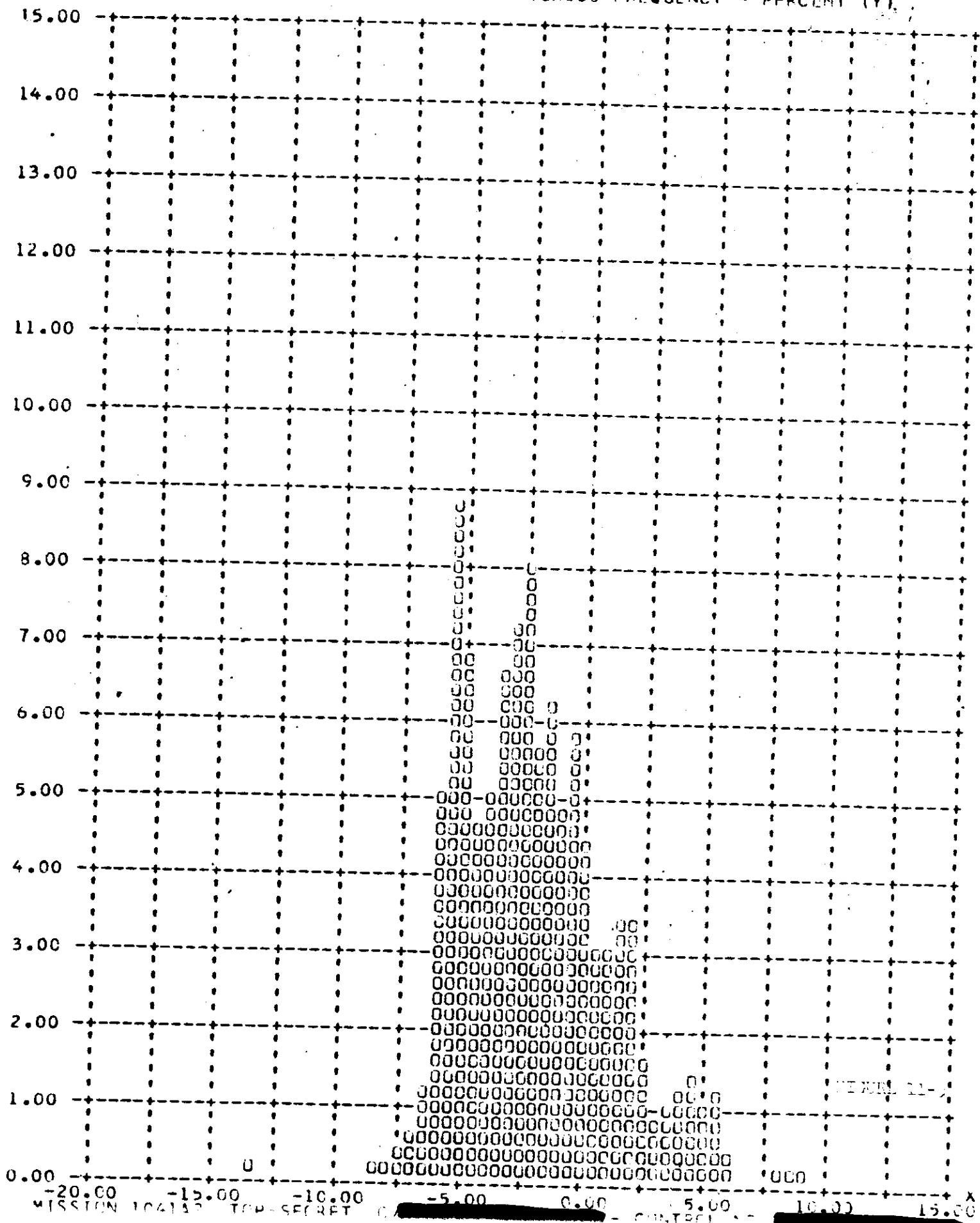


MISSION 1041A1 TOP SECRET C

CONTROL NO. [REDACTED]

MISSION 1041A2 TGP SECRET C - CONTROL NO. [REDACTED] - FRAMES 1-6 OF EACH UP OMITTED 96 PERCENT = 5.84

Y V/H RATIO ERROR - PERCENT (X) VERSUS FREQUENCY - PERCENT (Y).



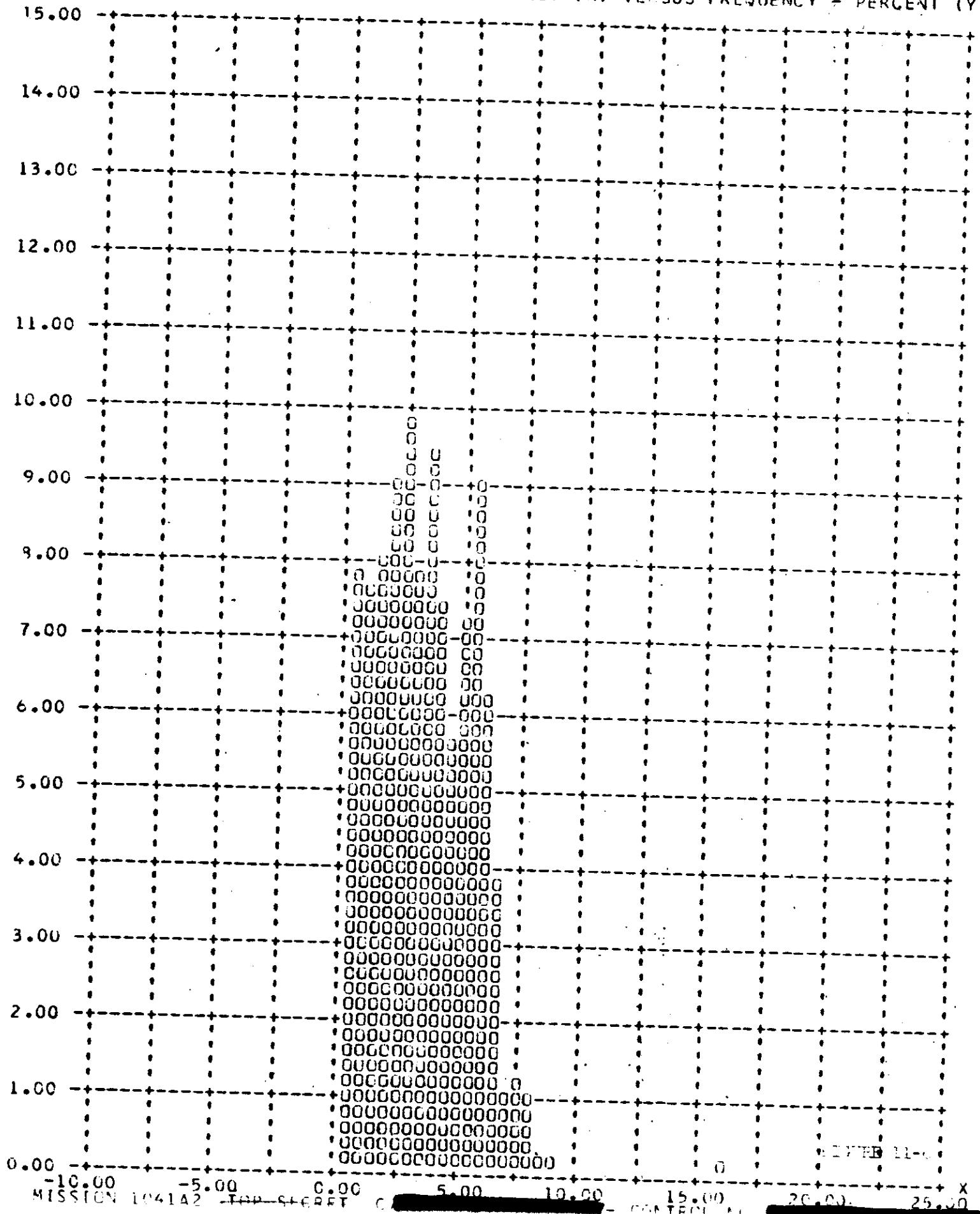
MISSION 1041A2 TGP SECRET C

CONTROL NO. [REDACTED]

MISSION 1041A2 ~~TOP SECRET~~ C

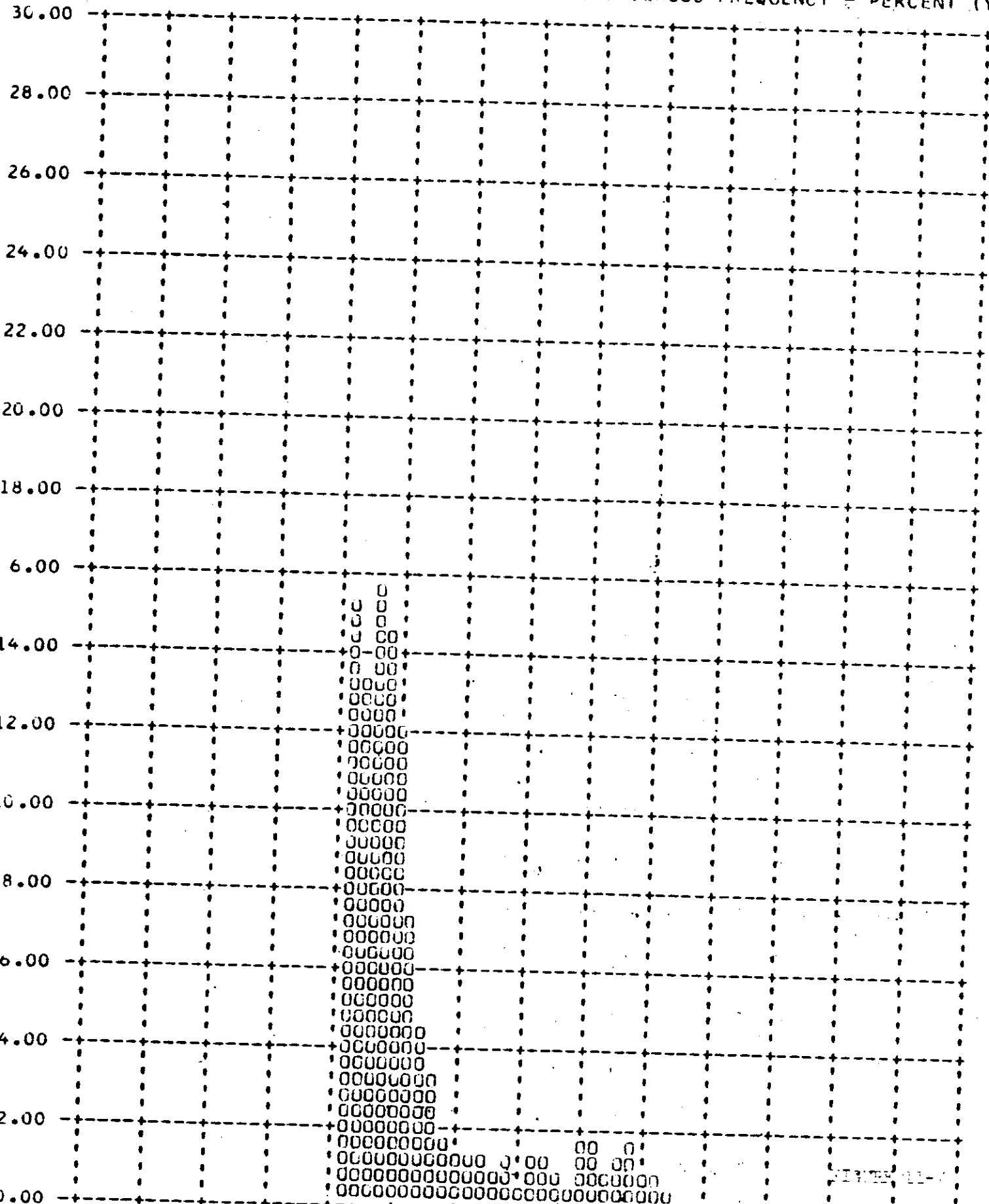
CONTROL NO. ~~C~~ FRAMES 1-6 OF EACH OP OMITTED 90 PERCENT = 5.72

Y ALONG TRACK RESOLUTION LIMIT - FEET (X) VERSUS FREQUENCY - PERCENT (Y)



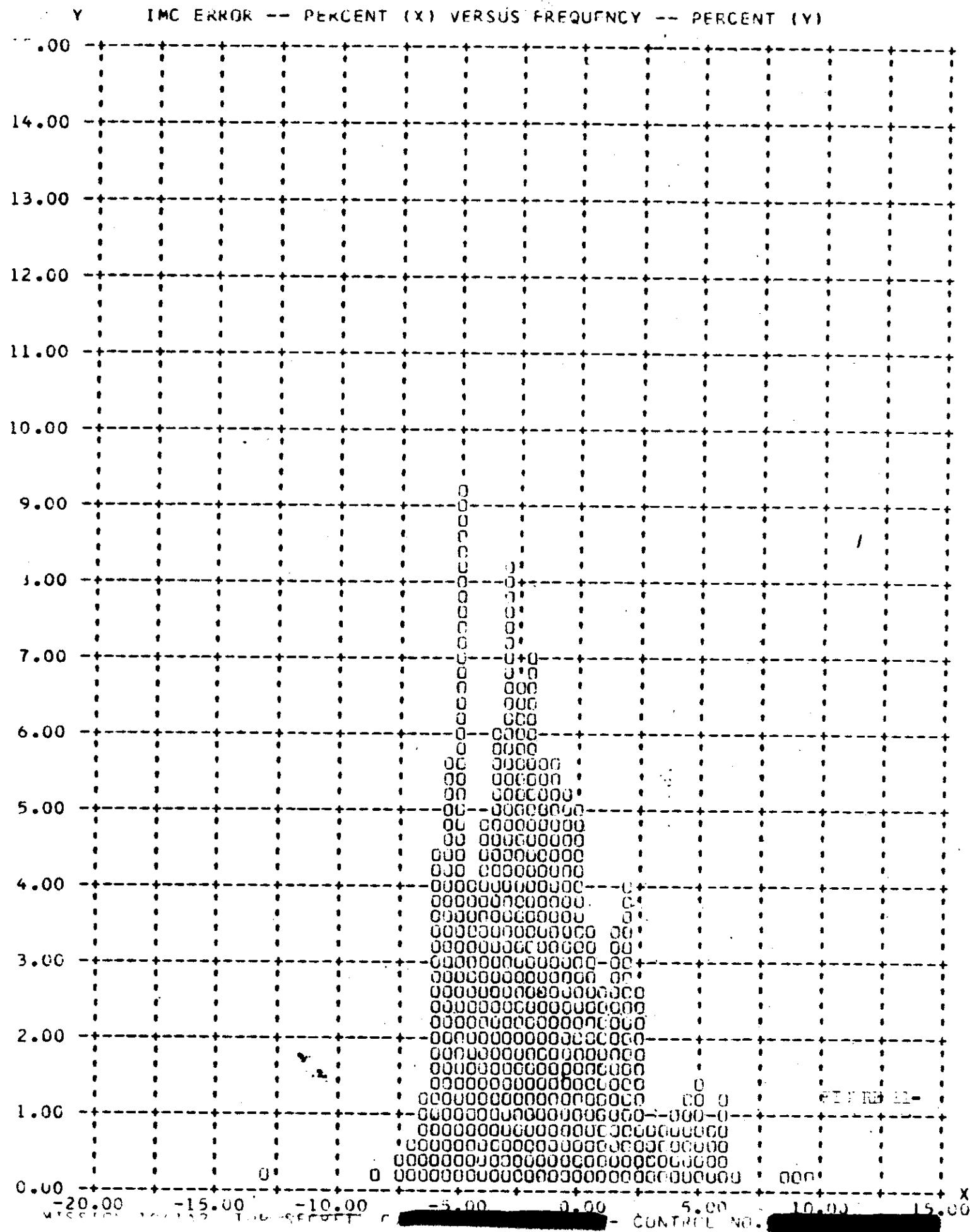
MISSION 1041A2 TOP SECRET C CONTROL NO. [REDACTED] 90 PERCENT = 2.98
FRAMES 1-6 OF EACH UP OMITTED

Y CROSS TRACK RESOLUTION LIMIT - FEET (X) VERSUS FREQUENCY - PERCENT (Y)

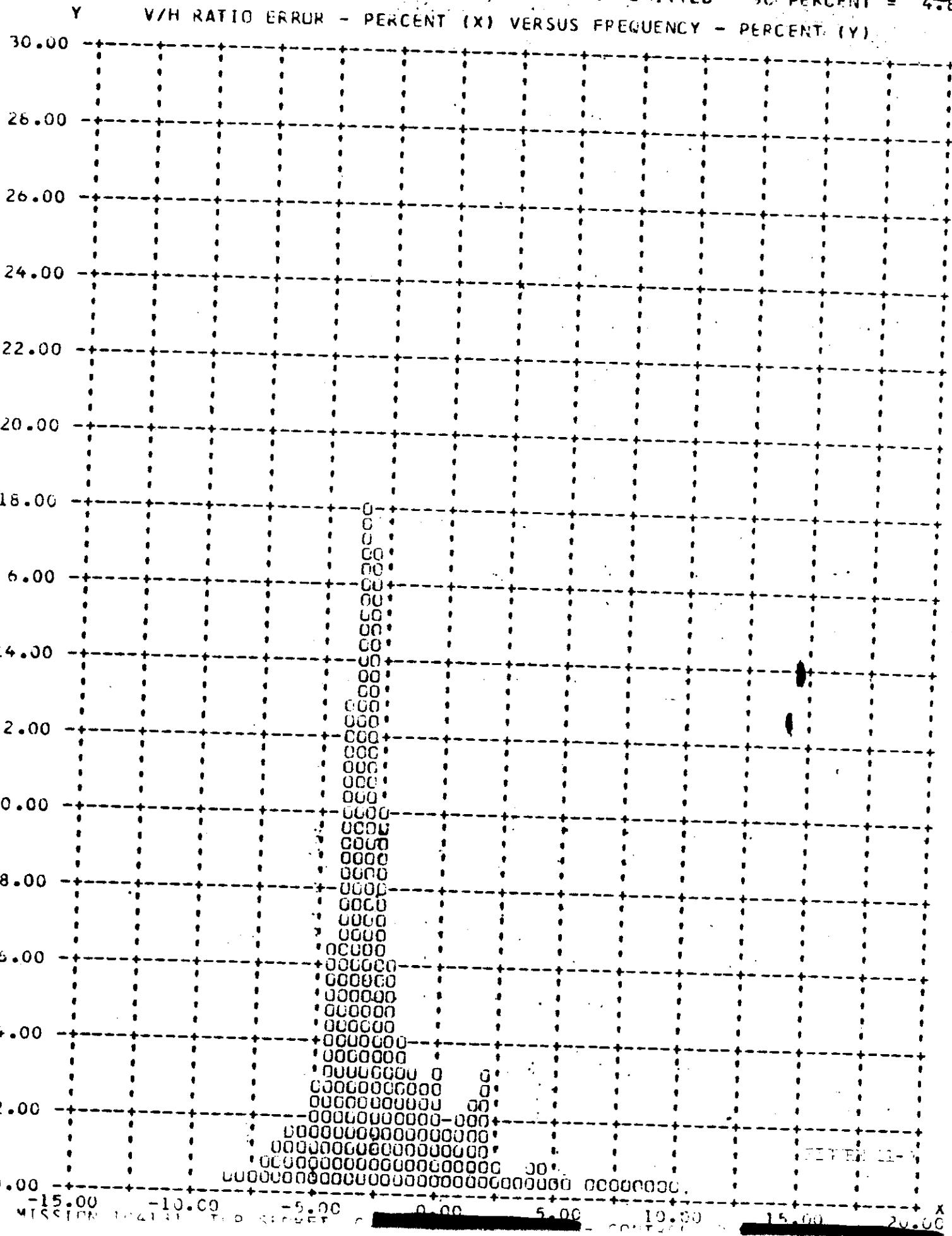


-4.00 -2.00 0.00 2.00 4.00 6.00 8.00 10.00
MISSION 1041A2 TOP SECRET C [REDACTED] CONTROL NO. [REDACTED]

MISSION 1041A2 ~~TOP SECRET~~ C/ CONTROL NO. ~~SECRET~~
FRAMES 1-6 OF EACH UP OMITTED 90 PERCENT = 5.74

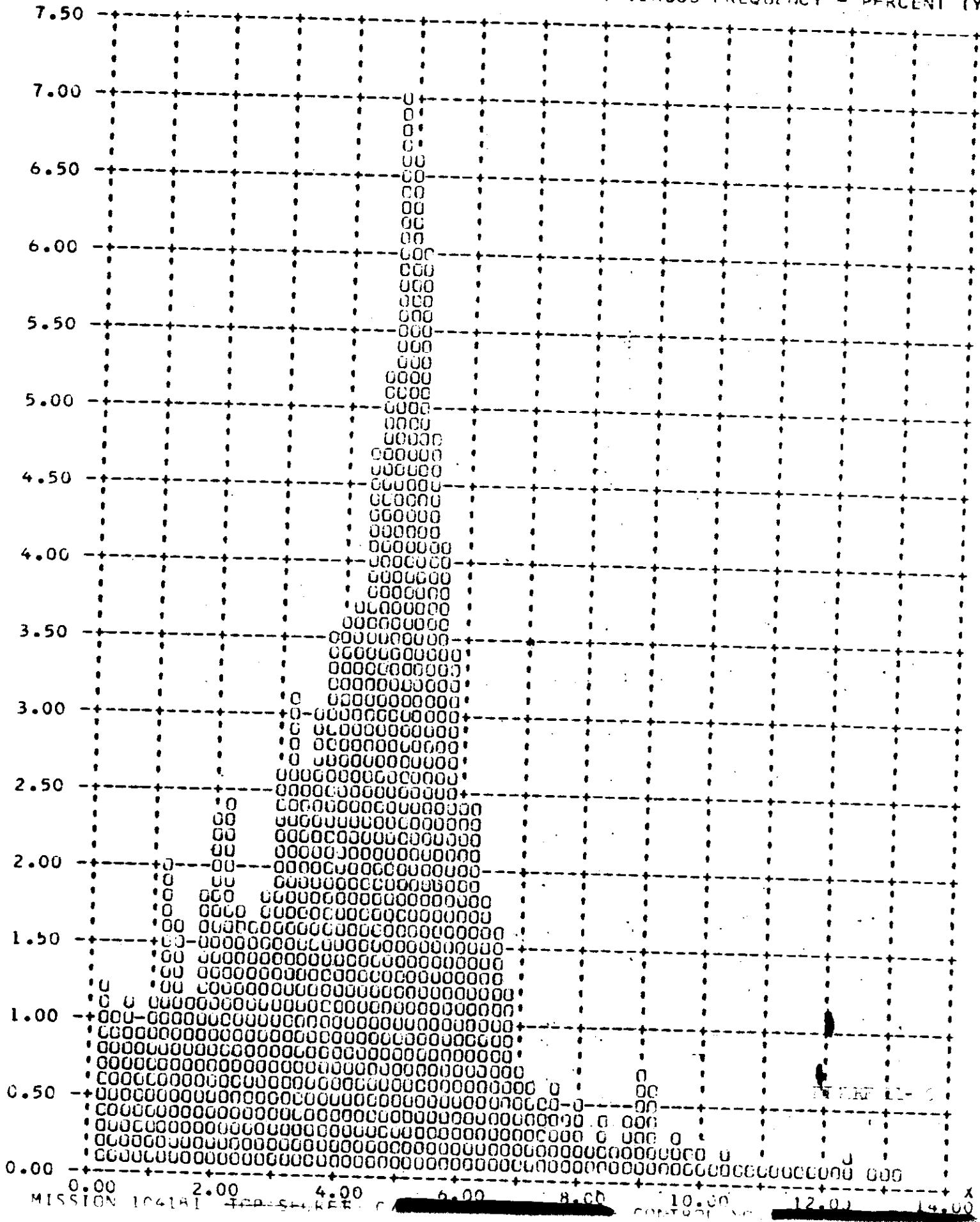


MISSION 104181 ~~TOP SECRET~~ C CONTROL NO. [REDACTED] 90 PERCENT = 4.86
FRAMES 1-6 OF EACH UP OMITTED



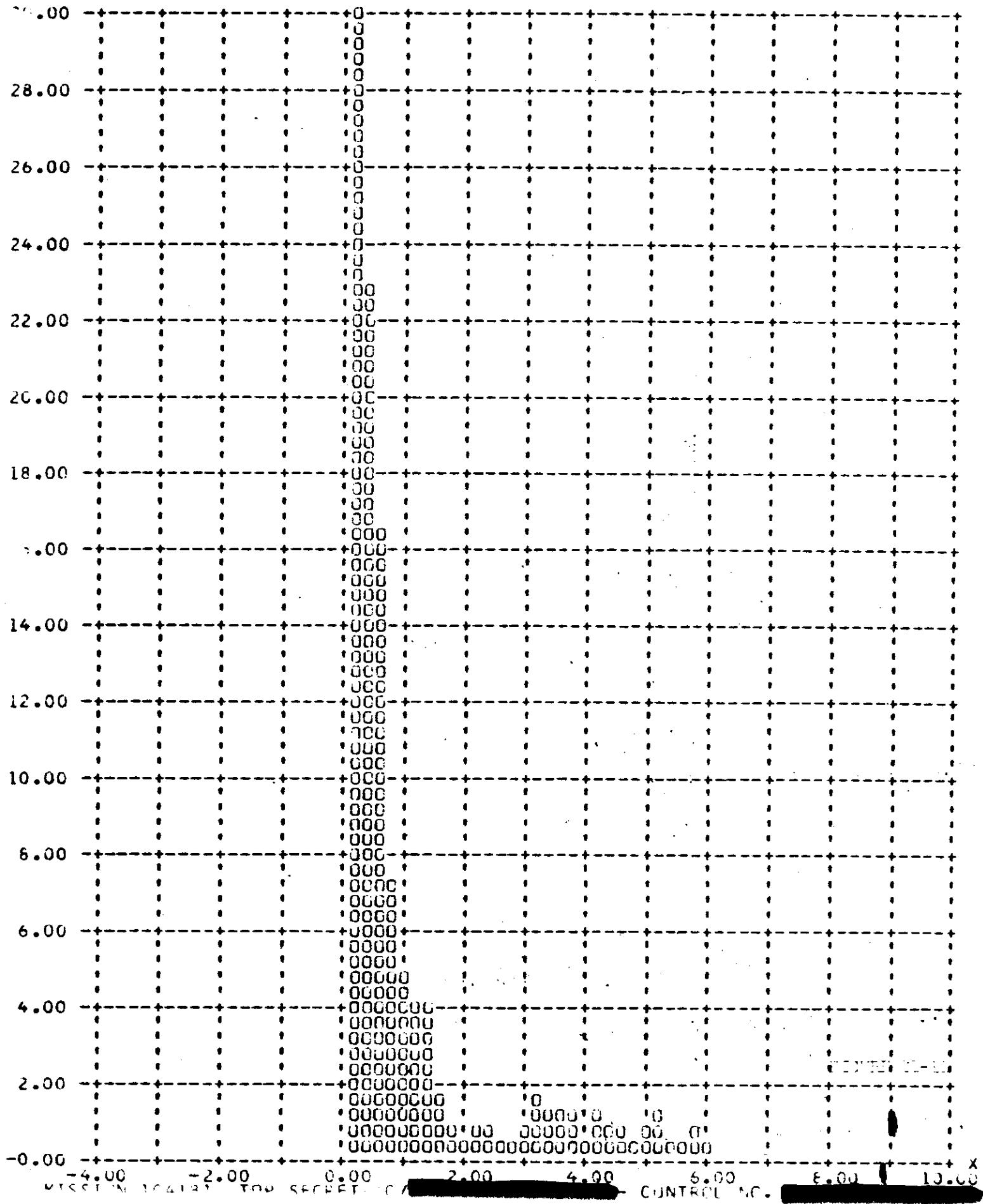
MISSION 104181 ~~TOP SECRET~~ C - CONTROL NO. ~~SECRET~~
FRAMES 1-6 OF EACH UP OMITTED. 90 PERCENT = 5.36

Y ALONG TRACK RESOLUTION LIMIT - FEET (X) VERSUS FREQUENCY - PERCENT (Y)



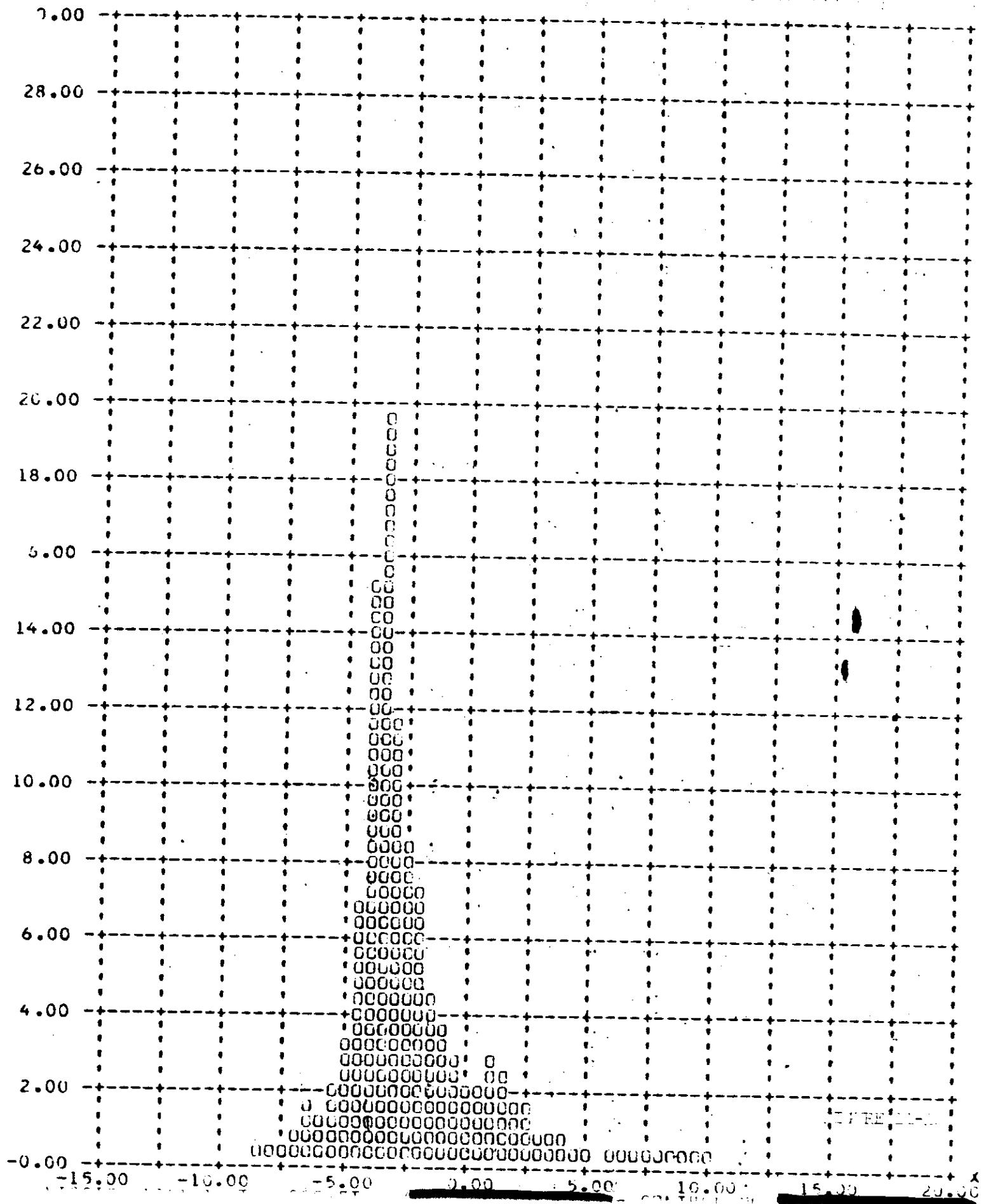
MISSION 104181 ~~TOP SECRET~~ C CONTROL NO. 90 PERCENT = 2.14
FRAMES 1-6 OF EACH UP OMITTED

Y CROSS TRACK RESOLUTION LIMIT - FEET (X) VERSUS FREQUENCY - PERCENT (Y)



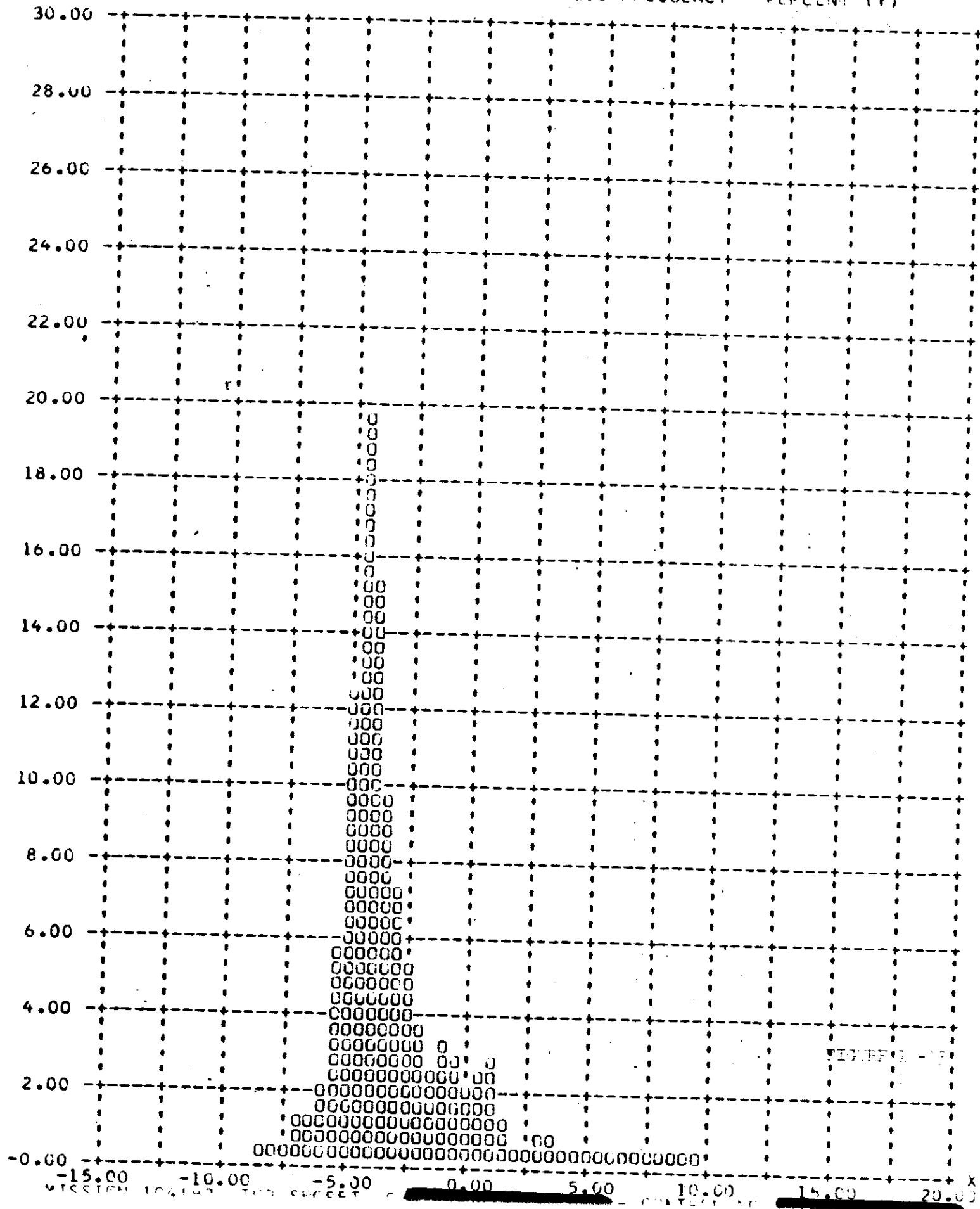
MISSION 104181 ~~TOP SECRET~~ C CONTROL NO. [REDACTED]
FRAMES 1-6 OF EACH DP OMITTED 90 PERCENT = 4.94

Y IMC ERROR -- PERCENT (X) VERSUS FREQUENCY -- PERCENT (Y)



MISSION 104182 ~~TOP SECRET~~ C CONTROL NO. [REDACTED]
FRAMES 1-6 OF EACH CP COMMITTED 90 PERCENT = 3.055

Y . V/H RATIO ERROR - PERCENT (X) VERSUS FREQUENCY - PERCENT (Y)

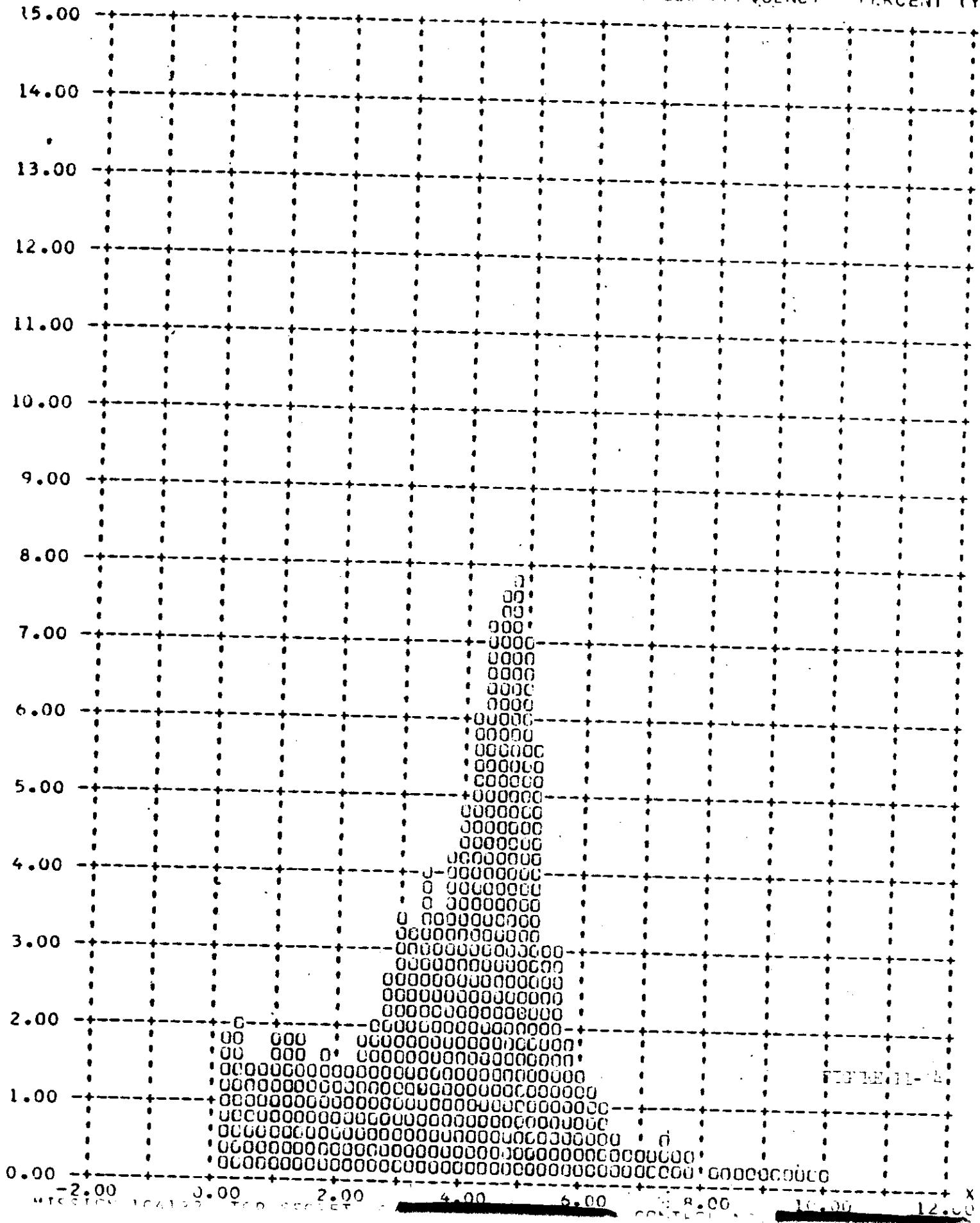


-15.00 -10.00 -5.00 0.00 5.00 10.00 15.00 20.00
MISSION 104182 ~~TOP SECRET~~

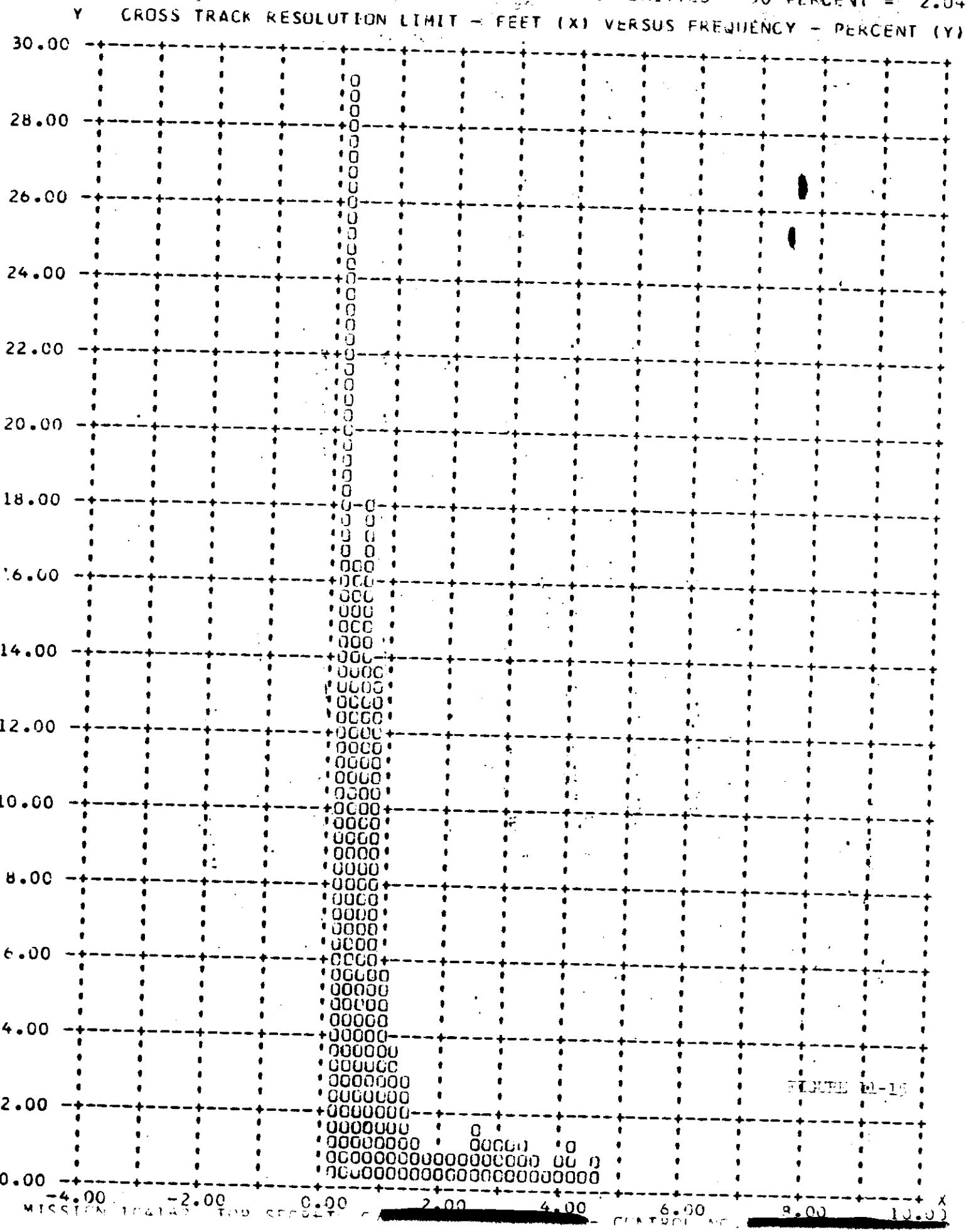
MISSION 104182 ~~TOP SECRET~~

C CONTROL NO. [REDACTED] - FRAMES 1-6 OF EACH UP OMITTED 90 PERCENT = 5.4b

Y ALONG TRACK RESOLUTION LIMIT - FEET (X) VERSUS FREQUENCY - PERCENT (Y)

