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TO:

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From:

SUBJECT: MISSION 1036-1 and 1036-2 FINAL REPORT

Enclosed is the Final Performance Evaluation Report for  
Mission 1036-1 and 1036-2.

Manager  
Advanced Projects

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CORONA J

PERFORMANCE EVALUATION REPORT

MISSION 1036-1 and 1036-2

FTV 1631, J-32

30 JUNE 1967

Approved [REDACTED]

[REDACTED] Manager  
Advanced Projects

Approved [REDACTED]

[REDACTED] Mgr.  
Program [REDACTED]

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**FOREWORD**

This report details the performance of the payload system during the operational phase of the Program [REDACTED] Flight Test Vehicle 1631.

Lockheed Missiles and Space Company has the responsibility for evaluating payload performance under the Level of Effort and "J" System contracts.

This document is the final payload test and performance evaluation report for Missions 1036-1 and 1036-2 which was launched on 9 August 1966.

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## INTRODUCTION

This report presents the final performance evaluation of Missions 1036-1 and 1036-2 of the Corona Program. The purpose of this report is to define the performance characteristics of the J-32 payload system and to identify the source of in-flight anomalies.

The performance evaluation was jointly conducted by representatives of Lockheed Missiles and Space Company (LMSC) and ITEK at the facilities of NPIC and AFSPPF. The off-line evaluation using Corona engineering photography acquired over the United States was performed at the individual contractors plants.

The quantitative data used for this report is obtained from government organizations. The diffuse density data, and MTF/AM resolution are produced by AFSPPF. The vehicle attitude error values, frame correlation times are made at NPIC who also supply the Processing Summary reports published by [REDACTED]

Computer programs developed by A/P are utilized to calculate and plot the frequency distribution of the various contributors to image smear to permit analysis and correlation of the conditions of photography to the information content and quality of the acquired pictures. Computer analysis of the exposure, processing and illumination data provides the necessary data to analyze the exposure criteria selected for the mission.

## SECTION 1

## SYSTEM PERFORMANCE

## A. MISSION OBJECTIVES

The payload section of Mission 1036, placed into orbit by Flight Test Vehicle #1631 and THORAD Booster #506, consisted of two panoramic cameras, two Stellar-Index cameras, two Mark 5A recovery capsules and a space structure to enclose the cameras and provide mounting surfaces for all equipment. Figure 1-1 presents an inboard profile of the J-32 payload system. This Corona "J" system is designed to acquire search and reconnaissance photography of selected areas of the earth from orbital altitudes. A six day -1 mission and a seven day -2 mission was planned.

## B. MISSION DESCRIPTION

The payload was launched from Vandenberg Air Force Base (VAFB) at 2046:03 Z (1346:03 PDT) on 9 August 1966. Ascent and injection were normal and the achieved orbit was within nominal tolerances. Tracking and command support was effected by the Air Force Satellite Control Facility consisting of tracking and command stations at [REDACTED]

[REDACTED] under central control of the Satellite Test Center at Sunnyvale, California. Mission 1036-1 consisted of a 7 day operation and was completed by air recovery on 16 August 1966. Mission 1036-2 was completed with an air recovery on 22 August 1966 following a 6 day photographic operation.

The comparison of the planned and actual orbit parameters is tabulated as follows:

## ORBITAL PARAMETERS

<u>Parameter</u>	<u>Predicted</u>	<u>Orbit 56 Actuals</u>
Period (Min.)	89.48	89.323
Perigee (N.M.)	105.1	102.399
Apogee (N.M.)	164.9	159.830
Inclination (Deg.)	100.2	100.114
Perigee Latitude (Deg. N.)	14.025	22.919
Eccentricity	0.008362	0.00804

## C. PANORAMIC CAMERAS

The Master instrument produced good image quality. The image quality was better on the -2 mission due to less atmospheric haze.

The Slave instrument operated satisfactorily and produced slightly better imagery than the Master.

## D. STELLAR-INDEX CAMERAS

The "A" S/I operated satisfactorily and most Stellar images appear as points rather than the usual odd shaped stars.

The "B" S/I operated normally.

The base plus fog density of the -1 and -2 Stellar film was unusually high at 0.54 density units.

## E. OTHER SUB-SYSTEMS

The clock, instrumentation, pressure make-up, command and thermal control subsystems performed satisfactorily.

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SCHEMATIC DRAWING PROVIDED - CONGMA J-32 SYSTEM

MISSION 1036

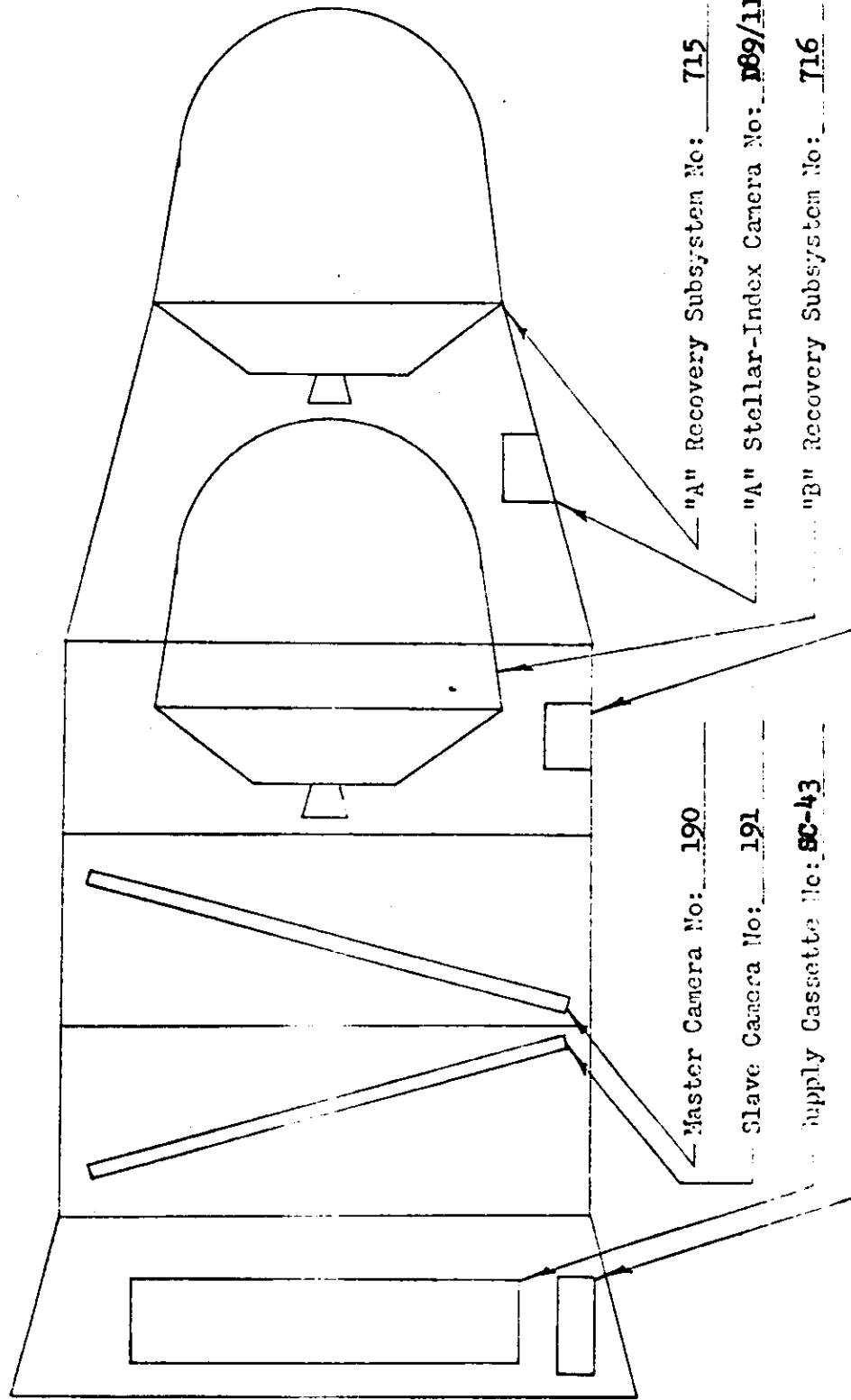


FIGURE 1-1

## SECTION 2

## PRE-FLIGHT SYSTEMS TESTS

## A. ENVIRONMENTAL TESTING

1. Test Objective

As a standard procedure, the J payload systems are subjected to thermal/altitude environmental testing which simulates orbital environment. One of the purposes of this test is to demonstrate the system susceptibility to corona discharge. Such discharge fogs the film thus degrading the operational photography.

2. Test Summary

The J-32 payload system was subjected to an environmental TASC Chamber test from January 7 through January 14, 1966.

Performance of the payload system was generally satisfactory except for excessive corona marking on the payload of the Master and Slave instruments. The input and output metering rollers were replaced and the system was returned to the test chamber on 9 February. Five orbits of dynamic instrument operations were conducted in the "A" mode only. There were 1200 cycles of payload exposed during the test. The corona markings met specifications.

The panoramic instruments operated satisfactorily. Instrument cycle periods varied from 2.8% fast to 2.5% slow. Cycle period data are tabulated in Table 2-1. The new DYMECT cycle period equipment was utilized for the first time and it compared closely ( $\pm 0.5\%$ ) with the Sanborn records. This equipment produces a continuous record of cycle period and V/h voltage. Analysis of the DYMECT data revealed that the panoramic cameras increased their rate by approximately 1% between the tenth and fortieth cycle.

The shutter in Stellar camera #106 failed to open during the first TASC run. The shutter was replaced and the S/I cameras operated satisfactorily during TASC test 2.

The clock accuracy was satisfactory. The clock/IRIG time correlation is shown in Table 2-2.

The pressure make-up system operated normally. Average gas consumption was 4.9 lbs/min.

The command system functioned properly for both bucket tests with no evidence of any malfunctions.

Cut-wrap and switchover to the "B" recovery sequence was normal.

#### B. RESOLUTION TEST

Resolution and theodolite tests were performed on 24 January 1966. Results of the thru-focus resolution tests of pan instruments 190 and 191 show the following characteristics:

##### Master Pan Instrument No. 190

Maximum high contrast resolution 168 lines/mm at +.001 focal position.

Maximum low contrast resolution 106 lines/mm at -.001 focal position.

##### Slave Instrument No. 191

Maximum high contrast resolution 172 lines/mm at 0.000 focal position.

Maximum low contrast resolution 112 lines/mm at 0.000 focal position.

The test data for both instruments is shown in Figures 2-1 and 2-2. Both instruments met the system requirements specification.

### C. LIGHT LEAK TEST

The J-32 system was tested for light leaks on 2 March and 4 March 1966. The reason for the second test was a light leak in a H.O. boot of both instruments. The second light leak test proved that the system was L/L acceptable.

### D. FLIGHT LOADING AND CERTIFICATION

J-32 system was shipped by trailer truck from A/P to VAFB, 1 August 1966, as the first Interim Phase III Factory to PAD delivery.

On 2 August, the system was available in the shipping trailer for inspection at the L Building. All access and camera doors were removed and the Master and Slave camera film paths examined. It was noted that the Master camera film was normally taut from supply to take-up cassette with the film riding over each roller in an acceptable manner. The Slave camera film was noticeably loose between the supply cassette and the input metering roller, but normally taut between the input metering roller and the take-up cassette. It appears that approximately 1 to 2 inches of film were pulled from the Slave supply spool during shipment to VAFB. The loose film in the Slave camera necessitated a rigorous examination, through access doors, of the entire film path to assure acceptable film thread-up before and during camera operation. Both the Master and Slave film tracked properly throughout the film path during camera operation. No special corrective action was necessary.

The shutters of the four horizon cameras and the two Stellar/Index cameras appeared to open and close normally.

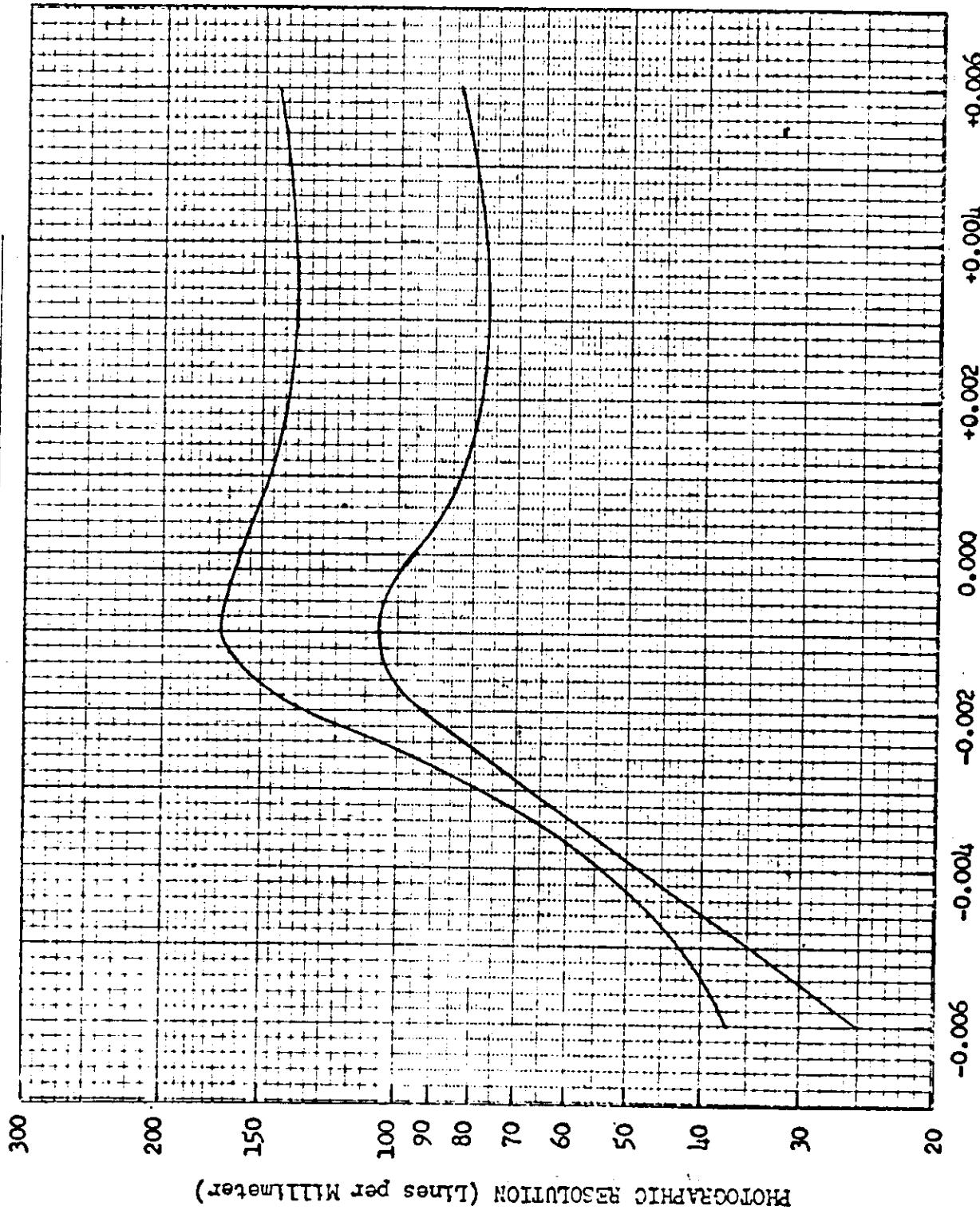
The four horizon camera boots, stellar baffles, and stellar boots were all painted dull black at A/P and rated acceptable for flight when examined for the last time at VAFB.

Interrogation of J-32 telemetry points demonstrated that no significant change occurred in system performance during camera operation at VAFB compared to camera operation at A/P.

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C/ [REDACTED] PRE-FLIGHT DYNAMIC RESOLUTION



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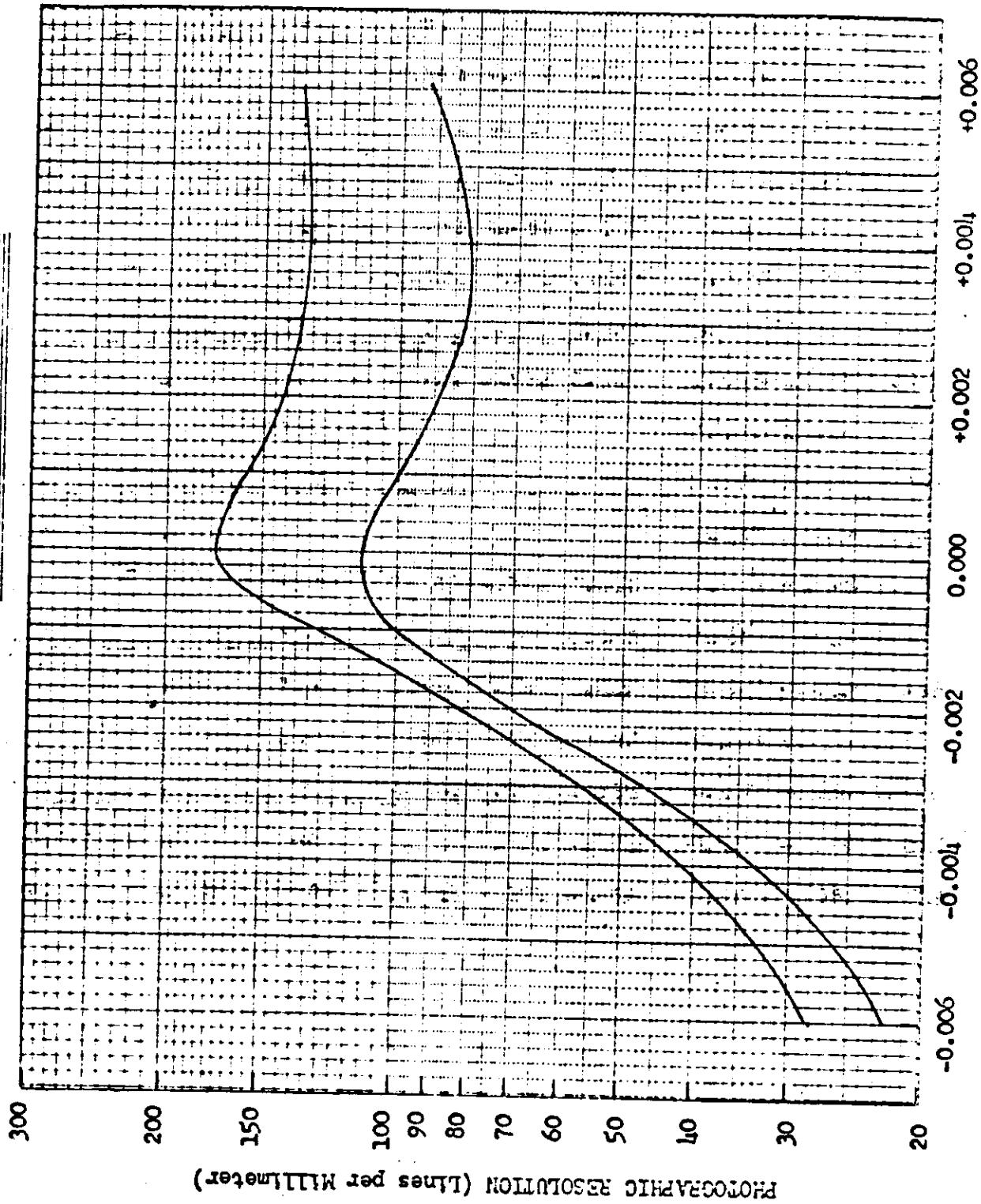
IA 1 07 7 3513 3551

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				INST 190	INST 191	190/191	
REV/MODE	RAMP	T.U.R.	ACT.	CAL.	DEV.	ACT. CAL. DEV.	DIFF.
11A 1	.7 .7	-0	3.514	3.550	0.00F	3.549 3.576	0.75F 1.00
11A 1	.7 .7	-0	3.513	3.550	0.03F	3.550 3.576	0.72F 1.05
11A 2	.7 .7	-0	3.547	3.550	0.07F	3.571 3.576	0.14F 0.68
11A 2	.7 .7	-0	3.531	3.550	0.52F	3.552 3.576	0.67F 0.59
11A 2	.7 .7	-0	3.516	3.550	0.95F	3.550 3.576	0.72F 0.97
11A 3	.6 .2	915	3.452	3.456	0.10F	3.481 3.481	0.01S 0.84
11A 3	.8 .2	976	3.301	3.513	0.37F	3.327 3.337	0.29F 0.79
11A 3	.6 .2	1068	3.095	3.116	0.66F	3.113 3.136	0.74F 0.58
11A 3	.8 .2	1150	2.915	2.932	0.58F	2.935 2.950	0.50F 0.69
12A 1	.6 .2	1761				2.189 2.206	0.77F
12A 1	.8 .2	1818				2.175 2.203	1.29F
12A 1	.8 .2	1890				2.170 2.202	1.44F
12A 2	.8 .2	457	4.680	4.710	0.63F	4.719 4.744	0.52F 0.83
12A 2	.8 .2	574	4.340	4.380	0.91F	4.370 4.413	0.97F 0.69
12A 2	.8 .2	714	3.940	3.981	1.03F	3.977 4.012	0.86F 0.94
12A 2	.8 .2	860	3.561	3.591	0.84F	3.594 3.618	0.66F 0.93
13A 1	4 .1	-0	4.346	4.323	0.53S	4.377 4.356	0.49S 0.71
13A 1	4 .1	-0	4.325	4.323	0.05S	4.367 4.356	0.26S 0.97
13A 1	4 .1	-0	4.312	4.323	0.26F	4.356 4.356	0.01S 1.02

TABLE 2-1

NON-SERIALIZED  
NO. [REDACTED]  
C/ [REDACTED] PRE-FLIGHT DYNAMIC RESOLUTION



THROUGH FOCUS INCREMENTS (Inches)

REV/MODE	RAMP	T.C.R.	ACT.	INST 190		INST 191		DIFF.			
				CAL.	DEV.	CAL.	DEV.				
13A	2	11	1	1710	2.337	2.317	0.85S	2.353	2.323	1.27S	0.56
13A	2	11	1	1745	2.293	2.286	0.12F	2.314	2.301	0.55S	0.92
13A	2	11	1	1772	2.281	2.282	0.04F	2.294	2.287	0.29S	0.67
13A	3	11	1	1790	2.242	2.274	1.41F				
13A	3	11	1	1817	2.234	2.264	1.34F				
13A	4	11	1	1858	2.241	2.254	0.57F	2.277	2.259	0.82S	1.61
13A	4	11	1	1873	2.247	2.251	0.19F	2.265	2.256	0.40S	0.80
13A	5	11	1	1885				2.246	2.254	0.38F	
13A	5	11	1	1903				2.236	2.253	0.76F	
13A	6	11	1	1936	2.258	2.246	0.43S	2.251	2.253	0.09F	-0.31
13A	6	11	1	1968	2.248	2.252	0.12F	2.258	2.256	0.07S	0.40
13A	6	11	1	1977	2.245	2.253	0.37F	2.256	2.258	0.09F	0.49
14A	1	11	1	2821	3.894	3.863	0.30S	3.912	3.893	0.50S	0.46
14A	1	11	1	2889	4.105	4.122	0.42F	4.135	4.154	0.45F	0.73
14A	1	11	1	2975	4.473	4.453	0.44F	4.512	4.526	0.31F	0.87
14A	1	11	1	3074	4.957	4.982	0.50F	5.007	5.016	0.19F	1.01
PS	1	8	2	C	5.464	5.419	0.64S	5.484	5.452	0.58S	0.37
PS	1	8	2	C	5.418	5.419	0.01F	5.457	5.452	0.09S	0.72
PS	1	8	2	0	5.406	5.419	0.23F	5.445	5.452	0.13F	0.72
PS	1	8	2	0	5.394	5.419	0.46F	5.437	5.452	0.28F	0.80

DEV. AND DIFF. ARE IN PERCENT

THE (-) SIGN INDICATES THAT INST 1 IS SLOWER THAN INST 2

F=FAST AND S=SLOW

TABLE 2-1

C/ [REDACTED] NO. [REDACTED]

## J-32 CLOCK CORR. TASC TEST NO. 1

IRIG REV	DAY-HR-MIN-SEC	IRIG SECONDS	CLOCK SECONDS	DELTA IRIG	DELTA CLOCK	ERROR
C1	8 8 43 12.390	722892.390	80744.249	---	---	---
C2	8 11 25 48.080	732348.080	90199.944	9455.690	9455.695	0.005
C4	8 13 28 53.680	739738.680	97590.530	7390.600	7390.536	-0.014
C5	8 15 37 48.175	747463.175	105320.034	7729.495	7729.504	0.009
C7	9 10 3 56.550	613836.550	171688.378	66368.375	66368.344	-0.031
C9	9 12 49 9.235	823749.235	181601.052	9912.685	9912.674	-0.011
11	10 5 25 37.860	894337.860	252189.735	70583.625	70588.682	0.058
13	10 11 14 13.031	904453.031	262304.895	10115.171	10115.160	-0.011
15	11 4 1 43.790	982903.790	340755.619	78450.758	78450.723	-0.035
16	11 11 57 8.300	993428.300	351280.142	10524.510	10524.523	0.013
01	11 14 33 55.925	1002835.925	360687.749	9407.625	9407.607	-0.018
02	12 8 53 6.290	1068785.290	426638.168	65950.364	65950.419	0.055
03	12 10 26 26.398	1074386.398	432238.277	5600.108	5600.109	0.001
04	12 11 57 16.537	1079836.537	437688.408	5450.139	5450.131	-0.008
07	13 8 57 59.138	1155479.138	513331.016	75642.600	75642.607	0.007
09	13 11 43 14.230	1165394.230	523246.107	9915.092	9915.091	-0.001
12	13 15 23 21.520	1178601.520	536453.388	13207.290	13207.281	-0.009

5 6 35 9.130-DELTA TIME

TOTAL ACCUM. ERROR 0.009

TABLE 2-2

**SECTION 3****FLIGHT OPERATIONS****A. SUMMARY**

All launch, ascent, and injection events occurred as programmed which resulted in achieving the desired orbit. The Agena tape recorder was used to record ascent thermal environment but failed 127 seconds into the ascent phase.