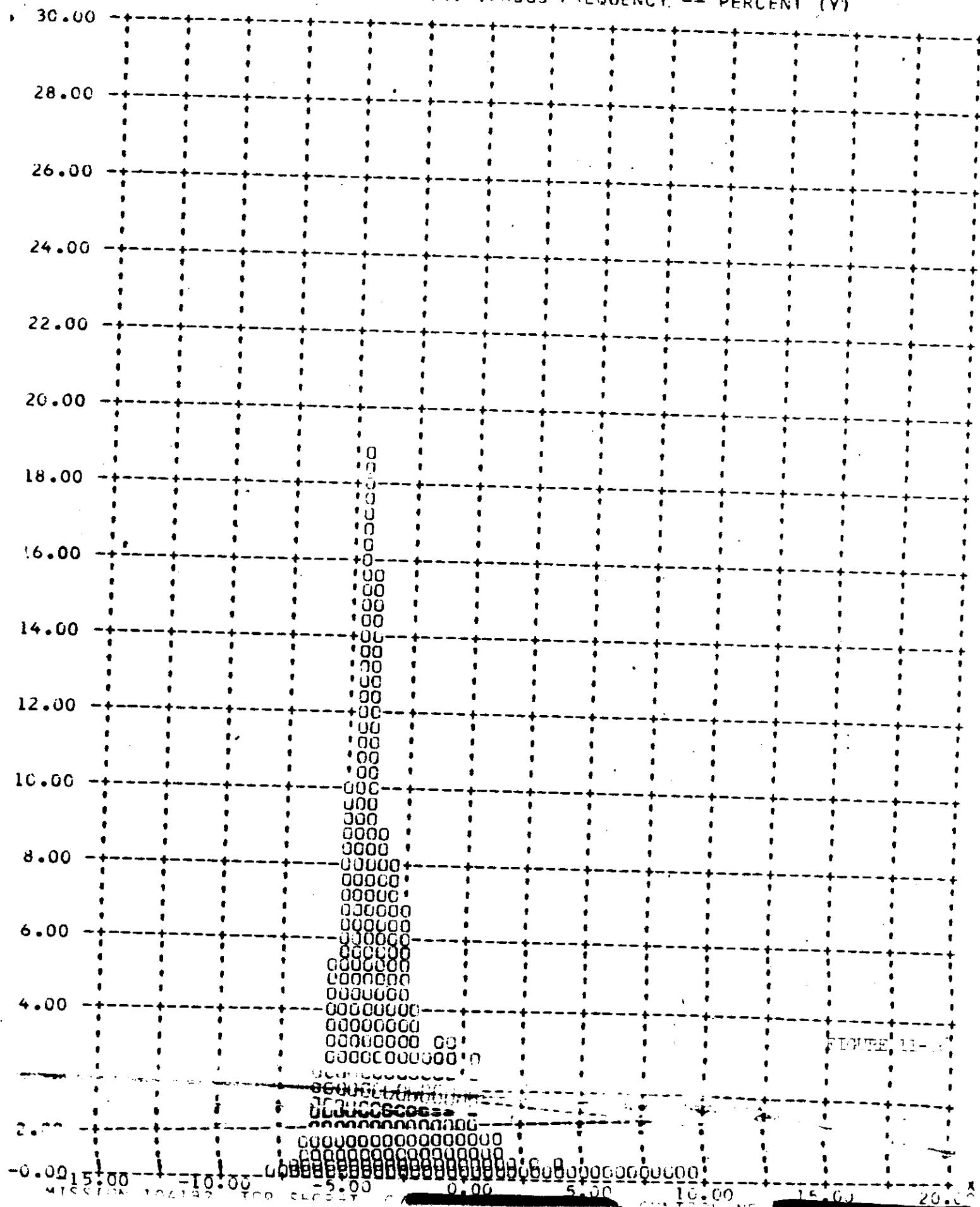


MISSION 104182 ~~TOP SECRET~~ C CONTROL NO. ~~SECRET~~
FRAMES 1-6 OF EACH UP OMITTED ~~TOP SECRET~~ 90 PERCENT = 2.04



MISSION 1041B2 - TOP SECRET C - CONTROL NO. [REDACTED] - 90 PERCENT = 5.51
FRAMES 1-6 OF EACH UP OMITTED

Y IMC ERROR -- PERCENT (X) VERSUS FREQUENCY -- PERCENT (Y)



SECTION 12

SYSTEM RELIABILITY

Reliability calculations for the payload are based on a sample beginning with M-7. Hence both the major part of the Lunar Program and the "J" Program are covered in the calculation. For certain auxiliaries, i.e., the Stellar-Index camera and the horizon cameras, the sample size is changed to recognize incorporation of modified equipment or new designs where reliability was one of the principal reasons for the modification. However, for primary mission function, the sample size is consistent with reliability reporting for the vehicle.

The reliability estimates of this section deal exclusively with the payload. Failures to achieve orbit or vehicle induced failures are thereby excluded. Recoveries before a complete mission has been completed are considered as full missions providing that early termination was caused by reasons not connected with payload operation. Film quality is not considered in the reliability estimate calculation. Hence, only electrical and mechanical functioning are considered.

The reliability estimate is also divided into primary and secondary functions. The primary functions are operation of the panoramic cameras, main camera door operation, operation of the payload clock, and recovery operations. The secondary mission functions are horizon camera operation excluding catastrophic open shutter failure mode; auxiliary data recording, and Stellar-Index camera operation. A summary of estimated reliability is shown in Tables 12-1.

Panoramic Camera Reliability

Sample Size - 179 opportunities to operate.

One failure - S/I Programmer on System J-19.

Assume - 3000 cycles per camera per mission.

Estimated Reliability = 99.1% at 50% confidence level.

Main Camera Door Reliability

Sample Size - 58 vehicles x 2 doors = 116 opportunities to operate
Estimated Reliability = 99.4% at 50% confidence level.

Payload Command and Control

Sample Size - 10,176 hours operation in sample

Two failures

Estimated Reliability = 97.5% at 50% confidence level

Payload Clock Reliability

Sample Size - 10,176 hours operation in sample

No failures

Estimated Reliability = 99.3% at 50% confidence level

Estimated Reliability of Payload Functioning on orbit = 97.6% at 50% confidence level

Recovery System Reliability

81 opportunities to recover

1 failure - improper separation due to water seal - cutter failure

Estimated Reliability = 97.9% at 50% confidence level

Stellar-Index Camera Reliability

Sample begins with J5.

Sample size = 25,930

Four failures

Estimated Reliability = 92.6% at 50% confidence level

Horizon Camera Reliability

Sample begins with J5 - 193,500 cycles

Estimated Reliability of Single Camera = 99.0% at 50% confidence level

Estimated Reliability of Four Horizon Cameras at a Parallel

Redundant System = 99.9% at 50% confidence level.

ESTIMATED RELIABILITY SUMMARY (AT 50% CONFIDENCE LEVEL)

ESTIMATED RELIABILITY SUMMARY

(AT 50% CONFIDENCE LEVEL)

| MISSION NUMBER | PRIMARY FUNCTIONS | | | | | | SECONDARY FUNCTIONS | | | | | |
|----------------|-------------------|--------|---------|--------------------------|---------|-------------|---------------------|---------|-------------|-----------------|---------|-------------|
| | PANORAMIC CAMERA | | | COMMAND & CONTROL SYSTEM | | | RECOVERY SYSTEM | | | HORIZON CAMERAS | | |
| | SAMPLE | SAMPLE | PAYOUTS | SAMPLE | PAYOUTS | RELIABILITY | SAMPLE | PAYOUTS | RELIABILITY | SAMPLE | PAYOUTS | RELIABILITY |
| 1020 | 76 | 5544 | 9544 | 0 | 96.9 | 96.9 | 43 | 10,680 | 2 | 89.9 | 48,000 | 0 |
| 1021 | 90.5 | 99.1 | 97.1 | 0 | 98.9 | 98.9 | 96.1 | 9830 | 2 | 89.1 | 46,500 | 0 |
| 1022 | 76 | 5376 | 5376 | 0 | 96.9 | 96.9 | 41 | 96.0 | 2 | 89.1 | 51,000 | 0 |
| 1023 | 90.5 | 99.4 | 97.0 | 0 | 98.6 | 98.6 | 45 | 11,550 | 2 | 90.7 | 54,000 | 0 |
| 1024 | 82 | 5784 | 5784 | 0 | 96.9 | 96.9 | 47 | 12,190 | 2 | 90.7 | 57,000 | 0 |
| 1025 | 82 | 6000 | 6000 | 0 | 96.2 | 96.2 | 49 | 13,040 | 2 | 91.1 | 57,000 | 0 |
| 1026 | 84 | 6240 | 6240 | 0 | 95.8 | 95.8 | 47 | 96.5 | 2 | 91.6 | 54,000 | 0 |
| 1027 | 86 | 6240 | 6240 | 0 | 96.0 | 96.0 | 49 | 13,890 | 2 | 91.1 | 57,000 | 0 |
| 1028 | 86 | 6480 | 6480 | 0 | 96.9 | 96.9 | 51 | 14,740 | 2 | 92.1 | 60,000 | 0 |
| 1029 | 90 | 6720 | 6720 | 0 | 96.4 | 96.4 | 53 | 15,165 | 2 | 92.6 | 64,500 | 0 |
| 1030 | 90 | 6744 | 6744 | 0 | 96.5 | 96.5 | 55 | 16,015 | 3 | 90.0 | 67,500 | 0 |
| 1031 | 92 | 6960 | 6960 | 0 | 96.7 | 96.7 | 57 | 16,580 | 3 | 90.7 | 70,500 | 0 |
| 1029 | 94 | 7200 | 7200 | 0 | 96.8 | 96.8 | 59 | 17,430 | 4 | 88.7 | 73,500 | 0 |
| 1030 | 96 | 7440 | 7440 | 0 | 99.1 | 99.1 | 61 | 18,280 | 4 | 89.3 | 76,500 | 0 |
| 1031 | 98 | 7704 | 7704 | 0 | 99.7 | 99.7 | 63 | 19,73 | 4 | 89.7 | 79,6 | 0 |

ESTIMATED RELIABILITY SUMMARY (AT 50% CONFIDENCE LEVEL)

TABLE 12-1

SECTION 13

SUMMARY DATA

The comparison of the operating parameters and the performance achieved by previous missions has been difficult due to the large volume of data that results from each mission. Some of the pertinent characteristics from prior missions have been summarized in Tables 13-1 through 13-3.

The summary data was started with Mission 1004 as the J-05 camera system was the first to incorporate the major modifications of the titanium drum and scan arm, four roller scan head and Corona J capabilities. Only those missions that culminated in the recovery of some photography have been listed, therefore Missions 1003, 1005 and 1006 are deleted.

MISSION SUMMARY

TOP SECRET C/ NO.

| MISSION NUMBER | PAYOUT NUMBER | VEHICLE NUMBER | LAUNCH DATE | LAUNCH TIME | ORBIT INCLINATION [°] | PENIGEE LOCATION [NM] (+N) | RECOVERY PASS | MASTER CAMERA NUMBER | SLAVE CAMERA NUMBER | SLIT FILTER TYPE | CAMERA NUMBER | |
|----------------|---------------|----------------|-------------|-------------|-----------------------|----------------------------|---------------|----------------------|---------------------|------------------|---------------|-----------|
| 1004 | J-08 | 1174 | 2/15/64 | 2138 Z | 74.9 | 99.9 | 28.0 | 19 | 124 | 0.250 | W-21 | 028/29/28 |
| 1006 | J-09 | 1176 | 6/4/64 | 2259 Z | 79.8 | 64.0 | 63.2 | 65 | 148 | 0.200 | W-21 | D42/48/37 |
| 1007 | J-07 | 1609 | 6/19/64 | 2316 Z | 85.0 | 59.2 | 41.5 | 65 | 128 | 0.200 | W-21 | 048/47/45 |
| 1008 | J-10 | 1177 | 7/10/64 | 2314 Z | 85.0 | 59.4 | 40.8 | 49 | 144 | 0.250 | W-25 | 049/43/43 |
| 1009 | J-12 | 1605 | 8/5/64 | 2316 Z | 80.1 | 58.6 | 39.6 | 49 | 150 | 0.200 | W-21 | 054/45/48 |
| 1010 | J-11 | 1178 | 9/14/64 | 2254 Z | 84.9 | 57.4 | 42.6 | 65 | 152 | 0.175 | W-21 | 038/38/34 |
| 1011 | J-3X | 1170 | 10/5/64 | 2150 Z | 79.9 | 59.3 | 50.9 | 65 | 144 | 0.200 | W-21 | 041/41/41 |
| 1012 | J-13 | 1179 | 10/17/64 | 2202 Z | 75.0 | 56.2 | 32.4 | 49 | 156 | 0.200 | W-21 | 057/57/57 |
| 1013 | J-15 | 1175 | 11/2/64 | 2130 Z | 80.0 | 100.0 | 85.0 | 65 | 158 | 0.225 | W-21 | D46/52/53 |
| 1014 | J-16 | 1180 | 11/18/64 | 2036 Z | 70.0 | 103.2 | 65.6 | 61 | 145 | 0.250 | W-25 | 139 |
| 1015 | J-17 | 1607 | 12/19/64 | 2110 Z | 74.9 | 56.7 | 21.6 | 61 | 175 | 0.250 | W-25 | 053/59/49 |
| 1016 | J-18 | 1608 | 1/18/65 | 2101 Z | 74.9 | 59.4 | 30.2 | 61 | 159 | 0.250 | W-25 | D50/44/46 |
| 1017 | J-14 | 1611 | 2/23/65 | 2144 Z | 75.0 | 97.2 | 85.9 | 61 | 145 | 0.250 | W-25 | D61/61/61 |
| 1018 | J-19 | 1612 | 3/25/65 | 2111 Z | 96.0 | 100.2 | 40.3 | 65 | 140 | 0.250 | W-25 | D58/58/58 |
| 1019 | J-04 | 1614 | 4/29/65 | 2149 Z | 86.0 | 99.1 | 27.1 | 60 | 122 | 0.250 | W-25 | D55/55/50 |
| 1020 | J-20 | 1613 | 6/8/65 | 2158 Z | 75.1 | 97.1 | 40.6 | 37 | 136 | 0.250 | W-25 | D59/59/55 |
| 1021 | J-21 | 1615 | 6/18/65 | 1603 Z | 75.0 | 109.2 | 24.3 | 61 | 166 | 0.175 | W-21 | D60/60/63 |
| 1022 | J-22 | 1617 | 7/19/65 | 2201 Z | 85.0 | 99.7 | 30.3 | 65 | 144 | 0.250 | W-25 | D25/27/25 |
| 1023 | J-23 | 1618 | 8/17/65 | 2100 Z | 70.0 | 97.8 | 29.0 | 61 | 168 | 0.250 | W-25 | D65/77/70 |
| 1024 | J-24 | 1619 | 9/22/65 | 2131 Z | 80.0 | 95.9 | 18.4 | 61 | 172 | 0.225 | W-25 | D17/19/82 |
| 1025 | J-20 | 1616 | 10/5/65 | 1746 Z | 75.0 | 112.9 | 44.3 | 61 | 161 | 0.175 | W-21 | D66/75/72 |
| 1026 | J-25 | 1620 | 10/28/65 | 2117 Z | 75.0 | 93.0 | 17.0 | 61 | 170 | 0.225 | W-25 | D59/72/84 |
| 1027 | J-27 | 1621 | 12/9/65 | 2110 Z | 80.0 | 97.4 | 17.3 | 33 | 164 | 0.250 | W-25 | D72/69/65 |
| 1028 | J-26 | 1610 | 12/24/65 | 2105 Z | 80.0 | 97.6 | 28.4 | 61 | 176 | 0.250 | W-25 | D68/74/83 |
| | | | | | | | | 144 | 177 | 0.175 | W-21 | D74/76/95 |

TABLE 13-1

MISSION SUMMARY

| MISSION NUMBER | PAYLOAD NUMBER | VEHICLE NUMBER | LAUNCH DATE | ORBIT TIME | INCLINATION (°) | PERIGEE ALTITUDE (MM) (°N) | RECOVERY PASS | MASTER CAMERA NUMBER | SLAVE CAMERA NUMBER | SLIT FILTER TYPE | STELLAR INDEX | CAMERA NUMBER |
|----------------|----------------|----------------|-------------|------------|-----------------|----------------------------|---------------|----------------------|---------------------|------------------|---------------|------------------|---------------|------------------|---------------|------------------|---------------|---------------|
| | | | | | | | | | | | | | | | | | (°) | (°N) |
| 1029 | J-27 | 1623 | 2/2/66 | 2122 2 | 75.1 | 99.5 | 23.5 | 81 | 160 | 178 | 0.275 | W-25 | 179 | 0.175 | W-21 | 079/94/91 | D76/70/84 | |
| 1030 | J-28 | 1622 | 3/9/66 | 2202 2 | 75.0 | 97.5 | 19.7 | 81 | 162 | 182 | 0.275 | W-25 | 183 | 0.175 | W-21 | D94/100/07 | 088/103/02 | |
| 1031 | J-30 | 1627 | 4/7/66 | 2202 2 | 75.1 | 104.5 | 23.3 | 113 | 177 | 184 | 0.225 | W-23A | 185 | 0.150 | W-21 | 083/101/89 | 088/103/06 | |
| 1032 | J-28 | 1626 | 5/3/66 | 1925 2 | — | — | — | — | — | 180 | 0.150 | W-21 | 181 | 0.150 | W-21 | 081/97/101 | 080/97/100 | |
| 1033 | J-33 | 1630 | 5/24/66 | 0213 2 | 65.1 | 102.0 | 60.7 | 82 | 178 | 194 | 0.200 | W-21 | 195 | 0.200 | W-21 | 091/105/109 | 084/102/75 | |
| 1034 | J-31 | 1626 | 6/2/66 | 2131 2 | 80.1 | 105.4 | 19.2 | 81 | 161 | 186 | 0.200 | W-23A | 187 | 0.150 | W-21 | 085/09/76 | 087/107/05 | |
| 1035 | J-36 | 1628 | 9/20/66 | 2114 2 | 86.0 | 99.3 | 29.1 | 81 | 190 | 188 | 0.225 | W-23A | 189 | 0.175 | W-21 | 095/112/113 | 094/104/116 | |
| 1036 | J-32 | 1631 | 9/9/66 | 2046 2 | 100.0 | 102.4 | 22.9 | 115 | 212 | 190 | 0.200 | W-23A | 191 | 0.160 | W-21 | 089/101/111 | 088/103/046 | |
| 1037 | J-38 | 1632 | 11/8/66 | 1957 2 | 100.0 | 91.9 | 14.3 | 66 | 197 | 198 | 0.225 | W-23A | 199 | 0.175 | W-21 | D90/128/128 | D90/136/134 | |
| 1038 | J-34 | 1629 | 1/14/67 | 2128 2 | 40.1 | 96.9 | 29.2 | 81 | 193 | 192 | 0.225 | W-23A | 193 | 0.175 | W-21 | 093/86/112 | 090/111/108 | |
| 1039 | J-39 | 1635 | 2/22/67 | 2202 2 | 80.0 | 97.0 | 30.2 | 81 | 177 | 206 | 0.225 | W-23A | 207 | 0.175 | W-21 | D03/181/132 | D03/181/132 | |
| 1040 | J-35 | 1636 | 3/30/67 | 1854 2 | 85.1 | 99.7 | 28.3 | 81 | 145 | 196 | 0.175 | W-21 | 197 | 0.225 | W-23A | 078/95/96 | 092/78/110 | |
| 1041 | J-40 | 1634 | 5/9/67 | 2152 2 | 86.1 | 100.1 | 33.0 | 93 | 215 | 208 | 0.225 | W-23A | 209 | 0.175 | W-21 | 0105/137/133 | 002/027/001 | |

PERFORMANCE SUMMARY

| MISSION NUMBER | CAMERA SERIAL NUMBER | N I P VALUE | VISUAL RES | AFSPPI | MTF/AIM | SLIT (μ) | SLIT AVERAGE | SLIT HIGH | SLIT LOW | 90% ATTITUDE ERROR (°) | | | 90% ATTITUDE RATES (2HZ) YAW | | | 90% V/H ERROR (°) | | | 90% RESOLUTION LIMIT (FEET) CROSS TRACK | | | | |
|----------------|----------------------|-------------|------------|--------|---------|----------|--------------|-----------|----------|------------------------|------|------|------------------------------|------|------|-------------------|------|------|-----------------------------------------|------|------|------|------|
| | | | | | | | | | | ALL | HIGH | LOW | PITCH | ROLL | YAW | PITCH | ROLL | YAW | PITCH | ROLL | YAW | | |
| 1004-1 | FWD 124 | 93 | 76 | 350 | 87 | 103 | 115 | 127 | 106 | 0.45 | 0.42 | 1.06 | 30.0 | 25.0 | 21.0 | 5.1 | 7.7 | 6.1 | 6.1 | 6.1 | 6.1 | | |
| 1004-2 | FWD AFT 125 | 85 | 76 | 350 | 88 | 93 | 113 | 120 | 117 | 124 | 0.42 | 0.40 | 30.0 | 29.0 | 29.0 | 29.0 | 4.9 | 6.8 | 6.5 | 6.5 | 6.5 | 6.5 | |
| 1005-1 | FWD 146 | 90 | 78 | 350 | 85 | 90 | 90 | 94 | 97 | 94 | 0.41 | 0.42 | 1.14 | 26.8 | 26.5 | 27.8 | 15.4 | 13.8 | 13.8 | 13.8 | 13.8 | 13.8 | |
| 1005-2 | FWD AFT 149 | 90 | 75 | 350 | 64 | 43 | 61 | 67 | 67 | 92 | 0.41 | 0.42 | 1.14 | 26.8 | 26.5 | 27.8 | 15.4 | 13.8 | 13.8 | 13.8 | 13.8 | 13.8 | |
| 1007-1 | FWD 144 | 85 | 80 | 60 | 60 | 82 | 82 | 82 | 82 | 91 | 0.58 | 0.46 | 1.43 | 37.6 | 23.9 | 29.9 | 3.6 | 3.1 | 3.1 | 3.1 | 3.1 | 3.1 | |
| 1007-2 | FWD AFT 145 | 85 | 79 | 350 | 63 | 43 | 61 | 67 | 67 | 92 | 0.41 | 0.42 | 1.14 | 26.8 | 26.5 | 27.8 | 15.4 | 13.8 | 13.8 | 13.8 | 13.8 | 13.8 | |
| 1009-1 | FWD 150 | 85 | 80 | 80 | 80 | 95 | 95 | 81 | 89 | 0.59 | 0.59 | 0.94 | 43.8 | 21.9 | 29.6 | 2.9 | 4.9 | 4.9 | 4.9 | 4.9 | 4.9 | | |
| 1009-2 | FWD AFT 151 | 85 | 82 | 350 | 73 | 43 | 61 | 66 | 66 | 95 | 0.58 | 0.58 | 0.94 | 43.8 | 21.9 | 29.6 | 2.9 | 4.9 | 4.9 | 4.9 | 4.9 | 4.9 | |
| 1009-3 | FWD 154 | 85 | 92 | 350 | 84 | 91 | 91 | 91 | 91 | 92 | 0.68 | 0.68 | 0.71 | 42.9 | 24.0 | 32.5 | 2.6 | 4.2 | 4.2 | 4.2 | 4.2 | 4.2 | |
| 1009-4 | FWD AFT 155 | 85 | 94 | 350 | 85 | 85 | 85 | 85 | 85 | 91 | 0.65 | 0.65 | 0.71 | 29.2 | 22.7 | 27.6 | 3.3 | 5.3 | 5.3 | 5.3 | 5.3 | 5.3 | |
| 1010-1 | FWD 152 | 85 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 96 | 0.93 | 0.93 | 0.93 | 33.6 | 23.9 | 27.2 | 2.6 | 4.9 | 4.9 | 4.9 | 4.9 | 4.9 | |
| 1010-2 | FWD AFT 153 | 85 | 92 | 350 | 86 | 80 | 81 | 80 | 80 | 92 | 0.93 | 0.93 | 0.93 | 33.6 | 23.6 | 30.6 | 4.5 | 2.3 | 2.3 | 2.3 | 2.3 | 2.3 | |
| 1011-1 | FWD 160 | 90 | 84 | 350 | 76 | 60 | 86 | 86 | 86 | 75 | 0.59 | 0.70 | 1.21 | 45.4 | 23.6 | 30.7 | 4.6 | 7.5 | 7.5 | 7.5 | 7.5 | 7.5 | |
| 1012-1 | FWD AFT 161 | 90 | 84 | 350 | 77 | 60 | 86 | 86 | 86 | 75 | 0.59 | 0.70 | 1.21 | 45.4 | 23.6 | 30.7 | 4.6 | 7.5 | 7.5 | 7.5 | 7.5 | 7.5 | |
| 1012-2 | FWD AFT 167 | 85 | 92 | — | — | 80 | 87 | 80 | 87 | 96 | 0.65 | 0.65 | 0.51 | — | 47.1 | 33.2 | — | 1.5 | 4.8 | 4.8 | 4.8 | 4.8 | 4.8 |
| 1013-1 | FWD AFT 158 | 85 | 89 | 84 | 84 | 96 | 96 | 96 | 96 | 91 | 0.97 | 0.77 | 1.05 | 45.2 | 30.7 | 20.4 | 5.9 | 5.3 | 5.3 | 5.3 | 5.3 | 5.3 | |
| 1014-1 | FWD AFT 159 | 85 | 77 | — | — | 80 | 92 | 80 | 91 | 95 | 0.64 | 0.64 | 0.64 | 36.9 | 29.0 | 32.3 | 3.7 | 7.6 | 7.6 | 7.6 | 7.6 | 7.6 | |
| 1014-2 | FWD AFT 162 | 80 | 67 | 63 | — | — | — | 78 | 74 | 86 | 0.62 | 0.62 | 0.62 | 41 | 34.8 | 36.4 | 38.1 | 34.5 | 34.5 | 34.5 | 34.5 | 34.5 | 34.5 |
| 1015-1 | FWD 158 | 85 | 87 | 86 | 86 | 86 | 86 | 86 | 86 | 90 | 0.65 | 0.65 | 0.65 | 47.0 | 29.4 | 38.2 | 2.2 | 6.4 | 6.4 | 6.4 | 6.4 | 6.4 | |
| 1015-2 | FWD AFT 141 | 85 | 83 | — | — | 80 | 73 | 80 | 97 | 90 | 0.64 | 0.64 | 0.64 | 46.9 | 29.2 | 38.2 | 2.2 | 6.4 | 6.4 | 6.4 | 6.4 | 6.4 | |
| 1016-1 | FWD AFT 132 | 85 | 85 | 85 | 85 | 85 | 85 | 85 | 85 | 90 | 0.59 | 0.61 | 0.61 | 39.1 | 27.1 | 36.2 | 3.3 | 5.3 | 5.3 | 5.3 | 5.3 | 5.3 | |
| 1016-2 | FWD AFT 133 | 85 | 80 | — | — | 80 | 91 | 80 | 94 | 92 | 0.72 | 0.83 | 2.01 | 48.9 | 30.2 | 40.4 | 2.0 | 5.5 | 5.5 | 5.5 | 5.5 | 5.5 | |
| 1017-1 | FWD AFT 140 | 85 | 72 | — | — | 80 | 75 | 80 | 97 | 90 | 0.65 | 0.65 | 0.65 | 42.2 | 27.3 | 39.9 | 2.2 | 5.4 | 5.4 | 5.4 | 5.4 | 5.4 | |
| 1017-2 | FWD AFT 165 | 85 | 85 | 85 | 85 | 85 | 85 | 85 | 85 | 91 | 0.69 | 0.69 | 0.69 | 36.5 | 32.0 | 38.5 | 1.6 | 6.1 | 6.1 | 6.1 | 6.1 | 6.1 | |
| 1018-1 | FWD AFT 122 | 85 | 79 | 77 | — | — | — | 80 | 82 | 92 | 0.90 | 0.91 | 0.91 | 47.4 | 36.7 | 36.2 | 1.8 | 5.6 | 5.6 | 5.6 | 5.6 | 5.6 | |
| 1018-2 | FWD AFT 123 | 85 | 84 | 80 | 74 | 80 | 75 | 75 | 75 | 77 | 0.90 | 0.90 | 0.90 | 34.7 | 30.7 | 34.6 | 1.8 | 5.6 | 5.6 | 5.6 | 5.6 | 5.6 | |

PERFORMANCE SUMMARY

| MISSION NUMBER | CAMERA SERIAL NUMBER | W.I.P. VALUE | VISUAL RES. | AFSPC MTF/AIM (μ) | MTF/AIM AVERAGE | SLIT AVERAGE (μ) | SLIT HIGH (μ) | SLIT LOW (μ) | 90% ATTITUDE ERROR (°) | | | 90% V/H ERROR (%) | 90% RESOLUTION LIMIT (FEET) |
|----------------|----------------------|--------------|-------------|-------------------|-----------------|------------------|---------------|--------------|------------------------|------|------|-------------------|-----------------------------|
| | | | | | | | | | PITCH | ROLL | YAW | | |
| 1019-1 | FWD 119 | 85 | 85 | 85 | 85 | 85 | 85 | 85 | 0.43 | 0.44 | 0.43 | 3.3 | 3.3 |
| | AFT 119 | — | — | — | — | — | — | — | 0.35 | 0.35 | 0.35 | 5.0 | 5.0 |
| 1020-1 | FWD 186 | 85 | 85 | 85 | 85 | 85 | 85 | 85 | 0.46 | 0.46 | 0.46 | 3.3 | 3.3 |
| | AFT 187 | — | — | — | — | — | — | — | 0.35 | 0.35 | 0.35 | 5.0 | 5.0 |
| 1020-2 | FWD 187 | 85 | 85 | 85 | 85 | 85 | 85 | 85 | 0.41 | 0.41 | 0.41 | 3.3 | 3.3 |
| | AFT 187 | — | — | — | — | — | — | — | 0.37 | 0.37 | 0.37 | 5.0 | 5.0 |
| 1021-1 | FWD 166 | 85 | 85 | 85 | 85 | 85 | 85 | 85 | 0.41 | 0.41 | 0.41 | 3.3 | 3.3 |
| | AFT 167 | — | — | — | — | — | — | — | 0.35 | 0.35 | 0.35 | 5.0 | 5.0 |
| 1021-2 | FWD 167 | 85 | 85 | 85 | 85 | 85 | 85 | 85 | 0.41 | 0.41 | 0.41 | 3.3 | 3.3 |
| | AFT 167 | — | — | — | — | — | — | — | 0.35 | 0.35 | 0.35 | 5.0 | 5.0 |
| 1022-1 | FWD 168 | 85 | 85 | 85 | 85 | 85 | 85 | 85 | 0.41 | 0.41 | 0.41 | 3.3 | 3.3 |
| | AFT 168 | — | — | — | — | — | — | — | 0.35 | 0.35 | 0.35 | 5.0 | 5.0 |
| 1022-2 | FWD 169 | 85 | 85 | 85 | 85 | 85 | 85 | 85 | 0.41 | 0.41 | 0.41 | 3.3 | 3.3 |
| | AFT 169 | — | — | — | — | — | — | — | 0.35 | 0.35 | 0.35 | 5.0 | 5.0 |
| 1023-1 | FWD 170 | 85 | 85 | 85 | 85 | 85 | 85 | 85 | 0.41 | 0.41 | 0.41 | 3.3 | 3.3 |
| | AFT 171 | — | — | — | — | — | — | — | 0.35 | 0.35 | 0.35 | 5.0 | 5.0 |
| 1023-2 | FWD 171 | 85 | 85 | 85 | 85 | 85 | 85 | 85 | 0.41 | 0.41 | 0.41 | 3.3 | 3.3 |
| | AFT 171 | — | — | — | — | — | — | — | 0.35 | 0.35 | 0.35 | 5.0 | 5.0 |
| 1024-1 | FWD 172 | 85 | 85 | 85 | 85 | 85 | 85 | 85 | 0.41 | 0.41 | 0.41 | 3.3 | 3.3 |
| | AFT 172 | — | — | — | — | — | — | — | 0.35 | 0.35 | 0.35 | 5.0 | 5.0 |
| 1024-2 | FWD 173 | 85 | 85 | 85 | 85 | 85 | 85 | 85 | 0.41 | 0.41 | 0.41 | 3.3 | 3.3 |
| | AFT 173 | — | — | — | — | — | — | — | 0.35 | 0.35 | 0.35 | 5.0 | 5.0 |
| 1025-1 | FWD 142 | 85 | 85 | 85 | 85 | 85 | 85 | 85 | 0.41 | 0.41 | 0.41 | 3.3 | 3.3 |
| | AFT 142 | — | — | — | — | — | — | — | 0.35 | 0.35 | 0.35 | 5.0 | 5.0 |
| 1025-2 | FWD 127 | 85 | 85 | 85 | 85 | 85 | 85 | 85 | 0.41 | 0.41 | 0.41 | 3.3 | 3.3 |
| | AFT 127 | — | — | — | — | — | — | — | 0.35 | 0.35 | 0.35 | 5.0 | 5.0 |
| 1026-1 | FWD 174 | 85 | 85 | 85 | 85 | 85 | 85 | 85 | 0.41 | 0.41 | 0.41 | 3.3 | 3.3 |
| | AFT 174 | — | — | — | — | — | — | — | 0.35 | 0.35 | 0.35 | 5.0 | 5.0 |
| 1026-2 | FWD 175 | 85 | 85 | 85 | 85 | 85 | 85 | 85 | 0.41 | 0.41 | 0.41 | 3.3 | 3.3 |
| | AFT 175 | — | — | — | — | — | — | — | 0.35 | 0.35 | 0.35 | 5.0 | 5.0 |
| 1027-1 | FWD 164 | 85 | 85 | 85 | 85 | 85 | 85 | 85 | 0.41 | 0.41 | 0.41 | 3.3 | 3.3 |
| | AFT 164 | — | — | — | — | — | — | — | 0.35 | 0.35 | 0.35 | 5.0 | 5.0 |
| 1028-1 | FWD 176 | 85 | 85 | 85 | 85 | 85 | 85 | 85 | 0.41 | 0.41 | 0.41 | 3.3 | 3.3 |
| | AFT 176 | — | — | — | — | — | — | — | 0.35 | 0.35 | 0.35 | 5.0 | 5.0 |
| 1028-2 | FWD 177 | 85 | 85 | 85 | 85 | 85 | 85 | 85 | 0.41 | 0.41 | 0.41 | 3.3 | 3.3 |
| | AFT 177 | — | — | — | — | — | — | — | 0.35 | 0.35 | 0.35 | 5.0 | 5.0 |
| 1029-1 | FWD 178 | 85 | 85 | 85 | 85 | 85 | 85 | 85 | 0.41 | 0.41 | 0.41 | 3.3 | 3.3 |
| | AFT 178 | — | — | — | — | — | — | — | 0.35 | 0.35 | 0.35 | 5.0 | 5.0 |
| 1030-1 | FWD 182 | 85 | 85 | 85 | 85 | 85 | 85 | 85 | 0.41 | 0.41 | 0.41 | 3.3 | 3.3 |
| | AFT 182 | — | — | — | — | — | — | — | 0.35 | 0.35 | 0.35 | 5.0 | 5.0 |
| 1030-2 | FWD 183 | 85 | 85 | 85 | 85 | 85 | 85 | 85 | 0.41 | 0.41 | 0.41 | 3.3 | 3.3 |
| | AFT 183 | — | — | — | — | — | — | — | 0.35 | 0.35 | 0.35 | 5.0 | 5.0 |
| 1031-1 | FWD 184 | 85 | 85 | 85 | 85 | 85 | 85 | 85 | 0.41 | 0.41 | 0.41 | 3.3 | 3.3 |
| | AFT 184 | — | — | — | — | — | — | — | 0.35 | 0.35 | 0.35 | 5.0 | 5.0 |
| 1031-2 | FWD 185 | 85 | 85 | 85 | 85 | 85 | 85 | 85 | 0.41 | 0.41 | 0.41 | 3.3 | 3.3 |
| | AFT 185 | — | — | — | — | — | — | — | 0.35 | 0.35 | 0.35 | 5.0 | 5.0 |
| 1033-1 | FWD 194 | 85 | 85 | 85 | 85 | 85 | 85 | 85 | 0.41 | 0.41 | 0.41 | 3.3 | 3.3 |
| | AFT 194 | — | — | — | — | — | — | — | 0.35 | 0.35 | 0.35 | 5.0 | 5.0 |
| 1033-2 | FWD 195 | 85 | 85 | 85 | 85 | 85 | 85 | 85 | 0.41 | 0.41 | 0.41 | 3.3 | 3.3 |
| | AFT 195 | — | — | — | — | — | — | — | 0.35 | 0.35 | 0.35 | 5.0 | 5.0 |