Both panoramic cameras operated satisfactorily throughout the flight. Average cycle rates on both instruments deviated from pre-flight calibrations by less than 2 per cent.

The pressure make-up system operated satisfactorily throughout the flight ending with 340 PSIA supply remaining.

The -1 and -2 Stellar/Index cameras, the clock, and the command system operated properly throughout the flight.

The instrumentation system operated properly throughout the flight except an intermittent accelerometer on ascent and the effects of the Agena tape recorder on commutated channels 11 and 13.

The internal environment was within tolerance throughout the flight. An ascent fairing temperature profile was obtained.

Both recovery systems operated properly. However 7 to 8 amps of current was present on the regulated return for 0.8 seconds from "A" bucket transfer to electrical disconnect.

**B. PANORAMIC CAMERA PERFORMANCE**

The camera system dynamics were normal on all engineering operations observed throughout the mission. The film transport system was smooth and had 99/101 clutch ratios of 6/6 for both instruments. Cycle rate data (Table 3-1) was less than 2 per cent from the pre-flight calibrations. The individual instrument rates matched to less than 0.5%. This close match of the individual rates was reflected in the overall consumption depleting the supply only 10 frames apart. The film supply was depleted on orbit 211, the last operate prior to the second recovery.

Panoramic Film Consumption

	<u>Actual</u>	
	<u>Master</u>	<u>Slave</u>
Sample - Off Spooling	19	19
Pre-Launch	147	142
-1 Mission	2905	2904
-2 Mission	2996	3001
<b>Total</b>	<b>6067</b>	<b>6066</b>

FMC Match

The V/H ramp to orbit match was acceptable throughout the flight. The following settings of RTC 6, 8 and 10 were used to attain the best match during the mission:

	<u>RTC</u>	<u>6</u>	<u>8</u>	<u>10</u>	
	6	7	6		Launch settings for nominal orbit.
	6	6	6		Changed at Rev. 4, [REDACTED] to compensate for orbit dispersions at launch.
	5	7	6		Changed at Rev. 14, [REDACTED] This change was based on more optimum orbital elements than was available for the previous change.
	5	6	7		Changed at Rev. 30, [REDACTED] Required to compensate for orbit decay. This setting was satisfactory for rest of flight.

## C. STELLAR/INDEX CAMERA PERFORMANCE

The -1 Stellar/Index camera operation was normal throughout the mission with telemetry indicating proper shutter, meter, programmer, and slew functions.

The -2 Stellar/Index operation was normal throughout the mission. Telemetry indicated proper shutter, meter, programmer and slewing functions. A post flight report indicated that the recovered length of the slewed index material was short

#### D. INSTRUMENTATION AND COMMAND SYSTEM PERFORMANCE

The instrumentation system operated properly throughout the flight except for one ascent accelerometer and the Agena tape recorder. The Agena tape recorder failed and lost power 126 seconds after lift-off. This caused severe loading to data connected to the input. Channel 11, temperature data, was affected on launch and several orbits for short periods of time. Channel 13, payload status was affected from orbit 115 thru orbit 118 and required command selector position verification from the Link II backup channel. This condition for channel 13 occurred again on orbit 212 and remained until orbit 215.

The radial accelerometer mounted on the transfer box cover became intermittent on ascent and produced unreliable data.

The command system operated properly throughout the mission. The mono-overlap delay operated properly at 12.0 seconds.

#### E. CLOCK SYSTEM PERFORMANCE

The payload clock system performed satisfactorily throughout the mission. The clock/system time correlation data obtained from the [redacted] acquisitions are included in Table 3-2.

#### F. PRESSURE MAKE-UP SYSTEM PERFORMANCE

The pressure make-up system performed satisfactorily throughout the mission. The mission consumed 2210 PSIA supply pressure for a duration of 239 minutes of operate. This resulted in an average consumption of 9.25 PSIA/minute.

#### G. THERMAL ENVIRONMENT

Temperature data obtained from the [redacted] acquisitions are contained in Table 3-3. Average master instrument temperatures started at 77°F and ended at 65°F through the flight. The average Slave instrument temperature range was from 73° to 61°.

Specific temperature plots vs Beta angle are included in Figures 3-1, 3-2, and 3-3.

Thermal environment of the fairing and aft barrel were recorded from Link II during ascent. These temperatures are summarized in Figures 3-4 and 3-5.

## J-32 190/191 FLIGHT CYCLE PERIOD DATA 8/7/66 THRU 8/22/66

REV. MODE	OP RAMP TUR N	SYSTEM A SECS	INST. 190		INST. 191		SYSTEM DEV. DIF.					
			ACTUAL CALIB.	UNIT	SYSTEM DEV.	ACTUAL UNIT		SYSTEM DEV.				
008	A	6	40	3.590	3.630	1.49S	1.12S	3.645	1.16S	1.54S	-0.41	
016	A	5	7	1605	2.309	2.342	1.55S	1.42S	2.365	2.29S	2.42S	0.98
032	A	5	6	1540	2.274	2.300	1.27S	1.16S	2.300	1.04S	1.16S	-0.00
048	A	5	6	1600	2.243	2.247	0.30S	0.20S	2.247	0.10S	0.20S	-0.00
064	A	5	6	1655	2.219	2.257	1.58S	1.69S	2.260	1.77S	1.83S	0.13
081	A	5	6	1700	2.217	2.250	1.37S	1.49S	2.260	2.06S	1.94S	0.44
105	A	5	6	190	3.387	3.415	1.17S	0.91S	3.428	0.84S	1.20S	0.38
113	A	5	6	1730	2.216	2.225	0.30S	0.42S	2.225	0.54S	0.42S	-0.00
121	B	5	6	230	3.372	3.410	1.40S	1.12S	3.413	0.85S	1.21S	0.09
129	B	5	6	1770	2.214	2.250	1.49S	1.61S	2.255	1.96S	1.84S	0.22
145	B	5	6	2033	2.213	2.235	0.85S	0.78S	2.230	0.88S	0.75S	-0.22
161	B	5	6	1895	2.212	2.232	0.77S	0.91S	2.228	0.86S	0.72S	-0.18
178	B	5	6	1850	2.212	2.250	1.57S	1.70S	2.245	1.60S	1.47S	-0.22

DEV. AND DIFF. ARE IN PERCENT

THE (-) SIGN INDICATES THAT INST 1 IS SLOWER THAN INST 2.

F=FAST AND S=SLOW

TABLE 3-1

## CLOCK SUMMARY

SYS TIME I/P	ORDER FIT 1	CL TIME I/P	COMP SYS TM	DELTA ST	REV
0.24524845D 05	0.1322436290	05	0.245248549D 05	-0.0099	7
0.74375021D 05	0.182093788D 06	0.743750178D 05	0.0032	16	
0.291158600 05	0.2232346370	06	0.291158700D 05	-0.0100	24
0.737762980 05	0.2678950580	06	0.737762945D 05	0.0036	32
0.285089080 05	0.3090276740	06	0.285089137D 05	-0.0057	40
0.731664040 05	0.3536851600	06	0.731664032D 05	0.0008	48
0.278849080 05	0.3948036660	06	0.278849124D 05	-0.0044	56
0.726884910 05	0.4396072380	06	0.726884879D 05	0.0031	64
0.273676980 05	0.4806864530	06	0.273677061D 05	-0.0081	72
0.771492720 05	0.5304680080	06	0.7714926500	0.0070	81
0.269161730 05	0.2976399500	05	0.269161668D 05	0.0062	89
0.318437930 05	0.3467161600	05	0.318437882D 05	0.0048	89
0.766806330 05	0.7952844900	05	0.766806247D 05	0.0083	97
0.261469430 05	0.1153947620	06	0.261469405D 05	0.0025	104
0.757236780 05	0.1649714930	06	0.757236754D 05	0.0026	113
0.305388960 05	0.2061867070	06	0.305388926D 05	0.0034	121
0.749812550 05	0.2506290620	06	0.749812511D 05	0.0039	129
0.297657530 05	0.2918135570	06	0.297657493D 05	0.0037	137
0.741907500 05	0.3362385500	06	0.741907458D 05	0.0042	145
0.288316400 05	0.3772794380	06	0.288316370D 05	0.0030	153
0.733812680 05	0.4210290650	06	0.733812675D 05	0.0005	161
0.334349240 05	0.4662827180	06	0.334349241D 05	-0.0001	169
0.778188460 05	0.5126666380	06	0.778188476D 05	-0.0016	178
0.272714060 05	0.1164828100	05	0.272714054D 05	0.0006	185
0.769175060 05	0.6129438400	05	0.769175122D 05	-0.0062	194
0.26370479D 05	0.9714735300	05	0.263704840D 05	-0.0050	201
0.762020880 05	0.1469789630	06	0.762020979D 05	-0.0099	210

A0=-0.1077187844D 06 A1= 0.100000007811D 01

SIGMA=0.00526 NO. POINTS= 27

RATIO OF CLOCK TIME TO SYS TIME= 0.9999999218900 00

SYS TIME I/P	ORDER FIT 2	CL TIME I/P	COMP SYS TM	DELTA ST	REV
0.24524845D 05	0.1322436290	06	0.245248470D 05	-0.0020	7
0.74375021D 05	0.182093788D 06	0.743750120D 05	0.0090	16	
0.291158600 05	0.2232346370	06	0.291158658D 05	-0.0058	24
0.737762980 05	0.2678950580	06	0.737762918D 05	0.0062	32
0.285089080 05	0.3090276740	06	0.285089123D 05	-0.0043	40
0.731664040 05	0.3536851600	06	0.731664031D 05	0.0009	48
0.278849080 05	0.3948036660	06	0.278849133D 05	-0.0053	56
0.726884910 05	0.4396072380	06	0.726884897D 05	0.0013	64
0.273676980 05	0.4806864530	06	0.273677086D 05	-0.0106	72
0.771492720 05	0.5304680080	06	0.771492682D 05	0.0034	81
0.269161730 05	0.2976399500	05	0.269161704D 05	0.0076	89
0.318437930 05	0.3467161600	05	0.318437919D 05	0.0011	89
0.766806330 05	0.7952844900	05	0.766806287D 05	0.0043	97
0.261469430 05	0.1153947620	06	0.261469446D 05	-0.0016	104
0.757236780 05	0.1649714930	06	0.757236795D 05	-0.0015	113
0.305388960 05	0.2061867070	06	0.305388966D 05	-0.0006	121
0.749812550 05	0.2506290620	06	0.749812547D 05	0.0003	129
0.297657530 05	0.2918135570	06	0.297657525D 05	0.0005	137
0.741907500 05	0.3362385500	06	0.741907484D 05	0.0016	145

TABLE 3-2

C/ [REDACTED] NO. [REDACTED]

0.288316400 05	0.3772714100 06	0.2883163890 05	0.0011	153
0.733812640 05	0.4218290650 06	0.7338126840 05	-0.0004	161
0.334349240 05	0.4682827180 06	0.3343472390 05	0.0001	169
0.778188460 05	0.5126666380 06	0.7781884620 05	-0.0002	178
0.272714060 05	0.1164823100 05	0.2727140280 05	0.0032	185
0.769175060 05	0.6127438400 05	0.7691750800 05	-0.0020	194
0.263704790 05	0.2714715200 05	0.2637047840 05	-0.0006	201
0.762020880 05	0.14697894630 06	0.7620209030 05	-0.0023	210

A0=-0.10771879800 06 A1= 0.1000000132540 01

A2=-0.4007009760564D-13

SIGMA=0.00373 NO. POINTS= 27

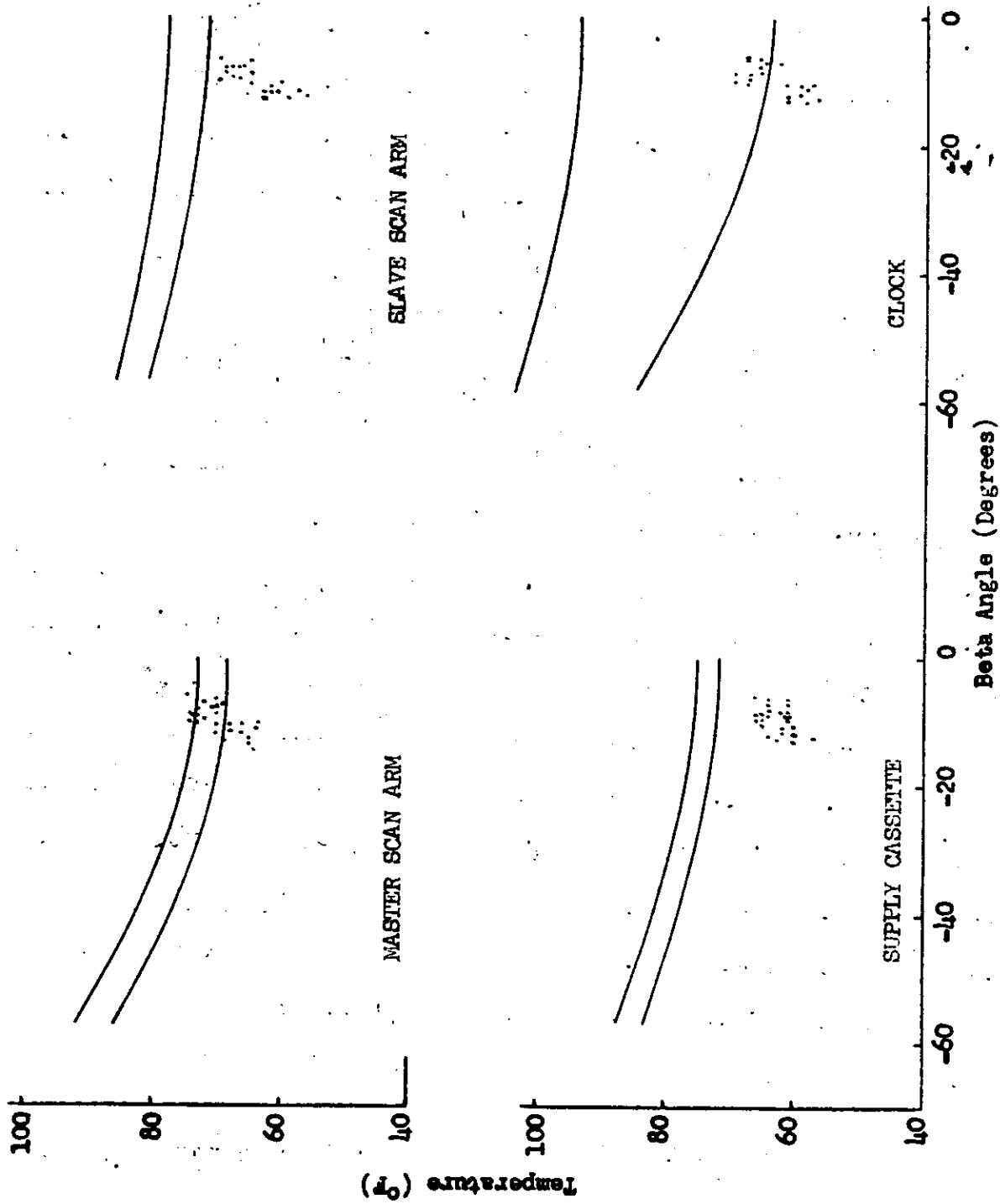
SIBSYS

TABLE 3-2



J-32 TEMPERATURE SUMMARY

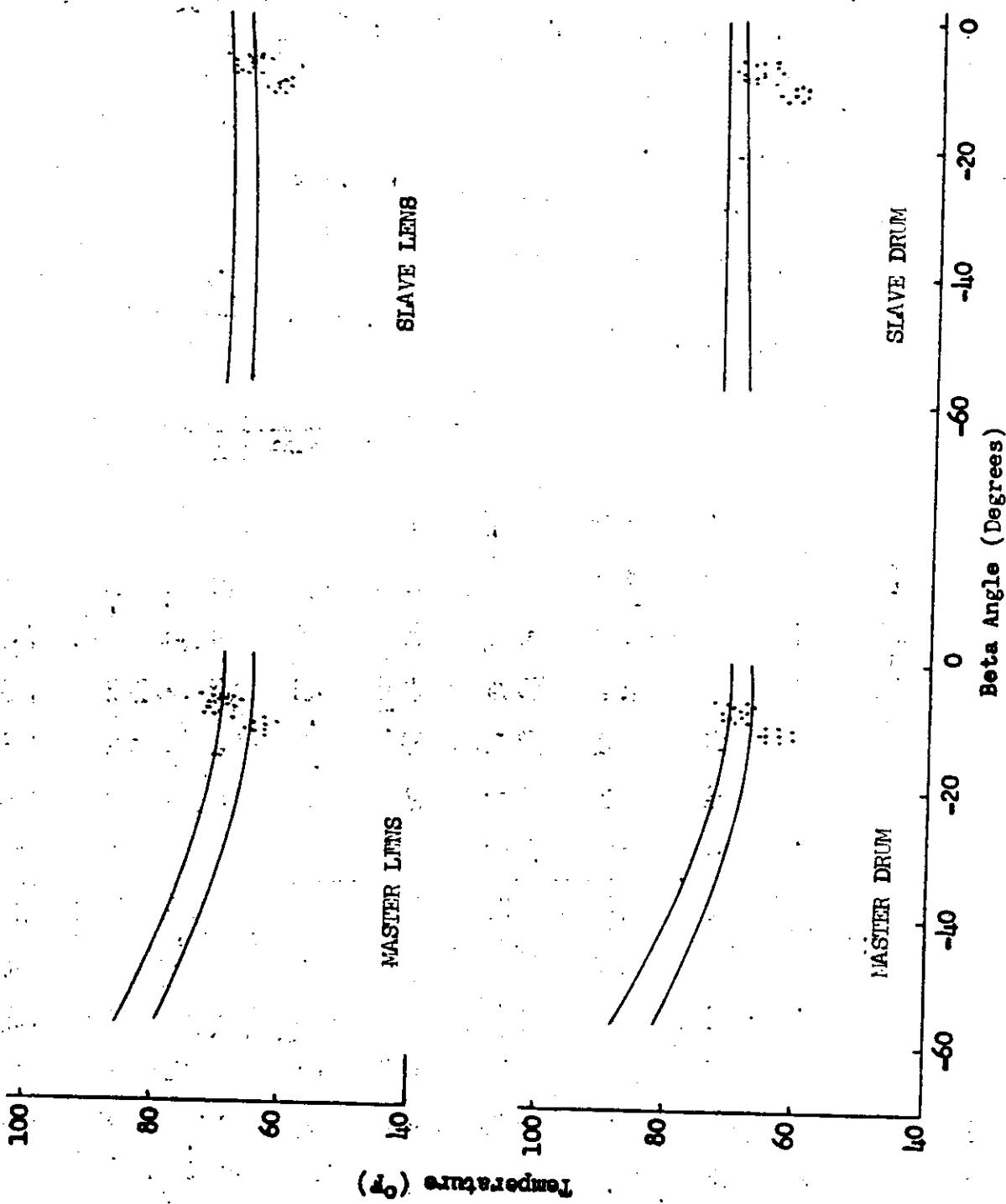
J-32 FLIGHT  
8/9/66 - 8/22/66



POT-050000

- NO -

J-32 FLIGHT  
8/9/66 - 8/22/66

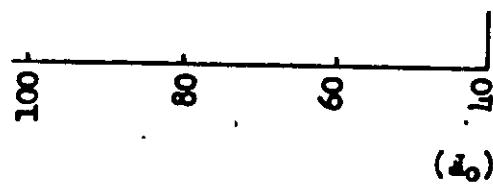


PICTURE 3-2

TOP SECRET C

J-32 FLIGHT  
8/9/66 - 8/22/66

SRV-1  
CASSETTE



SRV-2  
BATTERY

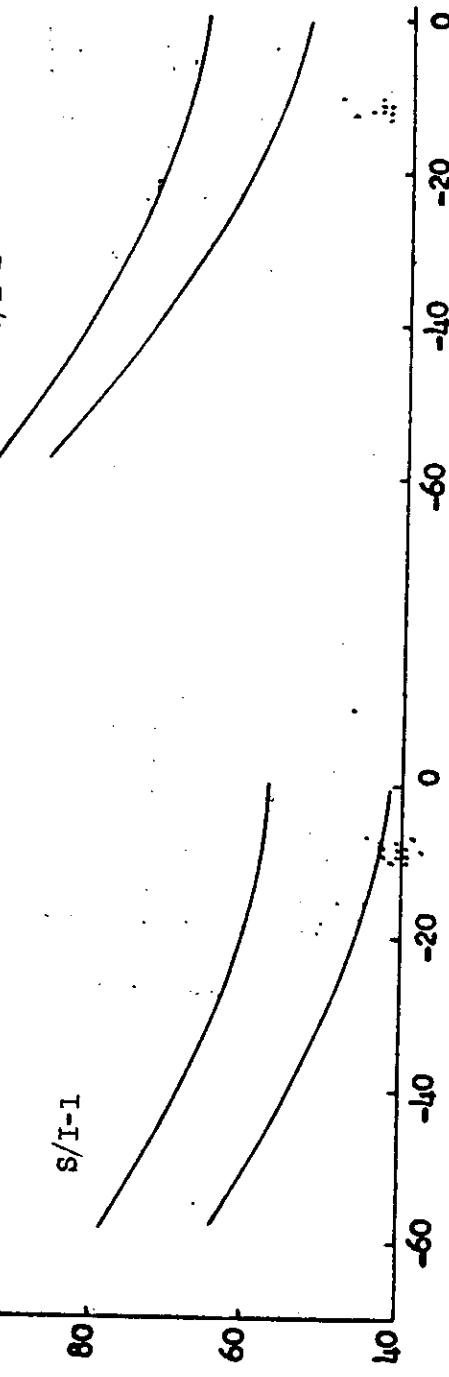
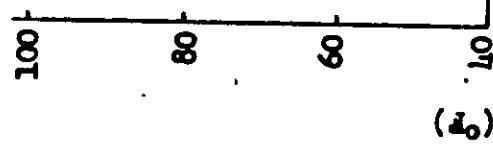


FIGURE 3-3

TOP SECRET C/

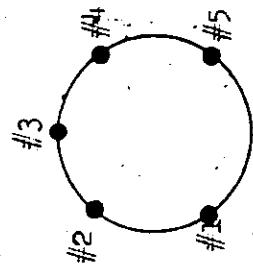
ASCENT HEATING

THORAD BOOSTER  
AGETIA 1631  
PAYLOAD J-32

BARREL

#1  
#2  
#3  
#4  
#5

CONIC



250

200

150

100

50

0

500

400

300

200

100

0

TIME FROM LIFT-OFF  
SECONDS

FIGURE 3-4

TOP SECRET C/

TOP SECRET [REDACTED]

C/ [REDACTED] NO. [REDACTED]

THORAD BOOSTER  
AGENA 1631  
PAYLOAD J-32

ASCENT HEATING

INCL. - 100 DEG.  
PERIGEE - 103 N.M.

50

100

150

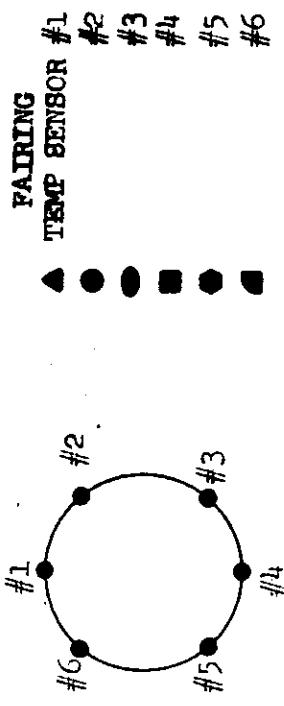
200

250

300

500  
400  
300  
200  
100  
0

TIME FROM LIFT-OFF  
SECONDS



## SECTION 4

## MISSION 1036-1 RECOVERY SYSTEM

SRV #715 was received at A/P on 27 September 1965. The receiving weight was 149.69 pounds. After modifications and incorporation of outstanding E.O.'s, the SRV was delivered to Systems Test for incorporation into the J-32 system.

The capsule was shipped to VAFB on 1 August 1966.

The -1 mission was successfully terminated by air-catch on orbit 115 on 16 August 1966. The predicted and actual impact points were as follows:

	<u>Latitude</u>	<u>Longitude</u>
Predicted	23° 4.4' N	168° 6.2' W
Actual	22° 46' N	168° 2' W

Telemetry data indicated that 7 to 8 amps of current was present on the +28V regulated return between transfer and electrical disconnect. The time duration was 0.80 seconds. The current was supplied by the pyro battery. Recovery event times are included in Table 4-1.

The condition of the recovered capsule was satisfactory with no damage other than normal paint blistering due to the re-entry environment.

## MISSION 1036-1

## RECOVERY SEQUENCE OF EVENTS

<u>Event</u>	<u>Delta Time (Seconds)</u>	
	<u>Actual</u>	<u>Nominal</u>
*Arm	76.91	77.0 ± 1.0
*Transfer	2.0	2.0 ± 0.25
Electrical Disconnect	0.82	0.900 ± 0.430
Separation	---	---
**Spin	3.34	3.4 ± 0.30
Retro	7.58	7.55 ± 0.45
Despin	10.68	10.75 ± 0.59
T/C Separation	1.50	1.5 ± 0.15
***"G" Switch Open	507.55	506.8
Parachute Cover Off	33.50	34.0 ± 1.5
Drogue Chute Deployed	0.68	0.63 ± 0.08
Main Chute Bag Separate	12.10	10.0 ± 3.0
Main Chute Deployed	0.55	0.52 ± 0.13
Main Chute Disreef	4.77	4.5 ± 0.80

\* From Separation

\*\* From Electrical Disconnect

\*\*\* From Retro

TABLE 4-1

## SECTION 5

## MISSION 1036-2 RECOVERY SYSTEM

SRV #716 was received at A/P on 27 September 1965. The receiving weight was 147.23 pounds. After modifications and incorporation of outstanding E.O.'s the unit was delivered to Systems Test for mating to the J-32 system.

The capsule was shipped to VAFB on 1 August 1966.

The -2 mission was successfully terminated by air-catch from orbit 212 on 22 August 1966. The impact point was as follows:

	<u>Latitude</u>	<u>Longitude</u>
Predicted	22° 31.7' N	165° 55.8' W
Actual	22° 31.0' N	165° 58' W

Event times are shown in Table 5-1.

The condition of the recovered capsule indicated no abnormal re-entry effects.

## MISSION 1036-2

## RECOVERY SEQUENCE OF EVENTS

<u>Event</u>	<u>Delta Time (Seconds)</u>	
	<u>Actual</u>	<u>Nominal</u>
*Arm	76.92	77.0 ± 1.0
*Transfer	2.0	2.0 ± 0.25
Electrical Disconnect	0.71	0.909 ± 0.430
Separation	- - -	- - -
**Spin	3.33	3.4 ± 0.30
Retro	7.56	7.55 ± 0.45
Despin	10.72	10.75 ± 0.59
T/C Separation	1.54	1.5 ± 0.15
***"G" Switch Open	504.81	506.6
Parachute Cover Off	34.18	34.0 ± 1.5
Drogue Chute Deployed	0.66	0.63 ± 0.08
Main Chute Bag Separate	12.06	10.0 ± 3.0
Main Chute Deployed	0.55	0.52 ± 0.13
Main Chute Disreef	4.33	4.45 ± 0.80

\* From Separation

\*\* From Electrical Disconnect

\*\*\* From Retro

TABLE 5-1

C [REDACTED] NO. [REDACTED]

## SECTION 6

## MASTER PANORAMIC CAMERA

## A. COMPONENT ASSIGNMENT

<u>Component</u>	<u>Serial Number</u>
Main Camera	190
Main Camera Lens	1842435
Supply Horizon Camera	287-06
Supply Horizon Camera Lens	E12893
Take-up Horizon Camera	287-G5
Take-up Horizon Camera Lens	E12891
Supply Cassette	SC-43

## B. CAMERA DATA AND FLIGHT SETTINGS

## Main Camera:

Lens	24" f/3.5
Slit Width	0.200"
Filter Type	Wratten 23A
Film Type	Eastman Type 3404

## Supply (Port) Horizon Camera:

Lens	55 mm f/6.3
Aperture Setting	f/6.3
Exposure Time	1/100 second
Filter Type	Wratten 25

## Take-up (Starboard) Horizon Camera:

Lens	55 mm f/6.3
Aperture Setting	f/8.0
Exposure Time	1/100 second
Filter Type	Wratten 25

## C. POST FLIGHT PERFORMANCE EVALUATION (Master Camera)

The Master camera produced 2852 frames (7933 feet) of photography during Mission 1036-1 and 3009 frames (7948 feet) during Mission 1036-2. The image quality was consistently good and rated better than Mission 1034 and comparable to Mission 1033.

Image quality produced by the Master camera was rated lower in sharpness than that produced by the Slave camera for Missions 1036-1 and 1036-2. The comparison was made by a visual evaluation at 20 to 50 x magnification of original negative and Duplicate Positive films. Master camera imagery is considered of lower quality primarily because of the added effect of haze light in the forward looking Master camera. The Master camera also used a wider exposure slit. The overall image quality of Mission 1036-2 was judged to be better than Mission 1036-1. This is attributed to the lower haze level in Mission 1036-2 as evidenced by viewing the Index camera photography.

One fixed target of unknown contrast and condition was recorded at Pahrump, Nevada. The average resolution from this target was judged to be somewhat greater than 12.5 feet. The MIP frames were rated 85.

Auxillary data recording such as H.O. fiducials, timing track, binary word, serial number, index marks, S/I slur pulse, and blanked pulse were operational throughout Mission 1036-1 and 1036-2. The start of pass mark failed after pass D-39 apparently due to lamp failure. Dendritic static discharge marks were present at random intervals along the film edge in Mission 1036-1 only. Edge static caused no degradation of terrain imagery.

The scan head rollers caused the usual minor scratch marks just within the format area under the binary word and at the take-up end of the mission on every frame of Mission 1036-1 and 1036-2. Normal heavy rail scratches are present throughout the mission. The format edge on the binary word side gradually became ragged as a result of emulsion dust accumulated from the rail scratches. No other degrading effect was observed.

Although extensive effort had been directed to elimination of light leaks, minor fog marks were present on the first, fifth and last frame of most passes. Degradation from light leaks was minor.

## SECTION 7

## SLAVE PANORAMIC CAMERA

## A. COMPONENT ASSIGNMENT

<u>Component</u>	<u>Serial Number</u>
Main Camera	191
Main Camera Lens	2022435
Supply Horizon Camera	285-06
Supply Horizon Camera Lens	E12904
Take-up Horizon Camera	281-G5
Take-up Horizon Camera Lens	E12905
Supply Cassette	SC-43

## B. CAMERA DATA AND FLIGHT SETTINGS

## Main Camera:

Lens	24" f/3.5
Slit Width	0.150"
Filter Type	Wratten 21
Film Type	Eastman Type 3404

## Supply (Starboard) Horizon Camera:

Lens	55 mm f/6.3
Aperture Setting	f/8.0
Exposure Time	1/100 second
Filter Type	Wratten 25

## Take-up (Port) Horizon Camera:

Lens	55 mm f/6.3
Aperture Setting	f/6.3
Exposure Time	1/100 second
Filter Type	Wratten 25

## C. POST FLIGHT PERFORMANCE EVALUATION (Slave Camera)

This camera produced 2853 frames (7955 feet) of photography during Mission 1036-1 and 3009 frames of photography (7958 feet) during Mission 1036-2. Visual comparison of the MIP frames for Mission 1036-1 and 1036-2 indicate that AFT camera photography is sharper than forward camera photography. Aft camera imagery is considered better primarily because of the reduced effect of haze light present in aft camera photography. It is also noted that the AFT camera used a narrower slit. The overall image quality of Mission 1036-2 was judged to be slightly better than Mission 1036-1. This is attributed to the lower haze level in Mission 1036-2 as evidenced by viewing the Index camera photography.

One fixed target of unknown contrast and condition was recorded at Pahrump, Nevada. The average resolution from this target was judged to be 8.5 feet on the aft-looking camera. The MIP frames were rated 85.

A minor region of soft imagery encompassing an area of approximately one square inch located at the camera number edge at the supply end of the format was first observed on pass D-203 and continued until the mission ended. The exact cause is unknown but may be caused by irregular tracking tension. Because of the minor significance of this anomaly at the end of the format no action will be taken.

C/ [REDACTED] NO. [REDACTED]

Auxillary data recording such as H.O. fiducials, timing track, binary word, serial number, index marks, blanked pulse, and start of pass mark were operational throughout Missions 1036-1 and 1036-2.

A few minor dendritic static discharge marks were noted along the film edge at random intervals. Dendritic static marks did not degrade terrain imagery.

Rail scratches were heavy and present throughout Mission 1036-1 and 1036-2. Minor scan head roller scratches were observed in each frame of the -1 and -2 missions. Scan head roller scratches were located inside the format under the binary word and at the take-up end of each frame. Degradation to terrain imagery was very minor. An intermittent emulsion scratch was found 1.22 inches into the format area measured from the camera number edge. Although this scratch occurred intermittently throughout the mission no known cause of the scratch was determined. The scratch was very fine and had no significant degrading effect upon terrain imagery.

Light leak fog was evidenced on the third from the last frame of some passes. Degradation to terrain imagery was minor.

## SECTION 8

### PANORAMIC CAMERA EXPOSURE

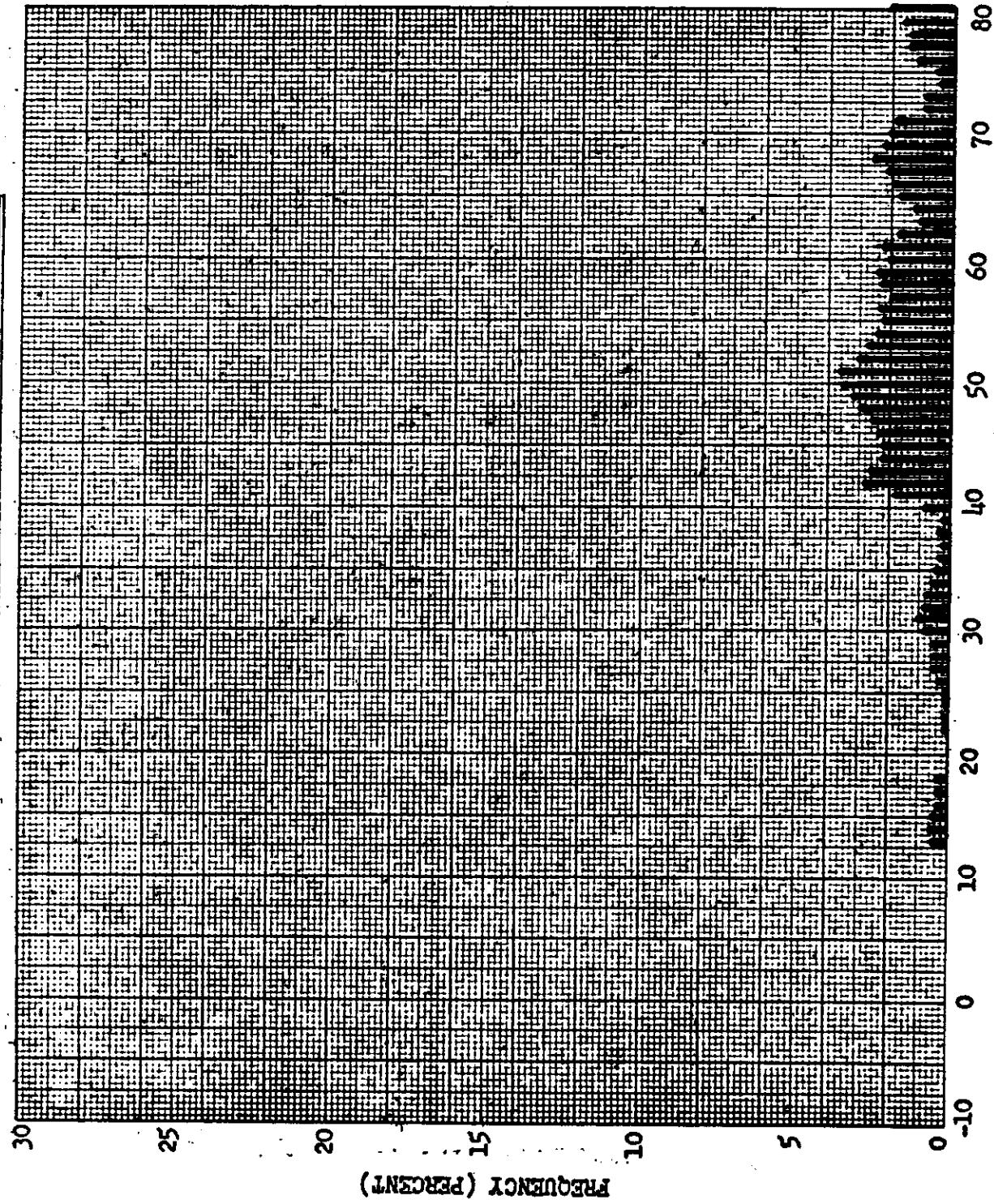
The Master camera contained a 0.200 inch slit and a Wratten 23A filter. The Slave camera had a 0.150 inch slit and a Wratten 21 filter. These conditions placed the nominal exposure between the full and the intermediate processing curve.

The frequency distributions of the solar elevations and solar azimuths encountered during the photographic operations are shown in Figures 8-1 to 8-4.

The nominal exposure times of the Master and Slave cameras are shown as a function of latitude for passes D-8, D-72, D-137 and D-201 in Figures 8-5 to 8-12. The predicted level of processing for the original negative is based on the in-flight performance estimate and is tabulated below with the processing levels reported by [REDACTED]

<u>Mission</u>	<u>Camera</u>		<u>% Primary</u>	<u>% Intermediate</u>	<u>% Full</u>
1036-1	FWD	Predicted	0	66.4	33.6
		Reported	8	14	78
1036-1	AFT	Predicted	0	4.7	95.3
		Reported	3	9	88
1036-2	FWD	Predicted	0	15.1	84.9
		Reported	1	19	80
1036-2	AFT	Predicted	0	3.5	96.5
		Reported	3	20	77

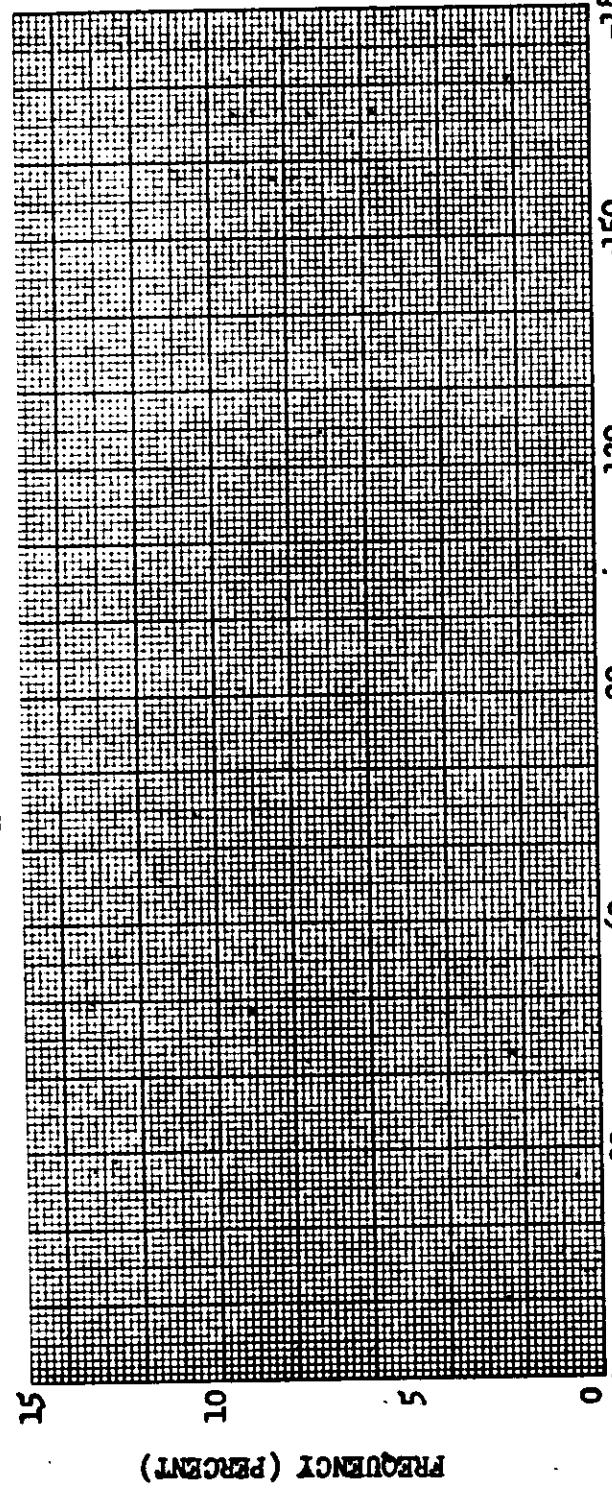
FIGURE 8-1

SOLAR ELEVATION FREQUENCY DISTRIBUTION

TOP SECRET

C [REDACTED] no. [REDACTED]

SOLAR AZIMUTH FREQUENCY DISTRIBUTION



Mission No: 1036-1

Payload No: J-32

Camera No: 190

Launch Date: 8/9/66

Launch Time: 2046 Z

Inclination: 100°

SIGN NOTATION

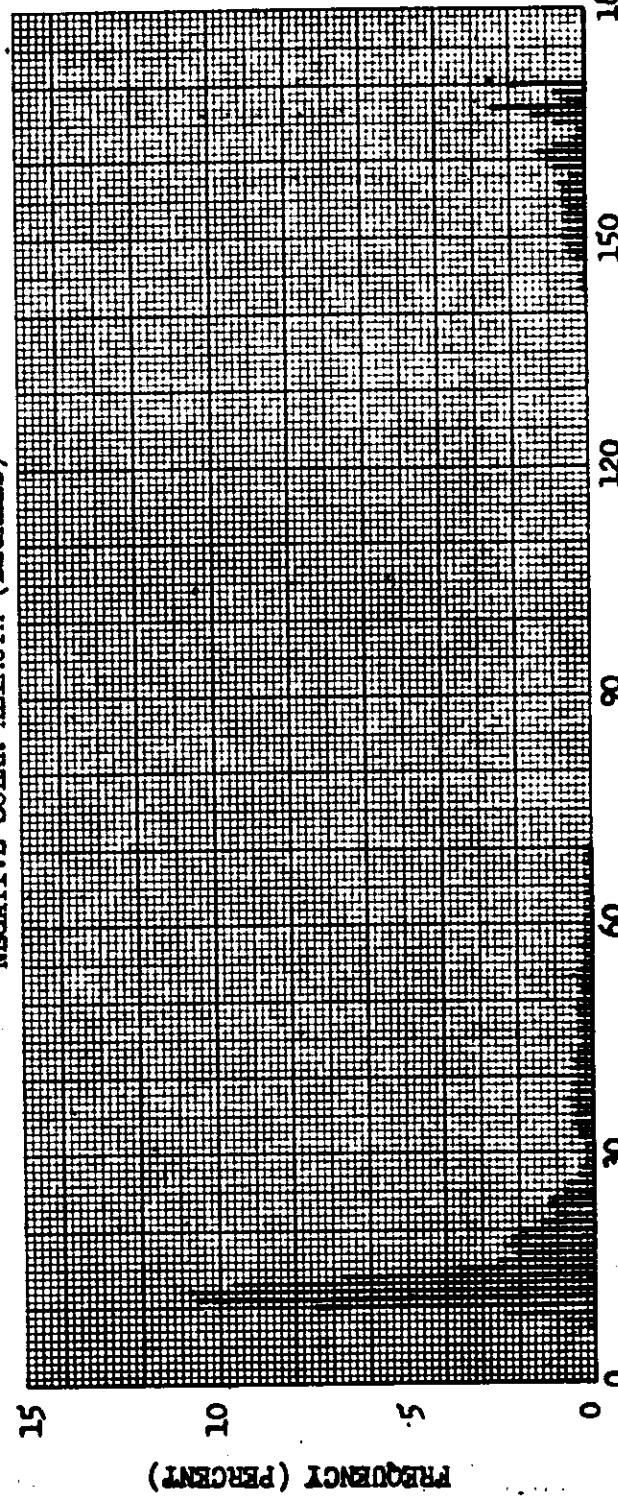


FIGURE R-2

TOP SECRET

NO.