PERFORMANCE SUMMARY

SUMMARY

| MISSION NUMBER | CAMERA | SERIAL NUMBER | M. I. P. VALUE | AFGPPF MTF/AIM | | 90% ATTITUDE ERROR (°) | | | 90% V/H | | | 90% RESOLUTION LIMIT (FEET) | | | I.M.C. ERROR | |
|----------------|--------|---------------|----------------|----------------|--------------------|------------------------|------|------|---------|------|------|-----------------------------|-------------|-----|--------------|--|
| | | | | AVERAGE | STANDARD DEVIATION | PITCH | ROLL | V/H | SITCH | ROLL | V/H | ALONG TRACK | CROSS TRACK | | | |
| 1034-1 | FWD | 168 | .80 | .78 | .01 | 0.20 | 0.19 | 0.99 | 19.3 | 20.4 | 24.9 | 15.0 | 17.8 | 5.5 | | |
| 1034-2 | AFT | 167 | .80 | .74 | .09 | 0.20 | 0.19 | 0.99 | 19.3 | 20.4 | 24.9 | 15.2 | 13.6 | 4.5 | | |
| 1035-1 | FWD | 169 | .65 | .69 | .06 | 0.34 | 0.26 | 0.33 | 21.1 | 28.9 | 16.2 | 9.7 | 10.4 | 7.1 | | |
| 1035-2 | AFT | 169 | .65 | .66 | .04 | 0.34 | 0.26 | 0.33 | 21.1 | 29.0 | 16.2 | 8.9 | 8.0 | 6.3 | | |
| 1036-1 | FWD | 180 | .85 | .86 | .01 | 0.16 | 0.53 | 2.39 | 18.9 | 27.9 | 35.9 | 4.0 | 4.8 | 4.0 | | |
| 1036-2 | AFT | 180 | .85 | .81 | .02 | 0.17 | 0.54 | 2.43 | 18.3 | 23.4 | 32.2 | 4.1 | 3.7 | 2.4 | | |
| 1037-1 | FWD | 181 | .85 | .82 | .01 | 0.16 | 0.50 | 3.02 | 18.4 | 30.1 | 27.6 | 3.2 | 4.0 | 3.6 | | |
| 1037-2 | AFT | 181 | .85 | .84 | .02 | 0.17 | 0.51 | 3.02 | 19.9 | 24.7 | 26.3 | 3.4 | 3.3 | 2.4 | | |
| 1038-1 | FWD | 182 | .85 | .84 | .01 | 0.16 | 0.56 | 0.60 | 31.2 | 25.6 | 29.5 | 3.4 | 5.1 | 5.8 | | |
| 1038-2 | AFT | 182 | .85 | .84 | .01 | 0.16 | 0.56 | 0.69 | 31.1 | 25.5 | 29.4 | 3.5 | 3.6 | 5.5 | | |
| 1039-1 | FWD | 183 | .85 | .84 | .01 | 0.16 | 0.50 | 0.40 | 33.0 | 23.7 | 23.3 | 3.3 | 3.8 | 6.5 | | |
| 1039-2 | AFT | 183 | .85 | .84 | .01 | 0.16 | 0.50 | 0.43 | 32.9 | 29.7 | 23.3 | 3.1 | 2.7 | 5.5 | | |
| 1040-1 | FWD | 184 | .85 | .84 | .01 | 0.16 | 0.56 | 0.60 | 31.2 | 25.6 | 29.5 | 3.4 | 5.1 | 5.8 | | |
| 1040-2 | AFT | 184 | .85 | .84 | .01 | 0.16 | 0.56 | 0.69 | 31.1 | 25.5 | 29.4 | 3.5 | 3.6 | 5.5 | | |
| 1041-1 | FWD | 185 | .85 | .84 | .01 | 0.16 | 0.50 | 0.40 | 33.0 | 23.7 | 23.3 | 3.3 | 3.8 | 6.5 | | |
| 1041-2 | AFT | 185 | .85 | .84 | .01 | 0.16 | 0.50 | 0.43 | 32.9 | 29.7 | 23.3 | 3.1 | 2.7 | 5.5 | | |
| 1042-1 | FWD | 186 | .85 | .84 | .01 | 0.16 | 0.56 | 0.60 | 31.2 | 25.6 | 29.5 | 3.4 | 5.1 | 5.8 | | |
| 1042-2 | AFT | 186 | .85 | .84 | .01 | 0.16 | 0.56 | 0.69 | 31.1 | 25.5 | 29.4 | 3.5 | 3.6 | 5.5 | | |
| 1043-1 | FWD | 187 | .85 | .84 | .01 | 0.16 | 0.50 | 0.30 | 26.5 | 52.5 | 26.2 | 6.3 | 6.0 | 6.1 | 10.3 | |
| 1043-2 | AFT | 187 | .85 | .84 | .01 | 0.16 | 0.50 | 0.32 | 1.18 | 33.8 | 36.6 | 6.5 | 5.4 | 5.9 | 6.5 | |
| 1044-1 | FWD | 188 | .85 | .84 | .01 | 0.16 | 0.56 | 0.67 | 20.0 | 46.7 | 39.9 | 3.5 | 4.1 | 3.7 | 5.5 | |
| 1044-2 | AFT | 188 | .85 | .84 | .01 | 0.16 | 0.56 | 0.69 | 21.7 | 34.4 | 34.4 | 3.4 | 3.3 | 3.7 | 5.5 | |
| 1045-1 | FWD | 189 | .85 | .84 | .01 | 0.16 | 0.59 | 0.61 | 2.98 | 18.7 | 27.3 | 3.4 | 3.6 | 3.6 | 5.5 | |
| 1045-2 | AFT | 189 | .85 | .84 | .01 | 0.16 | 0.59 | 0.63 | 2.98 | 19.0 | 27.8 | 3.1 | 3.6 | 3.6 | 5.5 | |
| 1046-1 | FWD | 190 | .85 | .84 | .01 | 0.16 | 0.56 | 0.67 | 23.1 | 37.5 | 28.5 | 6.2 | 4.6 | 5.2 | 5.2 | |
| 1046-2 | AFT | 190 | .85 | .84 | .01 | 0.16 | 0.56 | 0.69 | 23.1 | 30.2 | 30.0 | 4.6 | 5.5 | 5.4 | 4.7 | |
| 1047-1 | FWD | 191 | .85 | .84 | .01 | 0.16 | 0.59 | 0.61 | 2.98 | 19.0 | 27.3 | 3.1 | 3.6 | 3.6 | 5.5 | |
| 1047-2 | AFT | 191 | .85 | .84 | .01 | 0.16 | 0.59 | 0.63 | 2.98 | 19.3 | 27.8 | 3.1 | 3.6 | 3.6 | 5.5 | |
| 1048-1 | FWD | 192 | .85 | .84 | .01 | 0.16 | 0.56 | 0.67 | 23.1 | 37.5 | 28.5 | 6.2 | 4.6 | 5.2 | 5.2 | |
| 1048-2 | AFT | 192 | .85 | .84 | .01 | 0.16 | 0.56 | 0.69 | 23.1 | 30.2 | 30.0 | 4.6 | 5.5 | 5.4 | 4.7 | |
| 1049-1 | FWD | 193 | .85 | .84 | .01 | 0.16 | 0.59 | 0.61 | 2.98 | 19.0 | 27.3 | 3.1 | 3.6 | 3.6 | 5.5 | |
| 1049-2 | AFT | 193 | .85 | .84 | .01 | 0.16 | 0.59 | 0.63 | 2.98 | 19.3 | 27.8 | 3.1 | 3.6 | 3.6 | 5.5 | |
| 1050-1 | FWD | 194 | .85 | .84 | .01 | 0.16 | 0.56 | 0.67 | 23.1 | 37.5 | 28.5 | 6.2 | 4.6 | 5.2 | 5.2 | |
| 1050-2 | AFT | 194 | .85 | .84 | .01 | 0.16 | 0.56 | 0.69 | 23.1 | 30.2 | 30.0 | 4.6 | 5.5 | 5.4 | 4.7 | |
| 1051-1 | FWD | 195 | .85 | .84 | .01 | 0.16 | 0.59 | 0.61 | 2.98 | 19.0 | 27.3 | 3.1 | 3.6 | 3.6 | 5.5 | |
| 1051-2 | AFT | 195 | .85 | .84 | .01 | 0.16 | 0.59 | 0.63 | 2.98 | 19.3 | 27.8 | 3.1 | 3.6 | 3.6 | 5.5 | |
| 1052-1 | FWD | 196 | .85 | .84 | .01 | 0.16 | 0.56 | 0.67 | 23.1 | 37.5 | 28.5 | 6.2 | 4.6 | 5.2 | 5.2 | |
| 1052-2 | AFT | 196 | .85 | .84 | .01 | 0.16 | 0.56 | 0.69 | 23.1 | 30.2 | 30.0 | 4.6 | 5.5 | 5.4 | 4.7 | |
| 1053-1 | FWD | 197 | .85 | .84 | .01 | 0.16 | 0.59 | 0.61 | 2.98 | 19.0 | 27.3 | 3.1 | 3.6 | 3.6 | 5.5 | |
| 1053-2 | AFT | 197 | .85 | .84 | .01 | 0.16 | 0.59 | 0.63 | 2.98 | 19.3 | 27.8 | 3.1 | 3.6 | 3.6 | 5.5 | |
| 1054-1 | FWD | 198 | .85 | .84 | .01 | 0.16 | 0.56 | 0.67 | 23.1 | 37.5 | 28.5 | 6.2 | 4.6 | 5.2 | 5.2 | |
| 1054-2 | AFT | 198 | .85 | .84 | .01 | 0.16 | 0.56 | 0.69 | 23.1 | 30.2 | 30.0 | 4.6 | 5.5 | 5.4 | 4.7 | |
| 1055-1 | FWD | 199 | .85 | .84 | .01 | 0.16 | 0.59 | 0.61 | 2.98 | 19.0 | 27.3 | 3.1 | 3.6 | 3.6 | 5.5 | |
| 1055-2 | AFT | 199 | .85 | .84 | .01 | 0.16 | 0.59 | 0.63 | 2.98 | 19.3 | 27.8 | 3.1 | 3.6 | 3.6 | 5.5 | |
| 1056-1 | FWD | 200 | .85 | .84 | .01 | 0.16 | 0.56 | 0.67 | 23.1 | 37.5 | 28.5 | 6.2 | 4.6 | 5.2 | 5.2 | |
| 1056-2 | AFT | 200 | .85 | .84 | .01 | 0.16 | 0.56 | 0.69 | 23.1 | 30.2 | 30.0 | 4.6 | 5.5 | 5.4 | 4.7 | |
| 1057-1 | FWD | 201 | .85 | .84 | .01 | 0.16 | 0.59 | 0.61 | 2.98 | 19.0 | 27.3 | 3.1 | 3.6 | 3.6 | 5.5 | |
| 1057-2 | AFT | 201 | .85 | .84 | .01 | 0.16 | 0.59 | 0.63 | 2.98 | 19.3 | 27.8 | 3.1 | 3.6 | 3.6 | 5.5 | |
| 1058-1 | FWD | 202 | .85 | .84 | .01 | 0.16 | 0.56 | 0.67 | 23.1 | 37.5 | 28.5 | 6.2 | 4.6 | 5.2 | 5.2 | |
| 1058-2 | AFT | 202 | .85 | .84 | .01 | 0.16 | 0.56 | 0.69 | 23.1 | 30.2 | 30.0 | 4.6 | 5.5 | 5.4 | 4.7 | |
| 1059-1 | FWD | 203 | .85 | .84 | .01 | 0.16 | 0.59 | 0.61 | 2.98 | 19.0 | 27.3 | 3.1 | 3.6 | 3.6 | 5.5 | |
| 1059-2 | AFT | 203 | .85 | .84 | .01 | 0.16 | 0.59 | 0.63 | 2.98 | 19.3 | 27.8 | 3.1 | 3.6 | 3.6 | 5.5 | |
| 1060-1 | FWD | 204 | .85 | .84 | .01 | 0.16 | 0.56 | 0.67 | 23.1 | 37.5 | 28.5 | 6.2 | 4.6 | 5.2 | 5.2 | |
| 1060-2 | AFT | 204 | .85 | .84 | .01 | 0.16 | 0.56 | 0.69 | 23.1 | 30.2 | 30.0 | 4.6 | 5.5 | 5.4 | 4.7 | |
| 1061-1 | FWD | 205 | .85 | .84 | .01 | 0.16 | 0.59 | 0.61 | 2.98 | 19.0 | 27.3 | 3.1 | 3.6 | 3.6 | 5.5 | |
| 1061-2 | AFT | 205 | .85 | .84 | .01 | 0.16 | 0.59 | 0.63 | 2.98 | 19.3 | 27.8 | 3.1 | 3.6 | 3.6 | 5.5 | |
| 1062-1 | FWD | 206 | .85 | .84 | .01 | 0.16 | 0.56 | 0.67 | 23.1 | 37.5 | 28.5 | 6.2 | 4.6 | 5.2 | 5.2 | |
| 1062-2 | AFT | 206 | .85 | .84 | .01 | 0.16 | 0.56 | 0.69 | 23.1 | 30.2 | 30.0 | 4.6 | 5.5 | 5.4 | 4.7 | |
| 1063-1 | FWD | 207 | .85 | .84 | .01 | 0.16 | 0.59 | 0.61 | 2.98 | 19.0 | 27.3 | 3.1 | 3.6 | 3.6 | 5.5 | |
| 1063-2 | AFT | 207 | .85 | .84 | .01 | 0.16 | 0.59 | 0.63 | 2.98 | 19.3 | 27.8 | 3.1 | 3.6 | 3.6 | 5.5 | |
| 1064-1 | FWD | 208 | .85 | .84 | .01 | 0.16 | 0.56 | 0.67 | 23.1 | 37.5 | 28.5 | 6.2 | 4.6 | 5.2 | 5.2 | |
| 1064-2 | AFT | 208 | .85 | .84 | .01 | 0.16 | 0.56 | 0.69 | 23.1 | 30.2 | 30.0 | 4.6 | 5.5 | 5.4 | 4.7 | |
| 1065-1 | FWD | 209 | .85 | .84 | .01 | 0.16 | 0.59 | 0.61 | 2.98 | 19.0 | 27.3 | 3.1 | 3.6 | 3.6 | 5.5 | |
| 1065-2 | AFT | 209 | .85 | .84 | .01 | 0.16 | 0.59 | 0.63 | 2.98 | 19.3 | 27.8 | 3.1 | 3.6 | 3.6 | 5.5 | |
| 1066-1 | FWD | 210 | .85 | .84 | .01 | 0.16 | 0.56 | 0.67 | 23.1 | 37.5 | 28.5 | 6.2 | 4.6 | 5.2 | 5.2 | |
| 1066-2 | AFT | 210 | .85 | .84 | .01 | 0.16 | 0.56 | 0.69 | 23.1 | 30.2 | 30.0 | 4.6 | 5.5 | 5.4 | 4.7 | |
| 1067-1 | FWD | 211 | .85 | .84 | .01 | 0.16 | 0.59 | 0.61 | 2.98 | 19.0 | 27.3 | 3.1 | 3.6 | 3.6 | 5.5 | |
| 1067-2 | AFT | 211 | .85 | .84 | .01 | 0.16 | 0.59 | 0.63 | 2.98 | 19.3 | 27.8 | 3.1 | 3.6 | 3.6 | 5.5 | |
| 1068-1 | FWD | 212 | .85 | .84 | .01 | 0.16 | 0.56 | 0.67 | 23.1 | 37.5 | 28.5 | 6.2 | 4.6 | 5.2 | 5.2 | |
| 1068-2 | AFT | 212 | .85 | .84 | .01 | 0.16 | 0.56 | 0.69 | 23.1 | 30.2 | 30.0 | 4.6 | 5.5 | 5.4 | 4.7 | |
| 1069-1 | FWD | 213 | .85 | .84 | .01 | 0.16 | 0.59 | 0.61 | 2.98 | 19.0 | 27.3 | 3.1 | 3.6 | 3.6 | 5.5 | |
| 1069-2 | AFT | 213 | .85 | .84 | .01 | 0.16 | 0.59 | 0.63 | 2.98 | 19.3 | 27.8 | 3.1 | 3.6 | 3.6 | 5.5 | |
| 1070-1 | FWD | 214 | .85 | .84 | .01 | 0.16 | 0.56 | 0.67 | 23.1 | 37.5 | 28.5 | 6.2 | 4.6 | 5.2 | 5.2 | |
| 1070-2 | AFT | 214 | .85 | .84 | .01 | 0.16 | 0.56 | 0.69 | 23.1 | 30.2 | 30.0 | 4.6 | 5.5 | 5.4 | 4.7 | |
| 1071-1 | FWD | 215 | .85 | .84 | .01 | 0.16 | 0.59 | 0.61 | 2.98 | 19.0 | 27.3 | 3.1 | 3.6 | 3.6 | 5.5 | |
| 1071-2 | AFT | 215 | .85 | .84 | .01 | 0.16 | 0.59 | 0.63 | 2.98 | 19.3 | 27.8 | 3.1 | 3.6 | 3.6 | 5.5 | |
| 1072-1 | FWD | 216 | .85 | .84 | .01 | 0.16 | 0.56 | 0.67 | 23.1 | 37.5 | 28.5 | 6.2 | 4.6 | 5.2 | 5.2 | |
| 1072-2 | AFT | 216 | .85 | .84 | .01 | 0.16 | 0.56 | 0.69 | 23.1 | 30.2 | 30.0 | 4.6 | 5. | | | |

EXPOSURE - PROCESSING SUMMARY

TOP SECRET C

| MISSION NUMBER | CAMERA RANGE (') | SOLAR ELEVATION (°) | RANGE (') | PREDICTED PROCESSING | | | COMPUTED PROCESSING | | | TERRAIN D-MIN | | | TERRAIN D-MAX | | | CLOUD RANGE | | | OVER EXPOSED (%) | | | CLOUD COVER (%) | | | | |
|----------------|------------------|---------------------|-----------|----------------------|------|-----|---------------------|------|-----|---------------|------|------|---------------|------|------|-------------|------|------|------------------|------|------|-----------------|------|------|----|----|
| | | | | LOW | HIGH | F | LOW | HIGH | F | LOW | HIGH | MEAN | LOW | HIGH | MEAN | LOW | HIGH | MEAN | LOW | HIGH | MEAN | | | | | |
| 1004-1 | FWD | -13 | 61 | 25 | 128 | 5 | 76 | 19 | 4 | 70 | 17 | 0 | 79 | 21 | 0.24 | 1.89 | 0.83 | 0.78 | 0.43 | 2.43 | 1.97 | 202 | 4 | 31 | | |
| 1004-1 | AFT | -14 | 61 | 25 | 124 | 5 | 74 | 21 | 4 | 75 | 17 | 0 | 80 | 20 | 0.22 | 1.56 | 0.76 | 0.70 | 0.45 | 2.43 | 1.98 | 208 | 0 | 35 | | |
| 1004-2 | FWD | -14 | 66 | 10 | 131 | 5 | 76 | 17 | 4 | 87 | 50 | 13 | 63 | 4 | 0.23 | 1.50 | 0.63 | 0.73 | 0.36 | 2.30 | 1.84 | 190 | 1 | 26 | | |
| 1004-2 | AFT | -14 | 66 | 10 | 131 | 7 | 76 | 17 | 37 | 50 | 13 | 4 | 77 | 19 | 0.29 | 1.91 | 0.81 | 0.73 | 0.36 | 2.39 | 1.89 | 99 | 0 | 35 | | |
| 1005-1 | FWD | 58 | 86 | 52 | 140 | -1 | 99 | 0 | -1 | 51 | 48 | 0 | 51 | 49 | 0.23 | 1.81 | 0.71 | 0.68 | 0.80 | 2.3 | 1.89 | 98 | 0 | 27 | | |
| 1005-1 | AFT | 58 | 86 | 52 | 140 | -1 | 99 | 0 | -1 | 51 | 48 | 0 | 51 | 49 | 0.23 | 1.81 | 0.71 | 0.68 | 0.80 | 2.3 | 1.89 | 98 | 0 | 20 | | |
| 1005-2 | FWD | 52 | 64 | 36 | 147 | 2 | 96 | 0 | 30 | 41 | 29 | 1 | 59 | 30 | 0.21 | 1.44 | 0.53 | 0.50 | 0.56 | 2.28 | 0 | 22 | 0 | 60 | | |
| 1005-2 | AFT | 52 | 64 | 36 | 147 | 2 | 96 | 0 | 30 | 41 | 40 | 0 | 58 | 9 | 0.24 | 1.76 | 0.56 | 0.56 | 0.44 | 2.20 | 0 | 22 | 0 | 60 | | |
| 1007-1 | FWD | 12 | 49 | 50 | 103 | 0 | 95 | -1 | 40 | 79 | 0 | 25 | 75 | 0.86 | 2.27 | 0.52 | 0.47 | 0.62 | 2.20 | 1.44 | 47 | 1 | 44 | | | |
| 1007-1 | AFT | 12 | 49 | 50 | 102 | 0 | 100 | 0 | 100 | 102 | 0 | 26 | 74 | 0.77 | 1.7 | 0.58 | 0.55 | 0.78 | 2.51 | 1.52 | 52 | 1 | 45 | | | |
| 1007-2 | FWD | 38 | 57 | 53 | 112 | 0 | 125 | 75 | 3 | 28 | 49 | 0 | 26 | 74 | 0.26 | 1.23 | 0.51 | 0.48 | 0.70 | 2.32 | 1.44 | 40 | 0 | 60 | | |
| 1007-2 | AFT | 38 | 57 | 51 | 111 | 0 | 100 | 0 | 100 | 111 | 0 | 19 | 41 | 0 | 3.68 | 9 | 0.24 | 1.56 | 0.56 | 0.44 | 0.27 | 50 | 0 | 50 | | |
| 1008-1 | FWD | 50 | 51 | 50 | 102 | 0 | 100 | 0 | 100 | 102 | 0 | 4 | 32 | 64 | 1 | 3.5 | 64 | 0.32 | 1.48 | 0.56 | 0.62 | 0.58 | 1.95 | 1.50 | 30 | |
| 1008-1 | AFT | 50 | 51 | 50 | 102 | 0 | 100 | 0 | 100 | 102 | 0 | 4 | 32 | 64 | 1 | 3.5 | 64 | 0.32 | 1.48 | 0.56 | 0.62 | 0.58 | 1.95 | 1.50 | 30 | |
| 1009-2 | FWD | 23 | 58 | 35 | 138 | 2 | 98 | 0 | 3 | 100 | 0 | 3 | 100 | 0 | 4.27 | 69 | 0 | 2.5 | 75 | 0.86 | 2.27 | 0.52 | 55 | 1 | 45 | |
| 1009-2 | AFT | 23 | 58 | 35 | 138 | 2 | 98 | 0 | 3 | 100 | 0 | 3 | 100 | 0 | 4.27 | 69 | 0 | 2.5 | 75 | 0.86 | 2.27 | 0.52 | 55 | 1 | 45 | |
| 1010-1 | FWD | 18 | 47 | 47 | 83 | 0 | 21 | 79 | 0 | 13 | 87 | 0 | 9 | 91 | 0.28 | 1.44 | 0.52 | 0.47 | 0.64 | 2.21 | 1.57 | 54 | 1 | 45 | | |
| 1010-1 | AFT | 18 | 47 | 47 | 83 | 0 | 21 | 79 | 0 | 13 | 87 | 0 | 9 | 91 | 0.28 | 1.44 | 0.52 | 0.47 | 0.64 | 2.21 | 1.57 | 54 | 1 | 45 | | |
| 1010-2 | FWD | 15 | 52 | 36 | 132 | 0 | 100 | 0 | 100 | 132 | 0 | 100 | 0 | 100 | 0 | 1.25 | 73 | 0 | 3.66 | 52 | 0.52 | 1.87 | 0.52 | 63 | 1 | 27 |
| 1010-2 | AFT | 15 | 52 | 36 | 132 | 0 | 100 | 0 | 100 | 132 | 0 | 100 | 0 | 100 | 0 | 1.25 | 73 | 0 | 3.66 | 52 | 0.52 | 1.87 | 0.52 | 63 | 1 | 27 |
| 1011-1 | FWD | 22 | 55 | 35 | 138 | 2 | 98 | 0 | 4 | 47 | 49 | 0 | 56 | 44 | 0.26 | 1.47 | 0.52 | 0.47 | 0.64 | 2.21 | 1.57 | 54 | 1 | 45 | | |
| 1011-1 | AFT | 22 | 55 | 35 | 138 | 2 | 98 | 0 | 4 | 47 | 49 | 0 | 56 | 44 | 0.26 | 1.47 | 0.52 | 0.47 | 0.64 | 2.21 | 1.57 | 54 | 1 | 45 | | |
| 1012-1 | FWD | 0 | 45 | 50 | 71 | 0 | 64 | 36 | 7 | 56 | 37 | 0 | 65 | 35 | 0.25 | 1.30 | 0.59 | 0.53 | 0.54 | 2.39 | 1.40 | 42 | 0 | 40 | | |
| 1012-1 | AFT | 0 | 45 | 50 | 71 | 0 | 64 | 36 | 7 | 56 | 37 | 0 | 65 | 35 | 0.25 | 1.30 | 0.59 | 0.53 | 0.54 | 2.39 | 1.40 | 42 | 0 | 40 | | |
| 1012-2 | FWD | 0 | 45 | 57 | 34 | 106 | 0 | 77 | 23 | 6 | 44 | 50 | 0 | 49 | 51 | 0.30 | 1.20 | 0.58 | 0.56 | 0.57 | 2.32 | 1.49 | 42 | 0 | 40 | |
| 1012-2 | AFT | 0 | 45 | 57 | 34 | 106 | 0 | 77 | 23 | 6 | 44 | 50 | 0 | 49 | 51 | 0.30 | 1.20 | 0.58 | 0.56 | 0.57 | 2.32 | 1.49 | 42 | 0 | 40 | |
| 1013-1 | FWD | 56 | 88 | 66 | 128 | 5 | 76 | 19 | 4 | 70 | 17 | 0 | 79 | 21 | 0.24 | 1.89 | 0.83 | 0.78 | 0.43 | 2.43 | 1.97 | 27 | 1 | 45 | | |
| 1013-1 | AFT | 56 | 88 | 66 | 128 | 5 | 76 | 19 | 4 | 70 | 17 | 0 | 79 | 21 | 0.24 | 1.89 | 0.83 | 0.78 | 0.43 | 2.43 | 1.97 | 27 | 1 | 45 | | |
| 1014-1 | FWD | 59 | 14 | 69 | 116 | 0 | 21 | 79 | 0 | 36 | 71 | 0 | 61 | 0 | 0.24 | 1.87 | 0.81 | 0.76 | 0.43 | 2.43 | 1.97 | 28 | 1 | 45 | | |
| 1014-1 | AFT | 59 | 14 | 69 | 116 | 0 | 21 | 79 | 0 | 36 | 71 | 0 | 61 | 0 | 0.24 | 1.87 | 0.81 | 0.76 | 0.43 | 2.43 | 1.97 | 28 | 1 | 45 | | |
| 1014-2 | FWD | 44 | 18 | 18 | 122 | 0 | 125 | 76 | 0 | 92 | 2 | 0 | 70 | 0 | 0.24 | 1.86 | 0.81 | 0.76 | 0.43 | 2.43 | 1.97 | 28 | 1 | 45 | | |
| 1014-2 | AFT | 44 | 18 | 18 | 122 | 0 | 125 | 76 | 0 | 92 | 2 | 0 | 70 | 0 | 0.24 | 1.86 | 0.81 | 0.76 | 0.43 | 2.43 | 1.97 | 28 | 1 | 45 | | |
| 1015-1 | FWD | 11 | 30 | 21 | 98 | 0 | 100 | 0 | 100 | 100 | 0 | 10 | 90 | 0 | 1.15 | 63 | 0.24 | 1.86 | 0.81 | 0.76 | 0.43 | 2.43 | 1.97 | 28 | 1 | 45 |
| 1015-1 | AFT | 11 | 30 | 21 | 98 | 0 | 100 | 0 | 100 | 100 | 0 | 10 | 90 | 0 | 1.15 | 63 | 0.24 | 1.86 | 0.81 | 0.76 | 0.43 | 2.43 | 1.97 | 28 | 1 | 45 |
| 1017-1 | FWD | 5 | 59 | 13 | 76 | 0 | 73 | 0 | 73 | 0 | 73 | 0 | 59 | 0 | 0.24 | 1.86 | 0.81 | 0.76 | 0.43 | 2.43 | 1.97 | 28 | 1 | 45 | | |
| 1017-1 | AFT | 5 | 59 | 13 | 76 | 0 | 73 | 0 | 73 | 0 | 73 | 0 | 59 | 0 | 0.24 | 1.86 | 0.81 | 0.76 | 0.43 | 2.43 | 1.97 | 28 | 1 | 45 | | |
| 1018-1 | FWD | 44 | 14 | 64 | 14 | 76 | 0 | 73 | 0 | 73 | 0 | 59 | 0 | 0.24 | 1.86 | 0.81 | 0.76 | 0.43 | 2.43 | 1.97 | 28 | 1 | 45 | | | |
| 1018-1 | AFT | 44 | 14 | 64 | 14 | 76 | 0 | 73 | 0 | 73 | 0 | 59 | 0 | 0.24 | 1.86 | 0.81 | 0.76 | 0.43 | 2.43 | 1.97 | 28 | 1 | 45 | | | |
| 1018-2 | FWD | 77 | 14 | 14 | 136 | 0 | 132 | 0 | 132 | 0 | 132 | 0 | 59 | 0 | 0.24 | 1.86 | 0.81 | 0.76 | 0.43 | 2.43 | 1.97 | 28 | 1 | 45 | | |
| 1018-2 | AFT | 77 | 14 | 14 | 136 | 0 | 132 | 0 | 132 | 0 | 132 | 0 | 59 | 0 | 0.24 | 1.86 | 0.81 | 0.76 | 0.43 | 2.43 | 1.97 | 28 | 1 | 45 | | |

EXPOSURE - PROCESSING SUMMARY

EXPOSURE - PROCESSING SUMMARY

| MISSION NUMBER | CAMERA RANGE (ft) | SOLAR AZIMUTH (°) | PREDICTED PROCESSING TIME (s) | REPORTED PROCESSING TIME (s) | COMPUTED PROCESSING | | | | TERRAIN D-MIN | | | | TERRAIN D-MAX | | | | CLOUD D-MAX | | | | | | | | | | | | | |
|----------------|-------------------|-------------------|-------------------------------|------------------------------|---------------------|-----|----|-----|---------------|----|----|----|---------------|----|----|----|-------------|----|----|------|------|------|------|------|------|------|------|------|------|------|
| | | | | | T | F | P | T | L | H | M | D | L | H | M | D | L | H | M | D | | | | | | | | | | |
| 1034-1 | FWD | 23 | 77 | 163 | 0 | 36 | 4 | 3 | 21 | 76 | 0 | 20 | 60 | 0 | 25 | 1 | 80 | 0 | 50 | 0.55 | 2.42 | 1.58 | 1.61 | 0.89 | 2.45 | 2.22 | 2.26 | | | |
| | AFT | 23 | 77 | 10 | 163 | 0 | 35 | 45 | 2 | 31 | 67 | 0 | 26 | 65 | 0 | 25 | 1 | 80 | 0 | 55 | 1.55 | 2.35 | 1.55 | 1.60 | 0.97 | 2.44 | 2.19 | 2.25 | | |
| 1034-2 | FWD | 28 | 86 | 0 | 176 | 0 | 40 | 12 | 9 | 26 | 65 | 0 | 27 | 73 | 0 | 19 | 1 | 80 | 0 | 56 | 0.60 | 2.40 | 1.63 | 1.60 | 1.24 | 2.47 | 2.35 | 2.31 | | |
| | AFT | 30 | 86 | 0 | 178 | 0 | 41 | 55 | 5 | 37 | 57 | 0 | 36 | 66 | 0 | 26 | 1 | 80 | 0 | 57 | 0.62 | 2.40 | 1.63 | 1.60 | 1.09 | 2.48 | 2.32 | 2.29 | | |
| 1035-1 | FWD | 13 | 65 | 19 | 144 | 0 | 17 | 83 | 0 | 11 | 85 | 0 | 5 | 95 | 0 | 88 | 1 | 80 | 0 | 58 | 0.61 | 2.44 | 1.40 | 1.66 | 0.43 | 2.43 | 2.16 | 2.20 | | |
| | AFT | 13 | 65 | 18 | 144 | 0 | 16 | 85 | 0 | 14 | 85 | 0 | 9 | 91 | 0 | 86 | 1 | 80 | 0 | 59 | 0.62 | 2.42 | 1.46 | 1.65 | 0.43 | 2.42 | 2.15 | 2.21 | | |
| 1035-2 | FWD | 4 | 61 | 10 | 158 | 0 | 22 | 74 | 4 | 18 | 76 | 0 | 18 | 82 | 0 | 21 | 1 | 80 | 0 | 60 | 0.52 | 2.33 | 1.32 | 1.60 | 0.43 | 2.40 | 2.16 | 2.24 | | |
| | AFT | 5 | 61 | 8 | 158 | 0 | 23 | 77 | 1 | 20 | 79 | 0 | 12 | 88 | 0 | 21 | 1 | 80 | 0 | 60 | 0.53 | 2.32 | 1.32 | 1.60 | 0.43 | 2.40 | 2.16 | 2.24 | | |
| 1035-3 | FWD | 13 | 62 | 7 | 170 | 0 | 66 | 34 | 8 | 14 | 78 | - | 14 | 85 | 0 | 20 | 1 | 80 | 0 | 61 | 0.50 | 2.25 | 1.34 | 1.60 | 0.43 | 2.40 | 2.16 | 2.24 | | |
| | AFT | 16 | 63 | 5 | 171 | 0 | 65 | 35 | 9 | 19 | 85 | - | 19 | 85 | 0 | 20 | 1 | 80 | 0 | 62 | 0.48 | 2.20 | 1.34 | 1.60 | 0.43 | 2.40 | 2.16 | 2.24 | | |
| 1036-2 | FWD | 19 | 78 | 12 | 167 | 0 | 15 | 85 | 1 | 20 | 80 | 0 | 18 | 82 | 0 | 26 | 1 | 80 | 0 | 63 | 0.55 | 2.25 | 1.45 | 1.62 | 0.43 | 2.42 | 2.23 | 2.31 | | |
| | AFT | 12 | 78 | 9 | 168 | 0 | 4 | 96 | 4 | 20 | 77 | 0 | 17 | 83 | 0 | 28 | 1 | 80 | 0 | 64 | 0.47 | 2.20 | 1.45 | 1.61 | 0.43 | 2.40 | 2.22 | 2.30 | | |
| 1037-1 | FWD | 9 | 64 | 172 | 16 | 0 | 25 | 75 | 6 | 28 | 71 | 0 | 10 | 82 | 0 | 11 | 89 | 0 | 31 | 1 | 80 | 0.51 | 2.33 | 1.45 | 1.61 | 0.43 | 2.40 | 2.20 | 2.28 | |
| | AFT | 9 | 64 | 171 | 16 | 0 | 25 | 75 | 14 | 25 | 75 | 0 | 12 | 88 | 0 | 12 | 88 | 0 | 32 | 1 | 80 | 0.52 | 2.33 | 1.46 | 1.61 | 0.43 | 2.40 | 2.20 | 2.28 | |
| 1037-2 | FWD | 6 | 67 | 67 | 173 | - | 3 | 0 | 24 | 76 | - | 11 | 53 | 56 | 0 | 23 | 77 | 0 | 25 | 1 | 80 | 0.55 | 2.33 | 1.45 | 1.61 | 0.43 | 2.40 | 2.20 | 2.28 | |
| | AFT | 6 | 67 | 67 | 173 | - | 3 | 0 | 22 | 78 | 2 | 16 | 82 | - | 15 | 84 | 0 | 16 | 1 | 80 | 0.56 | 2.33 | 1.45 | 1.61 | 0.43 | 2.40 | 2.20 | 2.28 | | |
| 1038-1 | FWD | 5 | 68 | 18 | 131 | 0 | 22 | 78 | 1 | 15 | 82 | - | 14 | 86 | 0 | 14 | 86 | 0 | 25 | 1 | 80 | 0.67 | 2.33 | 1.51 | 1.62 | 0.43 | 2.40 | 2.21 | 2.29 | |
| | AFT | 5 | 68 | 18 | 130 | 0 | 22 | 78 | 1 | 15 | 82 | 0 | 15 | 85 | 0 | 13 | 88 | 0 | 25 | 1 | 80 | 0.67 | 2.33 | 1.51 | 1.62 | 0.43 | 2.40 | 2.21 | 2.29 | |
| 1038-2 | FWD | 7 | 80 | 1 | 164 | - | 37 | 62 | 0 | 15 | 85 | 0 | 13 | 88 | 0 | 21 | 73 | 0 | 26 | 74 | 0 | 19 | 0.61 | 2.49 | 0.77 | 1.56 | 0.43 | 2.40 | 2.21 | 2.29 |
| | AFT | 7 | 80 | 1 | 164 | - | 37 | 62 | 0 | 15 | 85 | 0 | 13 | 88 | 0 | 21 | 73 | 0 | 26 | 74 | 0 | 19 | 0.61 | 2.49 | 0.77 | 1.56 | 0.43 | 2.40 | 2.21 | 2.29 |
| 1039-1 | FWD | 7 | 65 | 27 | 140 | 0 | 62 | 36 | 6 | 22 | 70 | - | 24 | 75 | 0 | 22 | 53 | 0 | 25 | 1 | 80 | 0.53 | 2.33 | 1.51 | 1.62 | 0.43 | 2.40 | 2.21 | 2.29 | |
| | AFT | 7 | 65 | 27 | 140 | 0 | 60 | 40 | 6 | 22 | 70 | - | 24 | 75 | 0 | 22 | 53 | 0 | 25 | 1 | 80 | 0.67 | 2.33 | 1.51 | 1.62 | 0.43 | 2.40 | 2.21 | 2.29 | |
| 1039-2 | FWD | 8 | 75 | 10 | 164 | 0 | 61 | 35 | 19 | 38 | 43 | 5 | 41 | 56 | 0 | 24 | 55 | 0 | 25 | 1 | 80 | 0.59 | 2.33 | 1.51 | 1.62 | 0.43 | 2.40 | 2.21 | 2.29 | |
| | AFT | 6 | 75 | 10 | 164 | 0 | 47 | 51 | 20 | 45 | 55 | 7 | 37 | 56 | 0 | 27 | 51 | 0 | 25 | 1 | 80 | 0.67 | 2.33 | 1.51 | 1.62 | 0.43 | 2.40 | 2.21 | 2.29 | |
| 1040-1 | FWD | 11 | 73 | 149 | 15 | 0 | 79 | 21 | 0 | 31 | 59 | 2 | 35 | 63 | 0 | 25 | 1 | 80 | 0 | 71 | 0.71 | 2.45 | 1.71 | 1.74 | 0.38 | 2.45 | 2.21 | 2.29 | | |
| | AFT | 11 | 73 | 149 | 15 | 0 | 67 | 33 | 1 | 42 | 64 | 4 | 33 | 63 | 0 | 25 | 1 | 80 | 0 | 71 | 0.68 | 2.45 | 1.71 | 1.74 | 0.38 | 2.45 | 2.21 | 2.29 | | |
| 1040-2 | FWD | 12 | 68 | 68 | 149 | - | 21 | 0 | 65 | 34 | 73 | 5 | 35 | 64 | 0 | 25 | 1 | 80 | 0 | 72 | 0.67 | 2.38 | 1.65 | 1.64 | 0.36 | 2.44 | 2.15 | 2.23 | | |
| | AFT | 11 | 68 | 68 | 149 | - | 21 | 0 | 63 | 34 | 73 | 5 | 35 | 64 | 0 | 24 | 1 | 80 | 0 | 72 | 0.67 | 2.38 | 1.65 | 1.64 | 0.36 | 2.44 | 2.15 | 2.23 | | |
| 1041-1 | FWD | 10 | 66 | 66 | 30 | 129 | 0 | 100 | 0 | 7 | 40 | 53 | 0 | 46 | 84 | 0 | 14 | 2 | 14 | 0.56 | 2.42 | 1.72 | 1.74 | 0.47 | 2.45 | 2.12 | 2.20 | | | |
| | AFT | 9 | 66 | 66 | 30 | 129 | 0 | 100 | 0 | 7 | 40 | 53 | 0 | 46 | 84 | 0 | 14 | 2 | 14 | 0.56 | 2.42 | 1.72 | 1.74 | 0.47 | 2.45 | 2.12 | 2.20 | | | |
| 1041-2 | FWD | 28 | 78 | 14 | 126 | 0 | 99 | 0 | 23 | 76 | 67 | 0 | 23 | 77 | 0 | 17 | 64 | 0 | 17 | 1 | 62 | 0.62 | 2.38 | 1.62 | 1.61 | 0.46 | 2.44 | 2.19 | 2.25 | |
| | AFT | 28 | 78 | 14 | 126 | 0 | 99 | 0 | 23 | 76 | 67 | 0 | 23 | 77 | 0 | 17 | 64 | 0 | 17 | 1 | 62 | 0.62 | 2.38 | 1.62 | 1.61 | 0.46 | 2.44 | 2.19 | 2.25 | |

~~TOP SECRET~~

C/ [REDACTED] NO. [REDACTED]

SECTION A

APPENDIX

~~TOP SECRET~~ C/ [REDACTED]

~~TOP SECRET C~~

MISSION * 1041-1 * INSTRUMENT * FWD 6/27/67 DENSITY FREQ DISTR

| DENSITY VALUE | PRIMARY MIN MAX LIM | INTERMEDIATE MIN MAX LIM | FULL MIN MAX LIM | ALL LEVELS MIN MAX LIM |
|------------------|----------------------------------------------------|-----------------------------|---------------------|---------------------------|
| 0.01 | 0 | 0 | 0 | 0 |
| 0.02 | 00 | 00 | 0 | 00 |
| 0.03 | 000 | 000 | 0 | 000 |
| 0.04 | 0000 | 0000 | 0 | 0000 |
| 0.05 | 00000 | 00000 | 0 | 00000 |
| 0.06 | 000000 | 000000 | 0 | 000000 |
| 0.07 | 0000000 | 0000000 | 0 | 0000000 |
| 0.08 | 00000000 | 00000000 | 0 | 00000000 |
| 0.09 | 000000000 | 000000000 | 0 | 000000000 |
| 0.10 | 0000000000 | 0000000000 | 0 | 0000000000 |
| 0.11 | 00000000000 | 00000000000 | 0 | 00000000000 |
| 0.12 | 000000000000 | 000000000000 | 0 | 000000000000 |
| 0.13 | 0000000000000 | 0000000000000 | 0 | 0000000000000 |
| 0.14 | 00000000000000 | 00000000000000 | 0 | 00000000000000 |
| 0.15 | 000000000000000 | 000000000000000 | 0 | 000000000000000 |
| 0.16 | 0000000000000000 | 0000000000000000 | 0 | 0000000000000000 |
| 0.17 | 00000000000000000 | 00000000000000000 | 0 | 00000000000000000 |
| 0.18 | 000000000000000000 | 000000000000000000 | 0 | 000000000000000000 |
| 0.19 | 0000000000000000000 | 0000000000000000000 | 0 | 0000000000000000000 |
| 0.20 | 00000000000000000000 | 00000000000000000000 | 0 | 00000000000000000000 |
| 0.21 | 000000000000000000000 | 000000000000000000000 | 0 | 000000000000000000000 |
| 0.22 | 0000000000000000000000 | 0000000000000000000000 | 0 | 0000000000000000000000 |
| 0.23 | 00000000000000000000000 | 00000000000000000000000 | 0 | 00000000000000000000000 |
| 0.24 | 000000000000000000000000 | 00000000000000000000000 | 0 | 00000000000000000000000 |
| 0.25 | 0000000000000000000000000 | 00000000000000000000000 | 0 | 00000000000000000000000 |
| 0.26 | 00000000000000000000000000 | 00000000000000000000000 | 0 | 00000000000000000000000 |
| 0.27 | 000000000000000000000000000 | 00000000000000000000000 | 0 | 00000000000000000000000 |
| 0.28 | 0000000000000000000000000000 | 00000000000000000000000 | 0 | 00000000000000000000000 |
| 0.29 | 00000000000000000000000000000 | 00000000000000000000000 | 0 | 00000000000000000000000 |
| 0.30 | 000000000000000000000000000000 | 00000000000000000000000 | 0 | 00000000000000000000000 |
| 0.31 | 0000000000000000000000000000000 | 00000000000000000000000 | 0 | 00000000000000000000000 |
| 0.32 | 00000000000000000000000000000000 | 00000000000000000000000 | 0 | 00000000000000000000000 |
| 0.33 | 000000000000000000000000000000000 | 00000000000000000000000 | 0 | 00000000000000000000000 |
| 0.34 | 0000000000000000000000000000000000 | 00000000000000000000000 | 0 | 00000000000000000000000 |
| 0.35 | 00000000000000000000000000000000000 | 00000000000000000000000 | 0 | 00000000000000000000000 |
| 0.36 | 000000000000000000000000000000000000 | 00000000000000000000000 | 0 | 00000000000000000000000 |
| 0.37 | 0000000000000000000000000000000000000 | 00000000000000000000000 | 0 | 00000000000000000000000 |
| 0.38 | 00000000000000000000000000000000000000 | 00000000000000000000000 | 0 | 00000000000000000000000 |
| 0.39 | 000000000000000000000000000000000000000 | 00000000000000000000000 | 0 | 00000000000000000000000 |
| 0.40 | 0000000000000000000000000000000000000000 | 00000000000000000000000 | 0 | 00000000000000000000000 |
| 0.41 | 00000000000000000000000000000000000000000 | 00000000000000000000000 | 0 | 00000000000000000000000 |
| 0.42 | 000000000000000000000000000000000000000000 | 00000000000000000000000 | 0 | 00000000000000000000000 |
| 0.43 | 0000000000000000000000000000000000000000000 | 00000000000000000000000 | 0 | 00000000000000000000000 |
| 0.44 | 00000000000000000000000000000000000000000000 | 00000000000000000000000 | 0 | 00000000000000000000000 |
| 0.45 | 000000000000000000000000000000000000000000000 | 00000000000000000000000 | 0 | 00000000000000000000000 |
| 0.46 | 0000000000000000000000000000000000000000000000 | 00000000000000000000000 | 0 | 00000000000000000000000 |
| 0.47 | 00000000000000000000000000000000000000000000000 | 00000000000000000000000 | 0 | 00000000000000000000000 |
| 0.48 | 000000000000000000000000000000000000000000000000 | 00000000000000000000000 | 0 | 00000000000000000000000 |
| 0.49 | 0000000000000000000000000000000000000000000000000 | 00000000000000000000000 | 0 | 00000000000000000000000 |
| 0.50 | 00000000000000000000000000000000000000000000000000 | 00000000000000000000000 | 0 | 00000000000000000000000 |
| SUBTOTAL | 0 | 0 | 47 | 68 |
| | | | | 145 |

~~TOP SECRET C~~

TABLE A-1

~~TOP SECRET C~~

MISSION * 1041-1 * INSTRUMENT * FWD 6/27/67 DENSITY FREQ DISTR

| DENSITY VALUE | PRIMARY MIN MAX LIM | INTERMEDIATE MIN MAX LIM | FULL MIN MAX LIM | ALL LEVELS MIN MAX LIM |
|------------------|------------------------|-----------------------------|---------------------|---------------------------|
| 0.51 | 0 0 | 0 0 | 3 0 | 7 0 |
| 0.52 | 00 00 | 00 00 | 2 0 | 5 0 |
| 0.53 | 00 00 | 00 00 | 7 0 | 8 0 |
| 0.54 | 00 00 | 00 00 | 5 0 | 9 0 |
| 0.55 | 00 00 | 00 00 | 5 0 | 5 0 |
| 0.56 | 00 00 | 00 00 | 2 0 | 6 0 |
| 0.57 | 00 00 | 00 00 | 3 0 | 1 0 |
| 0.58 | 00 00 | 00 00 | 3 0 | 4 0 |
| 0.59 | 00 00 | 00 00 | 0 0 | 1 0 |
| 0.60 | 00 00 | 00 00 | 0 0 | 0 0 |
| 0.61 | 00 00 | 00 00 | 0 0 | 0 0 |
| 0.62 | 00 00 | 00 00 | 0 0 | 0 0 |
| 0.63 | 00 00 | 00 00 | 0 0 | 0 0 |
| 0.64 | 00 00 | 00 00 | 0 0 | 0 0 |
| 0.65 | 00 00 | 00 00 | 0 0 | 0 0 |
| 0.66 | 00 00 | 00 00 | 0 0 | 0 0 |
| 0.67 | 00 00 | 00 00 | 0 0 | 0 0 |
| 0.68 | 00 00 | 00 00 | 0 0 | 0 0 |
| 0.69 | 00 00 | 00 00 | 0 0 | 0 0 |
| 0.70 | 00 00 | 00 00 | 0 0 | 0 0 |
| 0.71 | 00 00 | 00 00 | 0 0 | 0 0 |
| 0.72 | 00 00 | 00 00 | 0 0 | 0 0 |
| 0.73 | 00 00 | 00 00 | 0 0 | 0 0 |
| 0.74 | 00 00 | 00 00 | 0 0 | 0 0 |
| 0.75 | 00 00 | 00 00 | 0 0 | 0 0 |
| 0.76 | 00 00 | 00 00 | 0 0 | 0 0 |
| 0.77 | 00 00 | 00 00 | 0 0 | 0 0 |
| 0.78 | 00 00 | 00 00 | 0 0 | 0 0 |
| 0.79 | 00 00 | 00 00 | 0 0 | 0 0 |
| 0.80 | 00 00 | 00 00 | 0 0 | 0 0 |
| 0.81 | 00 00 | 00 00 | 0 0 | 0 0 |
| 0.82 | 00 00 | 00 00 | 0 0 | 0 0 |
| 0.83 | 00 00 | 00 00 | 0 0 | 0 0 |
| 0.84 | 00 00 | 00 00 | 0 0 | 0 0 |
| 0.85 | 00 00 | 00 00 | 0 0 | 0 0 |
| 0.86 | 00 00 | 00 00 | 0 0 | 0 0 |
| 0.87 | 00 00 | 00 00 | 0 0 | 0 0 |
| 0.88 | 00 00 | 00 00 | 0 0 | 0 0 |
| 0.89 | 00 00 | 00 00 | 0 0 | 0 0 |
| 0.90 | 00 00 | 00 00 | 0 0 | 0 0 |
| 0.91 | 00 00 | 00 00 | 0 0 | 0 0 |
| 0.92 | 00 00 | 00 00 | 0 0 | 0 0 |
| 0.93 | 00 00 | 00 00 | 0 0 | 0 0 |
| 0.94 | 00 00 | 00 00 | 0 0 | 0 0 |
| 0.95 | 00 00 | 00 00 | 0 0 | 0 0 |
| 0.96 | 00 00 | 00 00 | 0 0 | 0 0 |
| 0.97 | 00 00 | 00 00 | 0 0 | 0 0 |
| 0.98 | 00 00 | 00 00 | 0 0 | 0 0 |
| 0.99 | 00 00 | 00 00 | 0 0 | 0 0 |
| 1.00 | 0 0 | 0 0 | 0 0 | 0 0 |
| SUBTOTAL | 0 0 | 0 0 | 52 21 | 110 30 |

~~TOP SECRET C~~

TABLE A-1

~~TOP SECRET~~ C

~~TOP SECRET~~ C

TABLE A-1

~~TOP SECRET C~~

MISSION * 1041-1 * INSTRUMENT * FWD 6/27/67 DENSITY FREQ DISTR

| DENSITY VALUE | PRIMARY | | | INTERMEDIATE | | | FULL | | | ALL LEVELS | | |
|------------------|---------|-----|-----|--------------|-----|-----|------|-----|-----|------------|-----|-----|
| | MIN | MAX | LIM | MIN | MAX | LIM | MIN | MAX | LIM | MIN | MAX | LIM |
| 1.51 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 4 | 0 | 0 | 0 | 0 |
| 1.52 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 1 | 0 | 0 | 0 | 0 |
| 1.53 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 1 | 0 | 0 | 0 | 0 |
| 1.54 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 1 | 0 | 0 | 0 | 0 |
| 1.55 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 1 | 0 | 0 | 0 | 0 |
| 1.56 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 1 | 0 | 0 | 0 | 0 |
| 1.57 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 1 | 0 | 0 | 0 | 0 |
| 1.58 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 1 | 0 | 0 | 0 | 0 |
| 1.59 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 1 | 0 | 0 | 0 | 0 |
| 1.60 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 1 | 0 | 0 | 0 | 0 |
| 1.61 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 1 | 0 | 0 | 0 | 0 |
| 1.62 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 1 | 0 | 0 | 0 | 0 |
| 1.63 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 1 | 0 | 0 | 0 | 0 |
| 1.64 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 1 | 0 | 0 | 0 | 0 |
| 1.65 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 1 | 0 | 0 | 0 | 0 |
| 1.66 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 1 | 0 | 0 | 0 | 0 |
| 1.67 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 1 | 0 | 0 | 0 | 0 |
| 1.68 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 1 | 0 | 0 | 0 | 0 |
| 1.69 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 1 | 0 | 0 | 0 | 0 |
| 1.70 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 1 | 0 | 0 | 0 | 0 |
| 1.71 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 1 | 0 | 0 | 0 | 0 |
| 1.72 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 1 | 0 | 0 | 0 | 0 |
| 1.73 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 1 | 0 | 0 | 0 | 0 |
| 1.74 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 1 | 0 | 0 | 0 | 0 |
| 1.75 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 1 | 0 | 0 | 0 | 0 |
| 1.76 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 1 | 0 | 0 | 0 | 0 |
| 1.77 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 1 | 0 | 0 | 0 | 0 |
| 1.78 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 1 | 0 | 0 | 0 | 0 |
| 1.79 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 1 | 0 | 0 | 0 | 0 |
| 1.80 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 1 | 0 | 0 | 0 | 0 |
| 1.81 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 1 | 0 | 0 | 0 | 0 |
| 1.82 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 1 | 0 | 0 | 0 | 0 |
| 1.83 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 1 | 0 | 0 | 0 | 0 |
| 1.84 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 1 | 0 | 0 | 0 | 0 |
| 1.85 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 1 | 0 | 0 | 0 | 0 |
| 1.86 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 1 | 0 | 0 | 0 | 0 |
| 1.87 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 1 | 0 | 0 | 0 | 0 |
| 1.88 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 1 | 0 | 0 | 0 | 0 |
| 1.89 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 1 | 0 | 0 | 0 | 0 |
| 1.90 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 1 | 0 | 0 | 0 | 0 |
| 1.91 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 1 | 0 | 0 | 0 | 0 |
| 1.92 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 1 | 0 | 0 | 0 | 0 |
| 1.93 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 1 | 0 | 0 | 0 | 0 |
| 1.94 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 1 | 0 | 0 | 0 | 0 |
| 1.95 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 1 | 0 | 0 | 0 | 0 |
| 1.96 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 1 | 0 | 0 | 0 | 0 |
| 1.97 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 1 | 0 | 0 | 0 | 0 |
| 1.98 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 1 | 0 | 0 | 0 | 0 |
| 1.99 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 1 | 0 | 0 | 0 | 0 |
| 2.00 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 1 | 0 | 0 | 0 | 0 |
| SUBTOTAL | 0 | 0 | 0 | 0 | 58 | 30 | 0 | 57 | 2 | 115 | 32 | |

~~TOP SECRET C~~

TABLE A-1

~~TOP SECRET C~~

MISSION * 1041-1 * INSTRUMENT * FWD 6/27/67 DENSITY FREQ. DISTR

| DENSITY VALUE | PRIMARY MIN MAX LIM | INTERMEDIATE MIN MAX LIM | FULL MIN MAX LIM | ALL LEVELS MIN MAX LIM |
|------------------|------------------------|-----------------------------|---------------------|---------------------------|
| 2.01 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.02 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.03 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.04 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.05 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.06 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.07 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.08 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.09 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.10 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.11 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.12 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.13 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.14 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.15 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.16 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.17 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.18 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.19 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.20 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.21 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.22 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.23 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.24 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.25 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.26 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.27 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.28 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.29 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.30 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.31 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.32 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.33 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.34 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.35 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.36 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.37 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.38 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.39 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.40 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.41 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.42 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.43 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.44 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.45 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.46 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.47 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.48 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.49 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.50 | 0 0 | 0 0 | 0 0 | 0 0 |
| SUBTOTAL | 0 0 | 0 0 | 1 16 83 | 0 15 129 |
| | | | | 1 31 212 |

~~TOP SECRET C~~

TABLE A-1

~~TOP SECRET C~~

MISSION * 1041-1 : * INSTRUMENT * FWD 6/27/67 DENSITY FREQ DISTR

| DENSITY VALUE | PRIMARY | | | INTERMEDIATE | | | FULL | | | ALL LEVELS | | |
|------------------|---------|-----|-----|--------------|-----|-----|------|-----|-----|------------|-----|-----|
| | MIN | MAX | LIM | MIN | MAX | LIM | MIN | MAX | LIM | MIN | MAX | LIM |
| 2.51 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2.52 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2.53 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2.54 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2.55 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2.56 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2.57 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2.58 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2.59 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2.60 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2.61 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2.62 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2.63 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2.64 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2.65 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2.66 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2.67 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2.68 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2.69 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2.70 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| SUBTOTAL | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| TOTAL | 0 | 0 | 0 | 107 | 107 | 117 | 126 | 126 | 133 | 233 | 233 | 250 |

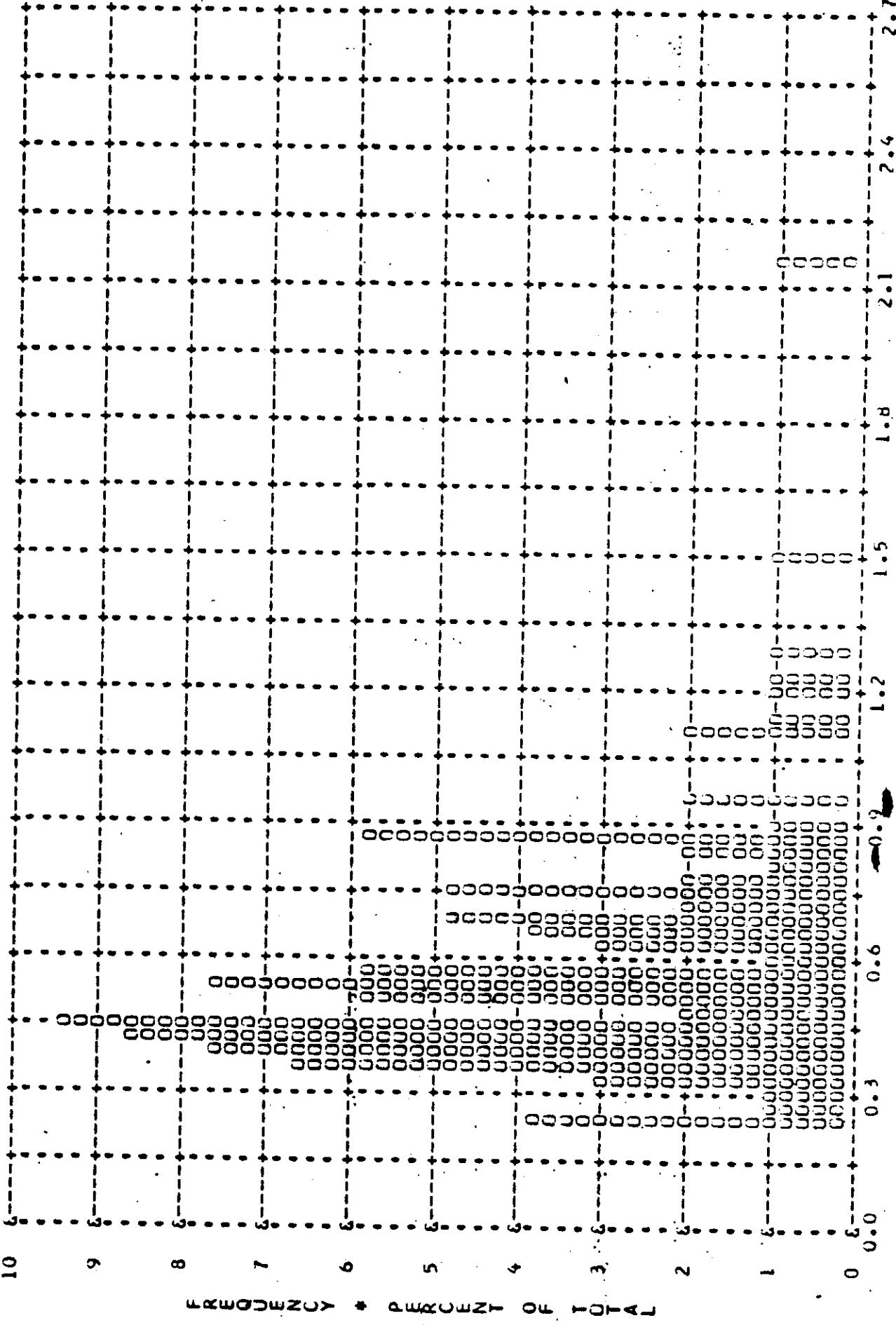
MISSION 1041-1 INSTR - FWD 6/27/67 PROCESSING AND EXPOSURE ANALYSIS

| PROCESS LEVEL | SAMPLE SIZE | UNDER EXPOSED | | UNDER PROCESSED | | CORRECT EXP&PROC | OVER PROCESSED | OVER EXPOSED |
|------------------|----------------|------------------|----|--------------------|----|---------------------|-------------------|-----------------|
| | | PC | PC | PC | PC | | | |
| PRIMARY | 0 | 0 | 0 | 0 | 0 | 0 | 54 | 54 |
| INTERMEDIATE | 107 | 0 | 0 | 22 | 68 | PC | 7 | PC |
| FULL | 126 | 10 | PC | 0 | 88 | PC | 2 | PC |
| ALL LEVELS | 233 | 6 | PC | 10 | 79 | PC | 4 | PC |
| PROCESS LEVEL | BASE & FOG | UNDER EXPOSED | | UNDER PROCESSED | | CORRECT EXP&PROC | OVER PROCESSED | OVER EXPOSED |
| PRIMARY | 0.01-0.09 | 0.01-0.13 | | 0.14-0.39 | | 0.40-0.90 | ----- | 0.91 AND UP |
| INTERMED | 0.10-0.17 | 0.01-0.20 | | 0.21-0.39 | | 0.40-0.90 | 0.91-1.34 | 1.35 AND UP |
| FULL | 0.18 AND UP | 0.01-0.39 | | ----- | | 0.40-0.90 | 0.91-1.69 | 1.70 AND UP |

~~TOP SECRET C~~

TABLE A-1

~~TOP SECRET C~~ MISSION * 1041-1 * INSTR * FWD * 6/27/67 PLOT OF D MIN * TERRAIN * PROCESSING * INTERMEDIATE
AIRTH MEAN * 0.60 * MEDIAN * 0.52 * STD DEV * 0.29 * RANGE * 0.22 TO 2.14 WITH 107 SAMPLES



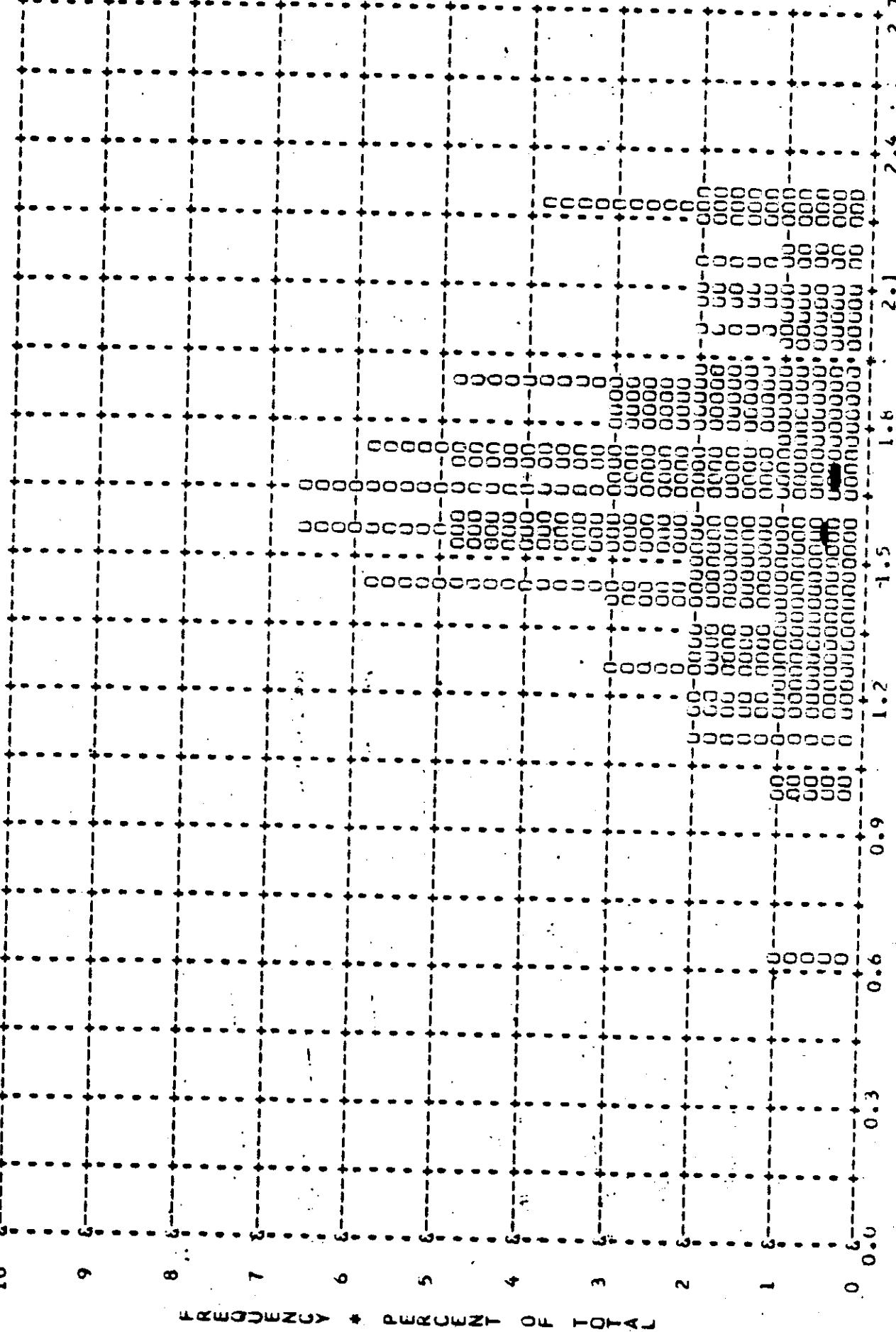
~~TOP SECRET C~~

* DENSITY *

~~TOP SECRET C~~

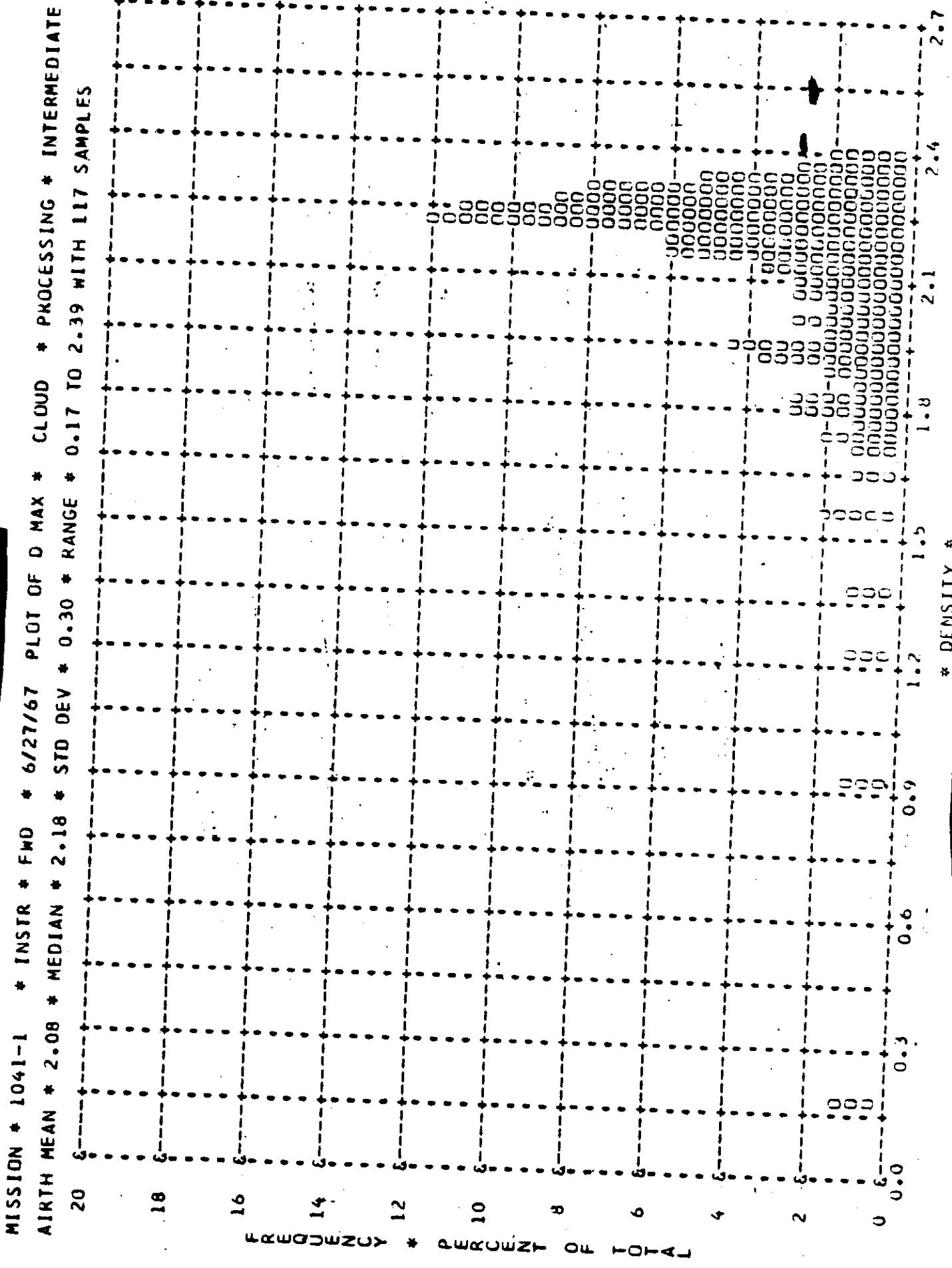
~~TOP SECRET C~~

MISSION * 1041-1 * INSTR * FWD * 6/27/67 PLOT OF D MAX * TERRAIN * PROCESSING * INTERMEDIATE
AIRTH MEAN * 1.65 * MEDIAN * 1.64 * STD DEV * 0.33 * RANGE * 0.62 TO 2.31 WITH 107 SAMPLES



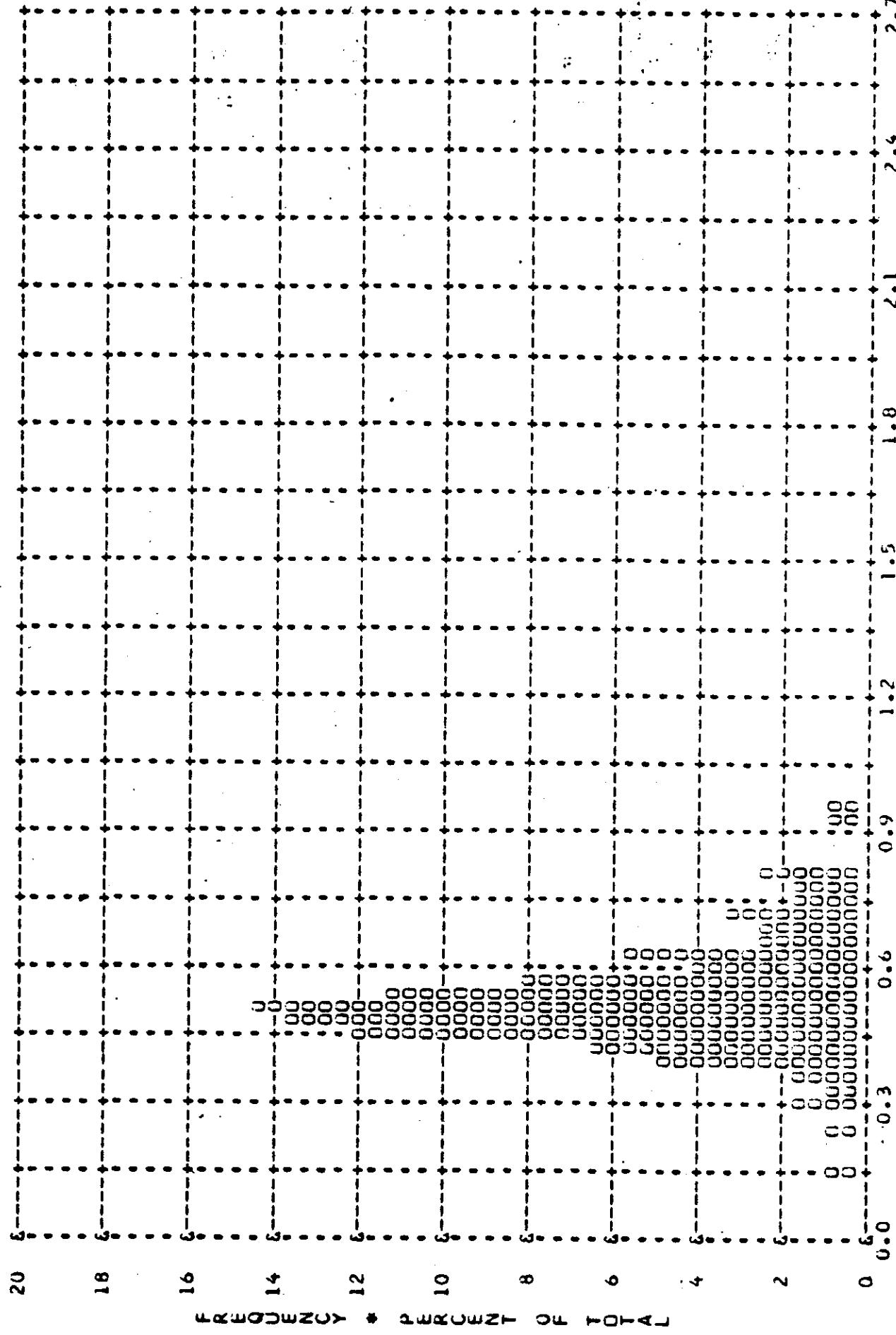
A-3

TOP SECRET C



~~TOP SECRET C~~

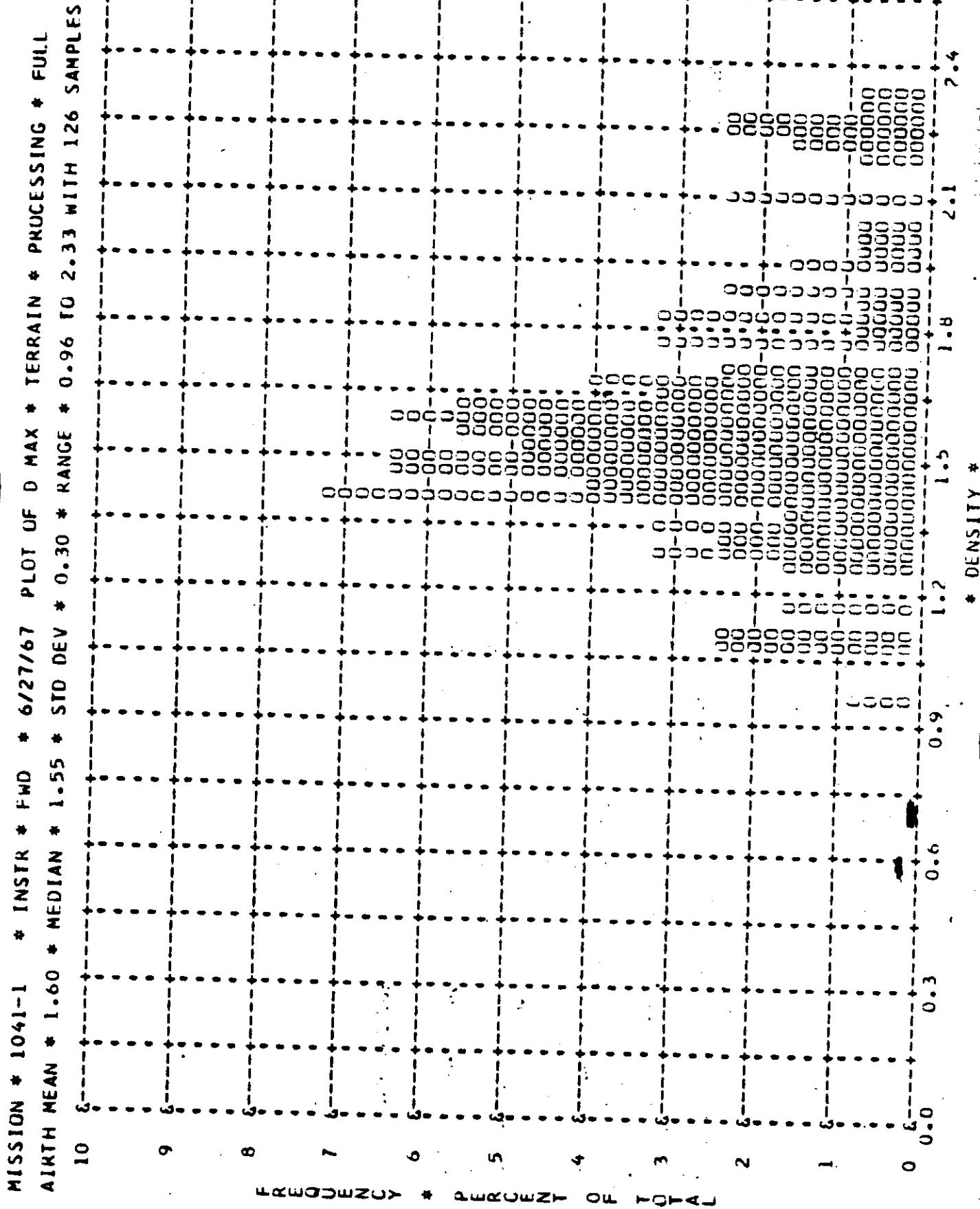
MISSION * 1041-1 * INSTR * FWD * 6/27/67 PLOT OF D MIN * TERRAIN * PROCESSING * FULL
AIRTH MEAN * 0.52 * MEDIAN * 0.50 * STD DEV * 0.12 * RANGE * 0.14 TO 0.94 WITH 126 SAMPLES