SOLAR ELEVATION FREQUENCY DISTRIBUTION

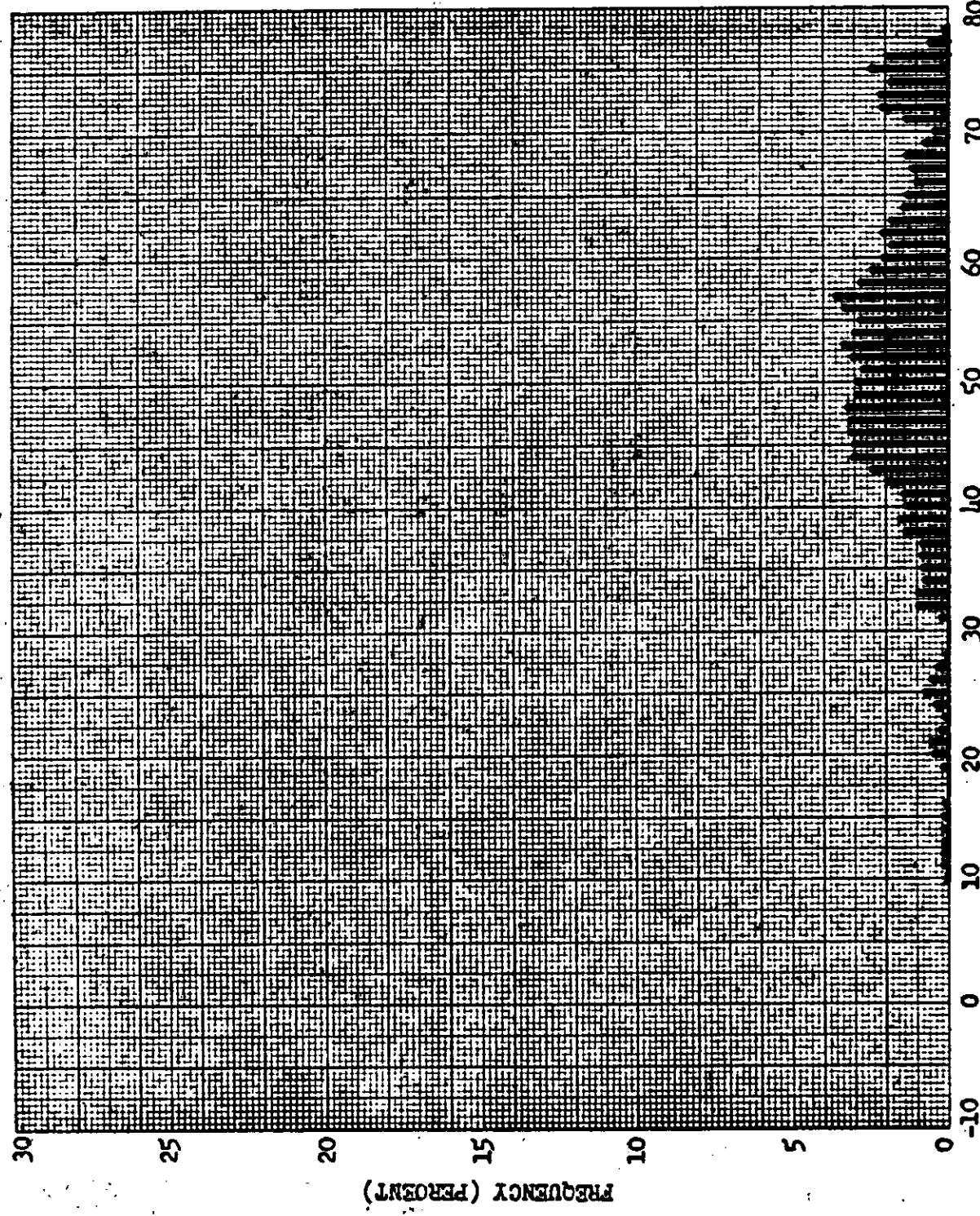
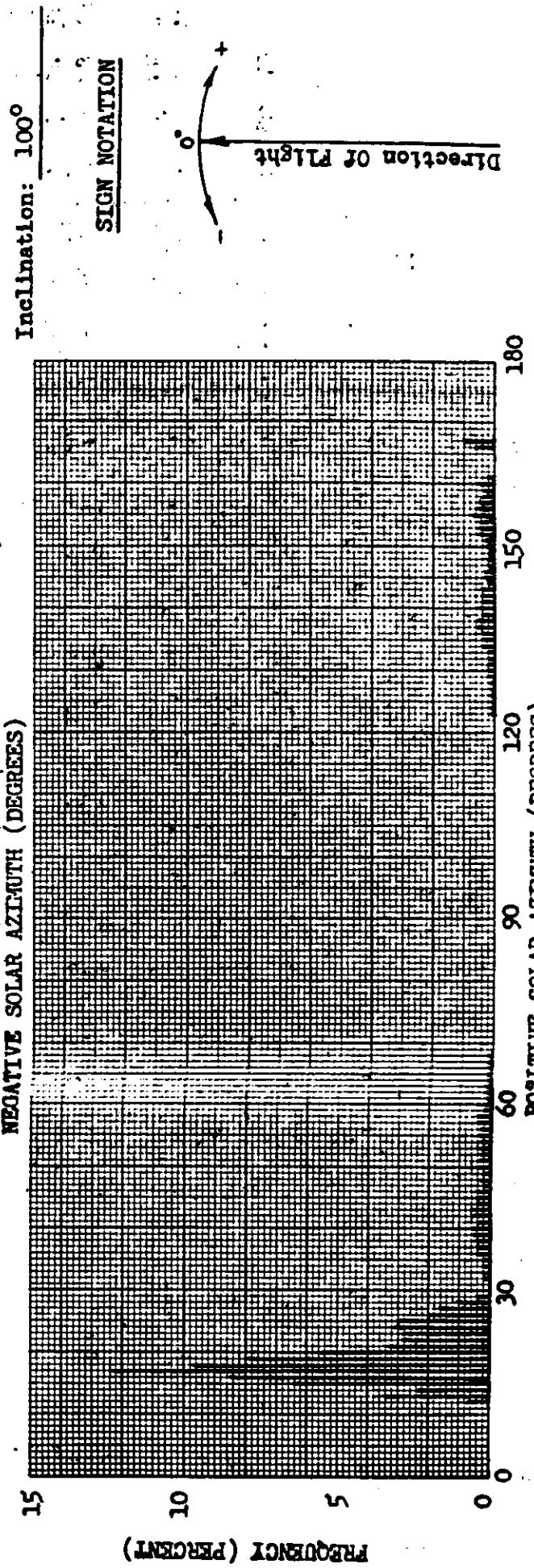
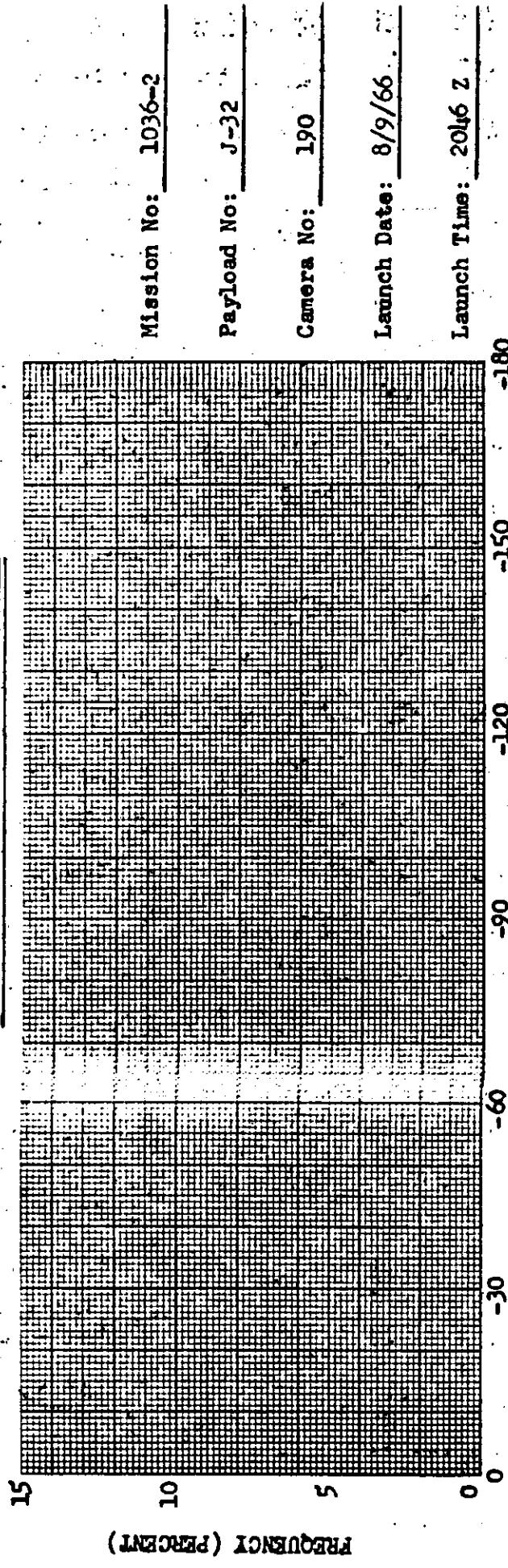


FIGURE B-3

TOP SECRET C

TOP SECRET  
C [REDACTED] NO.

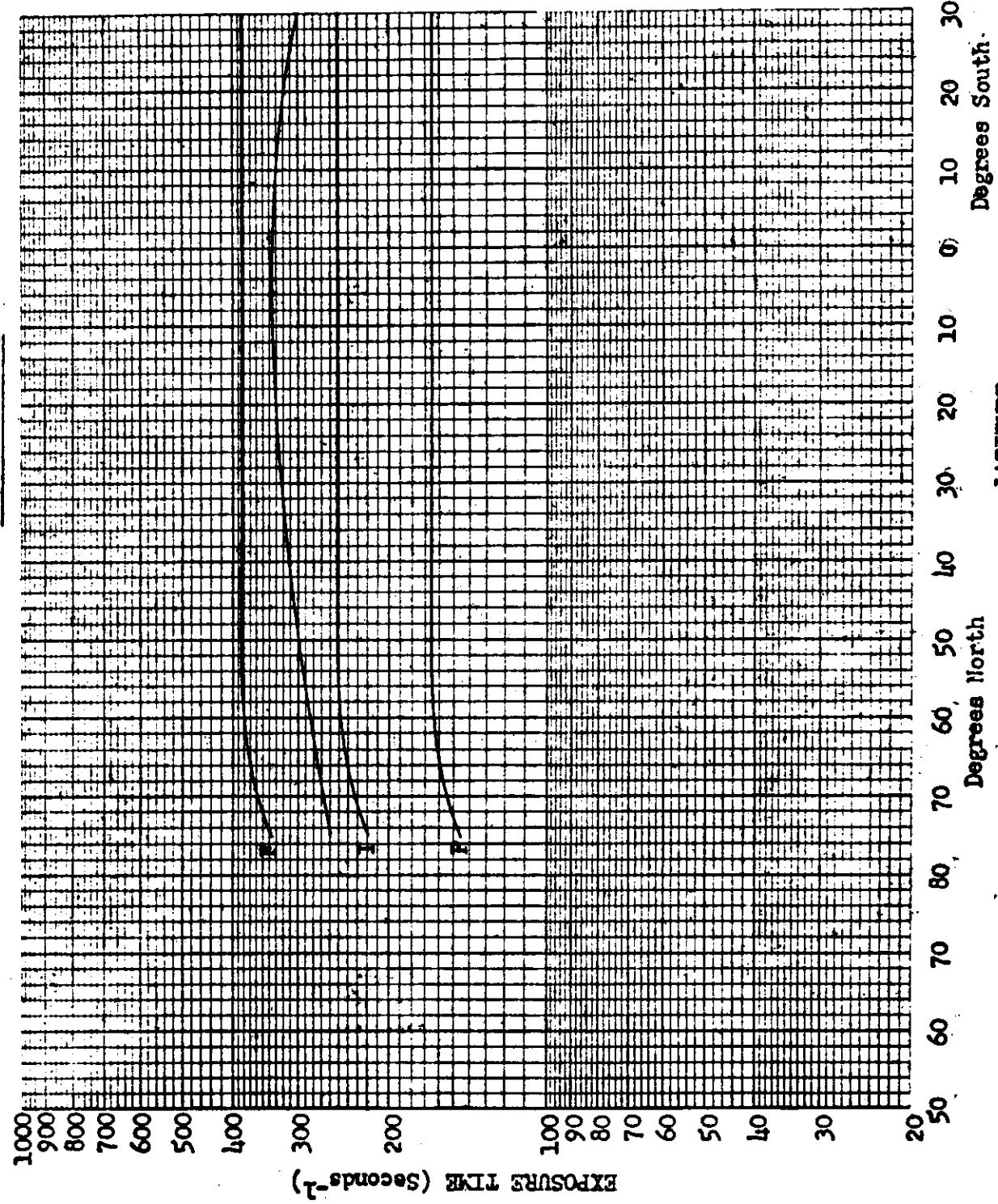
SOLAR AZIMUTH FREQUENCY-DISTRIBUTION



~~TOP SECRET~~

No.

EXPOSURE POINTS



TOP-SECRET

NO.

EXPOSURE POINTS

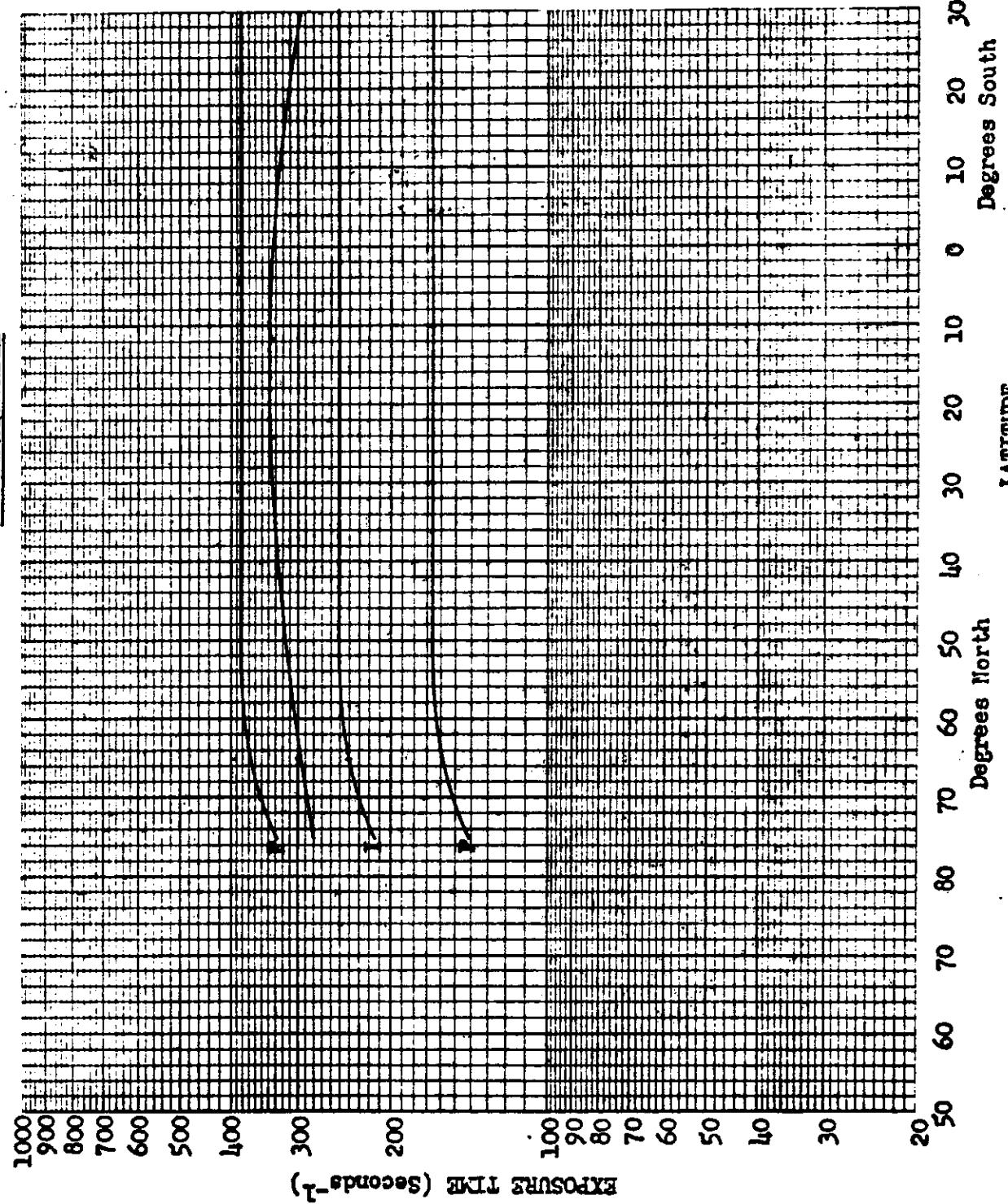


FIGURE 8-6

TOP-SECRET C

~~TOP SECRET~~  
C. [REDACTED] NO.