* DENSITY *

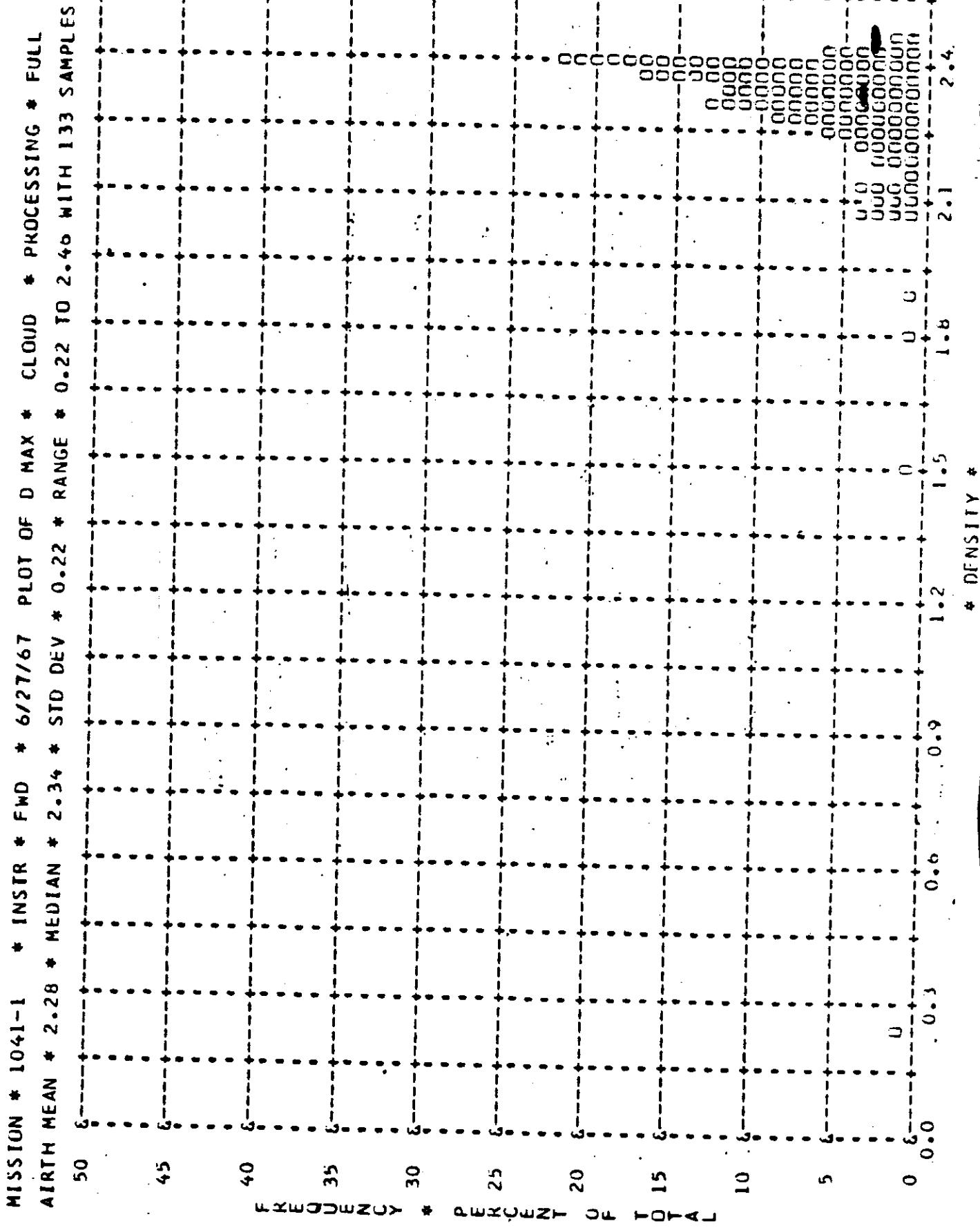
~~TOP SECRET C~~

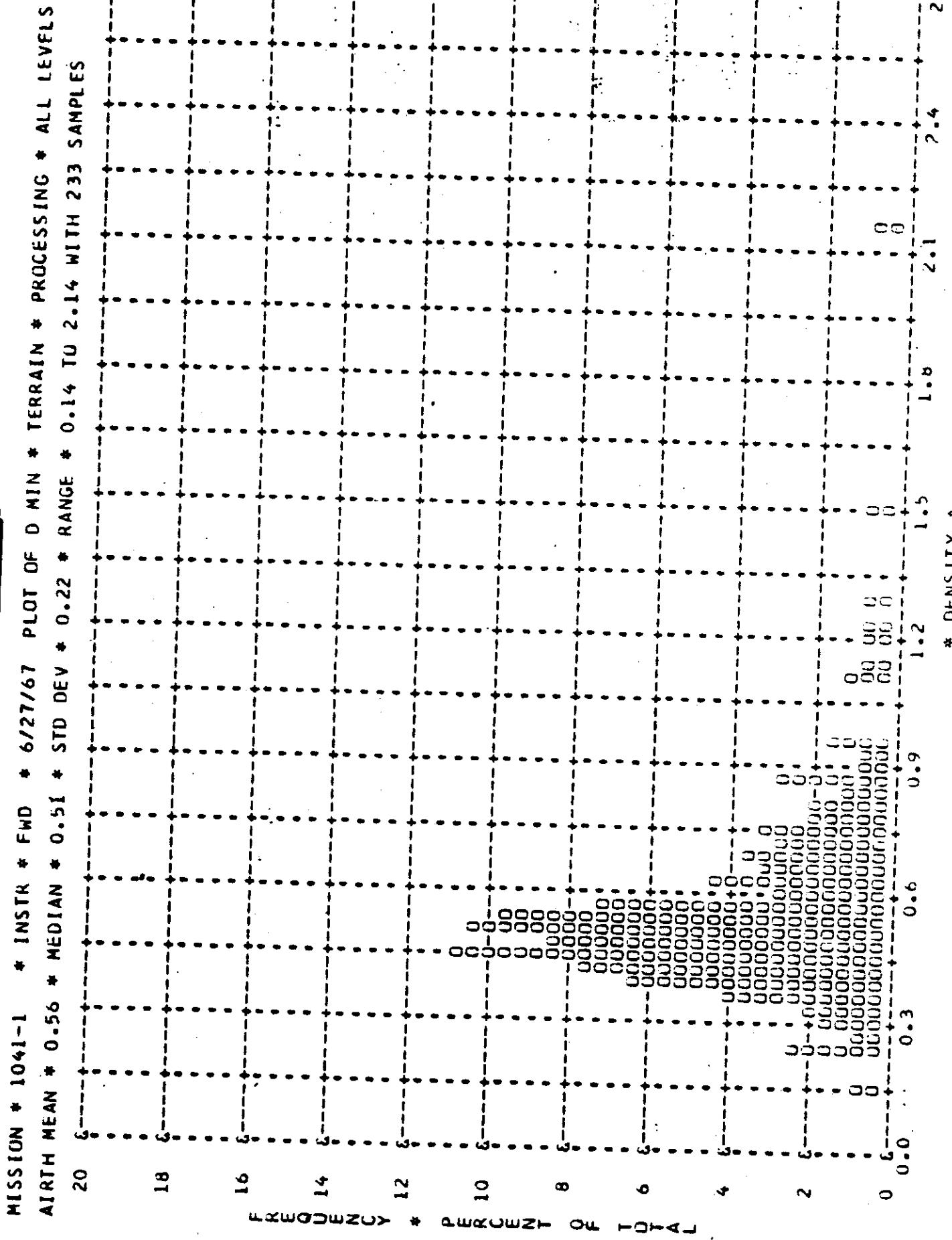
TOP SECRET C



TOP SECRET C

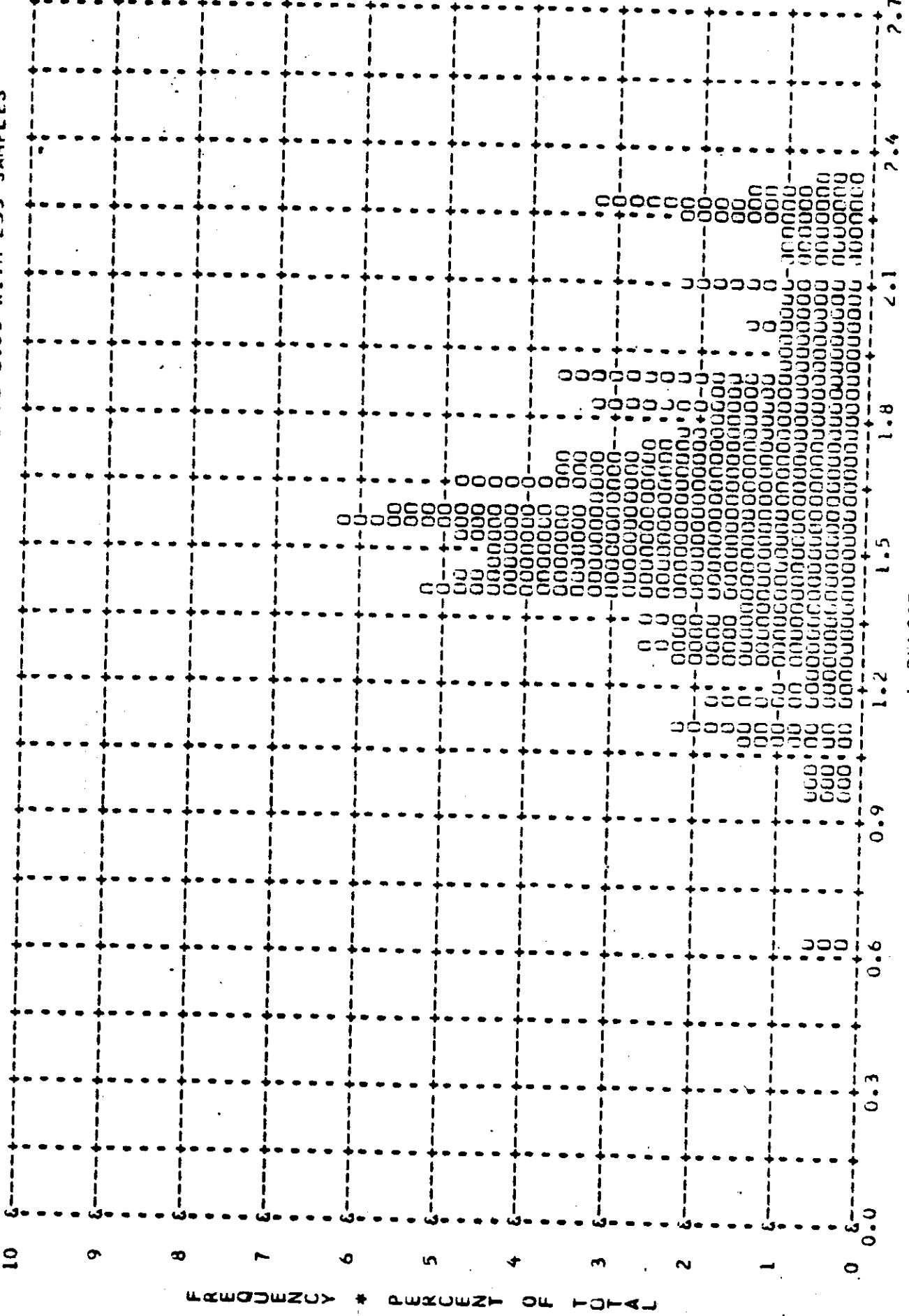
~~TOP SECRET C/~~





-TOP SECRET C

MISSION * 1041-1 * INSTR * FWD * 6/27/67 PLOT OF D MAX * TERRAIN * PROCESSING * ALL LEVELS
AIRT MEAN * 1.62 * MEDIAN * 1.58 * STU DEV * 0.31 * RANGE * 0.62 TO 2.33 WITH 233 SAMPLES

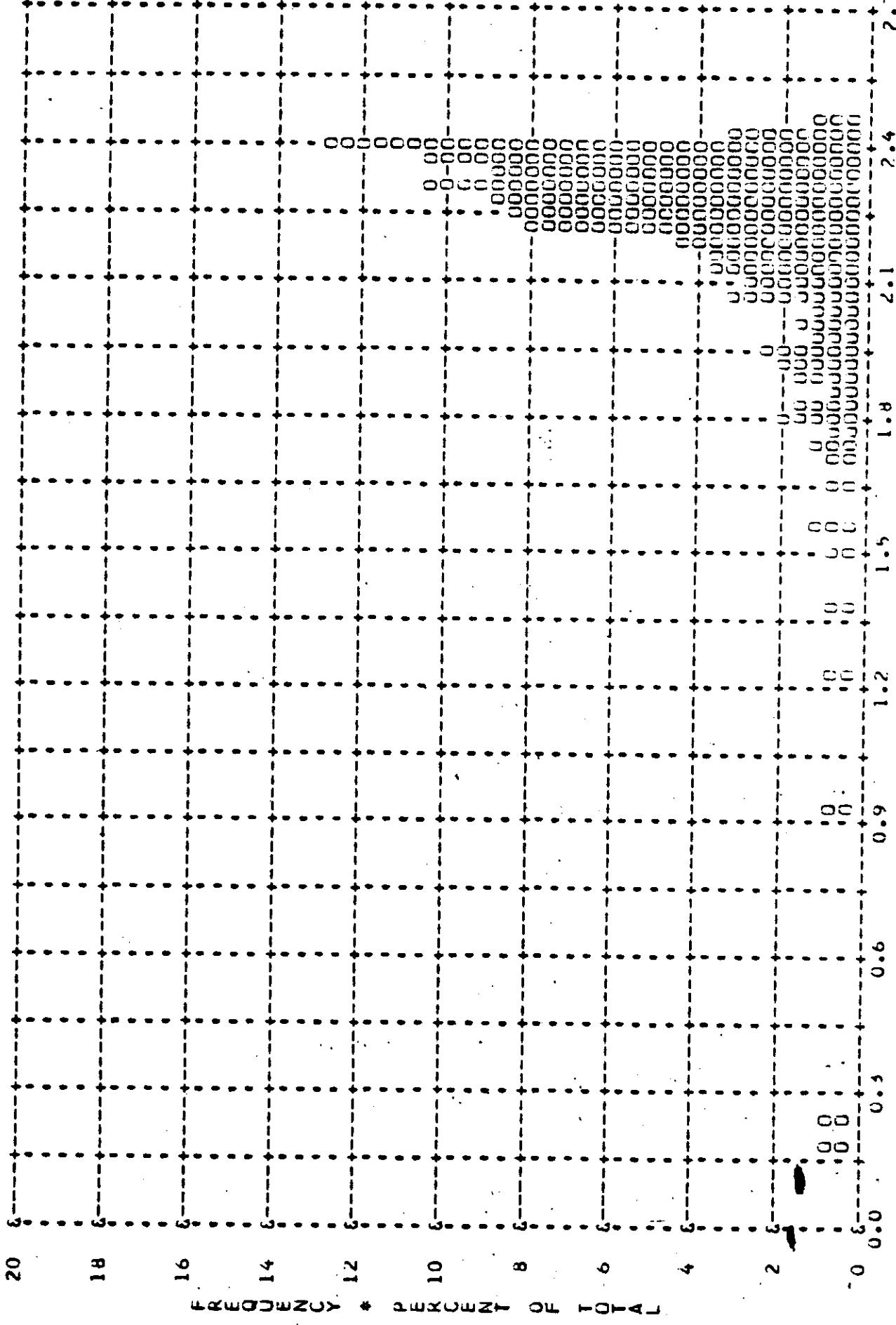


-TOP SECRET

~~TOP SECRET C~~

MISSION * 1041-1 * INSTR * FWD * 6/27/67 PLOT OF D MAX * CLOUD * PROCESSING * ALL LEVELS

AIRTH MEAN * 2.19 * MEDIAN * 2.26 * STD DEV * 0.28 * RANGE * 0.17 TO 2.46 WITH 250 SAMPLES



A-15

~~TOP SECRET C~~

* DENSITY *

~~TOP SECRET C~~

~~TOP SECRET C~~

~~TOP SECRET~~

~~TOP SECRET~~

TABLE A-2

~~TOP SECRET C~~

~~TOP SECRET~~ C

TABLE A-2

~~TOP SECRET~~ C

~~TOP SECRET~~ C

TABLE A-1

~~TOP SECRET C~~

| MISSION * 1041-1 * INSTRUMENT * AFT | 6/27/67 | DENSITY FREQ DISTR | | |
|-------------------------------------|---------------------|--------------------------|------------------|------------------------|
| DENSITY VALUE | PRIMARY MIN MAX LIM | INTERMEDIATE MIN MAX LIM | FULL MIN MAX LIM | ALL LEVELS MIN MAX LIM |
| 1.51 | 0 000 | 0 000 | 0 000 | 0 000 |
| 1.52 | 0 000 | 0 000 | 1 111 | 3 4 |
| 1.53 | 0 000 | 0 000 | 1 112 | 5 2 |
| 1.54 | 0 000 | 0 000 | 2 215 | 2 6 |
| 1.55 | 0 000 | 0 000 | 2 215 | 3 3 |
| 1.56 | 0 000 | 0 000 | 2 215 | 5 2 |
| 1.57 | 0 000 | 0 000 | 2 215 | 3 1 |
| 1.58 | 0 000 | 0 000 | 2 215 | 5 7 |
| 1.59 | 0 000 | 0 000 | 2 215 | 4 1 |
| 1.60 | 0 000 | 0 000 | 2 215 | 2 3 |
| 1.61 | 0 000 | 0 000 | 2 215 | 3 6 |
| 1.62 | 0 000 | 0 000 | 2 215 | 1 0 |
| 1.63 | 0 000 | 0 000 | 2 215 | 1 0 |
| 1.64 | 0 000 | 0 000 | 2 215 | 1 1 |
| 1.65 | 0 000 | 0 000 | 2 215 | 1 1 |
| 1.66 | 0 000 | 0 000 | 2 215 | 2 0 |
| 1.67 | 0 000 | 0 000 | 2 215 | 0 0 |
| 1.68 | 0 000 | 0 000 | 2 215 | 0 0 |
| 1.69 | 0 000 | 0 000 | 2 215 | 0 0 |
| 1.70 | 0 000 | 0 000 | 2 215 | 0 0 |
| 1.71 | 0 000 | 0 000 | 2 215 | 0 0 |
| 1.72 | 0 000 | 0 000 | 2 215 | 0 0 |
| 1.73 | 0 000 | 0 000 | 2 215 | 0 0 |
| 1.74 | 0 000 | 0 000 | 2 215 | 0 0 |
| 1.75 | 0 000 | 0 000 | 2 215 | 0 0 |
| 1.76 | 0 000 | 0 000 | 2 215 | 0 0 |
| 1.77 | 0 000 | 0 000 | 2 215 | 0 0 |
| 1.78 | 0 000 | 0 000 | 2 215 | 0 0 |
| 1.79 | 0 000 | 0 000 | 2 215 | 0 0 |
| 1.80 | 0 000 | 0 000 | 2 215 | 0 0 |
| 1.81 | 0 000 | 0 000 | 2 215 | 0 0 |
| 1.82 | 0 000 | 0 000 | 2 215 | 0 0 |
| 1.83 | 0 000 | 0 000 | 2 215 | 0 0 |
| 1.84 | 0 000 | 0 000 | 2 215 | 0 0 |
| 1.85 | 0 000 | 0 000 | 2 215 | 0 0 |
| 1.86 | 0 000 | 0 000 | 2 215 | 0 0 |
| 1.87 | 0 000 | 0 000 | 2 215 | 0 0 |
| 1.88 | 0 000 | 0 000 | 2 215 | 0 0 |
| 1.89 | 0 000 | 0 000 | 2 215 | 0 0 |
| 1.90 | 0 000 | 0 000 | 2 215 | 0 0 |
| 1.91 | 0 000 | 0 000 | 2 215 | 0 0 |
| 1.92 | 0 000 | 0 000 | 2 215 | 0 0 |
| 1.93 | 0 000 | 0 000 | 2 215 | 0 0 |
| 1.94 | 0 000 | 0 000 | 2 215 | 0 0 |
| 1.95 | 0 000 | 0 000 | 2 215 | 0 0 |
| 1.96 | 0 000 | 0 000 | 2 215 | 0 0 |
| 1.97 | 0 000 | 0 000 | 2 215 | 0 0 |
| 1.98 | 0 000 | 0 000 | 2 215 | 0 0 |
| 1.99 | 0 000 | 0 000 | 2 215 | 0 0 |
| 2.00 | 0 000 | 0 000 | 2 215 | 0 0 |
| SUBTOTAL | 0 000 | 0 000 | 1 50 35 | 9 53 103 44 |

~~TOP SECRET C~~

TABLE A-2

~~TOP SECRET C~~

| MISSION * 1041-1 | * INSTRUMENT * AFT | 6/27/67 | DENSITY FREQ DISTR | |
|------------------|------------------------|-----------------------------|---------------------|---------------------------|
| DENSITY VALUE | PRIMARY MIN MAX LIM | INTERMEDIATE MIN MAX LIM | FULL MIN MAX LIM | ALL LEVELS MIN MAX LIM |
| 2.01 | 0 0 | 0 0 | 0 2 | 0 0 |
| 2.02 | 0 0 | 0 0 | 0 1 | 0 0 |
| 2.03 | 0 0 | 0 0 | 0 1 | 0 0 |
| 2.04 | 0 0 | 0 0 | 0 1 | 0 0 |
| 2.05 | 0 0 | 0 0 | 0 1 | 0 0 |
| 2.06 | 0 0 | 0 0 | 0 1 | 0 0 |
| 2.07 | 0 0 | 0 0 | 0 1 | 0 0 |
| 2.08 | 0 0 | 0 0 | 0 1 | 0 0 |
| 2.09 | 0 0 | 0 0 | 0 1 | 0 0 |
| 2.10 | 0 0 | 0 0 | 0 1 | 0 0 |
| 2.11 | 0 0 | 0 0 | 0 1 | 0 0 |
| 2.12 | 0 0 | 0 0 | 0 1 | 0 0 |
| 2.13 | 0 0 | 0 0 | 0 1 | 0 0 |
| 2.14 | 0 0 | 0 0 | 0 1 | 0 0 |
| 2.15 | 0 0 | 0 0 | 0 1 | 0 0 |
| 2.16 | 0 0 | 0 0 | 0 1 | 0 0 |
| 2.17 | 0 0 | 0 0 | 0 1 | 0 0 |
| 2.18 | 0 0 | 0 0 | 0 1 | 0 0 |
| 2.19 | 0 0 | 0 0 | 0 1 | 0 0 |
| 2.20 | 0 0 | 0 0 | 0 1 | 0 0 |
| 2.21 | 0 0 | 0 0 | 0 1 | 0 0 |
| 2.22 | 0 0 | 0 0 | 0 1 | 0 0 |
| 2.23 | 0 0 | 0 0 | 0 1 | 0 0 |
| 2.24 | 0 0 | 0 0 | 0 1 | 0 0 |
| 2.25 | 0 0 | 0 0 | 0 1 | 0 0 |
| 2.26 | 0 0 | 0 0 | 0 1 | 0 0 |
| 2.27 | 0 0 | 0 0 | 0 1 | 0 0 |
| 2.28 | 0 0 | 0 0 | 0 1 | 0 0 |
| 2.29 | 0 0 | 0 0 | 0 1 | 0 0 |
| 2.30 | 0 0 | 0 0 | 0 1 | 0 0 |
| 2.31 | 0 0 | 0 0 | 0 1 | 0 0 |
| 2.32 | 0 0 | 0 0 | 0 1 | 0 0 |
| 2.33 | 0 0 | 0 0 | 0 1 | 0 0 |
| 2.34 | 0 0 | 0 0 | 0 1 | 0 0 |
| 2.35 | 0 0 | 0 0 | 0 1 | 0 0 |
| 2.36 | 0 0 | 0 0 | 0 1 | 0 0 |
| 2.37 | 0 0 | 0 0 | 0 1 | 0 0 |
| 2.38 | 0 0 | 0 0 | 0 1 | 0 0 |
| 2.39 | 0 0 | 0 0 | 0 1 | 0 0 |
| 2.40 | 0 0 | 0 0 | 0 1 | 0 0 |
| 2.41 | 0 0 | 0 0 | 0 1 | 0 0 |
| 2.42 | 0 0 | 0 0 | 0 1 | 0 0 |
| 2.43 | 0 0 | 0 0 | 0 1 | 0 0 |
| 2.44 | 0 0 | 0 0 | 0 1 | 0 0 |
| 2.45 | 0 0 | 0 0 | 0 1 | 0 0 |
| 2.46 | 0 0 | 0 0 | 0 1 | 0 0 |
| 2.47 | 0 0 | 0 0 | 0 1 | 0 0 |
| 2.48 | 0 0 | 0 0 | 0 1 | 0 0 |
| 2.49 | 0 0 | 0 0 | 0 1 | 0 0 |
| 2.50 | 0 0 | 0 0 | 0 1 | 0 0 |
| SUBTOTAL | 0 0 | 0 0 | 0 16 | 0 125 |
| | | | | 31 204 |

~~TOP SECRET C~~

TABLE A-2

~~TOP SECRET C~~

MISSION * 1041-1 * INSTRUMENT * AFT 6/27/67 DENSITY FRQ DISTR

| DENSITY VALUE | PRIMARY | | | INTERMEDIATE | | | FULL | | | ALL LEVELS | | |
|------------------|---------|-----|-----|--------------|-----|-----|------|-----|-----|------------|-----|-----|
| | MIN | MAX | LIM | MIN | MAX | LIM | MIN | MAX | LIM | MIN | MAX | LIM |
| 2.51 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2.52 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2.53 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2.54 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2.55 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2.56 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2.57 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2.58 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2.59 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2.60 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2.61 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2.62 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2.63 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2.64 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2.65 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2.66 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2.67 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2.68 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2.69 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2.70 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| SUBTOTAL | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| TOTAL | 0 | 0 | 0 | 102 | 102 | 119 | 113 | 113 | 134 | 215 | 215 | 253 |

MISSION 1041-1 INSTR - AFT 6/27/67 PROCESSING AND EXPOSURE ANALYSIS

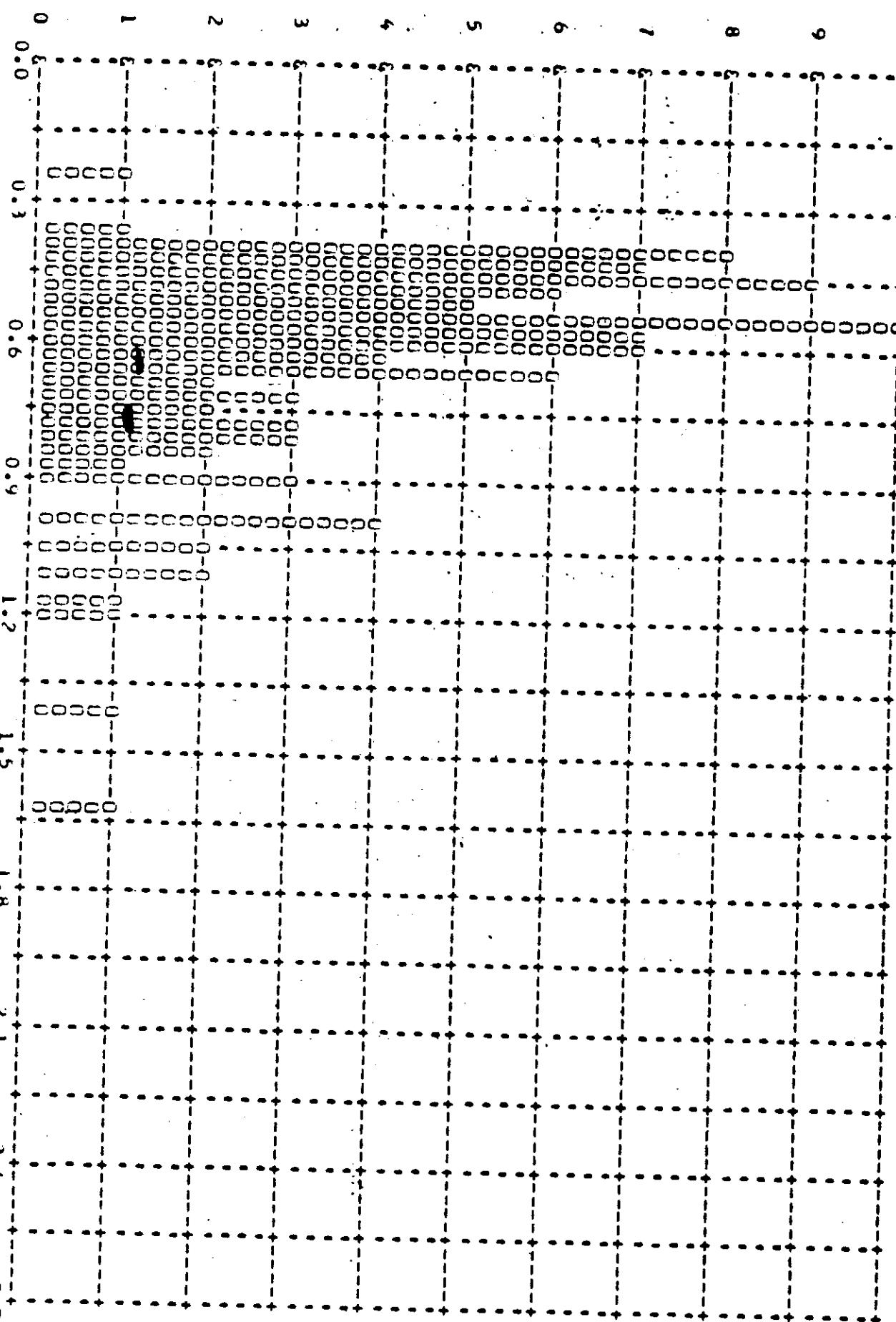
| PROCESS LEVEL | SAMPLE SIZE | UNDER EXPOSED | | UNDER PROCESSED | | CORRECT EXP&PROC | OVER PROCESSED | OVER EXPOSED | |
|------------------|----------------|------------------|-----------|--------------------|-------|---------------------|-------------------|-----------------|----|
| | | 0 | PC | 0 | PC | | | | 0 |
| PRIMARY | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| INTERMEDIATE | 102 | 0 | PC | 10 | PC | 78 | PC | 52 | PC |
| FULL | 113 | 2 | PC | 0 | PC | 92 | PC | 10 | PC |
| ALL LEVELS | 215 | 1 | PC | 5 | PC | 86 | PC | 6 | PC |
| PROCESS LEVEL | BASE & FOG | UNDER EXPOSED | | UNDER PROCESSED | | CORRECT EXP&PROC | OVER PROCESSED | OVER EXPOSED | |
| PRIMARY | 0.01-0.09 | 0.01-0.13 | 0.14-0.39 | 0.40-0.90 | ----- | ----- | 0.91 | AND UP | |
| INTERMED | 0.10-0.17 | 0.01-0.20 | 0.21-0.39 | 0.40-0.90 | ----- | 0.91-1.34 | 1.35 | AND UP | |
| FULL | 0.18 AND UP | 0.01-0.39 | ----- | 0.40-0.90 | ----- | 0.91-1.69 | 1.70 | AND UP | |

~~TOP SECRET C~~

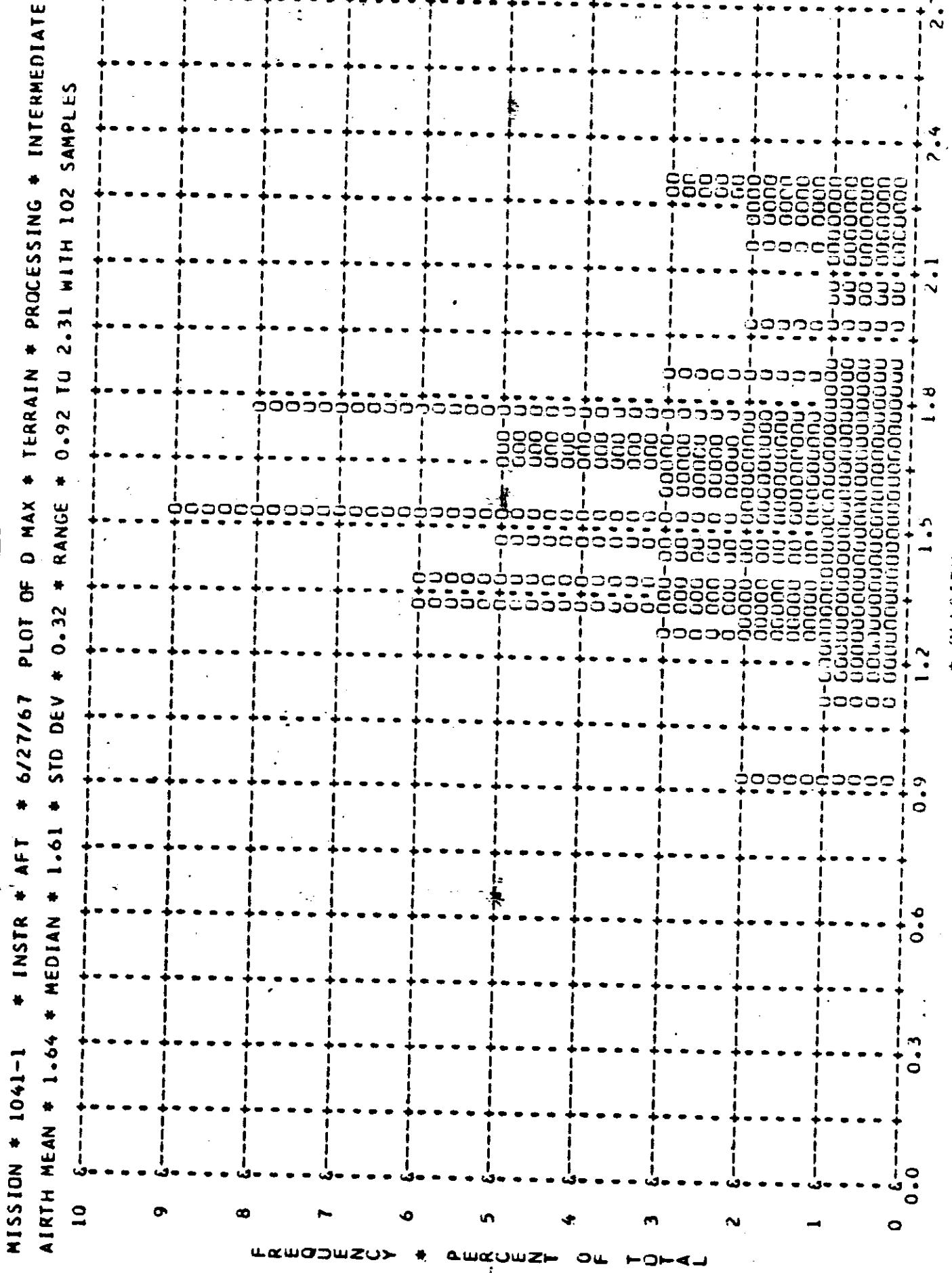
TABLE A-2

-TOP SECRET- C

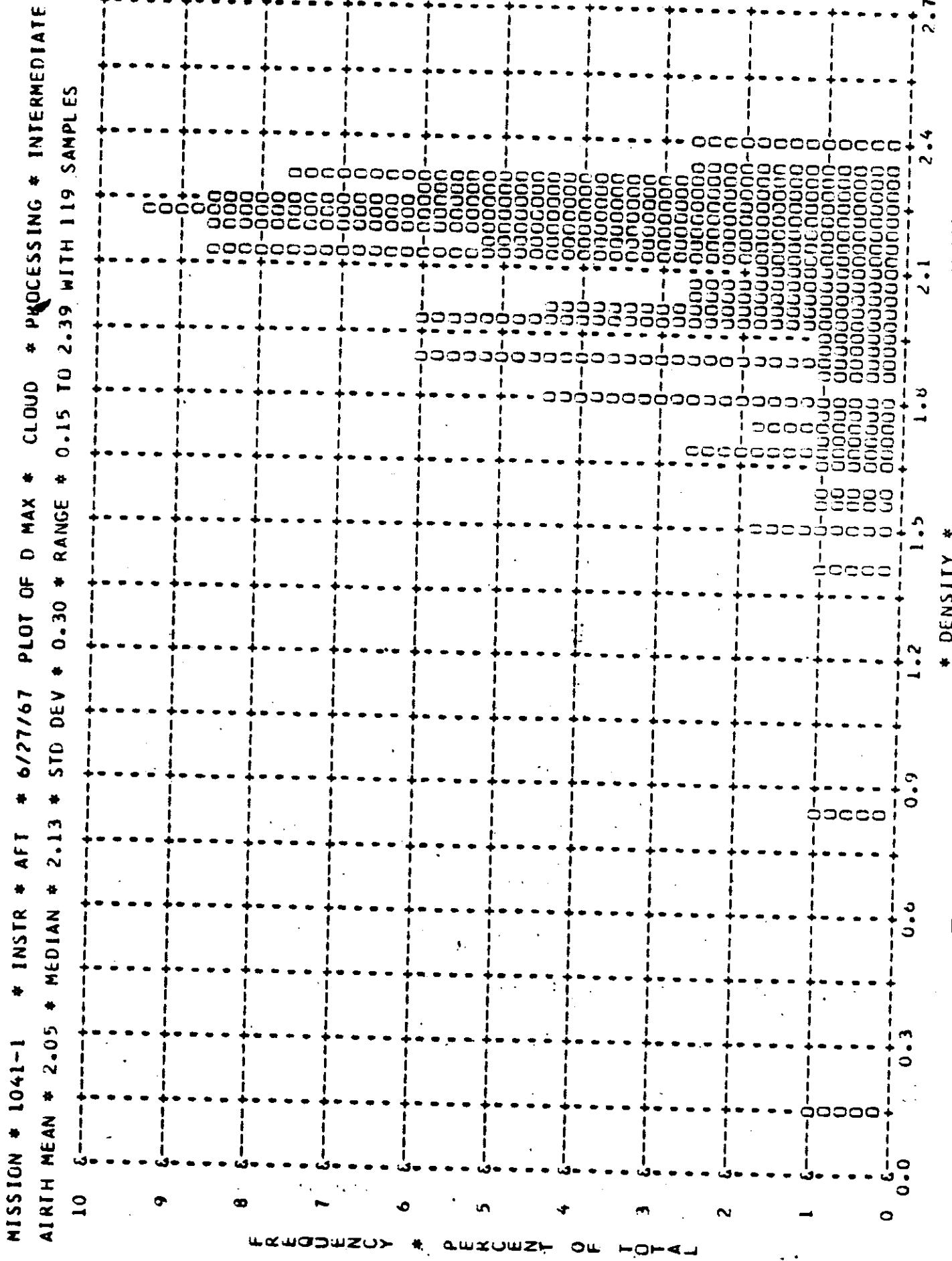
MISSION # 1041-1 * INSTR # AFT * 6/27/67 PLOT OF D MIN * TERRAIN * PROCESSING * INTERMEDIATE
AIRTH MEAN # 0.63 * MEDIAN # 0.57 * STD DEV # 0.24 * RANGE # 0.22 TO 1.62 WITH 102 SAMPLES



~~TOP SECRET C~~



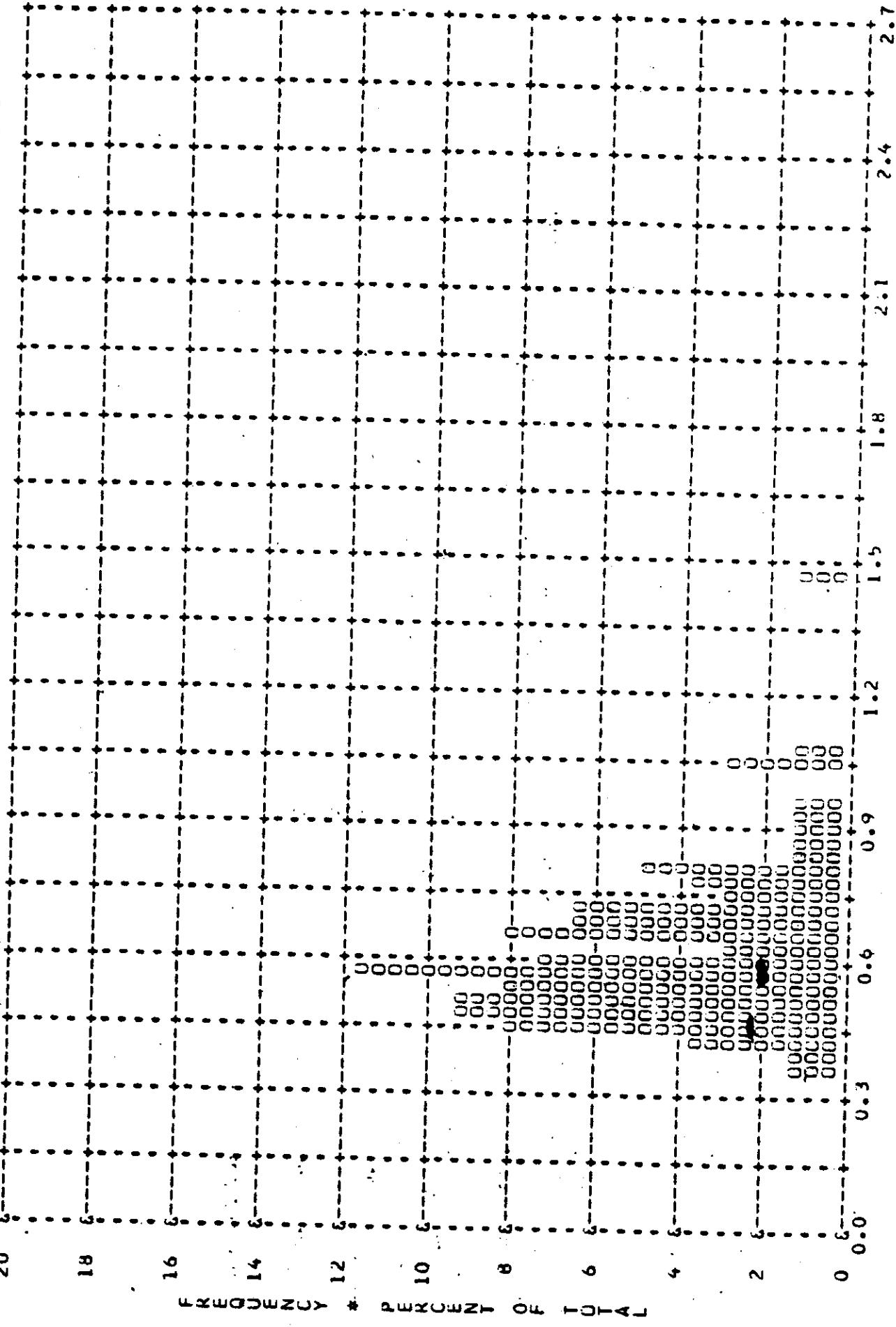
~~TOP SECRET~~ C



~~TOP SECRET~~ C

-TOP SECRET C

MISSION * 1041-1 * INSTR * AFT * 6/27/67 PLOT OF D MIN * TERRAIN * PROCESSING * FULL
AIRT MEAN * 0.62 * MEDIAN * 0.57 * STU DEV * 0.17 * RANGE * 0.36 TO 1.46 WITH 113 SAMPLES



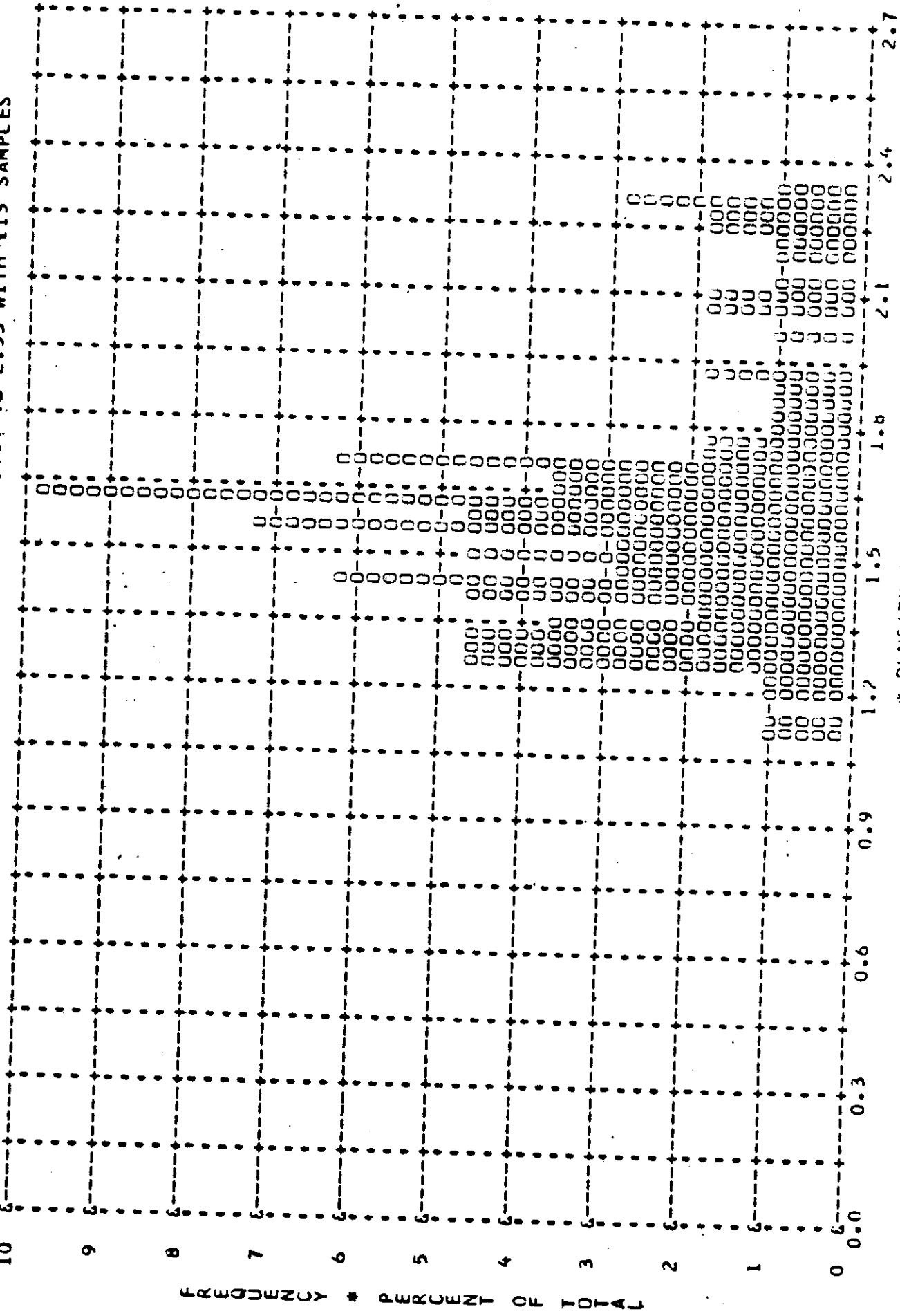
-TOP SECRET C

* DENSITY *

-TOP SECRET C

TOP SECRET C

MISSION * 1041-1 * INSTR * AFT * 6/27/67 PLOT OF D MAX * TERRAIN * PROCESSING * FULL
AIRTH MEAN * 1.61 * MEDIAN * 1.57 * STD DEV * 0.29 * RANGE * 1.09 TO 2.33 WITH 113 SAMPLES



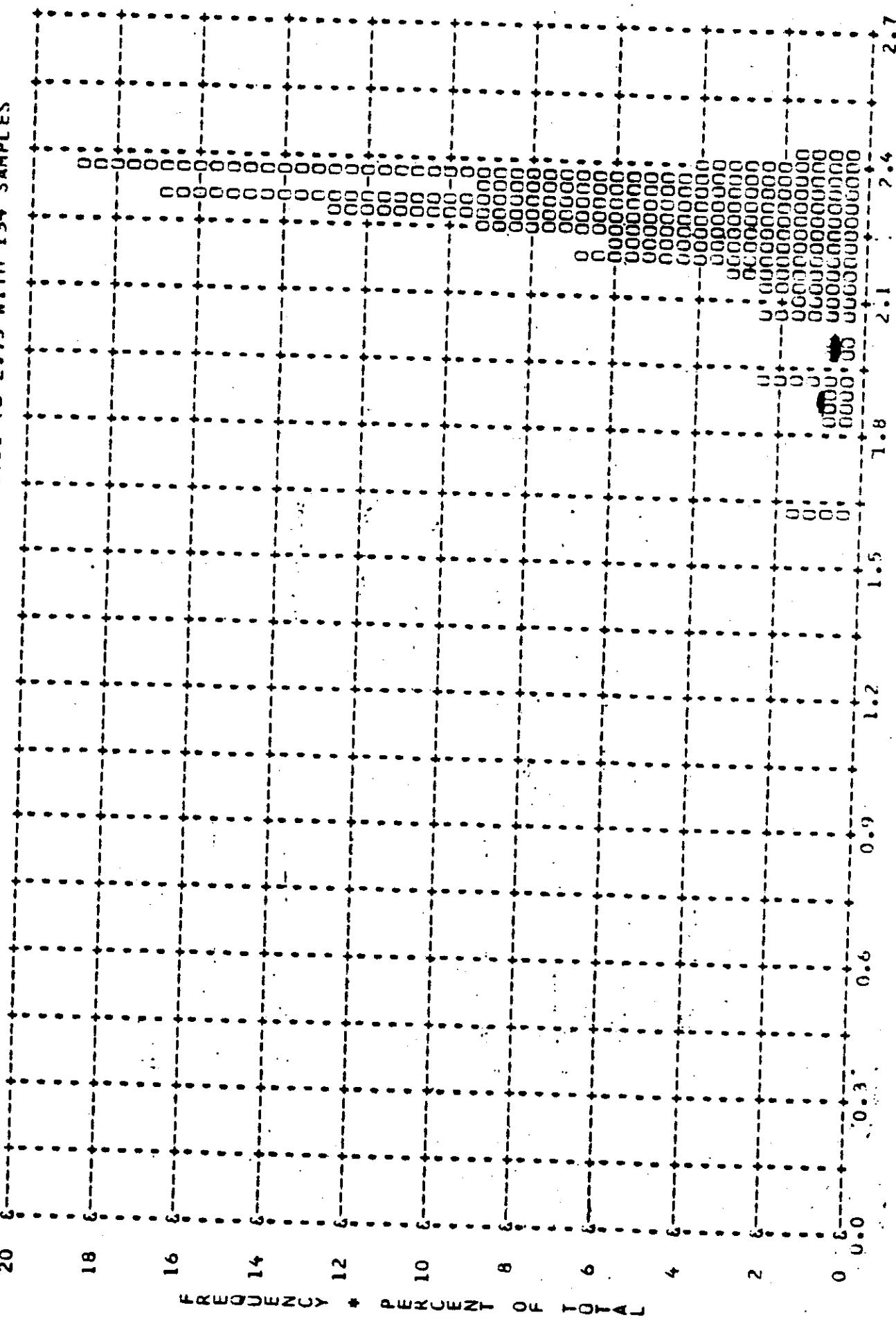
TOP SECRET C

* DENSITY *

TOP SECRET C

-TOP SECRET C

MISSION * 1041-1 * INSTR * AFT * 6/27/67 PLOT OF D MAX * CLOUD * PROCESSING * FULL
AIRTH MEAN * 2.25 * MEDIAN * 2.28 * STD DEV * 0.14 * RANGE * 1.61 TU 2.43 WITH 134 SAMPLES

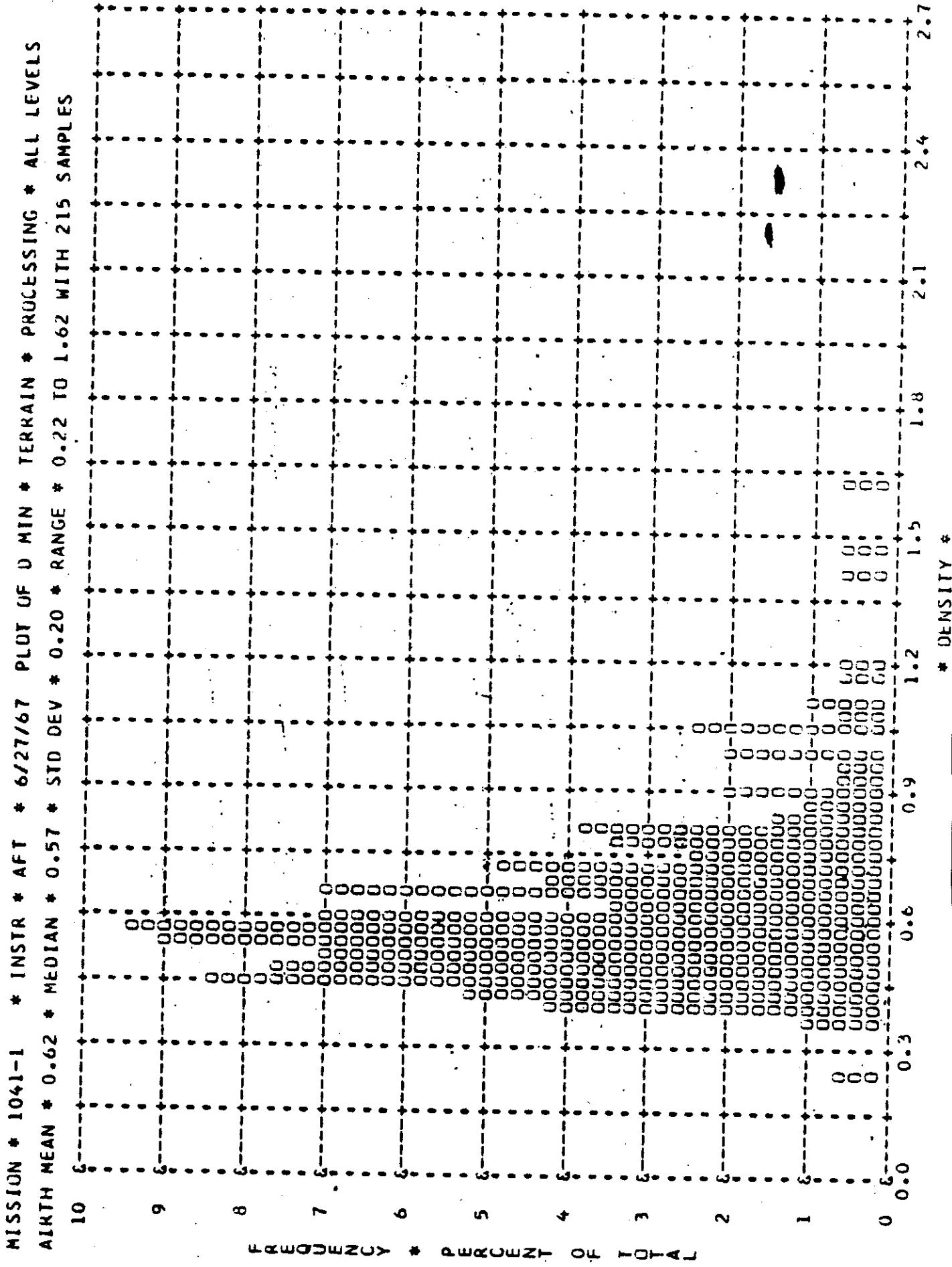


F-107 Rev A-11

* DENSITY *

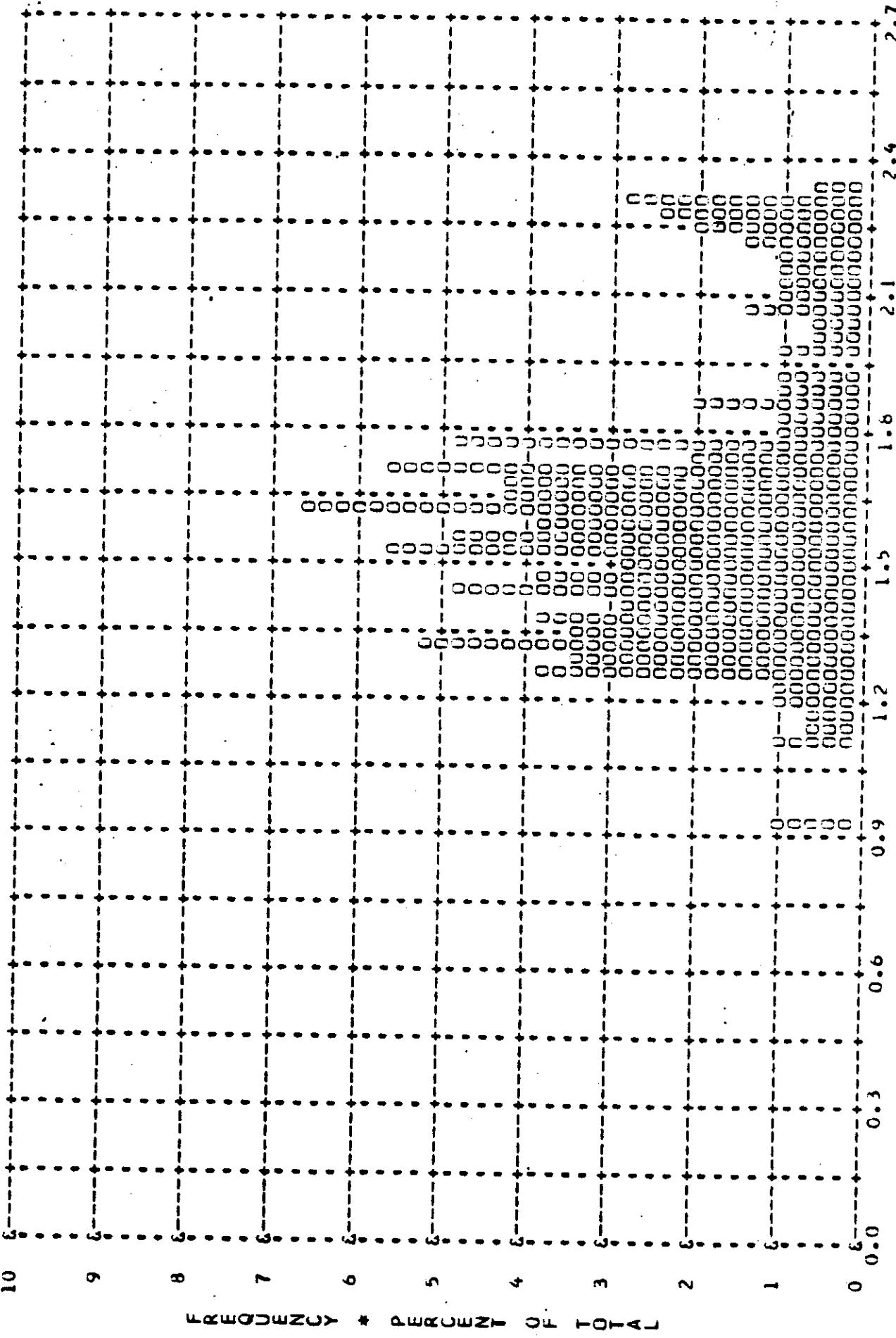
-TOP SECRET C

~~TOP SECRET C~~



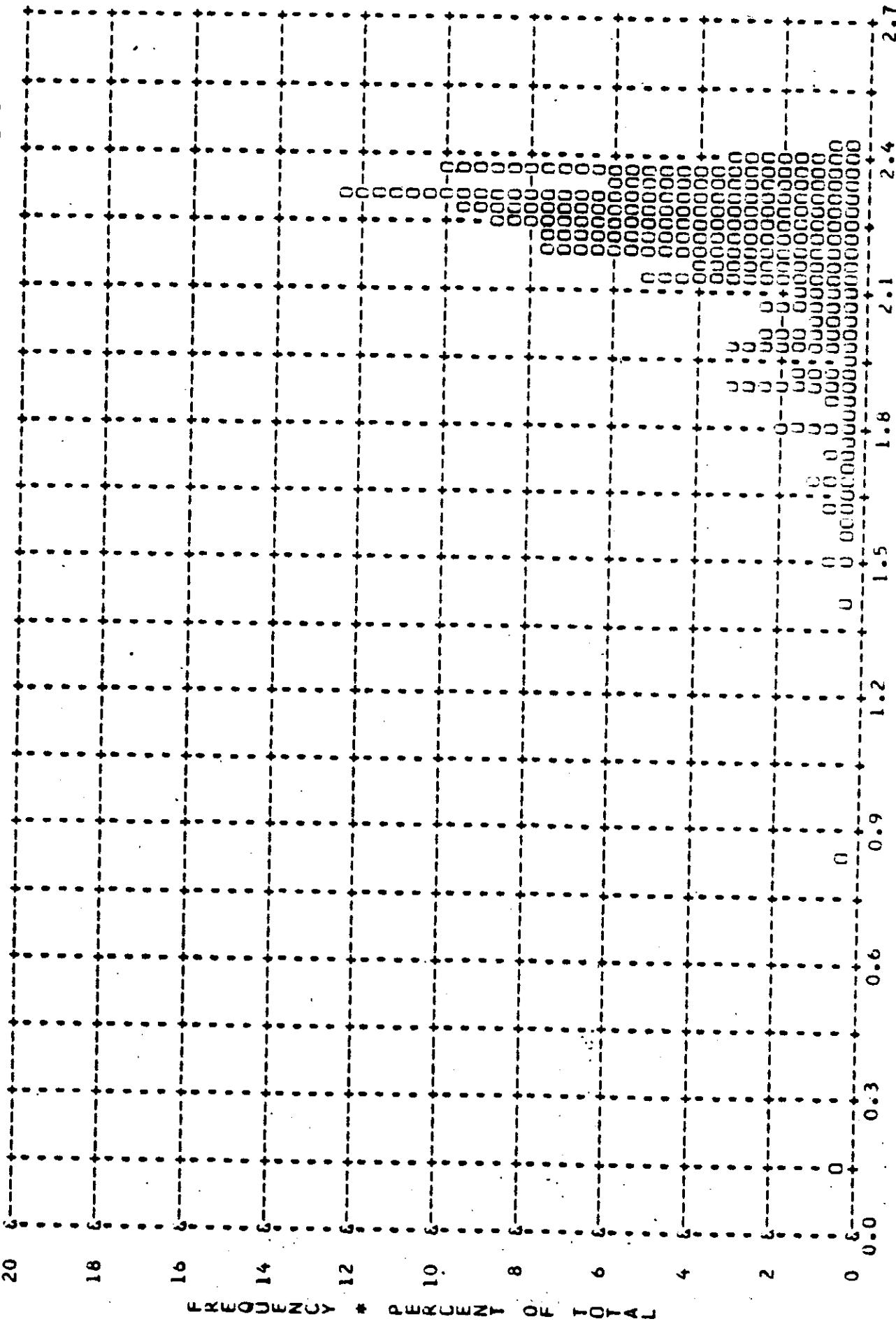
~~TOP SECRET C~~

MISSION * 1041-1 * INSTR * AFT * 6/27/67 PLOT OF D MAX * TERRAIN * PROCESSING * ALL LEVELS
AIRTH MEAN * 1.62 * MEDIAN * 1.58 * STD DEV * 0.31 * RANGE * 0.92 TO 2.33 WITH 215 SAMPLES



TOP SECRET C

MISSION * 1041-1 * INSTR * AFT * 6/27/67 PLOT OF D MAX * CLOUD * PROCESSING * ALL LEVELS
AIRTH MEAN * 2.15 * MEDIAN * 2.23 * STD DEV * 0.25 * RANGE * 0.15 TO 2.43 WITH 253 SAMPLES



TOP SECRET C

~~TOP SECRET C~~

MISSION * 1041-2 * INSTRUMENT * FWD * 6/27/67 DENSITY FREQ DISR

| DENSITY VALUE | PRIMARY MIN MAX LIM | INTERMEDIATE MIN MAX LIM | FULL MIN MAX LIM | ALL LEVELS MIN MAX LIM |
|------------------|------------------------|-----------------------------|---------------------|---------------------------|
| 0.01 | 0 | 0 | 0 | 0 |
| 0.02 | 00 | 00 | 00 | 00 |
| 0.03 | 00 | 00 | 00 | 00 |
| 0.04 | 00 | 00 | 00 | 00 |
| 0.05 | 00 | 00 | 00 | 00 |
| 0.06 | 00 | 00 | 00 | 00 |
| 0.07 | 00 | 00 | 00 | 00 |
| 0.08 | 00 | 00 | 00 | 00 |
| 0.09 | 00 | 00 | 00 | 00 |
| 0.10 | 00 | 00 | 00 | 00 |
| 0.11 | 00 | 00 | 00 | 00 |
| 0.12 | 00 | 00 | 00 | 00 |
| 0.13 | 00 | 00 | 00 | 00 |
| 0.14 | 00 | 00 | 00 | 00 |
| 0.15 | 00 | 00 | 00 | 00 |
| 0.16 | 00 | 00 | 00 | 00 |
| 0.17 | 00 | 00 | 00 | 00 |
| 0.18 | 00 | 00 | 00 | 00 |
| 0.19 | 00 | 00 | 00 | 00 |
| 0.20 | 00 | 00 | 00 | 00 |
| 0.21 | 00 | 00 | 00 | 00 |
| 0.22 | 00 | 00 | 00 | 00 |
| 0.23 | 00 | 00 | 00 | 00 |
| 0.24 | 00 | 00 | 00 | 00 |
| 0.25 | 00 | 00 | 00 | 00 |
| 0.26 | 00 | 00 | 00 | 00 |
| 0.27 | 00 | 00 | 00 | 00 |
| 0.28 | 00 | 00 | 00 | 00 |
| 0.29 | 00 | 00 | 00 | 00 |
| 0.30 | 00 | 00 | 00 | 00 |
| 0.31 | 00 | 00 | 00 | 00 |
| 0.32 | 00 | 00 | 00 | 00 |
| 0.33 | 00 | 00 | 00 | 00 |
| 0.34 | 00 | 00 | 00 | 00 |
| 0.35 | 00 | 00 | 00 | 00 |
| 0.36 | 00 | 00 | 00 | 00 |
| 0.37 | 00 | 00 | 00 | 00 |
| 0.38 | 00 | 00 | 00 | 00 |
| 0.39 | 00 | 00 | 00 | 00 |
| 0.40 | 00 | 00 | 00 | 00 |
| 0.41 | 00 | 00 | 00 | 00 |
| 0.42 | 00 | 00 | 00 | 00 |
| 0.43 | 00 | 00 | 00 | 00 |
| 0.44 | 00 | 00 | 00 | 00 |
| 0.45 | 00 | 00 | 00 | 00 |
| 0.46 | 00 | 00 | 00 | 00 |
| 0.47 | 00 | 00 | 00 | 00 |
| 0.48 | 00 | 00 | 00 | 00 |
| 0.49 | 00 | 00 | 00 | 00 |
| 0.50 | 00 | 00 | 00 | 00 |
| SUBTOTAL | 0 | 0 | 15 | 0 |
| | | | | 48 |
| | | | | 63 |

~~TOP SECRET C~~

TABLE A-3

~~TOP SECRET C~~

MISSION * 1041-2 * INSTRUMENT * FWD 6/27/67 DENSITY FREQ DISTR

| DENSITY VALUE | PRIMARY MIN MAX LIM | INTERMEDIATE MIN MAX LIM | FULL MIN MAX LIM | ALL LEVELS MIN MAX LIM |
|---------------|------------------------|-----------------------------|---------------------|---------------------------|
| 0.51 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.52 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.53 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.54 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.55 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.56 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.57 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.58 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.59 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.60 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.61 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.62 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.63 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.64 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.65 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.66 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.67 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.68 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.69 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.70 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.71 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.72 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.73 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.74 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.75 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.76 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.77 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.78 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.79 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.80 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.81 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.82 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.83 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.84 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.85 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.86 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.87 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.88 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.89 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.90 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.91 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.92 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.93 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.94 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.95 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.96 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.97 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.98 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.99 | 0 0 | 0 0 | 0 0 | 0 0 |
| 1.00 | 0 0 | 0 0 | 0 0 | 0 0 |
| SUBTOTAL | 0 0 | 0 0 | 30 2 | 115 145 |

~~TOP SECRET C~~

TABLE A-3

~~TOP SECRET C~~

MISSION * 1041-2 * INSTRUMFT * FWD 6/27/67 DENSITY FREQ DISTR

| DENSITY VALUE | PRIMARY MIN MAX LIM | INTERMEDIATE MIN MAX LIM | FULL MIN MAX LIM | ALL LEVELS MIN MAX LIM |
|---------------|----------------------------------------------------|-----------------------------|-------------------------|---------------------------|
| 1.01 | 0 | 0 | 0 | 0 |
| 1.02 | 00 | 00 | 00 | 2 |
| 1.03 | 000 | 000 | 000 | 1 |
| 1.04 | 0000 | 0000 | 0000 | 2 |
| 1.05 | 00000 | 00000 | 00000 | 1 |
| 1.06 | 000000 | 000000 | 000000 | 2 |
| 1.07 | 0000000 | 0000000 | 0000000 | 1 |
| 1.08 | 00000000 | 00000000 | 00000000 | 2 |
| 1.09 | 000000000 | 000000000 | 000000000 | 1 |
| 1.10 | 0000000000 | 0000000000 | 0000000000 | 2 |
| 1.11 | 00000000000 | 00000000000 | 00000000000 | 1 |
| 1.12 | 000000000000 | 000000000000 | 000000000000 | 2 |
| 1.13 | 0000000000000 | 0000000000000 | 0000000000000 | 1 |
| 1.14 | 00000000000000 | 00000000000000 | 00000000000000 | 2 |
| 1.15 | 000000000000000 | 000000000000000 | 000000000000000 | 1 |
| 1.16 | 0000000000000000 | 0000000000000000 | 0000000000000000 | 2 |
| 1.17 | 00000000000000000 | 00000000000000000 | 00000000000000000 | 1 |
| 1.18 | 000000000000000000 | 000000000000000000 | 000000000000000000 | 2 |
| 1.19 | 0000000000000000000 | 0000000000000000000 | 0000000000000000000 | 1 |
| 1.20 | 00000000000000000000 | 00000000000000000000 | 00000000000000000000 | 2 |
| 1.21 | 000000000000000000000 | 000000000000000000000 | 000000000000000000000 | 1 |
| 1.22 | 0000000000000000000000 | 0000000000000000000000 | 0000000000000000000000 | 2 |
| 1.23 | 00000000000000000000000 | 00000000000000000000000 | 00000000000000000000000 | 1 |
| 1.24 | 000000000000000000000000 | 00000000000000000000000 | 00000000000000000000000 | 2 |
| 1.25 | 0000000000000000000000000 | 00000000000000000000000 | 00000000000000000000000 | 1 |
| 1.26 | 00000000000000000000000000 | 00000000000000000000000 | 00000000000000000000000 | 2 |
| 1.27 | 000000000000000000000000000 | 00000000000000000000000 | 00000000000000000000000 | 1 |
| 1.28 | 0000000000000000000000000000 | 00000000000000000000000 | 00000000000000000000000 | 2 |
| 1.29 | 00000000000000000000000000000 | 00000000000000000000000 | 00000000000000000000000 | 1 |
| 1.30 | 000000000000000000000000000000 | 00000000000000000000000 | 00000000000000000000000 | 2 |
| 1.31 | 0000000000000000000000000000000 | 00000000000000000000000 | 00000000000000000000000 | 1 |
| 1.32 | 00000000000000000000000000000000 | 00000000000000000000000 | 00000000000000000000000 | 2 |
| 1.33 | 000000000000000000000000000000000 | 00000000000000000000000 | 00000000000000000000000 | 1 |
| 1.34 | 0000000000000000000000000000000000 | 00000000000000000000000 | 00000000000000000000000 | 2 |
| 1.35 | 00000000000000000000000000000000000 | 00000000000000000000000 | 00000000000000000000000 | 1 |
| 1.36 | 000000000000000000000000000000000000 | 00000000000000000000000 | 00000000000000000000000 | 2 |
| 1.37 | 0000000000000000000000000000000000000 | 00000000000000000000000 | 00000000000000000000000 | 1 |
| 1.38 | 00000000000000000000000000000000000000 | 00000000000000000000000 | 00000000000000000000000 | 2 |
| 1.39 | 000000000000000000000000000000000000000 | 00000000000000000000000 | 00000000000000000000000 | 1 |
| 1.40 | 0000000000000000000000000000000000000000 | 00000000000000000000000 | 00000000000000000000000 | 2 |
| 1.41 | 00000000000000000000000000000000000000000 | 00000000000000000000000 | 00000000000000000000000 | 1 |
| 1.42 | 000000000000000000000000000000000000000000 | 00000000000000000000000 | 00000000000000000000000 | 2 |
| 1.43 | 0000000000000000000000000000000000000000000 | 00000000000000000000000 | 00000000000000000000000 | 1 |
| 1.44 | 00000000000000000000000000000000000000000000 | 00000000000000000000000 | 00000000000000000000000 | 2 |
| 1.45 | 000000000000000000000000000000000000000000000 | 00000000000000000000000 | 00000000000000000000000 | 1 |
| 1.46 | 0000000000000000000000000000000000000000000000 | 00000000000000000000000 | 00000000000000000000000 | 2 |
| 1.47 | 00000000000000000000000000000000000000000000000 | 00000000000000000000000 | 00000000000000000000000 | 1 |
| 1.48 | 000000000000000000000000000000000000000000000000 | 00000000000000000000000 | 00000000000000000000000 | 2 |
| 1.49 | 0000000000000000000000000000000000000000000000000 | 00000000000000000000000 | 00000000000000000000000 | 1 |
| 1.50 | 00000000000000000000000000000000000000000000000000 | 00000000000000000000000 | 00000000000000000000000 | 2 |
| SUBTOTAL | 0 | 0 | 0 | 107 |
| | | | 98 | 21 |

~~TOP SECRET C~~

TABLE A-3

~~TOP SECRET C~~

MISSION * 1041-2 * INSTRUMENT * FWD 6/27/67 DENSITY FREQ DISTR

| DENSITY VALUE | PRIMARY MIN MAX LIM | INTERMEDIATE MIN MAX LIM | FULL MIN MAX LIM | ALL LEVELS MIN MAX LIM |
|---------------|------------------------|-----------------------------|---------------------|---------------------------|
| 1.51 | 0 0 | 0 0 | 0 0 | 0 0 |
| 1.52 | 0 0 | 0 0 | 0 0 | 1 0 |
| 1.53 | 0 0 | 0 0 | 0 0 | 0 0 |
| 1.54 | 0 0 | 0 0 | 0 0 | 0 0 |
| 1.55 | 0 0 | 0 0 | 0 0 | 0 0 |
| 1.56 | 0 0 | 0 0 | 0 0 | 0 0 |
| 1.57 | 0 0 | 0 0 | 0 0 | 0 0 |
| 1.58 | 0 0 | 0 0 | 0 0 | 0 0 |
| 1.59 | 0 0 | 0 0 | 0 0 | 0 0 |
| 1.60 | 0 0 | 0 0 | 0 0 | 0 0 |
| 1.61 | 0 0 | 0 0 | 0 0 | 0 0 |
| 1.62 | 0 0 | 0 0 | 0 0 | 0 0 |
| 1.63 | 0 0 | 0 0 | 0 0 | 0 0 |
| 1.64 | 0 0 | 0 0 | 0 0 | 0 0 |
| 1.65 | 0 0 | 0 0 | 0 0 | 0 0 |
| 1.66 | 0 0 | 0 0 | 0 0 | 0 0 |
| 1.67 | 0 0 | 0 0 | 0 0 | 0 0 |
| 1.68 | 0 0 | 0 0 | 0 0 | 0 0 |
| 1.69 | 0 0 | 0 0 | 0 0 | 0 0 |
| 1.70 | 0 0 | 0 0 | 0 0 | 0 0 |
| 1.71 | 0 0 | 0 0 | 0 0 | 0 0 |
| 1.72 | 0 0 | 0 0 | 0 0 | 0 0 |
| 1.73 | 0 0 | 0 0 | 0 0 | 0 0 |
| 1.74 | 0 0 | 0 0 | 0 0 | 0 0 |
| 1.75 | 0 0 | 0 0 | 0 0 | 0 0 |
| 1.76 | 0 0 | 0 0 | 0 0 | 0 0 |
| 1.77 | 0 0 | 0 0 | 0 0 | 0 0 |
| 1.78 | 0 0 | 0 0 | 0 0 | 0 0 |
| 1.79 | 0 0 | 0 0 | 0 0 | 0 0 |
| 1.80 | 0 0 | 0 0 | 0 0 | 0 0 |
| 1.81 | 0 0 | 0 0 | 0 0 | 0 0 |
| 1.82 | 0 0 | 0 0 | 0 0 | 0 0 |
| 1.83 | 0 0 | 0 0 | 0 0 | 0 0 |
| 1.84 | 0 0 | 0 0 | 0 0 | 0 0 |
| 1.85 | 0 0 | 0 0 | 0 0 | 0 0 |
| 1.86 | 0 0 | 0 0 | 0 0 | 0 0 |
| 1.87 | 0 0 | 0 0 | 0 0 | 0 0 |
| 1.88 | 0 0 | 0 0 | 0 0 | 0 0 |
| 1.89 | 0 0 | 0 0 | 0 0 | 0 0 |
| 1.90 | 0 0 | 0 0 | 0 0 | 0 0 |
| 1.91 | 0 0 | 0 0 | 0 0 | 0 0 |
| 1.92 | 0 0 | 0 0 | 0 0 | 0 0 |
| 1.93 | 0 0 | 0 0 | 0 0 | 0 0 |
| 1.94 | 0 0 | 0 0 | 0 0 | 0 0 |
| 1.95 | 0 0 | 0 0 | 0 0 | 0 0 |
| 1.96 | 0 0 | 0 0 | 0 0 | 0 0 |
| 1.97 | 0 0 | 0 0 | 0 0 | 0 0 |
| 1.98 | 0 0 | 0 0 | 0 0 | 0 0 |
| 1.99 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.00 | 0 0 | 0 0 | 0 0 | 0 0 |
| SUBTOTAL | 0 0 | 0 0 | 37 26 | 1 58 19 95 45 |

~~TOP SECRET C~~

TABLE A-3

~~TOP SECRET~~

MISSION # 1041-2 * INSTRUMENT # EWD

.6/27/67

DENSITY FREQ DISTR

| DENSITY VALUE | PRIMARY | | | INTERMEDIATE | | | FULL | | | ALL LEVELS | | |
|------------------|---------|-----|-----|--------------|-----|-----|------|-----|-----|------------|-----|-----|
| | MIN | MAX | LIM | MIN | MAX | LIM | MIN | MAX | LIM | MIN | MAX | LIM |
| 2.01 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 31 | 34 | 14 |
| 2.02 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 13 | 34 | 14 |
| 2.03 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 33 | 33 | 14 |
| 2.04 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 35 | 35 | 14 |
| 2.05 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 24 | 37 | 14 |
| 2.06 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 11 | 11 | 10 |
| 2.07 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2.08 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2.09 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2.10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2.11 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2.12 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2.13 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2.14 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2.15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2.16 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2.17 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2.18 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2.19 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2.20 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2.21 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2.22 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2.23 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2.24 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2.25 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2.26 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2.27 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2.28 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2.29 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2.30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2.31 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2.32 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2.33 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2.34 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2.35 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2.36 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2.37 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2.38 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2.39 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2.40 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2.41 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2.42 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2.43 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2.44 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2.45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2.46 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2.47 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2.48 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2.49 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2.50 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| SUBTOTAL | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 16 | 171 | 229 |

~~TOP SECRET~~

TABLE A-3

~~TOP SECRET C~~

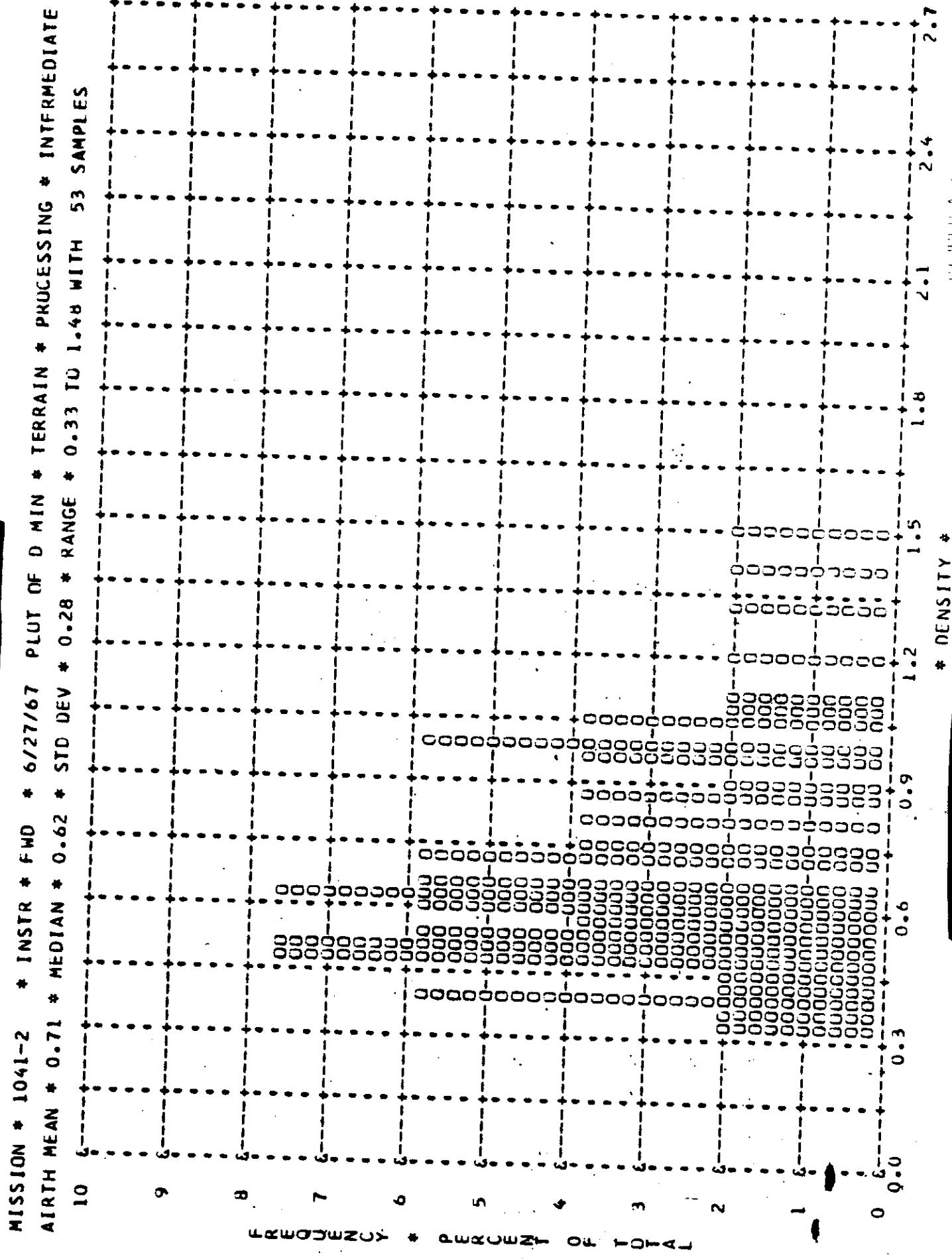
MISSION * 1041-2 * INSTRUMENT * FWD 6/27/67 DENSITY FREQ UISTR

| DENSITY VALUE | PRIMARY | | | INTERMEDIATE | | | FULL | | | ALL LEVELS | | |
|------------------|---------|-----|-----|--------------|-----|-----|------|-----|-----|------------|-----|-----|
| | MIN | MAX | LIM | MIN | MAX | LIM | MIN | MAX | LIM | MIN | MAX | LIM |
| 2.51 | 0 | 0. | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2.52 | 00 | 0 | 00 | 00 | 0 | 00 | 00 | 0 | 00 | 00 | 0 | 0 |
| 2.53 | 00 | 0 | 00 | 00 | 0 | 00 | 00 | 0 | 00 | 00 | 0 | 0 |
| 2.54 | 00 | 0 | 00 | 00 | 0 | 00 | 00 | 0 | 00 | 00 | 0 | 0 |
| 2.55 | 00 | 0 | 00 | 00 | 0 | 00 | 00 | 0 | 00 | 00 | 0 | 0 |
| 2.56 | 00 | 0 | 00 | 00 | 0 | 00 | 00 | 0 | 00 | 00 | 0 | 0 |
| 2.57 | 00 | 0 | 00 | 00 | 0 | 00 | 00 | 0 | 00 | 00 | 0 | 0 |
| 2.58 | 00 | 0 | 00 | 00 | 0 | 00 | 00 | 0 | 00 | 00 | 0 | 0 |
| 2.59 | 00 | 0 | 00 | 00 | 0 | 00 | 00 | 0 | 00 | 00 | 0 | 0 |
| 2.60 | 00 | 0 | 00 | 00 | 0 | 00 | 00 | 0 | 00 | 00 | 0 | 0 |
| 2.61 | 00 | 0 | 00 | 00 | 0 | 00 | 00 | 0 | 00 | 00 | 0 | 0 |
| 2.62 | 00 | 0 | 00 | 00 | 0 | 00 | 00 | 0 | 00 | 00 | 0 | 0 |
| 2.63 | 00 | 0 | 00 | 00 | 0 | 00 | 00 | 0 | 00 | 00 | 0 | 0 |
| 2.64 | 00 | 0 | 00 | 00 | 0 | 00 | 00 | 0 | 00 | 00 | 0 | 0 |
| 2.65 | 00 | 0 | 00 | 00 | 0 | 00 | 00 | 0 | 00 | 00 | 0 | 0 |
| 2.66 | 00 | 0 | 00 | 00 | 0 | 00 | 00 | 0 | 00 | 00 | 0 | 0 |
| 2.67 | 00 | 0 | 00 | 00 | 0 | 00 | 00 | 0 | 00 | 00 | 0 | 0 |
| 2.68 | 00 | 0 | 00 | 00 | 0 | 00 | 00 | 0 | 00 | 00 | 0 | 0 |
| 2.69 | 00 | 0 | 00 | 00 | 0 | 00 | 00 | 0 | 00 | 00 | 0 | 0 |
| 2.70 | 00 | 0 | 00 | 00 | 0 | 00 | 00 | 0 | 00 | 00 | 0 | 0 |
| SUBTOTAL | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| TOTAL | 0 | 0 | 0 | 53 | 53 | 84 | 177 | 177 | 192 | 230 | 230 | 275 |