EXPOSURE POINTS

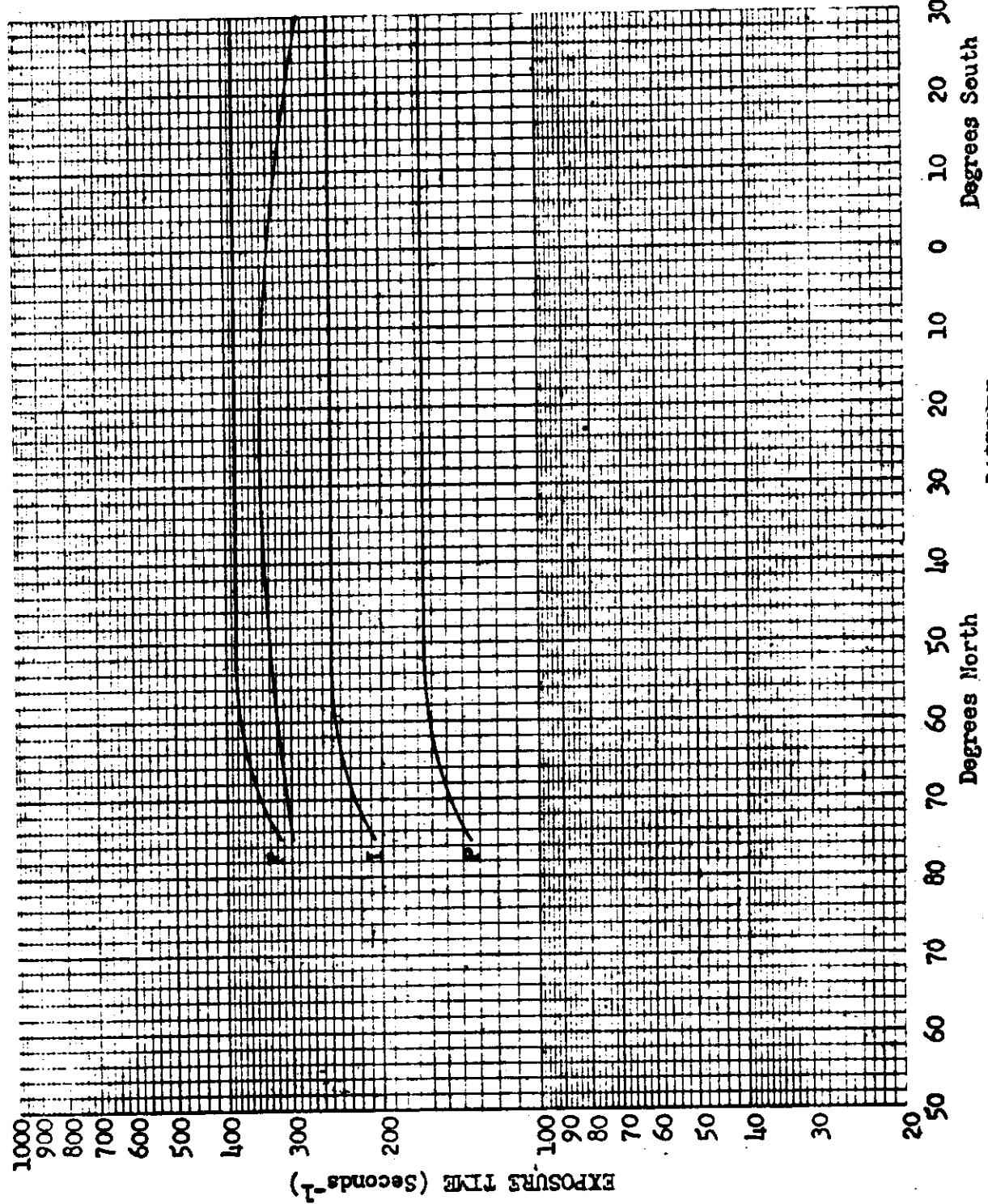


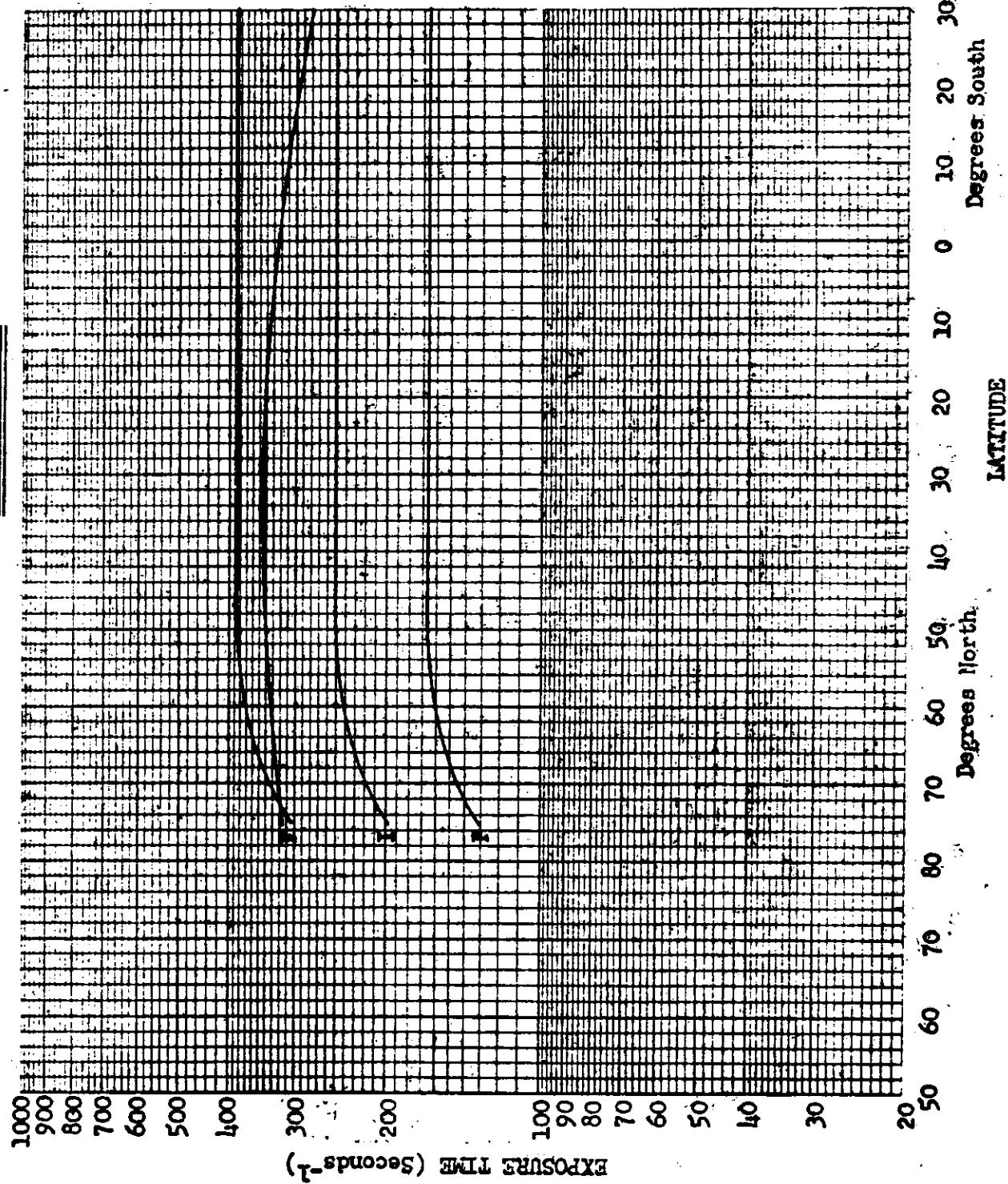
FIGURE 8-7

~~TOP SECRET~~ C/

FIGURE 8-8

TOP SECRET C

TOE SPOT NO.  
EXPOSURE POINTS



Mission No: 1026

Payload No: J-32

Camera No: 191

Pass No: \_\_\_\_\_ 8

Launch Date: 8/9/66

Launch Time: 2016 2

Slit width: .150

Filter Type: Watten 21

Digitized by srujanika@gmail.com

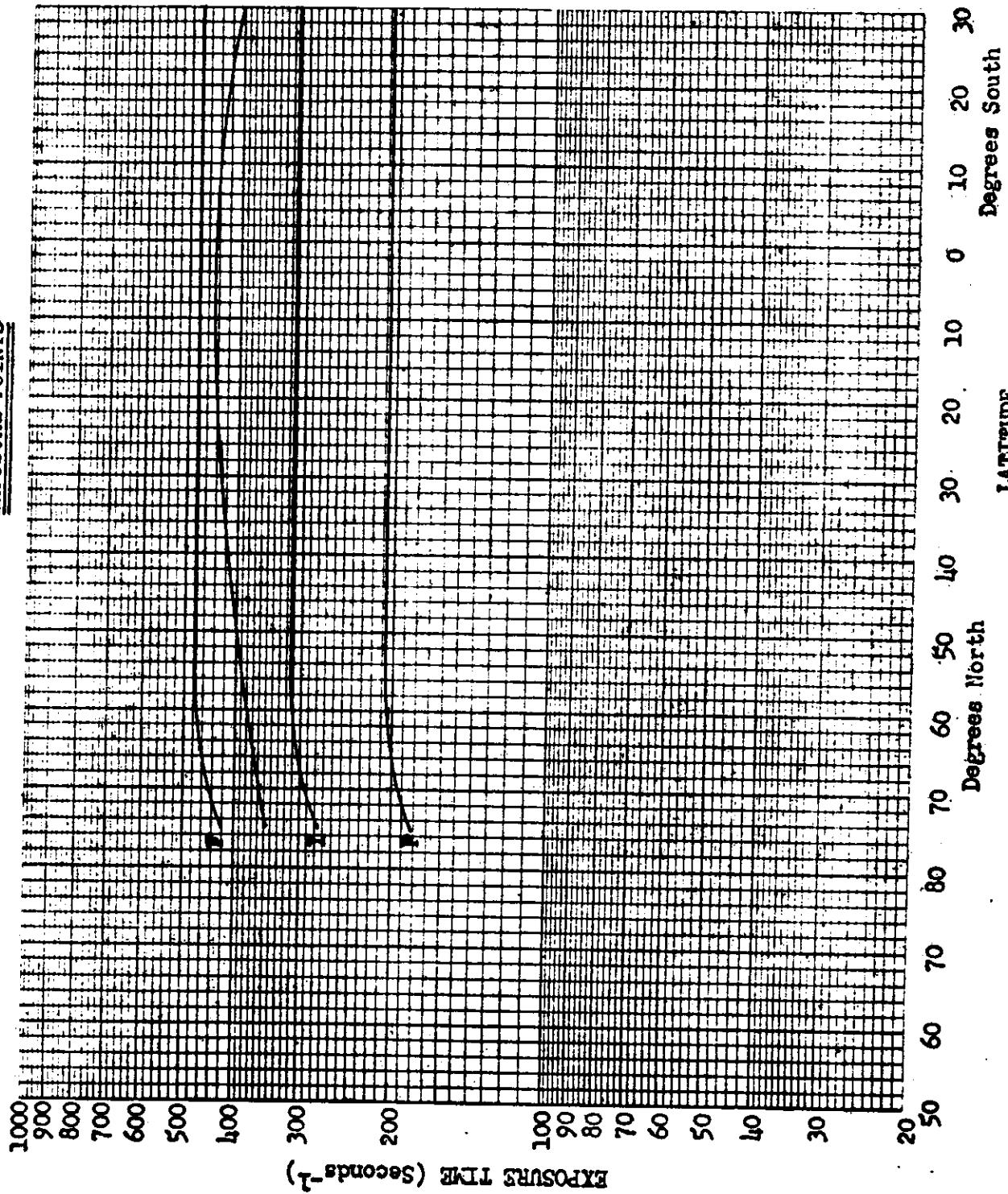
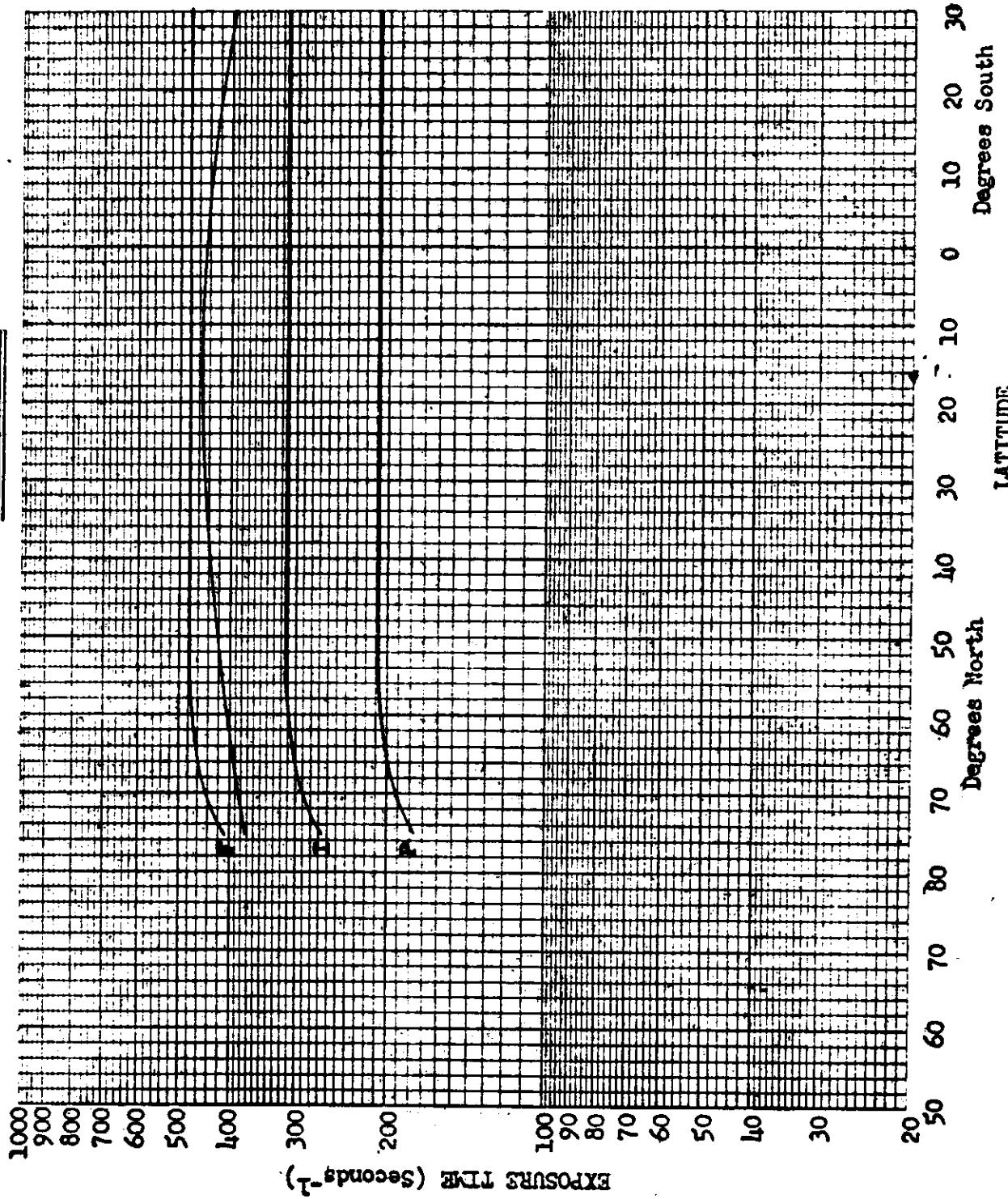


FIGURE 8-9

C 15

TOP SECRET  
C [REDACTED] NO.  
EXPOSURE POINTS



Mod. Specimen  
Exposure Points  
C [REDACTED] NO.

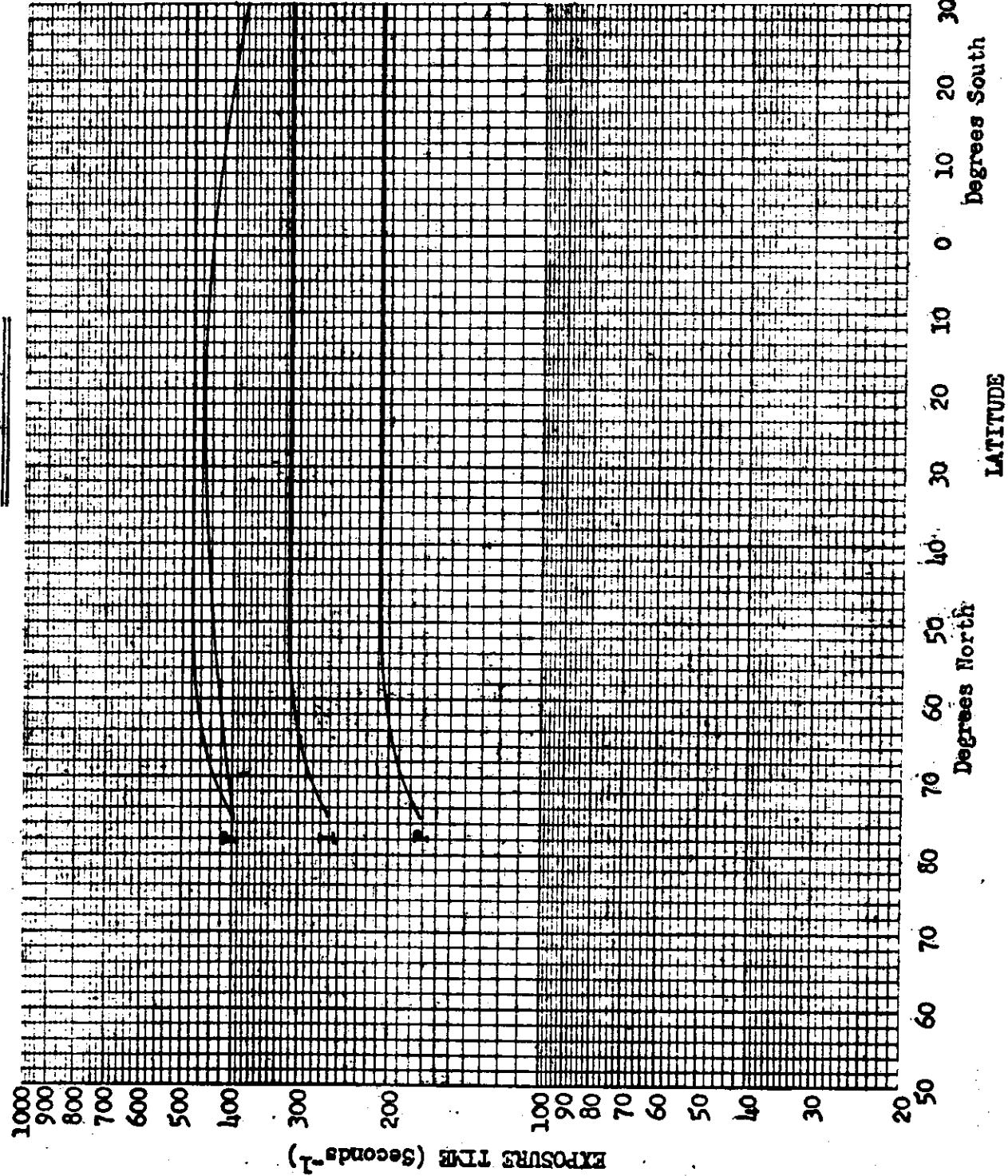
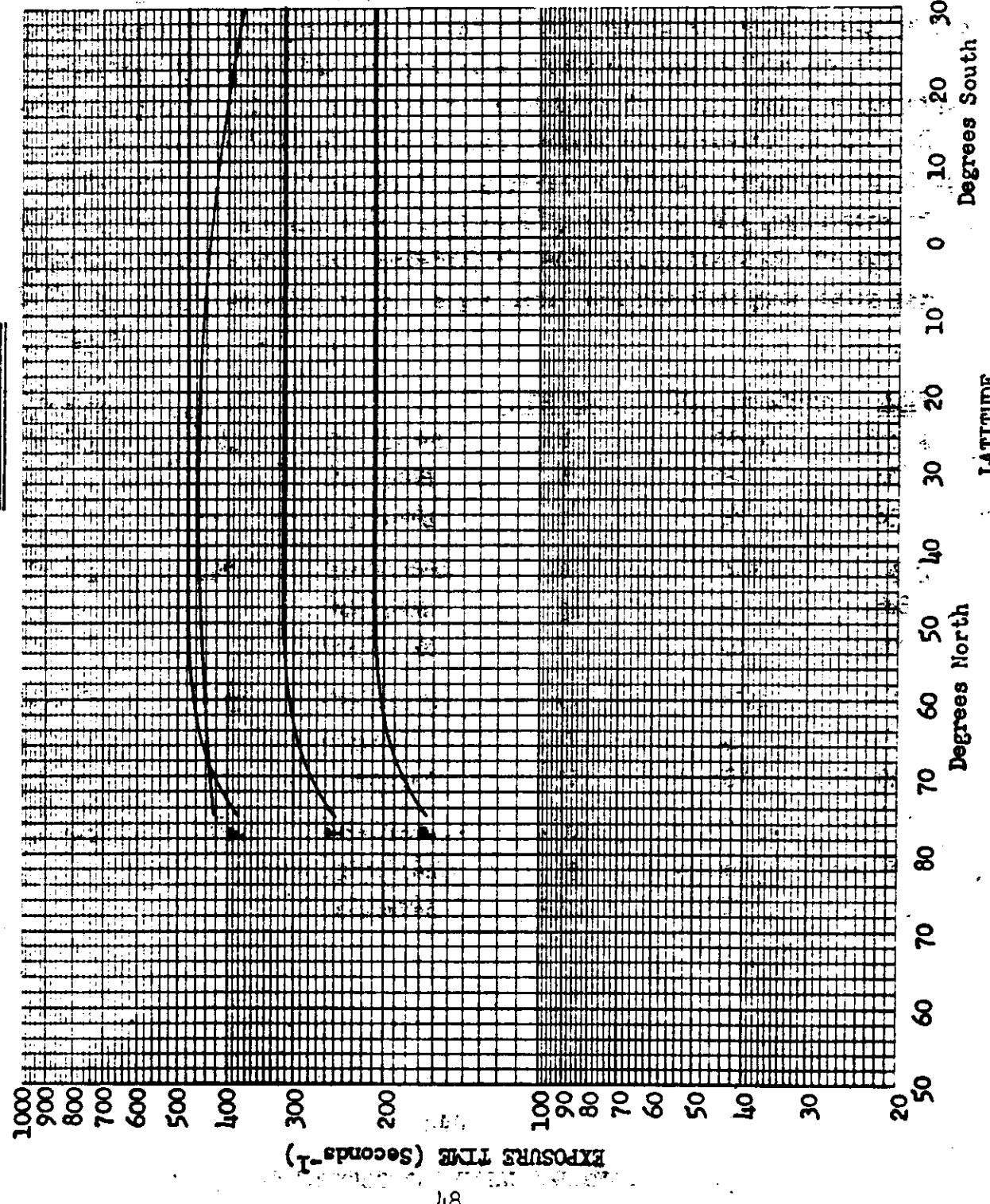


FIGURE 8-11

TOP SECRET C [REDACTED]

TOP SECRET  
NO.

EXPOSURE POINTS



## SECTION 9

## DIFFUSE DENSITY MEASUREMENTS

The diffuse density measurements made by AFSPPF were computer sorted at A/P to permit analysis of the density ranges encountered at the three processing levels. A study of sorting techniques showed that no absolute method was available to separate the density values as the accuracy of the Processing History published by [REDACTED] appears rather low and processing transition phases are not accounted for. The sorting technique selected uses the base plus fog density values where measurements up to 0.09 density are considered as having received Primary processing 0.10 to 0.17 as Intermediate and above 0.17 density as Full. The percentage of original negative that was processed at each level, based on the computer sort, is tabulated below with the predicted and reported processing percentages.

<u>Mission</u>	<u>Camera</u>		<u>Primary</u>	<u>Intermediate</u>	<u>Full</u>
1036-1	FWD	Predicted	0	66.4	33.6
		Reported	8	14	78
		Computed	1	14	85
1036-1	AFT	Predicted	0	4.7	95.3
		Reported	3	9	88
		Computed	0	10	90
1036-2	FWD	Predicted	0	15.1	84.9
		Reported	1	19	80
		Computed	0	18	82
1036-2	AFT	Predicted	0	3.5	96.5
		Reported	3	20	77
		Computed	0	17	83

The tabulations of density frequency distributions for Missions 1036-1 and 1036-2 are included in Appendix A, Table A-1 thru A-4. The graphical presentation of the density distribution are computer plotted in Appendix A, Figures A-1 thru A-39.

A summary of the processing and exposure analysis is shown in Table 9-1. The terrain D-Min criteria, (range) for proper exposure and processing is 0.40 to 0.90 density units. The area measured for D-Min is selected subjectively and is not necessarily the absolute D-Min in the photography.

A density range chart Figure 9-1 is included in this report. This type of chart for Missions 1004 to 1031 is included in the A/P final report for Mission 1031..

These charts are produced from the same density measurements previously mentioned in this section. The computer produced the mean, median and range figures for the various processing levels used. The chart includes the number of frames (samples) in which the density measurements were made. These measurements are made on approximately every tenth frame throughout the mission.

# J MISSION DENSITY RANGES

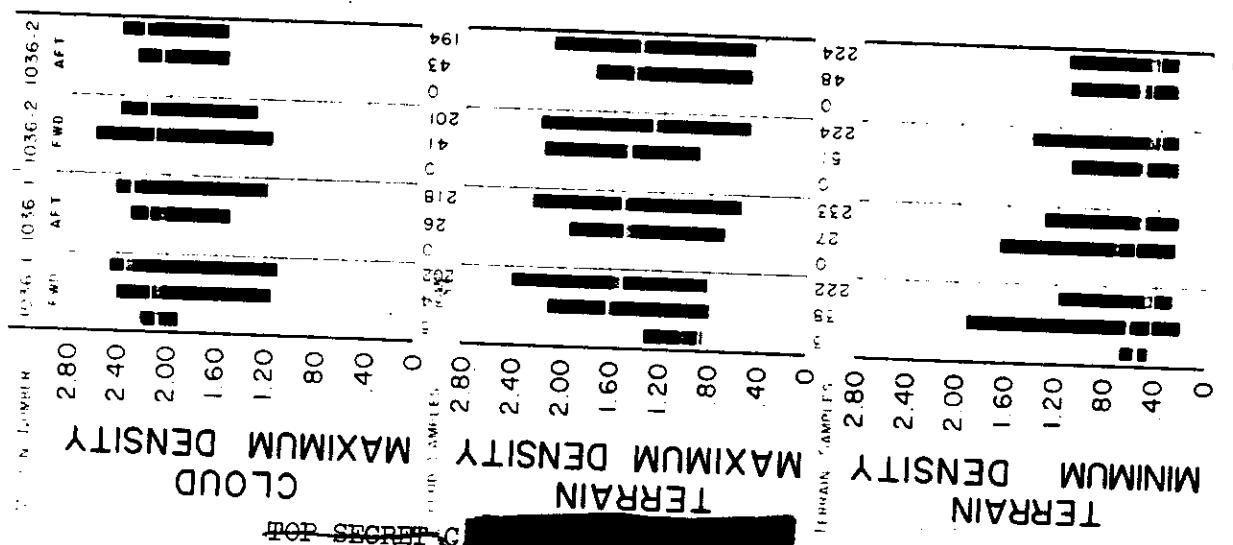


FIGURE 9-1

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C/ [REDACTED] NO. [REDACTED]

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TOP SECRET

CONTROL NO.

MISSION 1036-1 INSTR - FRWD 11/28/66

PROCESS LEVEL SAMPLE SIZE UNDER EXPOSED PROCESSED CORRECT EXP+PROC OVER PROCESSED OVER EXPOSED

PRIMARY 3 0 PC 0 PC 100 PC 0 PC 0 PC  
INTERMEDIATE 38 5 PC 34 PC 39 PC 13 PC 8 PC  
FULL 222 38 PC 30 PC 61 PC 0 PC 0 PC  
ALL LEVELS 263 33 PC 5 PC 59 PC 2 PC 1 PC

MISSION 1036-1 INSTR - AFT 11/28/66

PROCESS LEVEL SAMPLE SIZE UNDER EXPOSED PROCESSED CORRECT EXP+PROC OVER PROCESSED OVER EXPOSED

PRIMARY 0 0 PC 0 PC 19 PC 0 PC 0 PC  
INTERMEDIATE 27 0 PC 14 PC 52 PC 26 PC 4 PC  
FULL 233 14 PC 0 PC 83 PC 3 PC 0 PC  
ALL LEVELS 260 12 PC 2 PC 80 PC 5 PC 0 PC

MISSION 1036-2 INSTR - FRWD 11/28/66

PROCESS LEVEL SAMPLE SIZE UNDER EXPOSED PROCESSED CORRECT EXP+PROC OVER PROCESSED OVER EXPOSED

PRIMARY 0 0 PC 0 PC 33 PC 0 PC 0 PC  
INTERMEDIATE 51 0 PC 46 PC 61 PC 6 PC 0 PC  
FULL 224 38 PC 6 PC 51 PC 3 PC 0 PC  
ALL LEVELS 275 38 PC 6 PC 53 PC 3 PC 0 PC

MISSION 1036-2 INSTR - AFT 11/28/66

PROCESS LEVEL SAMPLE SIZE UNDER EXPOSED PROCESSED CORRECT EXP+PROC OVER PROCESSED OVER EXPOSED

PRIMARY 0 0 PC 0 PC 25 PC 0 PC 0 PC  
INTERMEDIATE 48 0 PC 34 PC 65 PC 10 PC 0 PC  
FULL 224 28 PC 4 PC 63 PC 2 PC 0 PC  
ALL LEVELS 272 28 PC 4 PC 64 PC 4 PC 0 PC

PROCESS LEVEL BASE + FOG UNDER EXPOSED PROCESSED CORRECT EXP+PROC OVER PROCESSED OVER EXPOSED

PRIMARY 0.01-0.09 0.01-0.13 0.14-0.39 0.40-0.90 ----- 0.91 AND UP  
INTERMED 0.10-0.17 0.01-0.20 0.21-0.39 0.40-0.90 0.91-1.34 1.35 AND UP  
FULL 0.1A AND UP 0.01-0.39 0.40-0.90 0.40-0.90 0.91-1.69 1.70 AND UP

TOP SECRET

CONTROL NO.

TABLE 9-1

C/ [REDACTED] NO. [REDACTED]

## SECTION 10

## PERFORMANCE MEASUREMENTS

The photography acquired by both panoramic cameras during Missions 1036-1 and 1036-2 received a MIP rating of 85. A summary is tabulated below of the MTF/AIM resolution values measured by AFSPPF and reported in cycles/mm. The microdensitometer slit used was 1 micron by .80 microns.

<u>Mission</u>	<u>Camera</u>	<u>Cycles/mm</u>	<u>Avg.</u>	<u>Ground Resolution</u>
1036-1	FWD	89		
			81	15.4'
1036-2	FWD	73		
1036-1	APT	94		
			89	13.9'
1036-2	APT	84		

The details of the measurement and computing techniques, targets measured and target locations are fully reported in the evaluation report published by AFSPPF and are not included in this report. These values were determined by using the "Interim MTF/AIM Program" technique.

## SECTION 11

## MISSION 1036-1 STELLAR-INDEX CAMERA

## A. COMPONENT ASSIGNMENT

<u>Component</u>	<u>Serial Number</u>
Camera	D-89
Index Reseau	110
Stellar Reseau	111

## B. CAMERA DATA AND FLIGHT SETTINGS

## Stellar Camera:

Lens	85 mm f/1.8
Exposure Time	2 seconds
Filter Type	None
Film Type	Eastman Type 3401

## Index Camera:

Lens	38 mm f/4.5
Exposure Time	1/500 second
Filter Type	Wratten 21
Film Type	Eastman Type 3400

## C. POST FLIGHT EVALUATION

The Stellar/Index film recovered consisted of 415 frames of photography from each film path of S/I D-89-110-111. Stellar frames 4, 7, 9, and 93 contained minus density streaks termed jettisoned fuel particles in previous reports. Stellar images are present in all frames of photography. Approximately 10 star images appear in each frame at the beginning of Mission 1036-1 and gradually increase in number until approximately 20 stars are present at the end of Mission 1036-1. Most stellar images appear as points rather than the odd shaped marks observed on most previous missions. Point imagery is attributed to a chance condition of the Master and Slave camera being dynamically balanced during the stellar shutter open time of 2 seconds.

C/ [REDACTED] NO. [REDACTED]

The base plus fog level of the stellar film was unusually high at an average value of 0.54. The Normal base plus fog level from previous missions is approximately 0.2. The unusually high base plus fog level caused the loss of all reseau imagery. The uniform high fog level is attributed to viscous processing used for the first time to develop stellar photography one stop more than the usual "full" level. Normally full processed type 3401 stellar film has an E.I. of approximately 64. One additional stop of processing would produce an E.I. of approximately 128. Processing was reported in control. The film manufacturer has postulated that something in the flight environment (possibly temperature) has caused the stellar film to be sensitive to viscous processor chemical fogging. Future corrective action will consist of a reduction in viscous processing by approximately one stop in order to reduce the base plus fog level to an acceptable level. The type 3401 film in the radiation pack that flew in SRV #1 was not fogged and has a normal base plus fog level of 0.15. The radiation film pack was processed by A/P. In flight temperatures of Mission 1036 were in control and comparable to recent previous missions.

The index camera reseau edge was imaged on a small portion of terrain imagery in each corner of index photography. Degradation of terrain imagery was small. Insufficient masking of the index camera reseau plate was attributed as the cause of reseau edge exposure. Reseau masking procedures at Boston will be investigated and corrective action taken to prevent recurrence of this problem in the future.

## SECTION 12

## MISSION 1036-2 STELLAR-INDEX CAMERA

## A. COMPONENT ASSIGNMENT

<u>Component</u>	<u>Serial Number</u>
Camera	D-88
Index Reseau	108
Stellar Reseau	106

## B. CAMERA DATA AND FLIGHT SETTINGS

## Stellar Camera:

Lens	85 mm f/1.8
Exposure Time	1 second
Filter Type	None
Film Type	Eastman Type 3401

## Index Camera:

Lens	38 mm f/4.5
Exposure Time	1/500 second
Filter Type	Wratten 21
Film Type	Eastman Type 3400

**C. POST FLIGHT EVALUATION**

S/I #D-88/108/106 operated normally throughout Mission 1036-2. The stellar and index cameras each produced 432 frames of photography. Stellar film base plus fog level was abnormally high at an average level of 0.60. For discussion of high stellar base plus fog see Section 12C, Paragraph 2.

Approximately 12 stars were recorded in each frame of stellar photography. Baffle flare fog was low.

Continuous plus density marking occurred near the ends of stellar records 1036-1 and 1036-2. This type marking has been observed on previous missions and is attributed to static discharging. Static fog marks occurred outside the active format.

## SECTION 13

## VEHICLE ATTITUDE

The vehicle attitude errors for both Mission 1036-1 and 1036-2 were derived from the reduction of the Stellar camera photography. This attitude data is supplied to A/P by MPIC.

The attitude errors for each frame and the attitude control rates are calculated at the A/P computer facility. The computer also plots the frequency distribution of the rates and errors. Figures 13-1 through 13-6 show these distributions for Mission 1036-1 and Figures 13-7 through 13-12 for Mission 1036-2.

The summary table below lists the maximum attitude errors and rates that were experienced during 90% of the FWD camera photographic operations, excluding the first six frames of each operation, and the total range of the errors and rates.