MISSION 1041-2 INSTR - FWD 6/27/67 PROCESSING AND EXPOSURE ANALYSIS

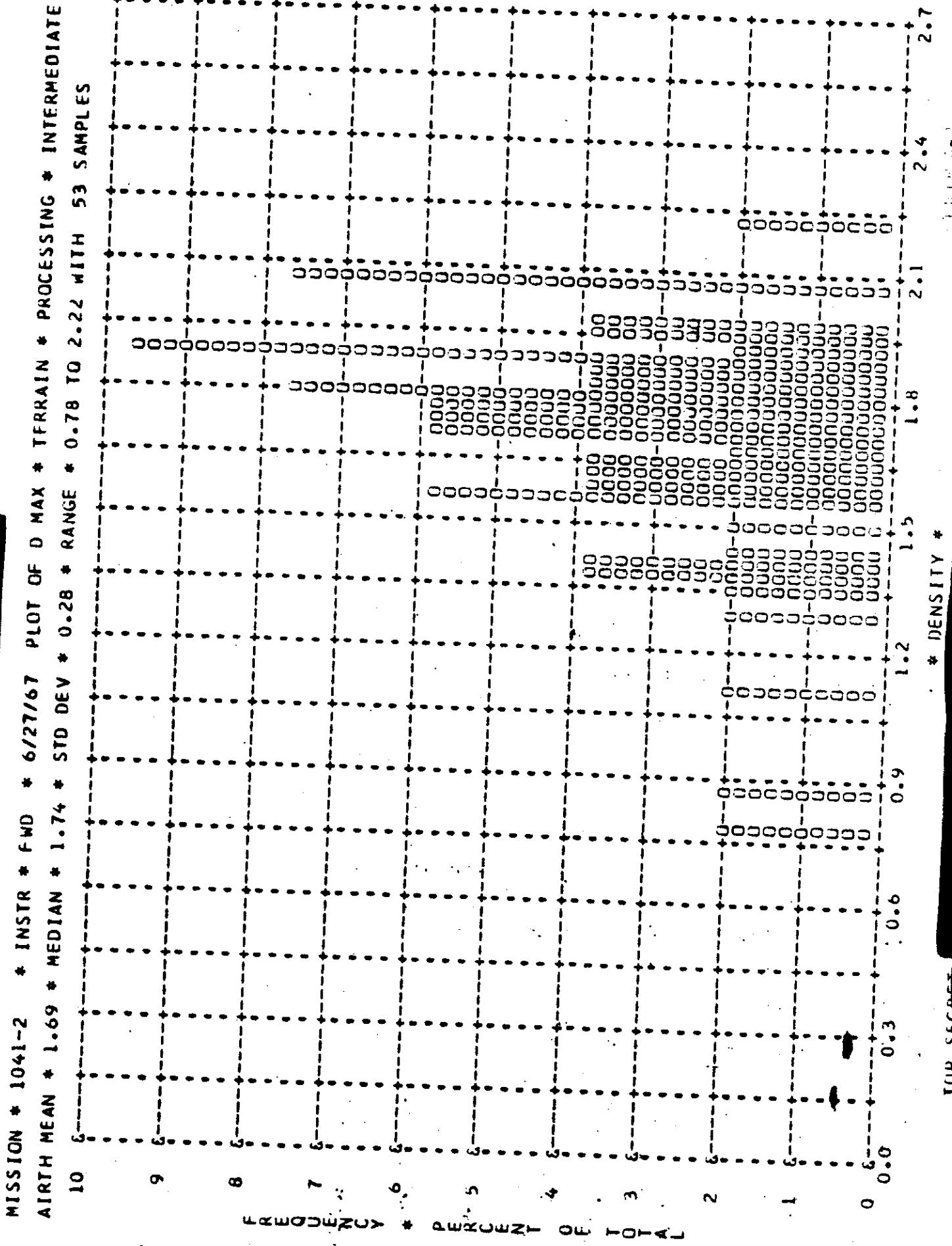
| PROCESS LEVEL | SAMPLE SIZE | UNDER EXPOSED | | UNDER PROCESSED | | CORRECT EXP&PRGC | OVER PROCESSED | OVER EXPOSED | |
|------------------|----------------|------------------|-----------|--------------------|-----------|---------------------|-------------------|-----------------|--------|
| | | EXPOSED | PROCESSED | EXPOSED | PROCESSED | | | | |
| PRIMARY | 0 | 0 | PC | 0 | PC | 0 | PC | 0 | |
| INTERMEDIATE | 53 | 0 | PC | 9 | PC | 66 | PC | 27 | PC |
| FULL | 177 | 5 | PC | 0 | PC | 85 | PC | 21 | PC |
| ALL LEVELS | 230 | 4 | PC | 2 | PC | 80 | PC | 10 | PC |
| PROCESS LEVEL | BASE & FOG | UNDER EXPOSED | | UNDER PROCESSED | | CORRECT EXP&PROC | OVER PROCESSED | OVER EXPOSED | |
| PRIMARY | 0.01-0.09 | 0.01-0.13 | | 0.14-0.39 | | 0.40-0.90 | ----- | 0.91 | AND UP |
| INTERMED | 0.10-0.17 | 0.01-0.20 | | 0.21-0.39 | | 0.40-0.90 | 0.91-1.34 | 1.35 | AND UP |
| FULL | 0.18 AND UP | 0.01-0.39 | | ----- | | 0.40-0.90 | 0.91-1.69 | 1.70 | AND UP |

TABLE A-3



-TOP SECRET C

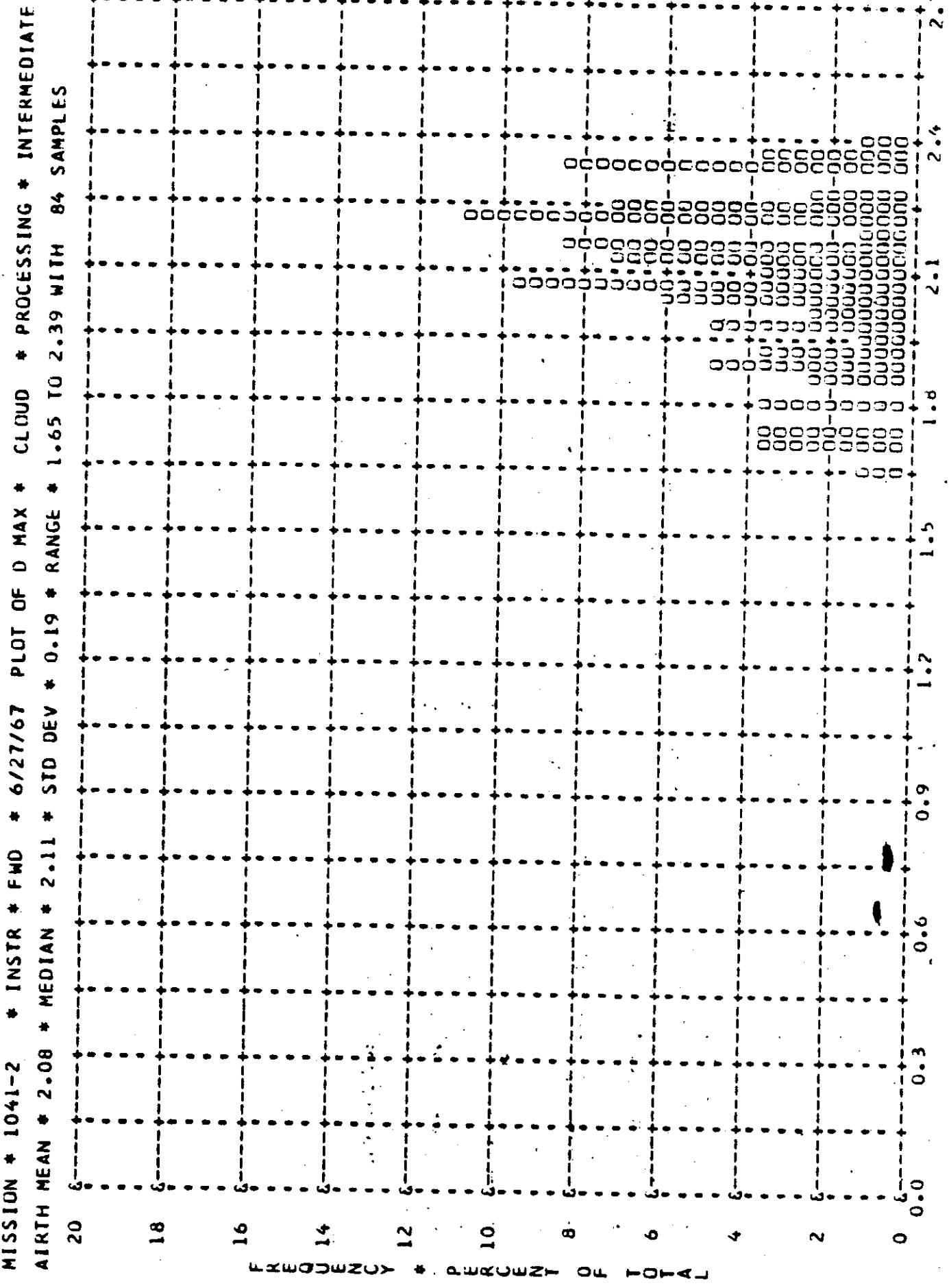
PJ ADULT A-100



TOP SECRET-C

TOP SECRET

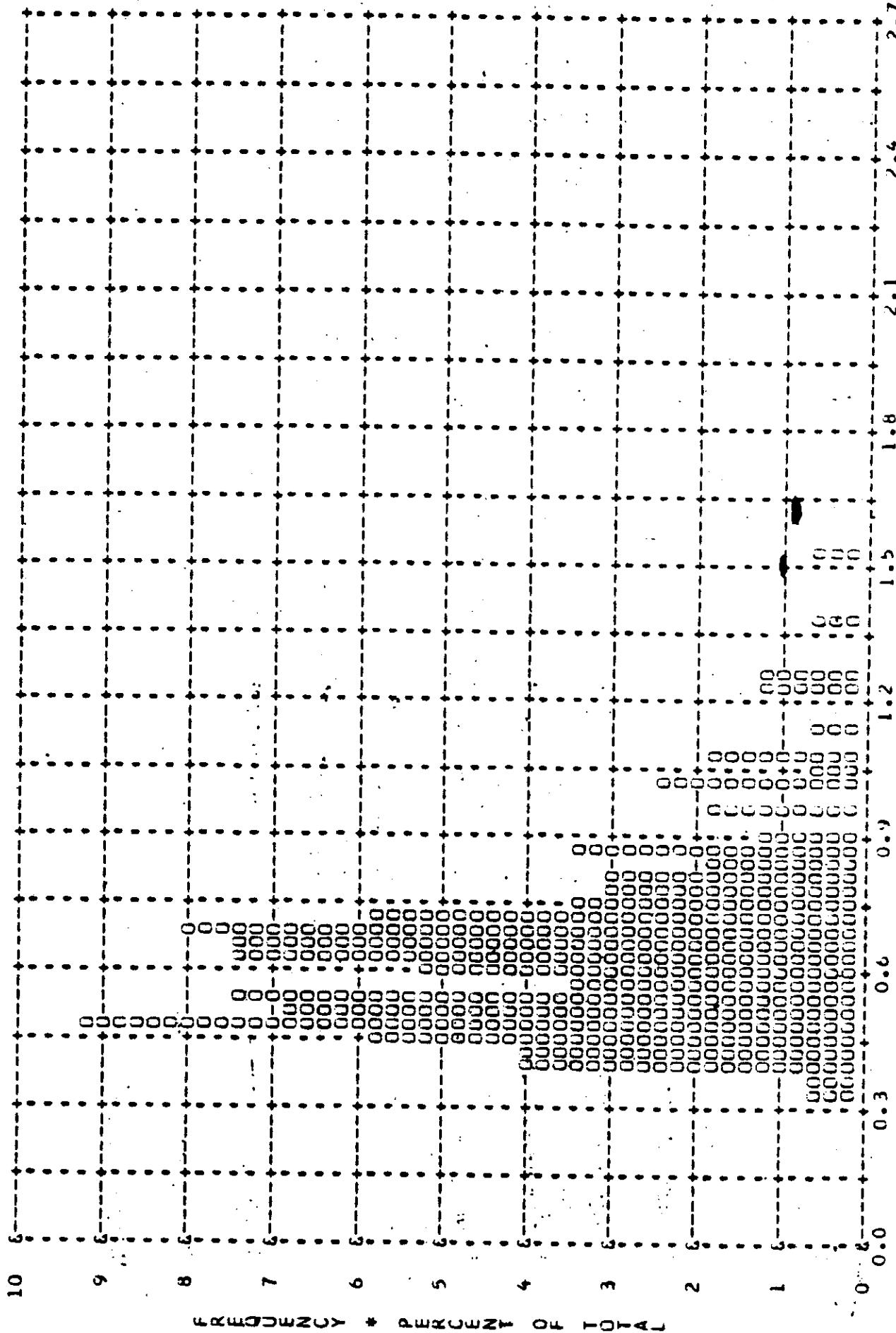
~~TOP SECRET C~~



~~TOP SECRET C~~

-TOP SECRET C

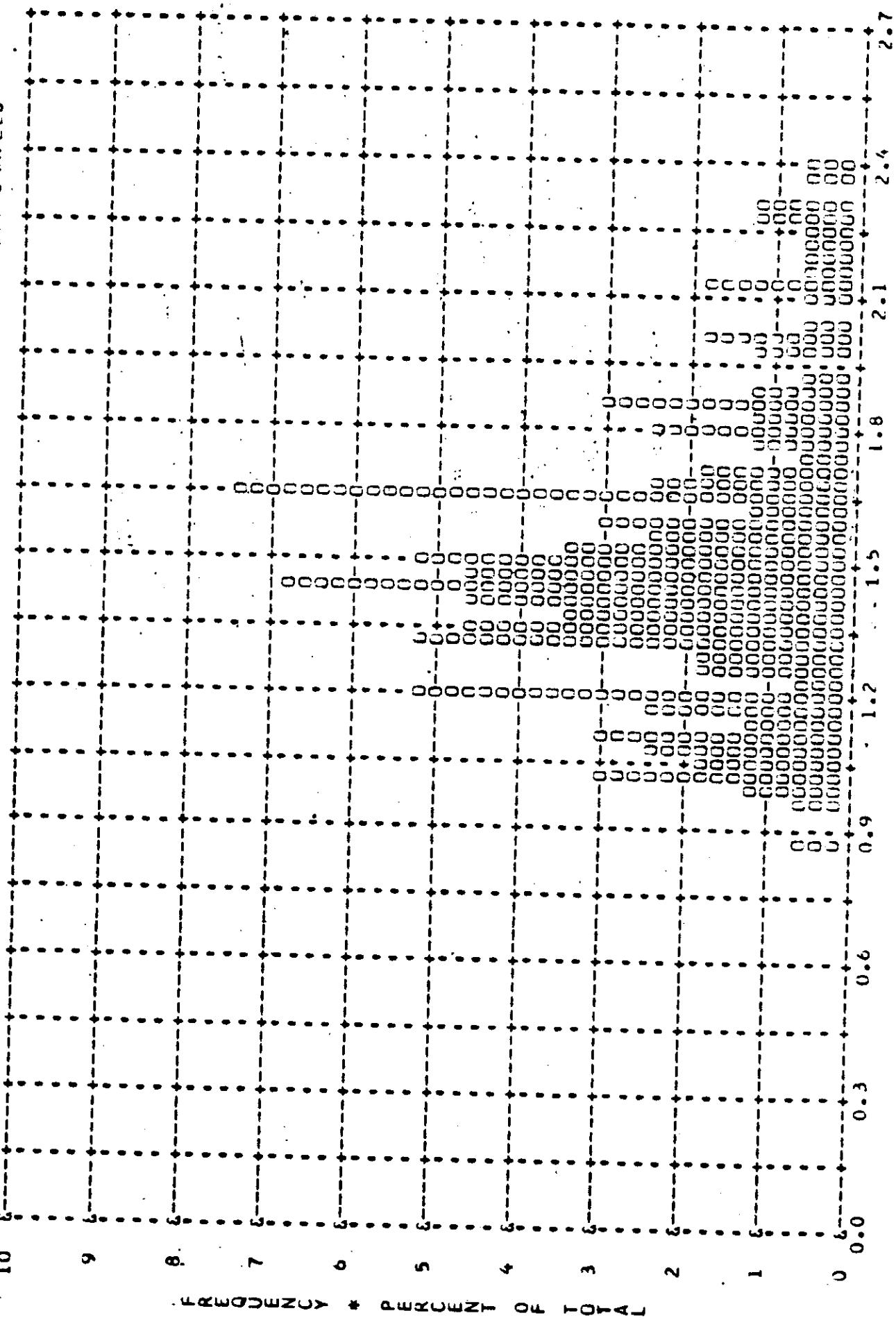
MISSION * 1041-2 * INSTR * FWD * 6/27/67 PLUT OF D MIN * TERRAIN * PROCESSING * FULL
AIRTH MEAN * 0.65 * MEDIAN * 0.62 * STD DEV * 0.21 * RANGE * 0.31 TO 1.51 WITH 177 SAMPLES



* DENSITY *

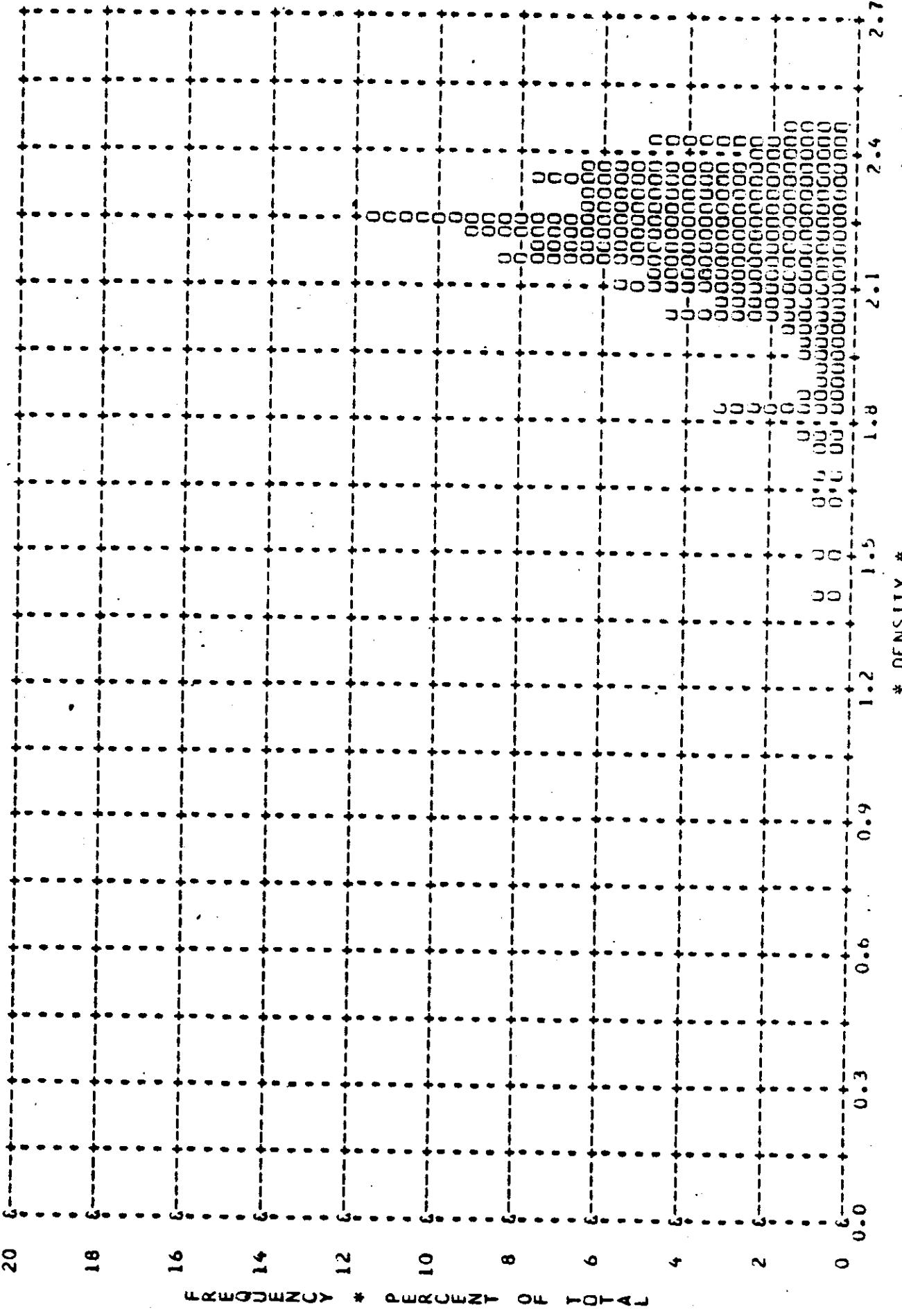
-TOP SECRET C

MISSION * 1041-2 * INSTR * FMD * 6/27/67 PLOT OF D MAX * TERRAIN * PROCESSING * FULL
AIRTH MEAN * 1.50 * MEDIAN * 1.45 * STD DEV * 0.33 * RANGE * 0.85 TO 2.38 WITH 177 SAMPLES



~~TOP SECRET~~

MISSION * 1041-2 * INSTR * FWD * 6/27/67 PLOT OF D MAX * CLOUD * PROCESSING * FULL
AIRTH MEAN * 2.18 * MEDIAN * 2.21 * STD DEV * 0.18 * RANGE * 1.40 TO 2.46 WITH 192 SAMPLES



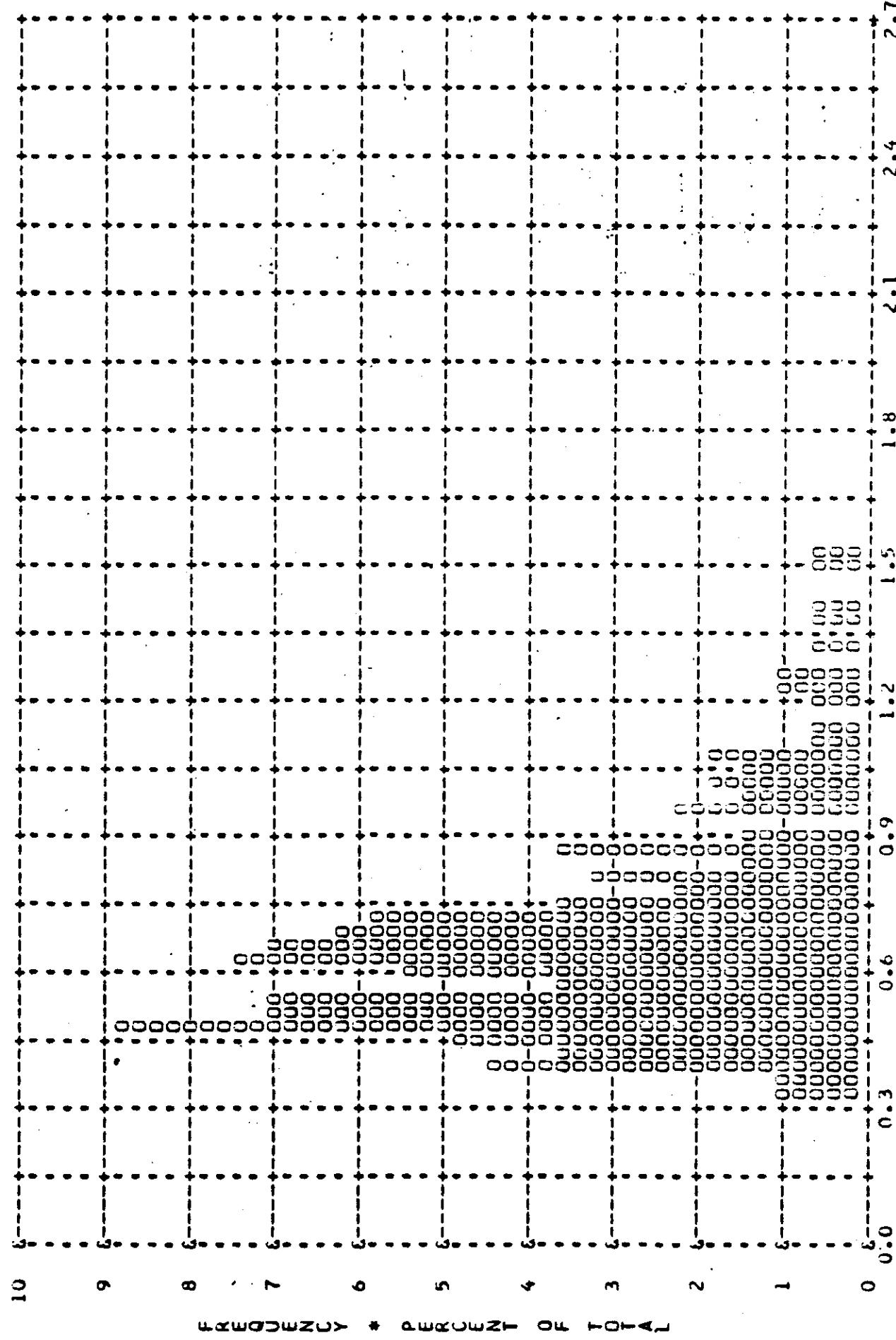
~~TOP SECRET~~

* DENSITY *

TOP SECRET

-TOP SECRET C

MISSION * 1041-2 * INSTR * FWD * 6/27/67 PLOT OF D MIN * TERRAIN * PROCESSING * ALL LEVELS
AIRTH MEAN * 0.66 * MEDIAN * 0.62 * STD DEV * 0.23 * RANGE * 0.31 TO 1.51 WITH 230 SAMPLES



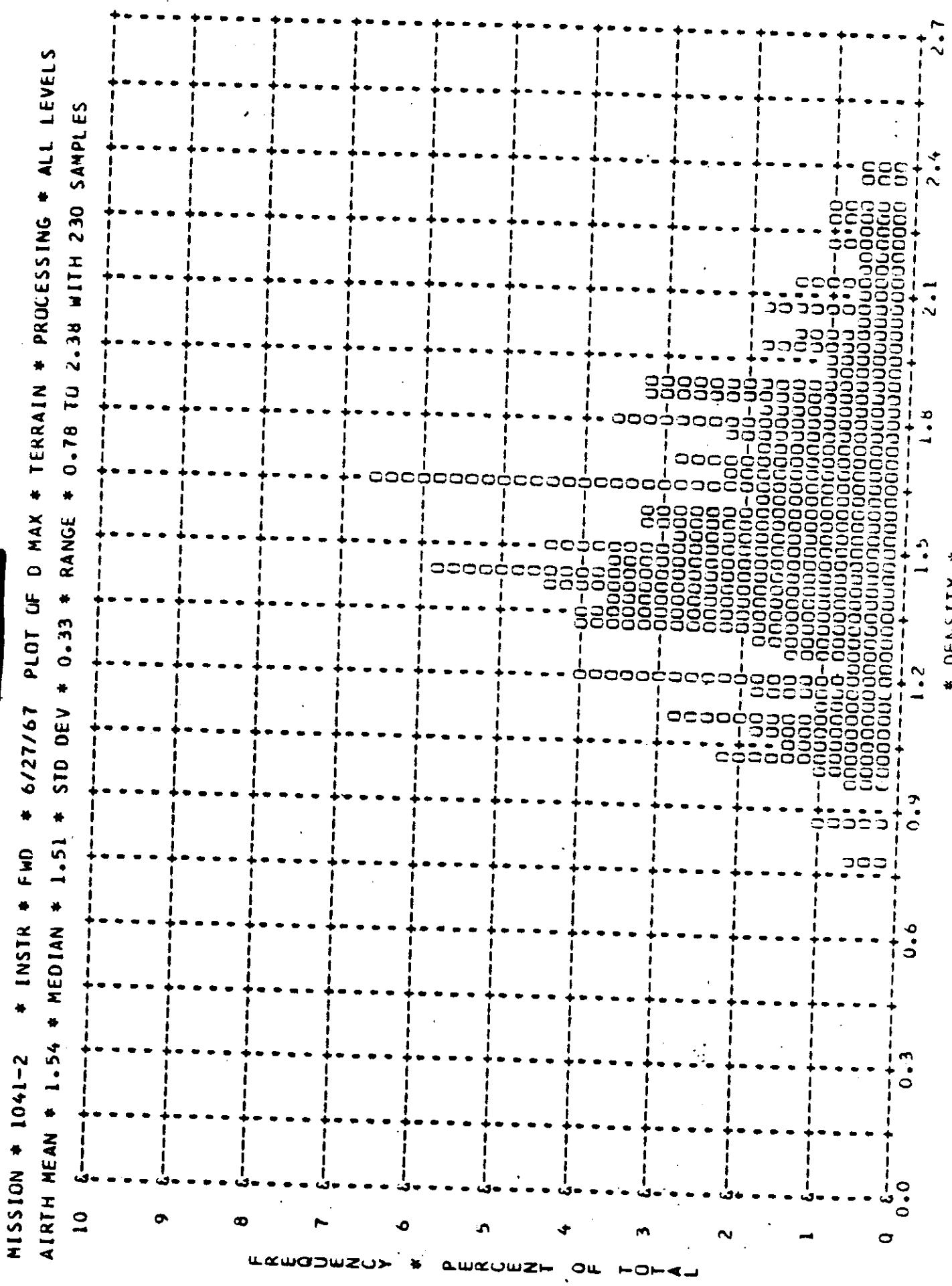
* DENSITY *

-TOP SECRET C

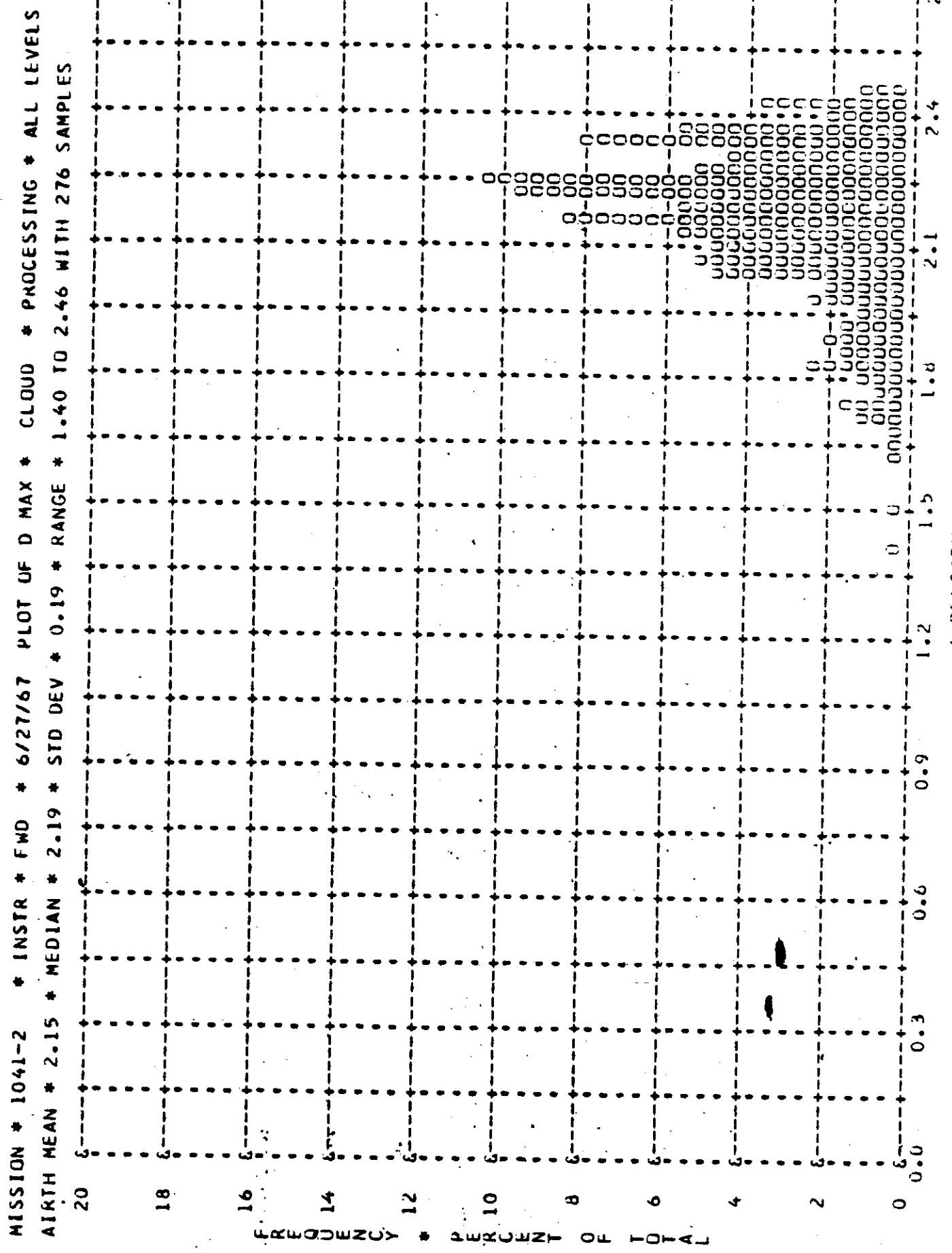
2.7

2.4
2.1
1.8
1.5
1.2
0.9
0.6
0.3
0.0

TOP SECRET C



-TOP SECRET C



-TOP SECRET C

* DENSITY *

-TOP SECRET C

~~TOP SECRET C~~

MISSION * 1041-2 * INSTRUMENT * AFT 6/27/67 DENSITY FREQ DISTR

| DENSITY VALUE | PRIMARY MIN MAX LIM | INTERMEDIATE MIN MAX LIM | FULL MIN MAX LIM | ALL LEVELS MIN MAX LIM |
|------------------|------------------------|-----------------------------|---------------------|---------------------------|
| 0.01 | 0 | 0 | 0 | 0 |
| 0.02 | 000 | 000 | 000 | 000 |
| 0.03 | 000 | 000 | 000 | 000 |
| 0.04 | 000 | 000 | 000 | 000 |
| 0.05 | 000 | 000 | 000 | 000 |
| 0.06 | 000 | 000 | 000 | 000 |
| 0.07 | 000 | 000 | 000 | 000 |
| 0.08 | 000 | 000 | 000 | 000 |
| 0.09 | 000 | 000 | 000 | 000 |
| 0.10 | 000 | 000 | 000 | 000 |
| 0.11 | 000 | 000 | 000 | 000 |
| 0.12 | 000 | 000 | 000 | 000 |
| 0.13 | 000 | 000 | 000 | 000 |
| 0.14 | 000 | 000 | 000 | 000 |
| 0.15 | 000 | 000 | 000 | 000 |
| 0.16 | 000 | 000 | 000 | 000 |
| 0.17 | 000 | 000 | 000 | 000 |
| 0.18 | 000 | 000 | 000 | 000 |
| 0.19 | 000 | 000 | 000 | 000 |
| 0.20 | 000 | 000 | 000 | 000 |
| 0.21 | 000 | 000 | 000 | 000 |
| 0.22 | 000 | 000 | 000 | 000 |
| 0.23 | 000 | 000 | 000 | 000 |
| 0.24 | 000 | 000 | 000 | 000 |
| 0.25 | 000 | 000 | 000 | 000 |
| 0.26 | 000 | 000 | 000 | 000 |
| 0.27 | 000 | 000 | 000 | 000 |
| 0.28 | 000 | 000 | 000 | 000 |
| 0.29 | 000 | 000 | 000 | 000 |
| 0.30 | 000 | 000 | 000 | 000 |
| 0.31 | 000 | 000 | 000 | 000 |
| 0.32 | 000 | 000 | 000 | 000 |
| 0.33 | 000 | 000 | 000 | 000 |
| 0.34 | 000 | 000 | 000 | 000 |
| 0.35 | 000 | 000 | 000 | 000 |
| 0.36 | 000 | 000 | 000 | 000 |
| 0.37 | 000 | 000 | 000 | 000 |
| 0.38 | 000 | 000 | 000 | 000 |
| 0.39 | 000 | 000 | 000 | 000 |
| 0.40 | 000 | 000 | 000 | 000 |
| 0.41 | 000 | 000 | 000 | 000 |
| 0.42 | 000 | 000 | 000 | 000 |
| 0.43 | 000 | 000 | 000 | 000 |
| 0.44 | 000 | 000 | 000 | 000 |
| 0.45 | 000 | 000 | 000 | 000 |
| 0.46 | 000 | 000 | 000 | 000 |
| 0.47 | 000 | 000 | 000 | 000 |
| 0.48 | 000 | 000 | 000 | 000 |
| 0.49 | 000 | 000 | 000 | 000 |
| 0.50 | 000 | 000 | 000 | 000 |
| SUBTOTAL | 0 | 0 | 25 | 64 |
| | | | | 89 |