	Mission 1036-1		Mission 1036-2	
<u>Value</u>	<u>90%</u>	<u>Range</u>	<u>90%</u>	<u>Range</u>
Pitch Error ( $^{\circ}$ )	0.76	-1.30 to +0.25	0.94	-1.40 to +0.35
Roll Error ( $^{\circ}$ )	0.96	+0.22 to +1.32	0.70	-0.12 to +0.98
Yaw Error ( $^{\circ}$ )	0.60	-0.85 to +0.65	0.40	-0.58 to +0.74
Pitch Rate ( $^{\circ}/\text{hr.}$ )	31.20	-54 to +64	33.00	-72 to +52
Roll Rate ( $^{\circ}/\text{hr.}$ )	25.59	-80 to +95	29.72	-85 to +55
Yaw Rate ( $^{\circ}/\text{hr.}$ )	29.51	-70 to +58	23.33	-50 to +80

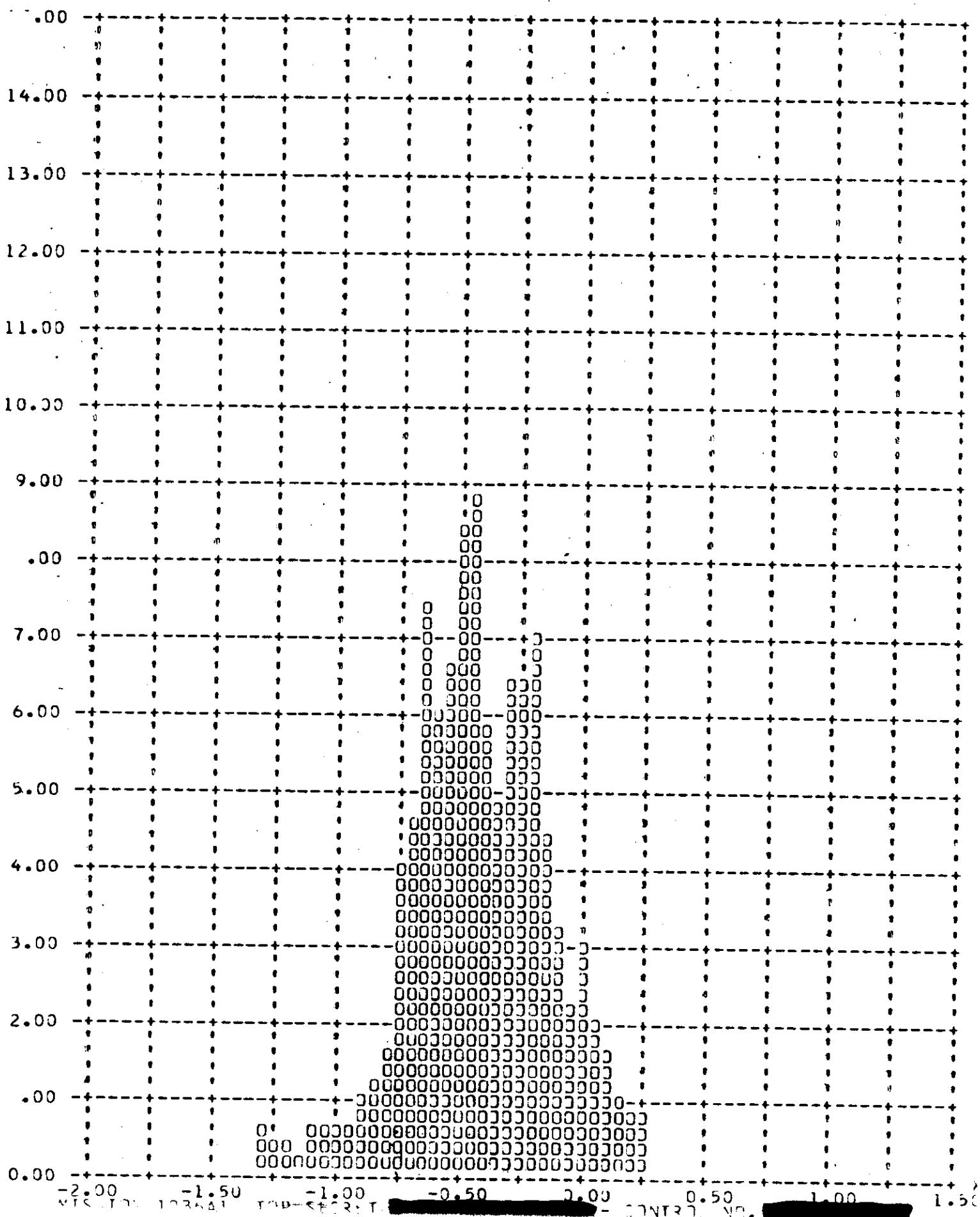
The performance of the attitude control system is comparable to the control systems used on recent missions. The panoramic photography was not degraded by the attitude control system.

MISSION 1036A1 TOP SECRET

- CONTROL NO.

FRAMES 1-6 OF EACH OP OMITTED 90 PERCENT = 0.76

Y PITCH ANGLE ERROR - DEGREES (X) VERSUS FREQUENCY - PERCENT (Y)

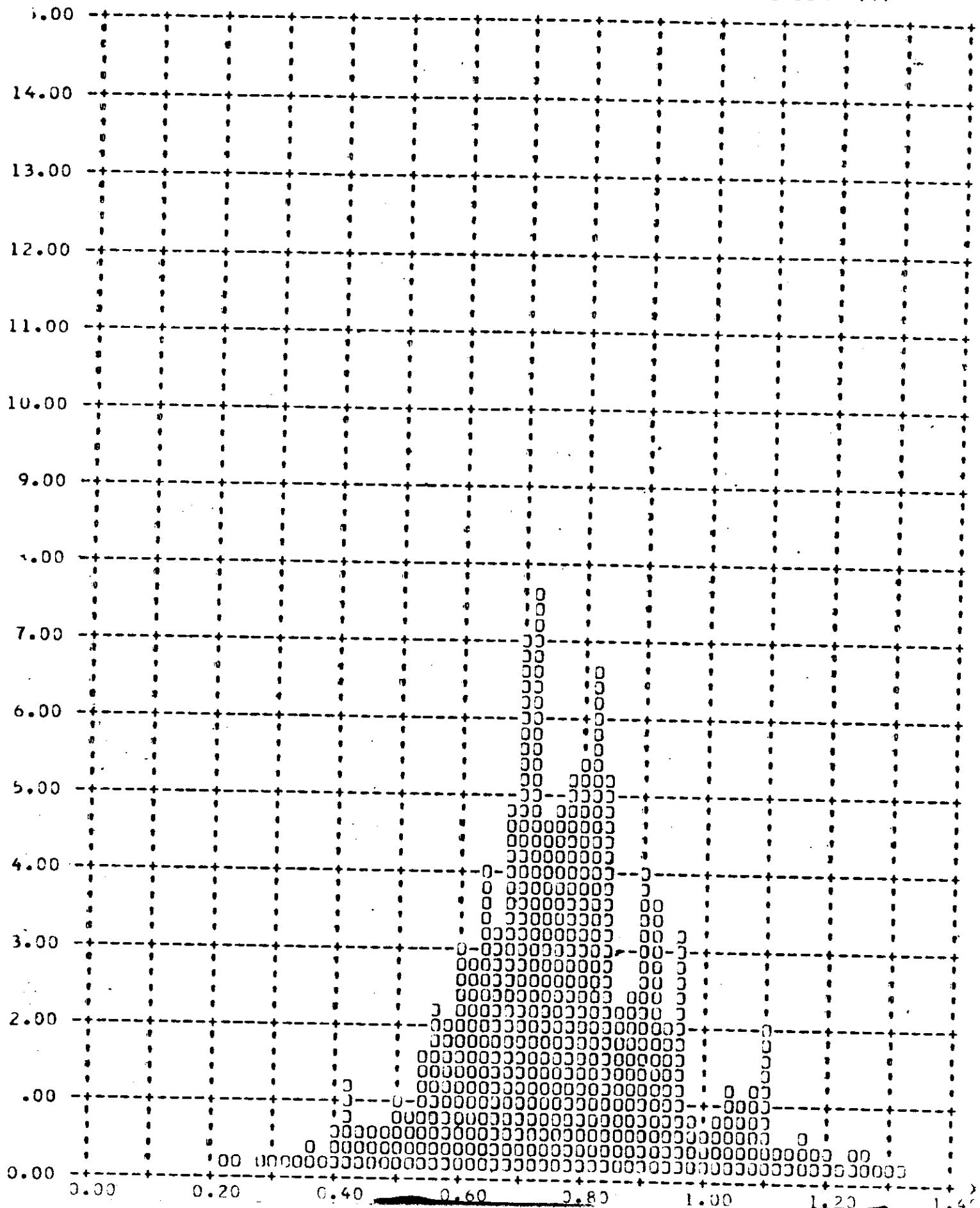


NFC 1036A1 TDB-REF T

- CONTROL NO.

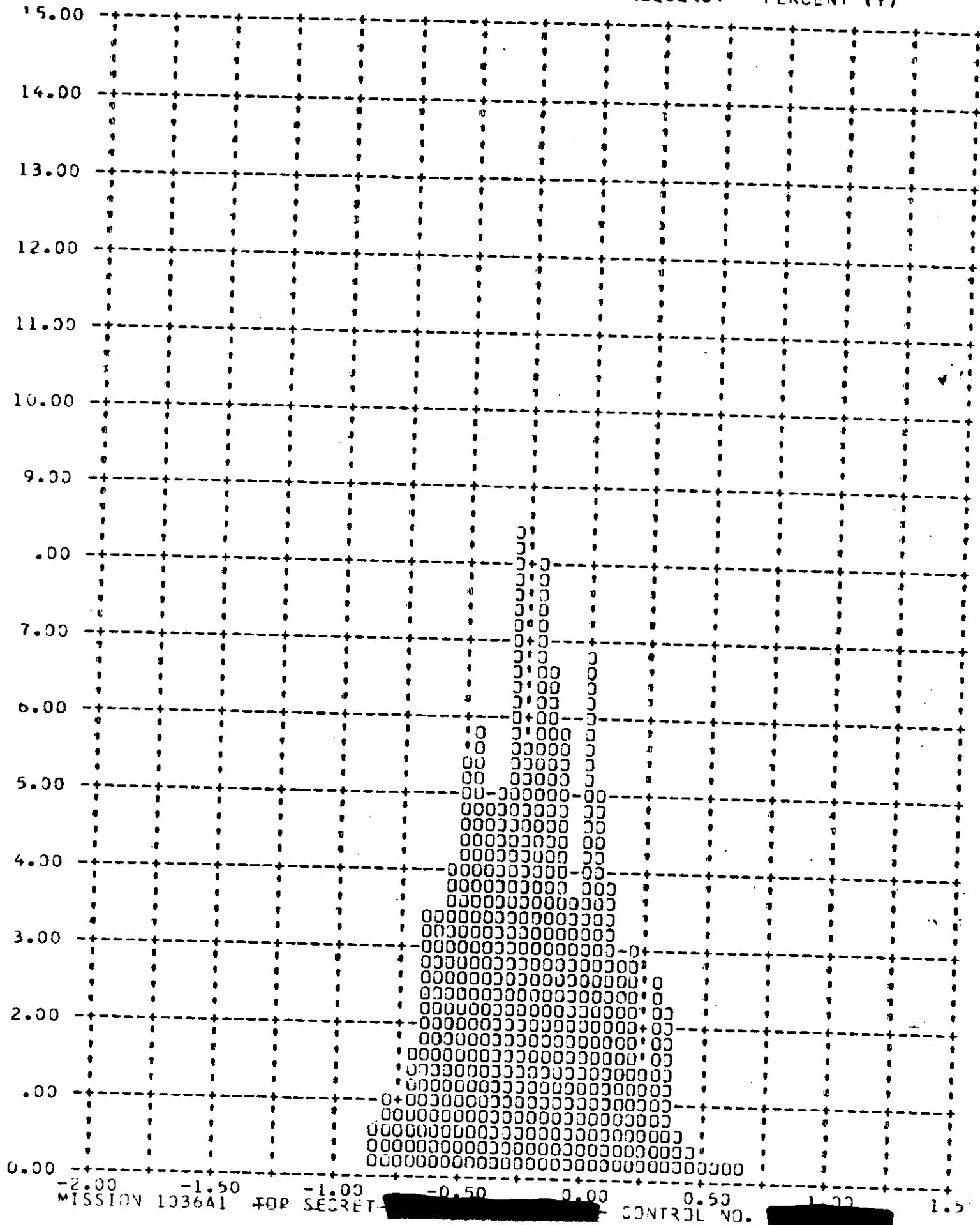
FRAMES 1-6 OF EACH OP OMITTED 90 PERCENT = 0.96

Y ROLL ANGLE ERROR - DEGREES (X) VERSUS FREQUENCY - PERCENT (Y)



FRAMES 1-6 OF EACH OP OMITTED 90 PERCENT = 0.63

## Y YAW ANGLE ERROR - DEGREES (X) VERSUS FREQUENCY - PERCENT (Y)



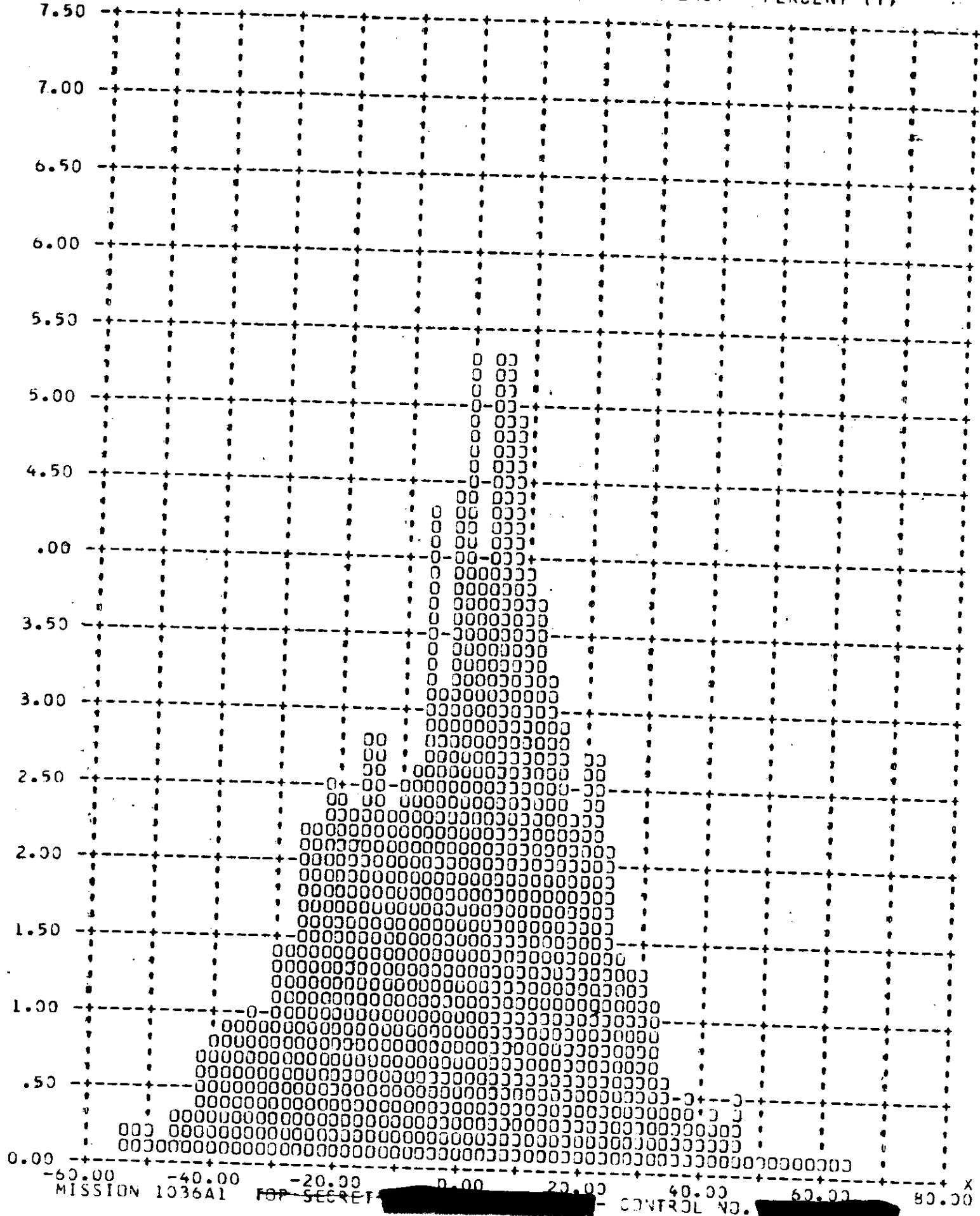
MISSION 1036A1

TOP SECRET

- CONTROL NO.

FRAMES 1-6 OF EACH DP OMITTED 90 PERCENT = 31.20

Y PITCH RATE ERROR - DEG/HOUR (X) VERSUS FREQUENCY - PERCENT (Y)



MISSION 1036A1

TOP SECRET

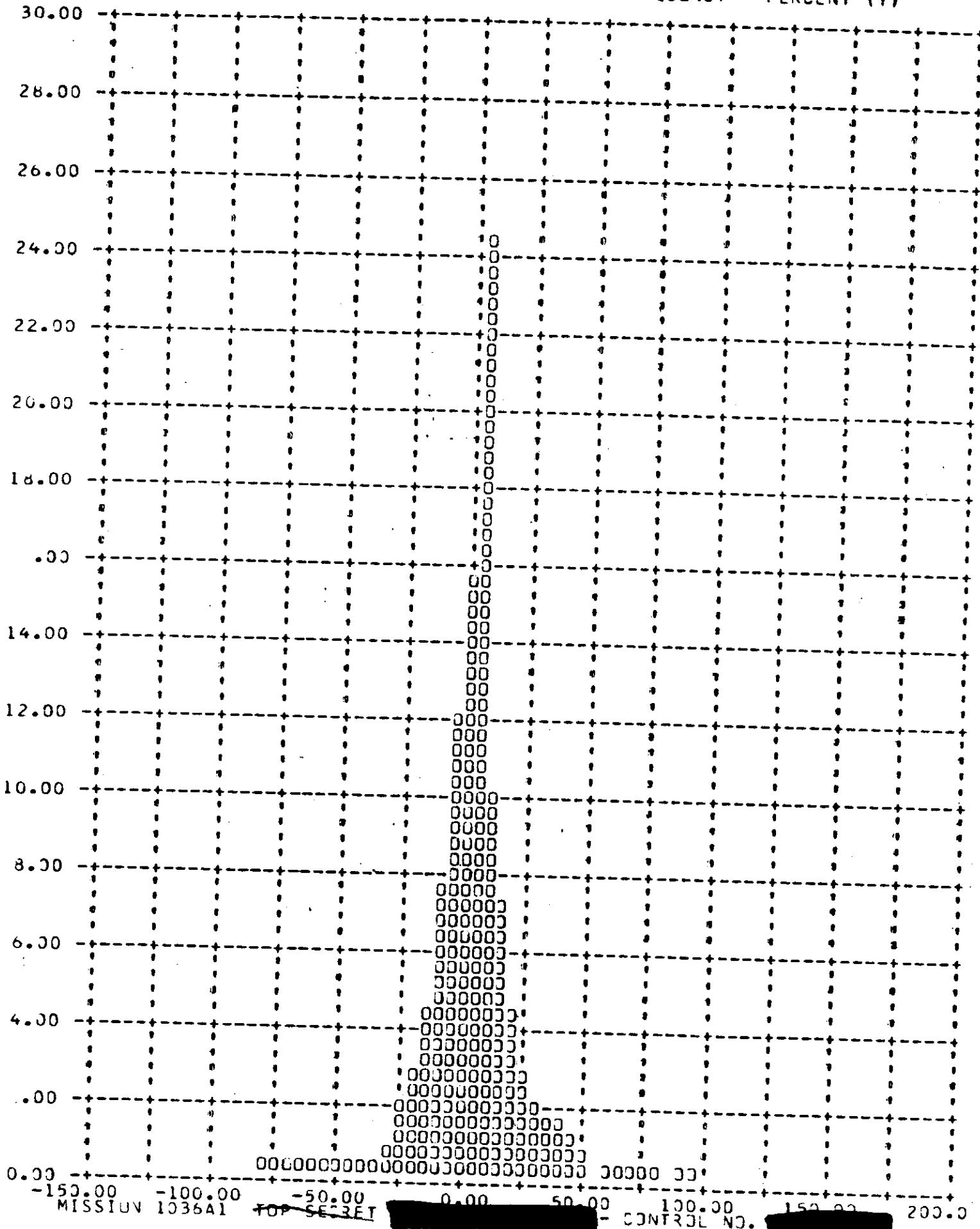
- CONTROL NO.

MISSION 1036A1 TOP SECRET

- CONTROL NO.

FRAMES 1-6 OF EACH OP OMITTED 90 PERCENT = 25.59

## Y ROLL RATE ERROR - DEG/HOUR (X) VERSUS FREQUENCY - PERCENT (Y)



MISSION 1036A1 TOP SECRET

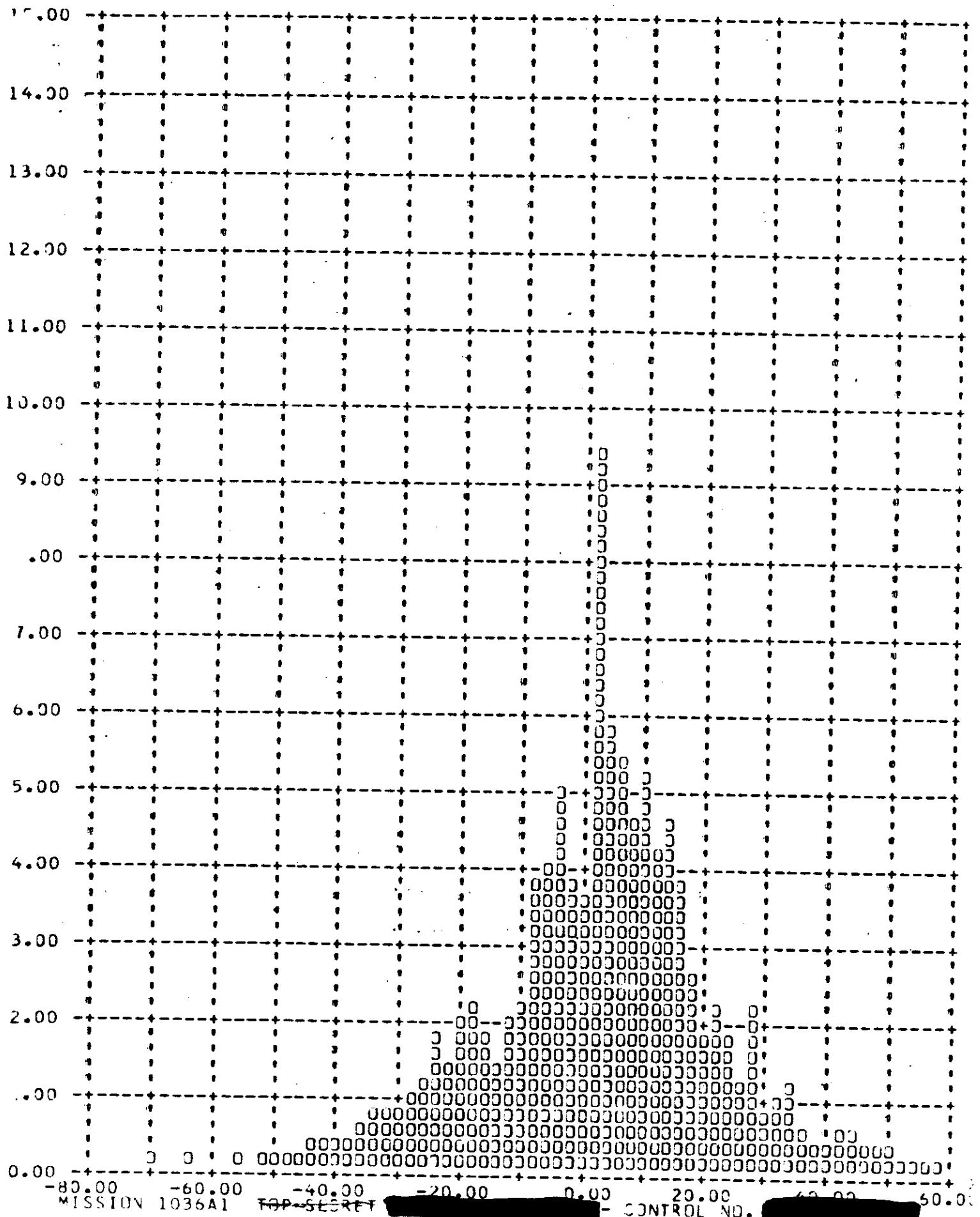
- CONTROL NO.

MISSION 1036A1 ~~TOP SECRET~~

CONTROL NO.

FRAMES 1-6 OF EACH OP OMITTED 90 PERCENT = 29.51

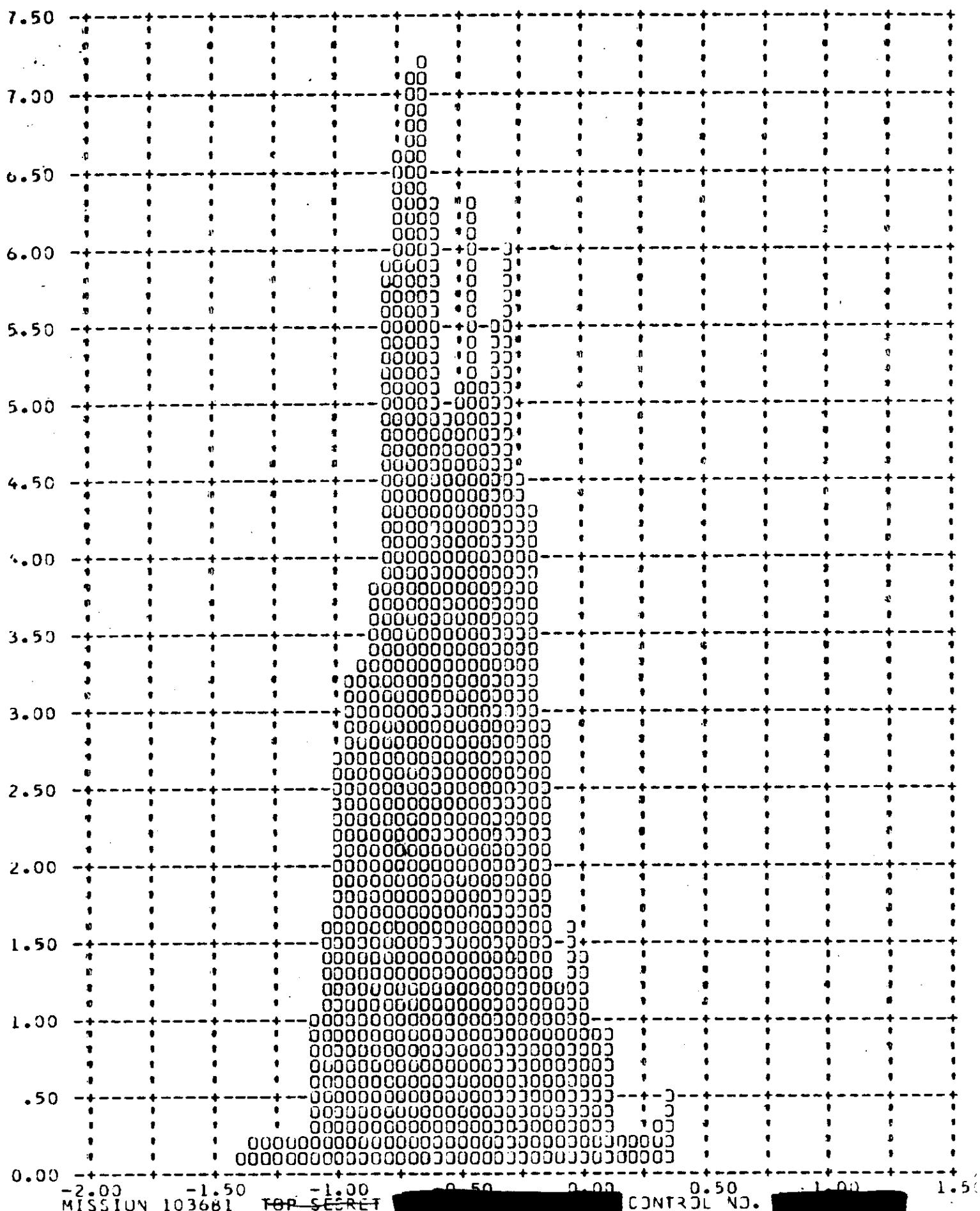
Y YAW RATE ERROR - DEG/HOUR (X) VERSUS FREQUENCY - PERCENT (Y)

MISSION 1036A1 ~~TOP SECRET~~

CONTROL NO.

FRAMES 1-6 OF EACH OP OMITTED 90 PERCENT = 0.94

## Y PITCH ANGLE ERROR - DEGREES (X) VERSUS FREQUENCY - PERCENT (Y)

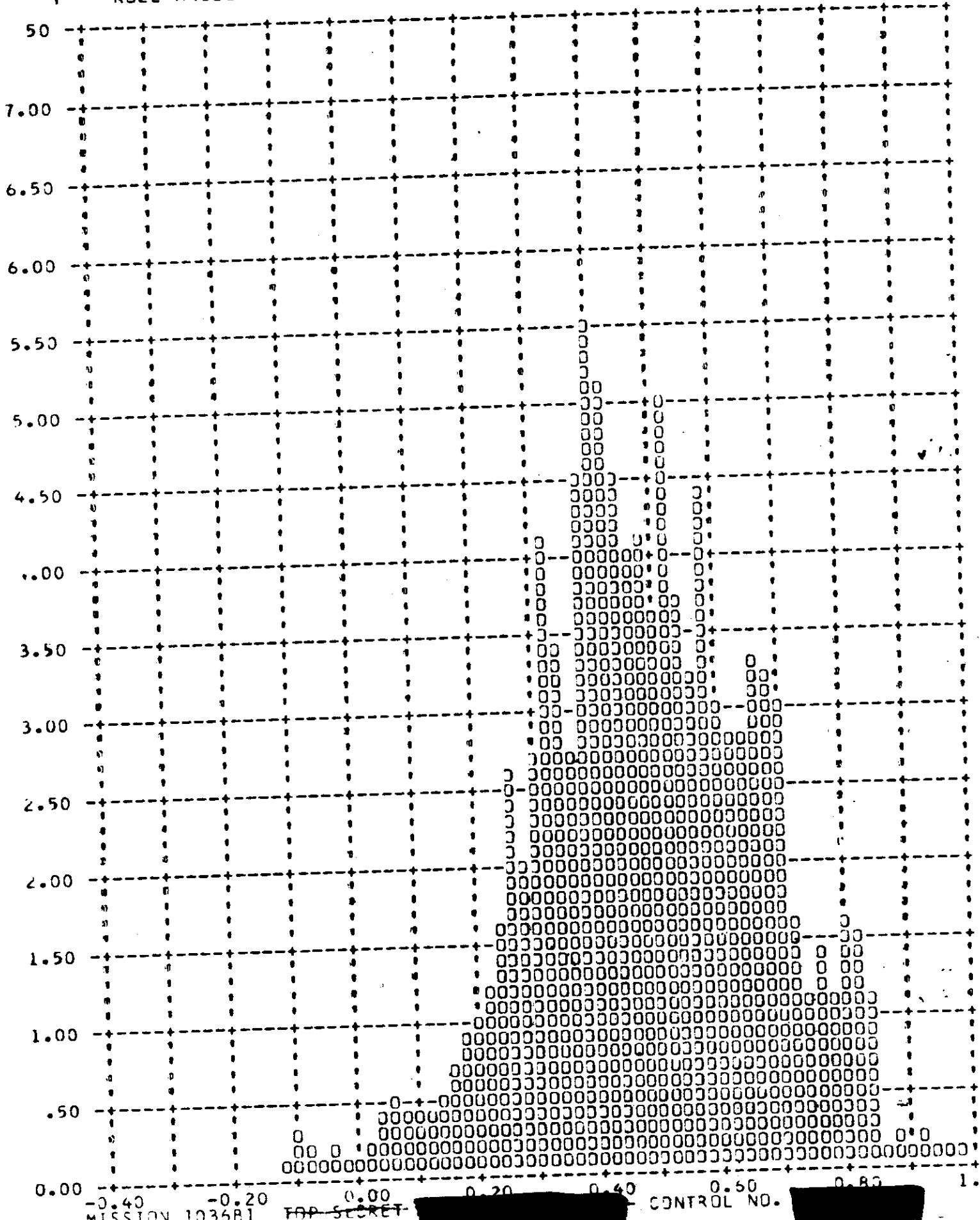


MISSION 1036B1 ~~TOP SECRET~~

- CONTROL NO.

FRAMES 1-6 OF EACH DP OMITTED 90 PERCENT = 0.70

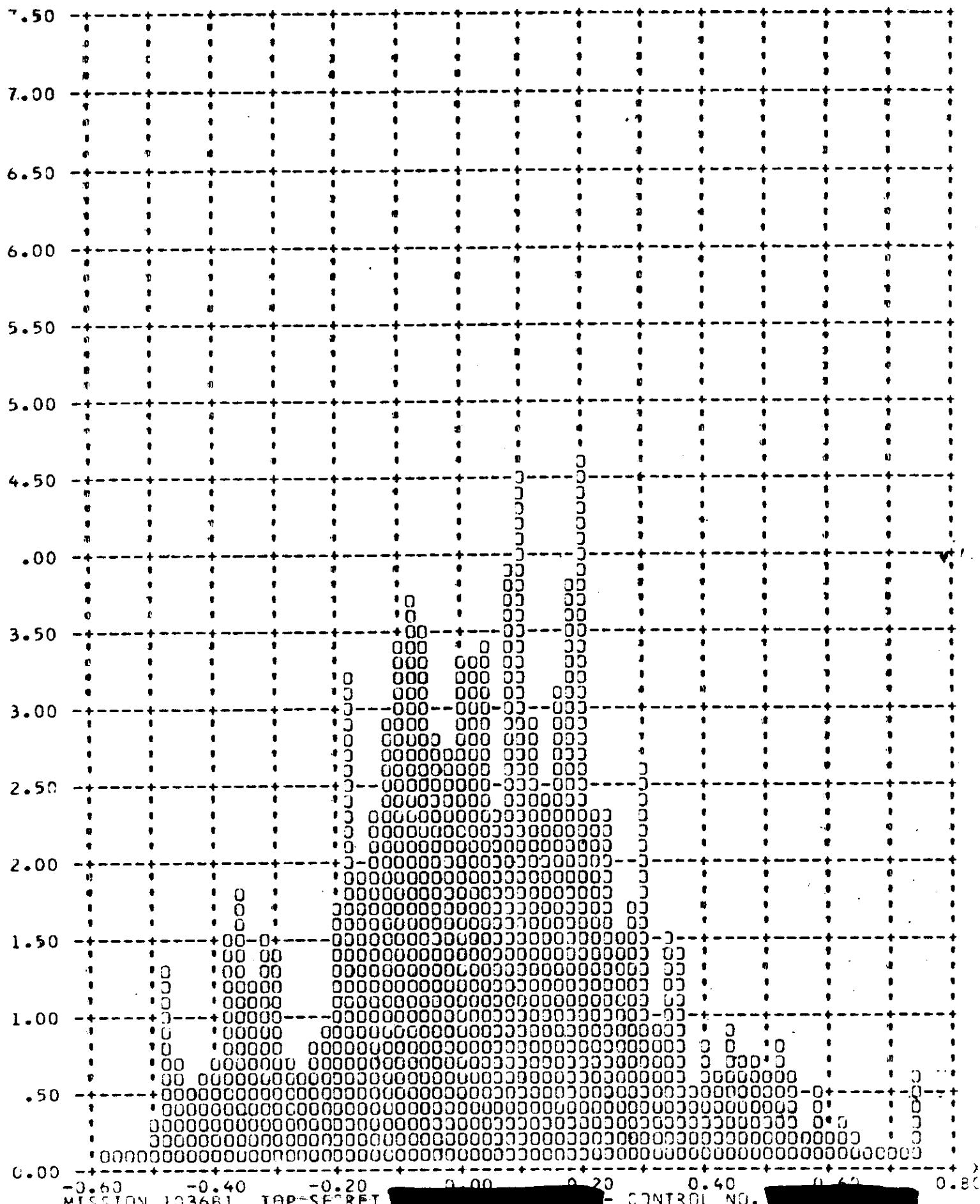
## Y ROLL ANGLE ERROR - DEGREES (X) VERSUS FREQUENCY - PERCENT (Y)

MISSION 1036B1 ~~TOP SECRET~~

- CONTROL NO.

FRAMES 1-6 OF EACH DP DMITTED 90 PERCENT = 0.40

## Y YAW ANGLE ERROR - DEGREES (X) VERSUS FREQUENCY - PERCENT (Y)

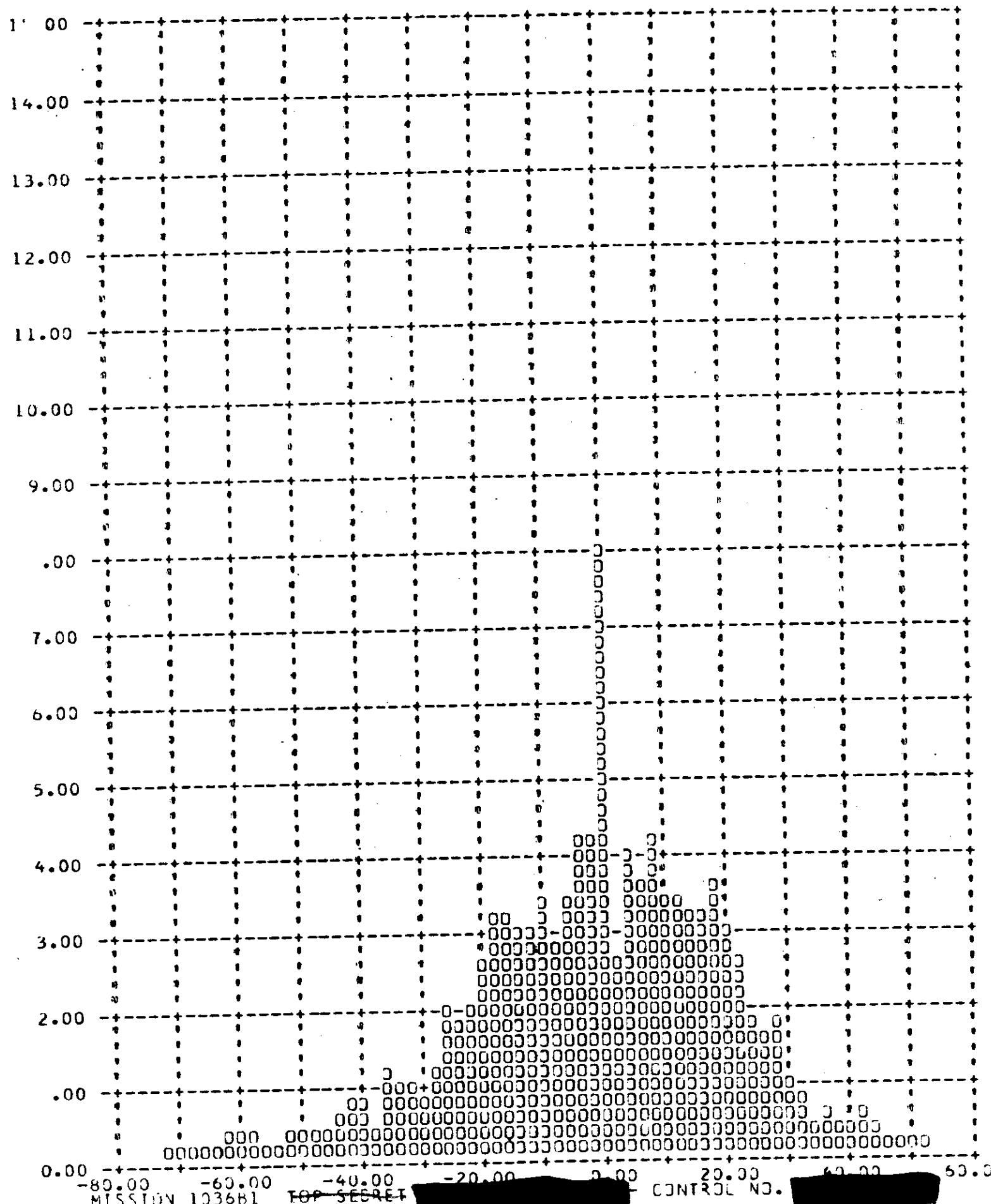


MISSION 103681 ~~TOP SECRET~~

CONTROL NO.

FRAMES 1-6 OF EACH OP OMITTED 90 PERCENT = 33.00

Y PITCH RATE ERROR - DEG/HOUR (X) VERSUS FREQUENCY - PERCENT (Y)

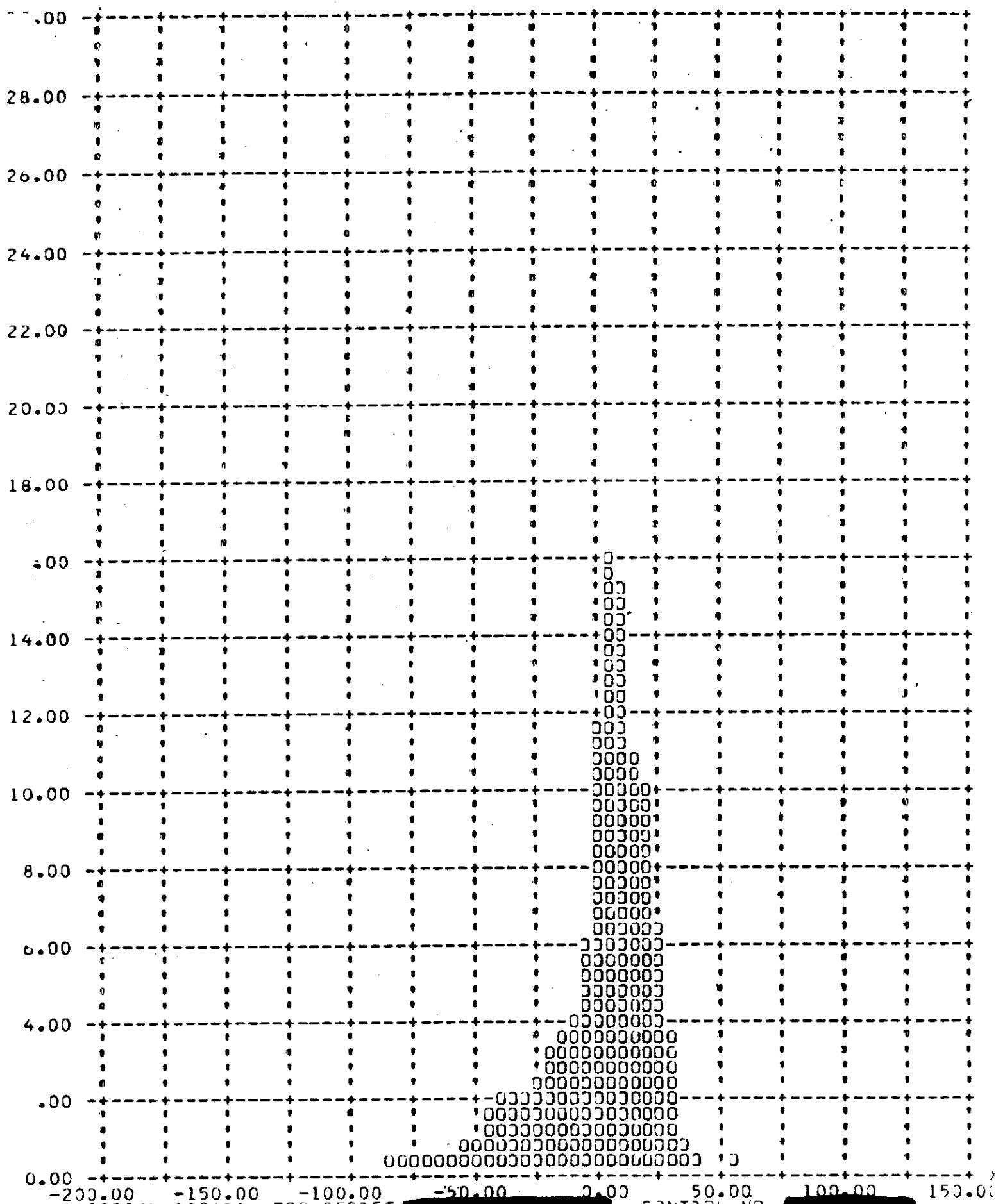


MISSION 103681 ~~TOP SECRET~~

CONTROL NO.

FRAMES 1-6 OF EACH OP OMITTED 90 PERCENT = 29.72

## Y ROLL RATE ERROR - DEG/HOUR (X) VERSUS FREQUENCY - PERCENT (Y)



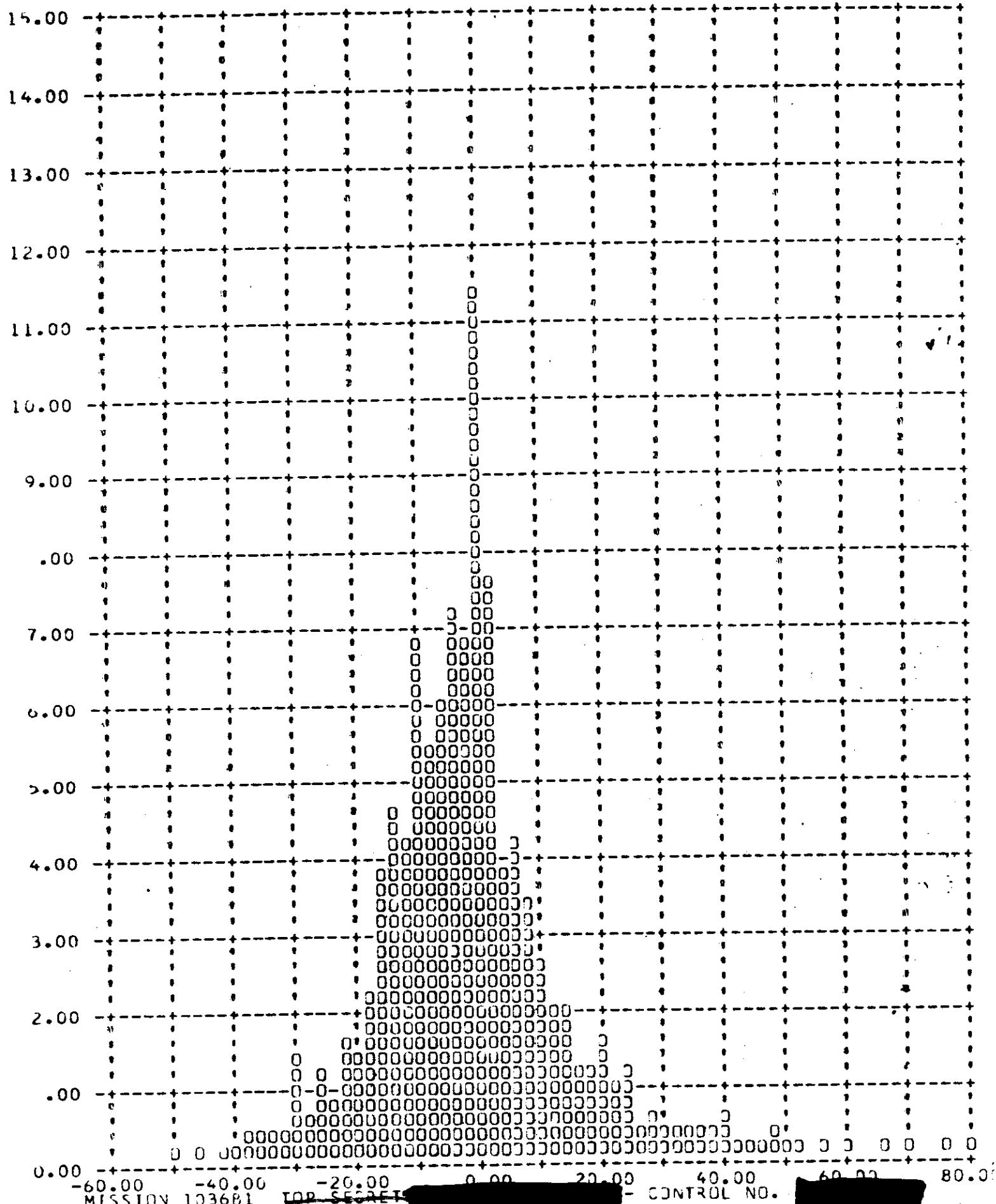
MISSION 103681

TOP SECRET

CONTROL NO.

FRAMES 1-6 OF EACH OP OMITTED 90 PERCENT = 23.33

## Y YAW RATE ERROR - DEG/HOUR (X) VERSUS FREQUENCY - PERCENT (Y)



MISSION 103681

TOP SECRET

CONTROL NO.

~~TOP SECRET~~  
C/ [REDACTED] -30. [REDACTED]  
**SECTION 14**

#### IMAGE SMEAR ANALYSIS

The frame correlation tape supplied to A/P by NFIC contains the binary time word of each frame of photography. A computer program has been assembled at A/P which calculates the exposure time of each frame and compares the camera cycle rate with the ephemeris to calculate the V/h mismatch. This data is combined with the vehicle attitude error and rate values of each frame and the crab error caused by earth rotation at the latitude of each frame. The program outputs the total along track and cross track IMC error and the limit of ground resolution that can be acquired by a camera regardless of focal length and system capabilities.

The computer rejects the first six frames of all operations as the large V/h error induced by camera start-up is not representative of the overall system operations. The frequency distribution of the V/h errors and resolution limits are computer plotted and are shown in Figures 14-1 through 14-12.

The summary table 14-1 presents the maximum V/h ratio errors and resolution limits that existed during 90% of the photographic operations and the total range of values during all operations that were computed.