~~TOP SECRET C~~

TABLE A-4

~~TOP SECRET C~~

MISSION * 1041-2 * INSTRUMENT * AFT 6/27/67 DENSITY FREQ DISTR

| DENSITY VALUE | PRIMARY MIN MAX LIM | INTERMEDIATE MIN MAX LIM | FULL MIN MAX LIM | ALL LEVELS MIN MAX LIM |
|------------------|------------------------|-----------------------------|---------------------|---------------------------|
| 0.51 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.52 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.53 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.54 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.55 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.56 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.57 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.58 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.59 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.60 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.61 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.62 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.63 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.64 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.65 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.66 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.67 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.68 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.69 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.70 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.71 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.72 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.73 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.74 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.75 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.76 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.77 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.78 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.79 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.80 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.81 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.82 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.83 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.84 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.85 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.86 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.87 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.88 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.89 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.90 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.91 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.92 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.93 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.94 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.95 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.96 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.97 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.98 | 0 0 | 0 0 | 0 0 | 0 0 |
| 0.99 | 0 0 | 0 0 | 0 0 | 0 0 |
| 1.00 | 0 0 | 0 0 | 0 0 | 0 0 |
| SUBTOTAL | 0 0 | 0 0 | 46 100 | 146 7 |

~~TOP SECRET C~~

TABLE A-4

~~TOP SECRET C~~

| MISSION # 1041-2 * INSTRUMENT * AFT | 6/27/67 | DENSITY FREQ DISTR | | |
|-------------------------------------|---------------------|--------------------------|------------------|------------------------|
| DENSITY VALUE | PRIMARY MIN MAX LIM | INTERMEDIATE MIN MAX LIM | FULL MIN MAX LIM | ALL LEVELS MIN MAX LIM |
| 1.01 | 0 0 0 | 0 0 0 | 0 0 0 | 0 0 0 |
| 1.02 | 0 0 0 | 0 0 0 | 0 0 0 | 0 0 0 |
| 1.03 | 0 0 0 | 0 0 0 | 0 0 0 | 0 0 0 |
| 1.04 | 0 0 0 | 0 0 0 | 0 0 0 | 0 0 0 |
| 1.05 | 0 0 0 | 0 0 0 | 0 0 0 | 0 0 0 |
| 1.06 | 0 0 0 | 0 0 0 | 0 0 0 | 0 0 0 |
| 1.07 | 0 0 0 | 0 0 0 | 0 0 0 | 0 0 0 |
| 1.08 | 0 0 0 | 0 0 0 | 0 0 0 | 0 0 0 |
| 1.09 | 0 0 0 | 0 0 0 | 0 0 0 | 0 0 0 |
| 1.10 | 0 0 0 | 0 0 0 | 0 0 0 | 0 0 0 |
| 1.11 | 0 0 0 | 0 0 0 | 0 0 0 | 0 0 0 |
| 1.12 | 0 0 0 | 0 0 0 | 0 0 0 | 0 0 0 |
| 1.13 | 0 0 0 | 0 0 0 | 0 0 0 | 0 0 0 |
| 1.14 | 0 0 0 | 0 0 0 | 0 0 0 | 0 0 0 |
| 1.15 | 0 0 0 | 0 0 0 | 0 0 0 | 0 0 0 |
| 1.16 | 0 0 0 | 0 0 0 | 0 0 0 | 0 0 0 |
| 1.17 | 0 0 0 | 0 0 0 | 0 0 0 | 0 0 0 |
| 1.18 | 0 0 0 | 0 0 0 | 0 0 0 | 0 0 0 |
| 1.19 | 0 0 0 | 0 0 0 | 0 0 0 | 0 0 0 |
| 1.20 | 0 0 0 | 0 0 0 | 0 0 0 | 0 0 0 |
| 1.21 | 0 0 0 | 0 0 0 | 0 0 0 | 0 0 0 |
| 1.22 | 0 0 0 | 0 0 0 | 0 0 0 | 0 0 0 |
| 1.23 | 0 0 0 | 0 0 0 | 0 0 0 | 0 0 0 |
| 1.24 | 0 0 0 | 0 0 0 | 0 0 0 | 0 0 0 |
| 1.25 | 0 0 0 | 0 0 0 | 0 0 0 | 0 0 0 |
| 1.26 | 0 0 0 | 0 0 0 | 0 0 0 | 0 0 0 |
| 1.27 | 0 0 0 | 0 0 0 | 0 0 0 | 0 0 0 |
| 1.28 | 0 0 0 | 0 0 0 | 0 0 0 | 0 0 0 |
| 1.29 | 0 0 0 | 0 0 0 | 0 0 0 | 0 0 0 |
| 1.30 | 0 0 0 | 0 0 0 | 0 0 0 | 0 0 0 |
| 1.31 | 0 0 0 | 0 0 0 | 0 0 0 | 0 0 0 |
| 1.32 | 0 0 0 | 0 0 0 | 0 0 0 | 0 0 0 |
| 1.33 | 0 0 0 | 0 0 0 | 0 0 0 | 0 0 0 |
| 1.34 | 0 0 0 | 0 0 0 | 0 0 0 | 0 0 0 |
| 1.35 | 0 0 0 | 0 0 0 | 0 0 0 | 0 0 0 |
| 1.36 | 0 0 0 | 0 0 0 | 0 0 0 | 0 0 0 |
| 1.37 | 0 0 0 | 0 0 0 | 0 0 0 | 0 0 0 |
| 1.38 | 0 0 0 | 0 0 0 | 0 0 0 | 0 0 0 |
| 1.39 | 0 0 0 | 0 0 0 | 0 0 0 | 0 0 0 |
| 1.40 | 0 0 0 | 0 0 0 | 0 0 0 | 0 0 0 |
| 1.41 | 0 0 0 | 0 0 0 | 0 0 0 | 0 0 0 |
| 1.42 | 0 0 0 | 0 0 0 | 0 0 0 | 0 0 0 |
| 1.43 | 0 0 0 | 0 0 0 | 0 0 0 | 0 0 0 |
| 1.44 | 0 0 0 | 0 0 0 | 0 0 0 | 0 0 0 |
| 1.45 | 0 0 0 | 0 0 0 | 0 0 0 | 0 0 0 |
| 1.46 | 0 0 0 | 0 0 0 | 0 0 0 | 0 0 0 |
| 1.47 | 0 0 0 | 0 0 0 | 0 0 0 | 0 0 0 |
| 1.48 | 0 0 0 | 0 0 0 | 0 0 0 | 0 0 0 |
| 1.49 | 0 0 0 | 0 0 0 | 0 0 0 | 0 0 0 |
| 1.50 | 0 0 0 | 0 0 0 | 0 0 0 | 0 0 0 |
| SUBTOTAL | 0 0 0 | 0 0 0 | 21 0 0 | 84 0 0 |
| | | | | 105 |

~~TOP SECRET C~~

CABLE A-4

~~TOP SECRET C~~

~~TOP SECRET C~~

TABLE A-4

~~TOP SECRET C~~

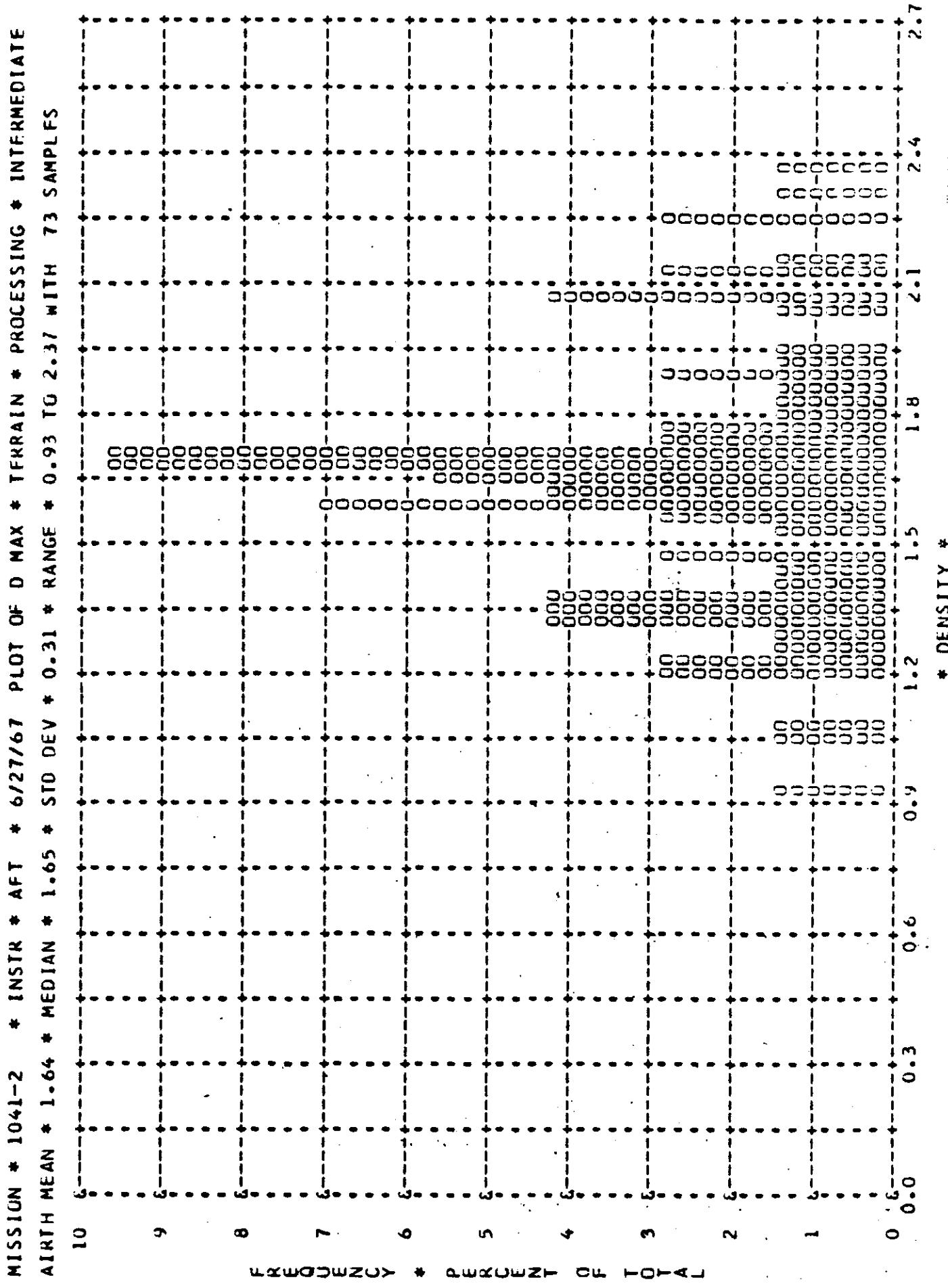
MISSION * 1041-2 * INSTRUMENT * AFT 6/27/67 DENSITY FREQ DISTR

| DENSITY VALUE | PRIMARY MIN MAX LIM | INTERMEDIATE MIN MAX LIM | FULL MIN MAX LIM | ALL LEVELS MIN MAX LIM |
|---------------|------------------------|-----------------------------|---------------------|---------------------------|
| 2.01 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.02 | 0 0 | 0 0 | 1 0 | 1 1 |
| 2.03 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.04 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.05 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.06 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.07 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.08 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.09 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.10 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.11 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.12 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.13 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.14 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.15 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.16 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.17 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.18 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.19 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.20 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.21 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.22 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.23 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.24 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.25 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.26 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.27 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.28 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.29 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.30 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.31 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.32 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.33 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.34 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.35 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.36 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.37 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.38 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.39 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.40 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.41 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.42 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.43 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.44 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.45 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.46 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.47 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.48 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.49 | 0 0 | 0 0 | 0 0 | 0 0 |
| 2.50 | 0 0 | 0 0 | 0 0 | 0 0 |
| SUBTOTAL | 0 0 | 0 0 | 11 73 | 0 t3 158 |

~~TOP SECRET C~~

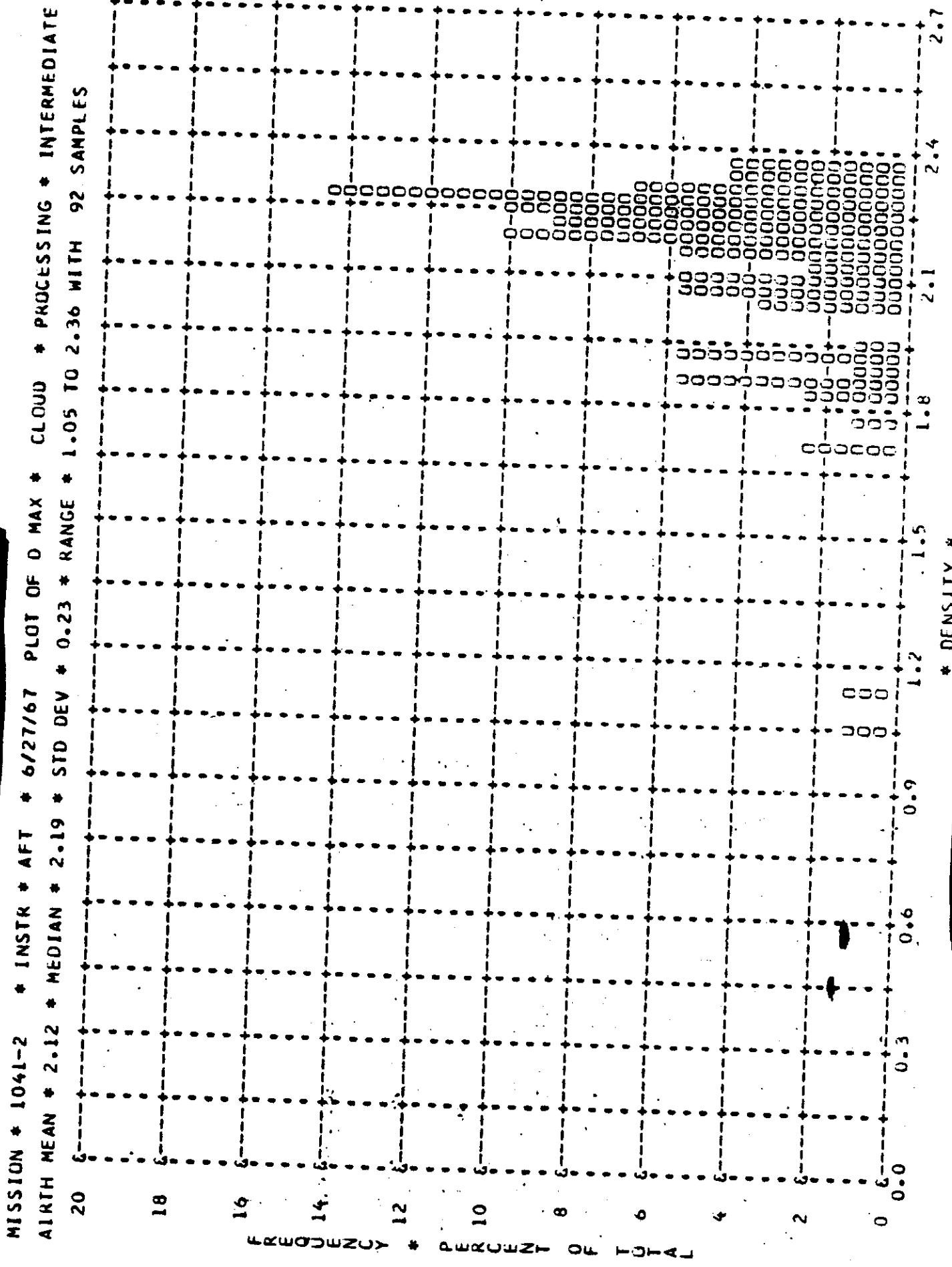
TABLE A-4

-TOP SECRET C



TOP SECRET C

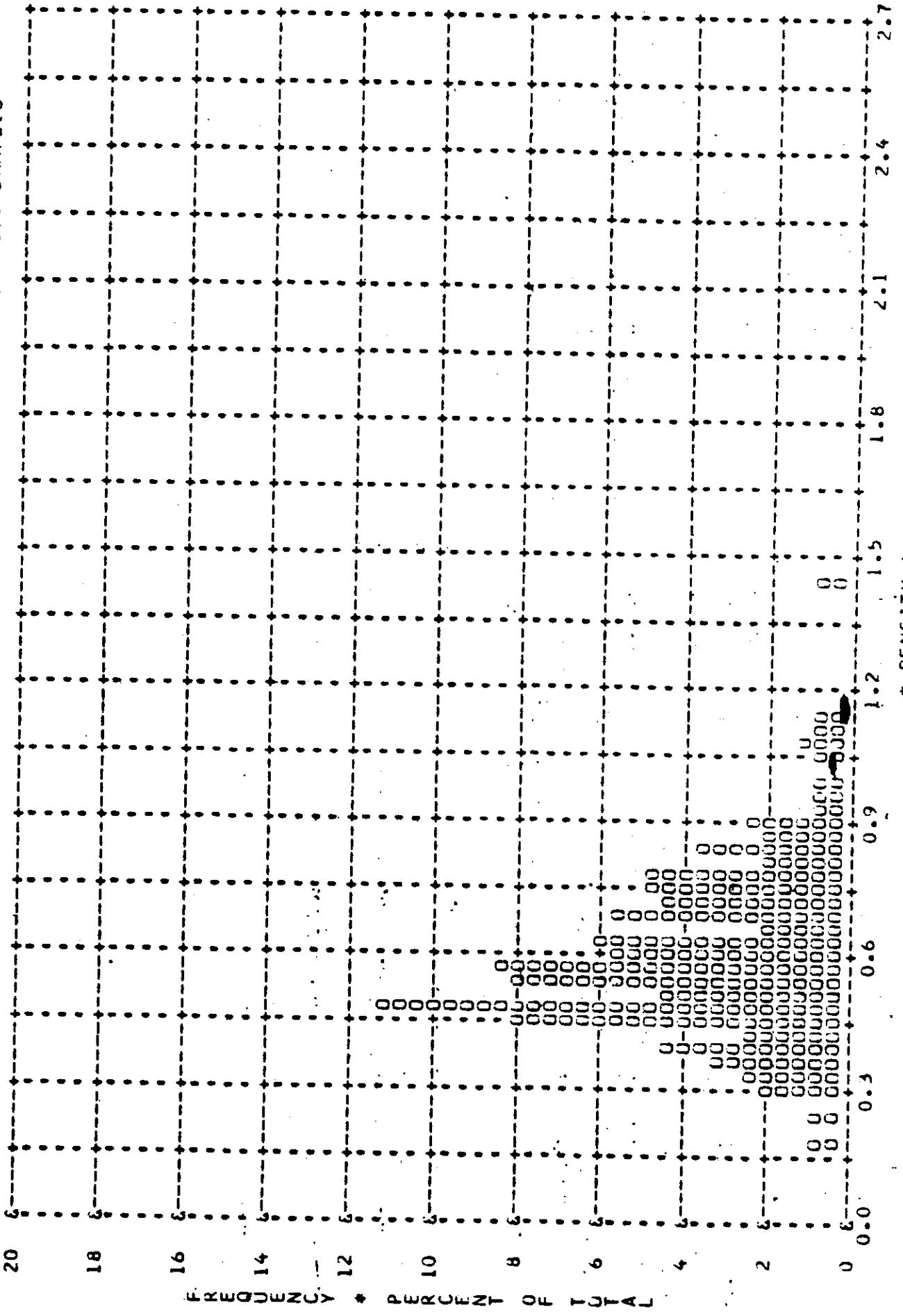
-TOP SECRET-C



1041-2

-TOP-SECRET C

MISSION * 1041-2 * INSTR * AFT * 6/27/67 PLOT OF D MIN * TERRAIN * PROCESSING * FULL
AIRTH MEAN * 0.60 * MEDIAN * 0.57 * STD DEV * 0.19 * RANGE * 0.17 TO 1.42 WITH 170 SAMPLES

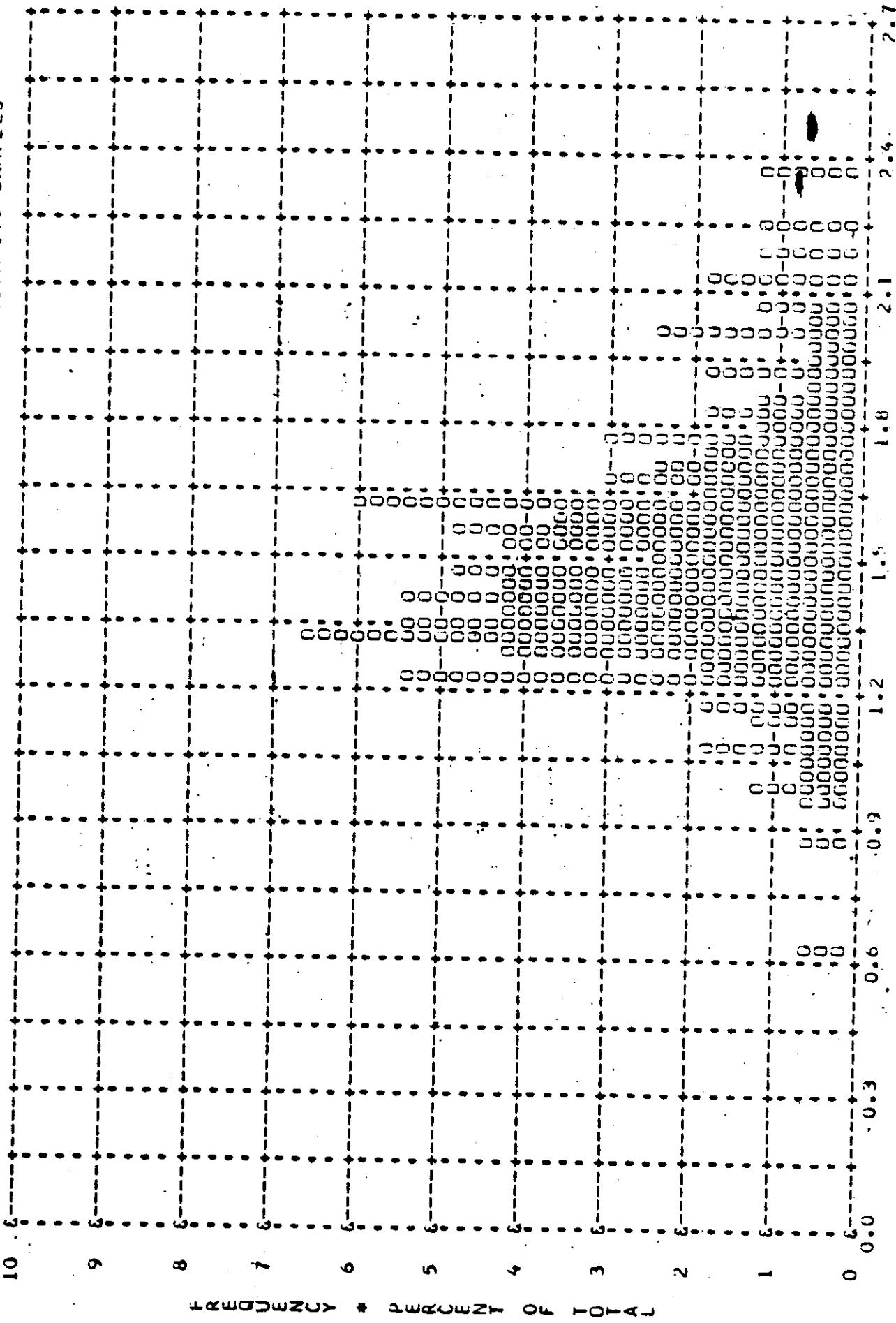


-TOP-SECRET C

* DENSITY *

-TOP-SECRET C

MISSION * 1041-2 * INSTR * AFT * 6/27/67 PLOT OF D MAX * TERRAIN * PROCESSING * FULL
AIRT MEAN * 1.52 * MEDIAN * 1.47 * STD DEV * 0.30 * RANGE * 0.62 TO 2.37 WITH 170 SAMPLES



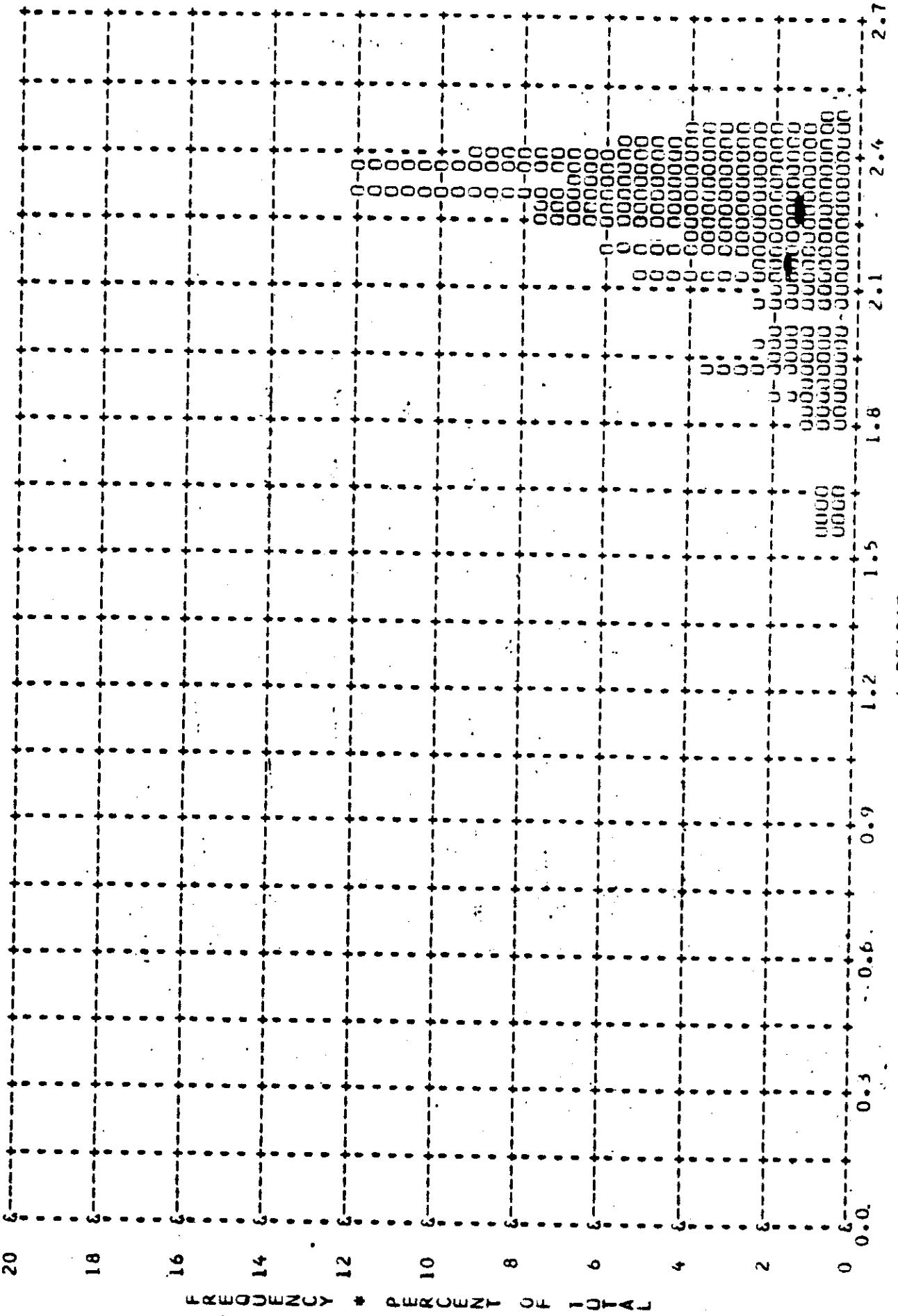
TOP SECRET C

* DENSITY *

TOP SECRET C

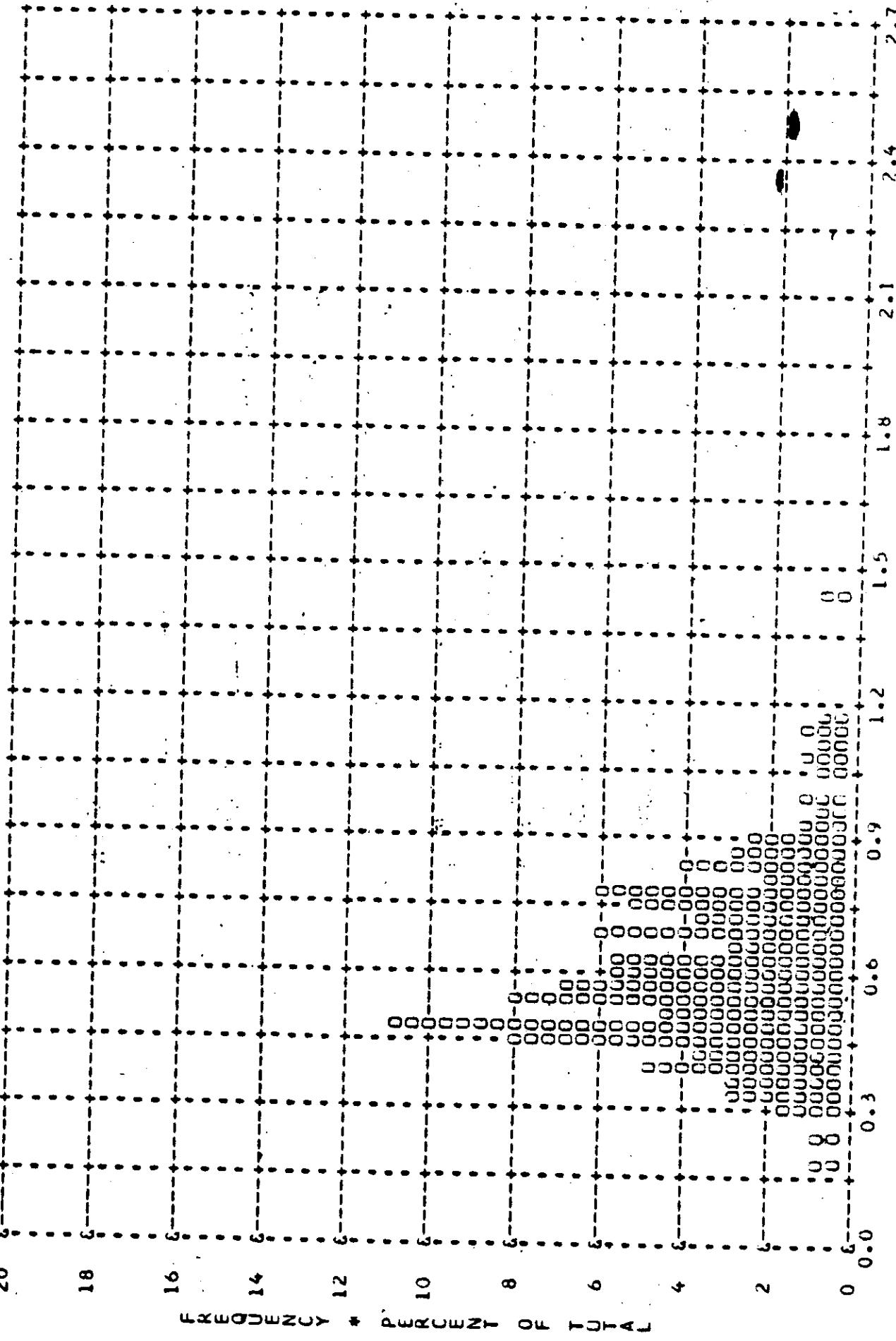
~~TOP SECRET C~~

MISSION * 1041-2 * INSTR * AFT * 6/27/67 PLOT OF D MAX * CLOUD * PROCESSING * FULL
AIRTH MEAN * 2.23 * MEDIAN * 2.28 * STD DEV * 0.19 * RANGE * 1.56 TO 2.47 WITH 186 SAMPLES



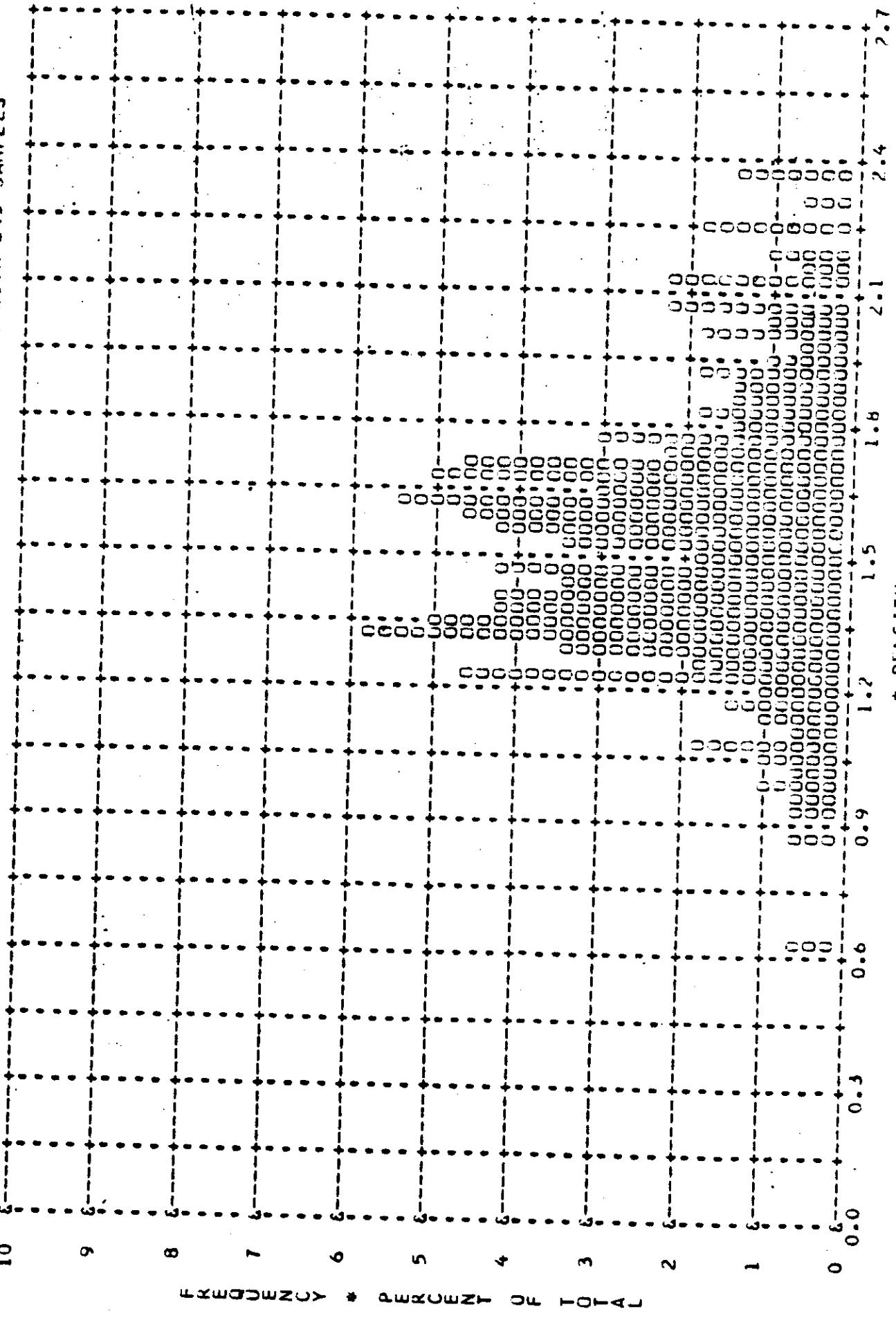
~~TOP SECRET~~ C

MISSION * 1041-2 * INSTR * AFT * 6/27/67 PLOT OF D MIN * TERRAIN * PROCESSING * ALL LEVELS
AIRTH MEAN * 0.60 * MEDIAN * 0.57 * STD DEV * 0.19 * RANGE * 0.17 TO 1.42 WITH 243 SAMPLES

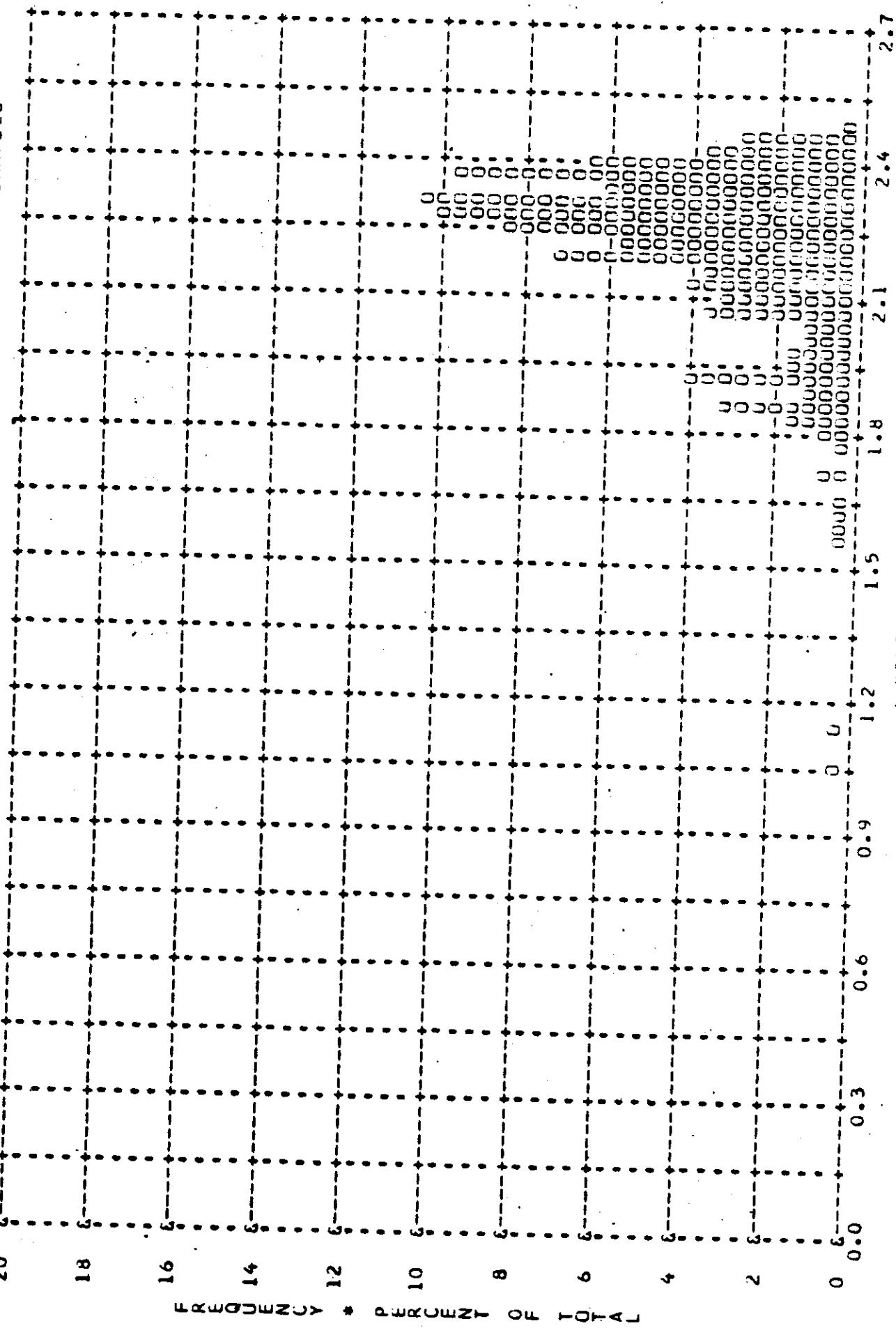


PAGE - 4

MISSION * 1041-2 * INSTR * AFT * 6/27/67 PLOT OF D MAX * TERRAIN * PROCESSING * ALL LEVELS
AIRTH MEAN * 1.55 * MEDIAN * 1.54 * STD DEV * 0.31 * RANGE * 0.62 TO 2.37 WITH 243 SAMPLES



MISSION * 1041-2 * INSTR * AFT * 6/27/67 PLOT OF D MAX * CLOUD * PROCESSING * ALL LEVELS
AIRTH MEAN * 2.19 * MEDIAN * 2.25 * STD DEV * 0.21 * RANGE * 1.05 TU 2.47 WITH 278 SAMPLES

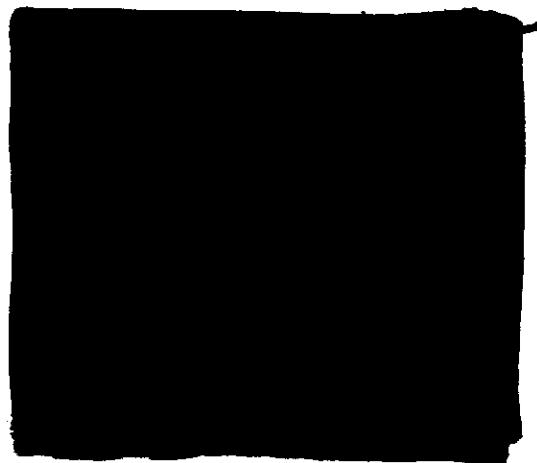


~~TOP SECRET C~~

Distribution:

Copy No.

To



~~TOP SECRET C~~