TOP SECRET

C NO. [REDACTED]

MISSION 1036  
V/H RATIO AND RESOLUTION LIMITS

UNIT	CAMERA	MISSION 1036-1		MISSION 1036-2	
		204	Range	204	Range
v/h Ratio Toler	FWD	3.44	-8.4 to +2.2	3.33	-10.4 to +1.4
	AFT	3.28	-7.6 to +2.0	3.05	-9.2 to +1.0
Along Track Resolution Limit	FWD	5.13	0.2 to 7.4	3.79	0.2 to 9.8
	AFT	3.62	0.2 to 5.4	2.65	0.2 to 6.0
Cross Track Resolution Limit	FWD	6.76	0.2 to 8.6	6.53	0.2 to 8.4
	AFT	5.10	0.2 to 6.4	4.91	0.2 to 6.2

TABLE 14-1

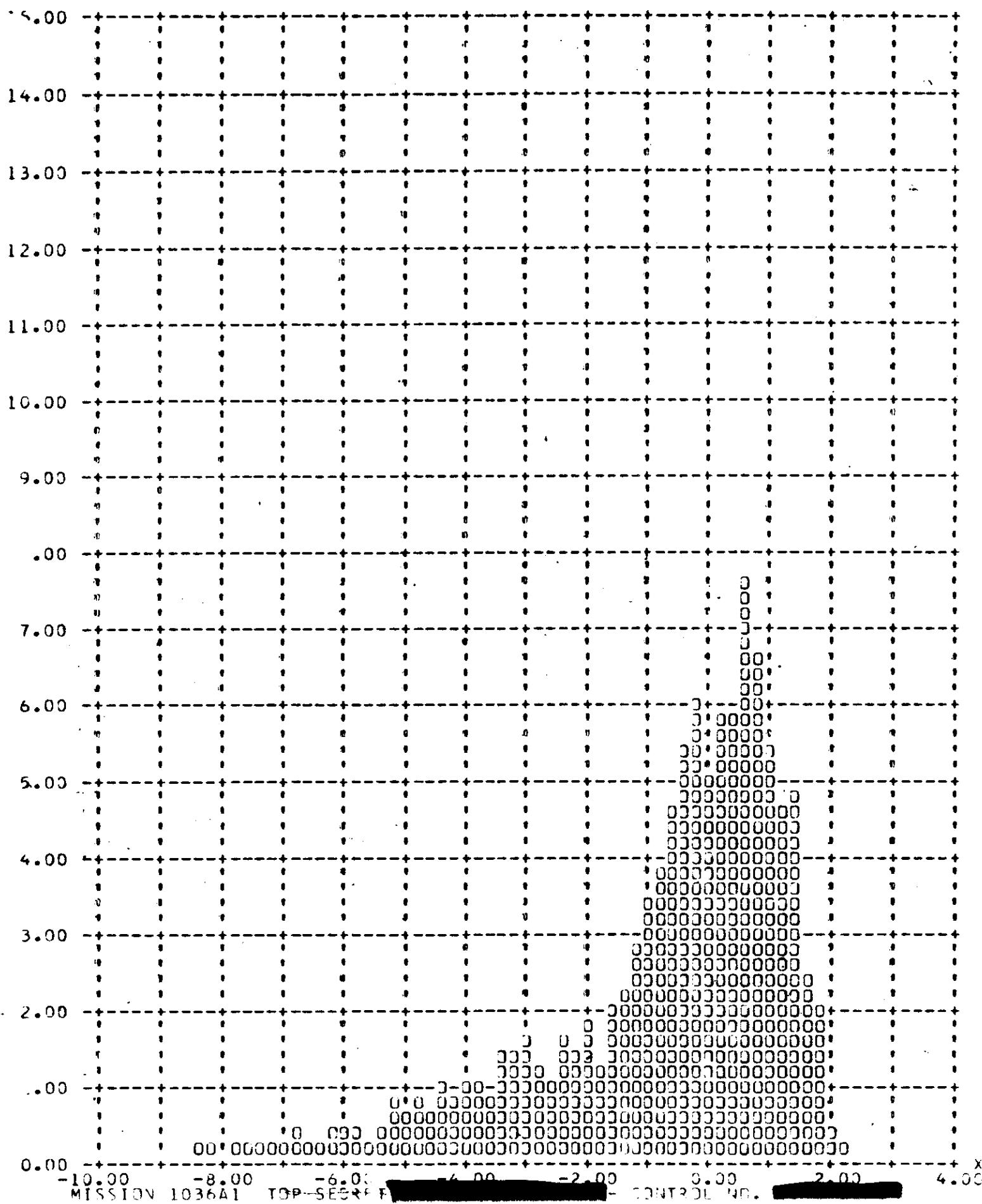
TOP SECRET C

MISSION 1036A1 ~~TOP SECRET~~

- CONTROL NO.

FRAMES 1-6 OF EACH DP OMITTED 90 PERCENT = 3.44

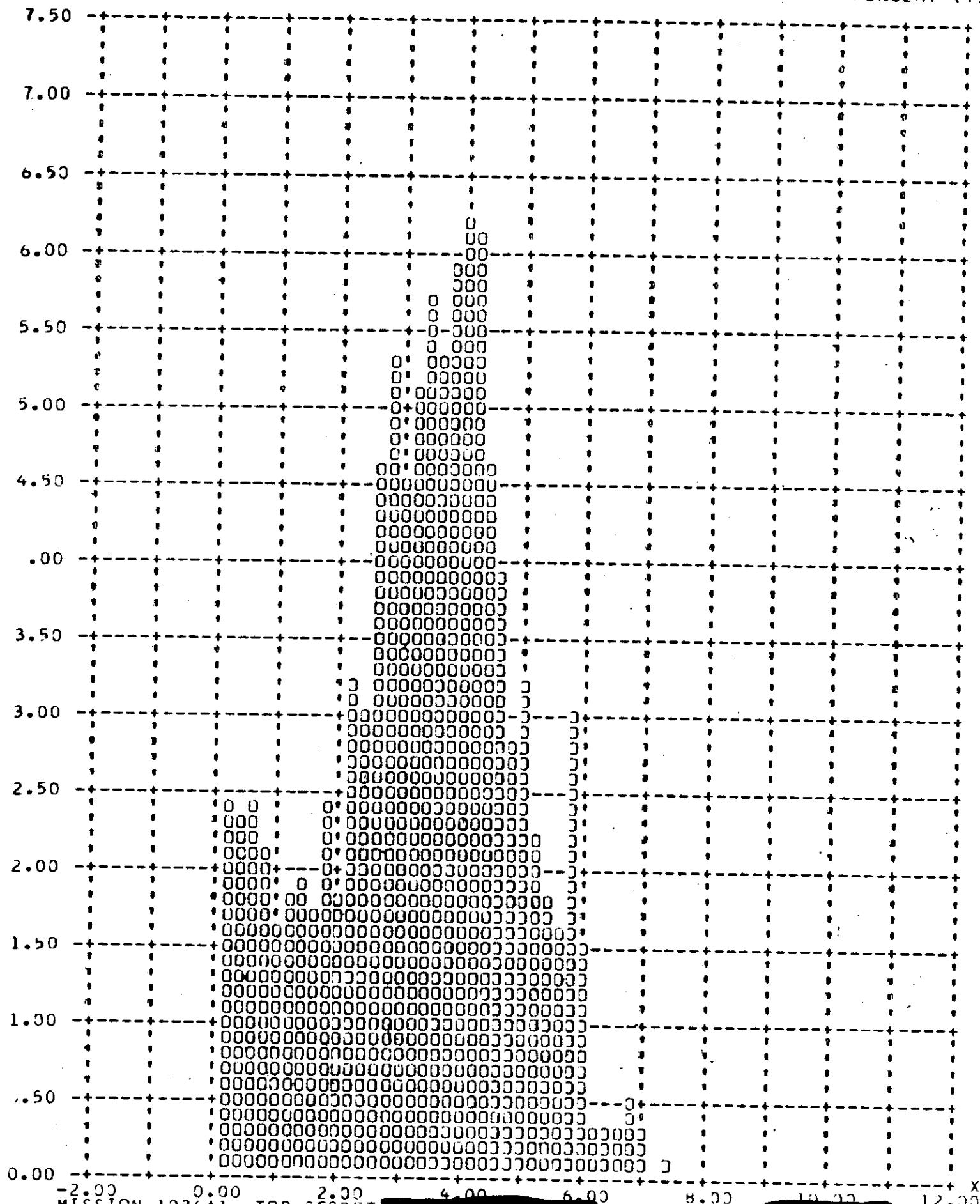
Y V/H RATIO ERROR - PERCENT (X) VERSUS FREQUENCY - PERCENT (Y)

MISSION 1036A1 ~~TOP SECRET~~

- CONTROL NO.

FRAMES 1-6 OF EACH OP OMITTED 90 PERCENT = 5.13

## Y ALONG TRACK RESOLUTION LIMIT - FEET (X) VERSUS FREQUENCY - PERCENT (Y)



FRAMES 1-6 OF EACH OF UNLITTED 90 PERCENT = 6.7

Y CROSS TRACK RESOLUTION LIMIT - FEET (X) VERSUS FREQUENCY - PERCENT (Y)

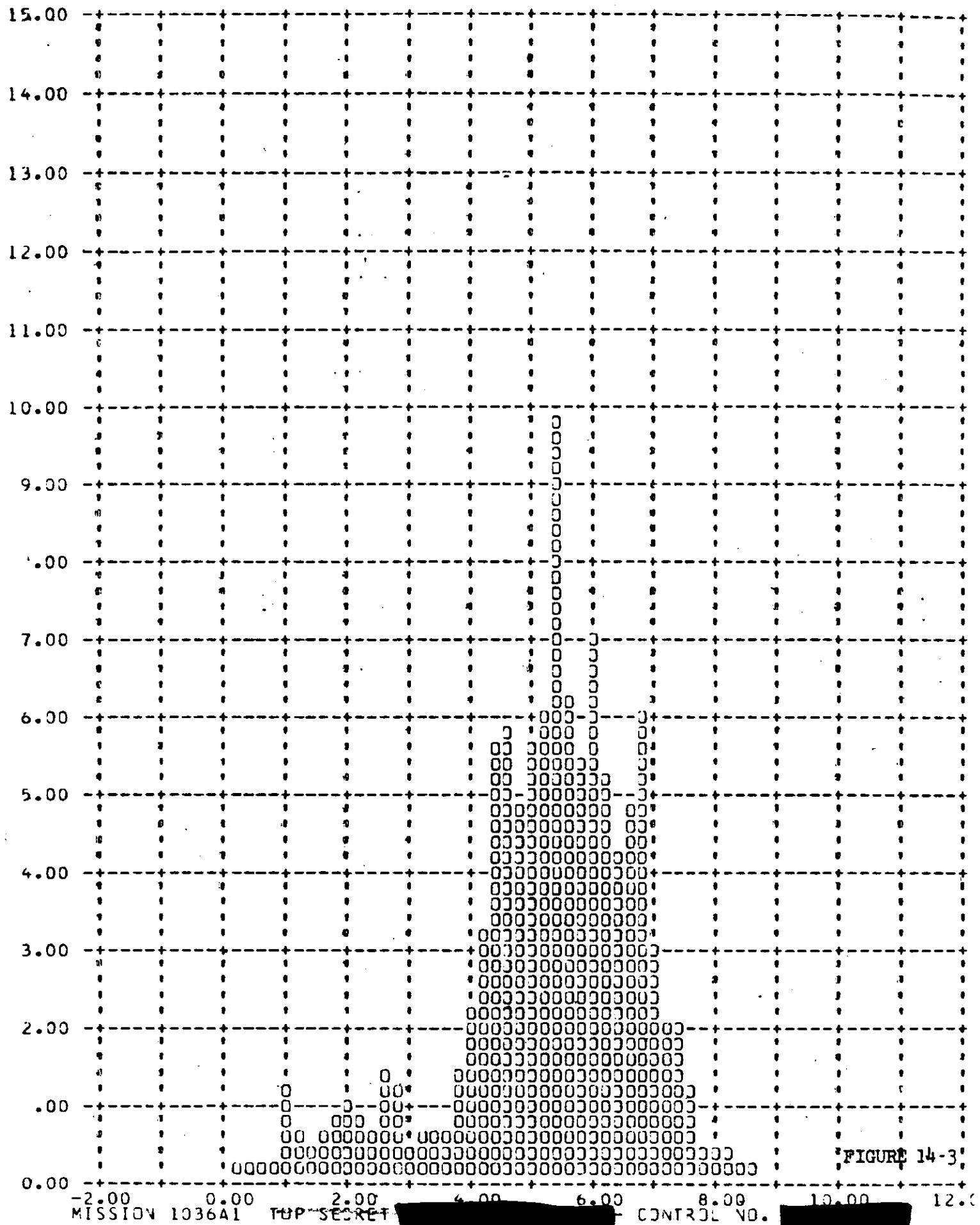


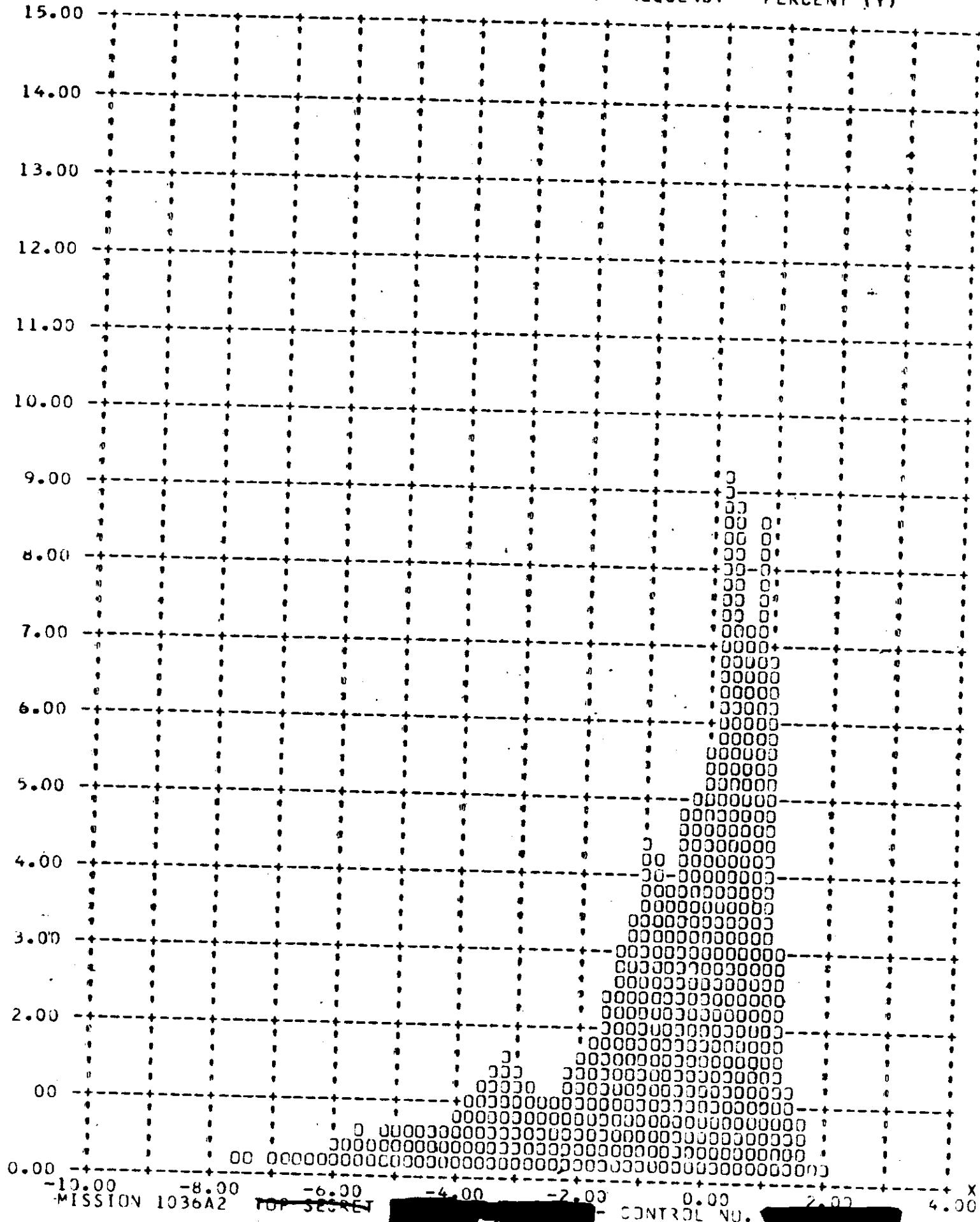
FIGURE 14-3

MISSION 1036A1 TOP SECRET [REDACTED]

CONTROL NO. [REDACTED]

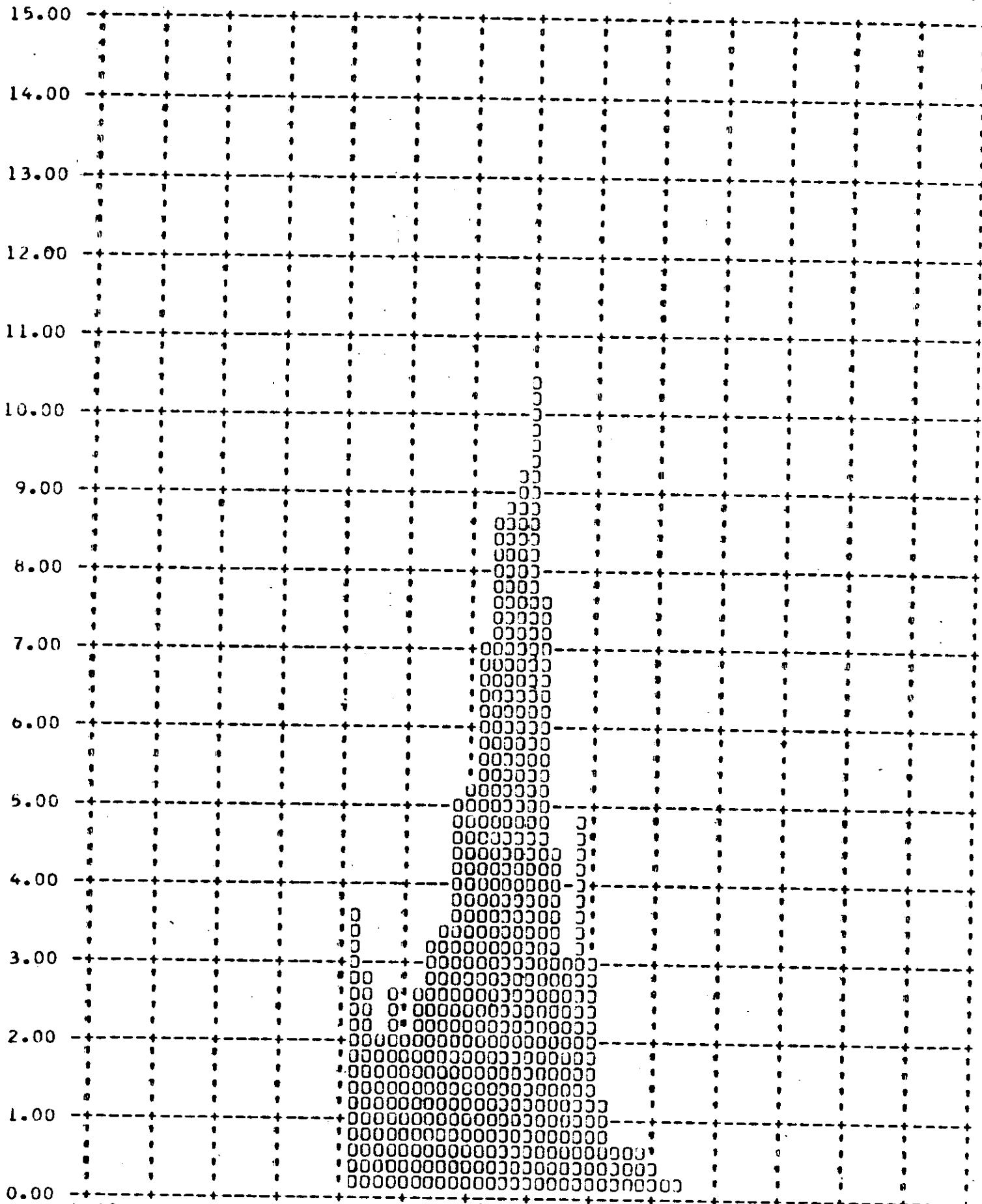
FRAMES 1-6 OF EACH DP OMITTED 90 PERCENT = 3.1

## Y V/H RATIO ERROR - PERCENT (X) VERSUS FREQUENCY - PERCENT (Y)



FRAMES 1-6 OF EACH DP OMITTED 90 PERCENT = 3.0

## Y ALONG TRACK RESOLUTION LIMIT - FEET (X) VERSUS FREQUENCY - PERCENT (%)



FRAMES 1-6 OF EACH OP OMITTED 90 PERCENT = 5.1

Y CROSS TRACK RESOLUTION LIMIT - FEET (X) VERSUS FREQUENCY - PERCENT (Y)

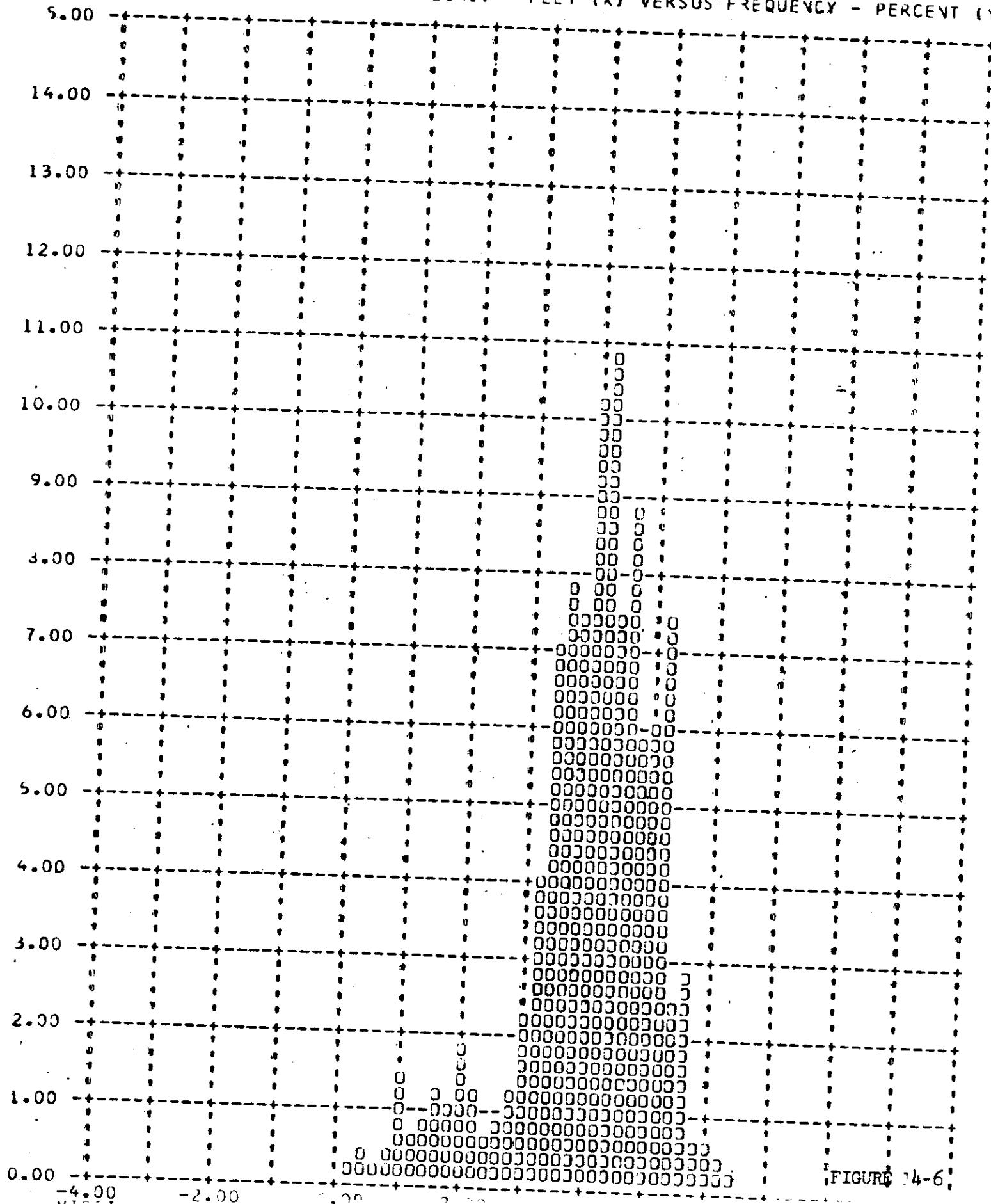
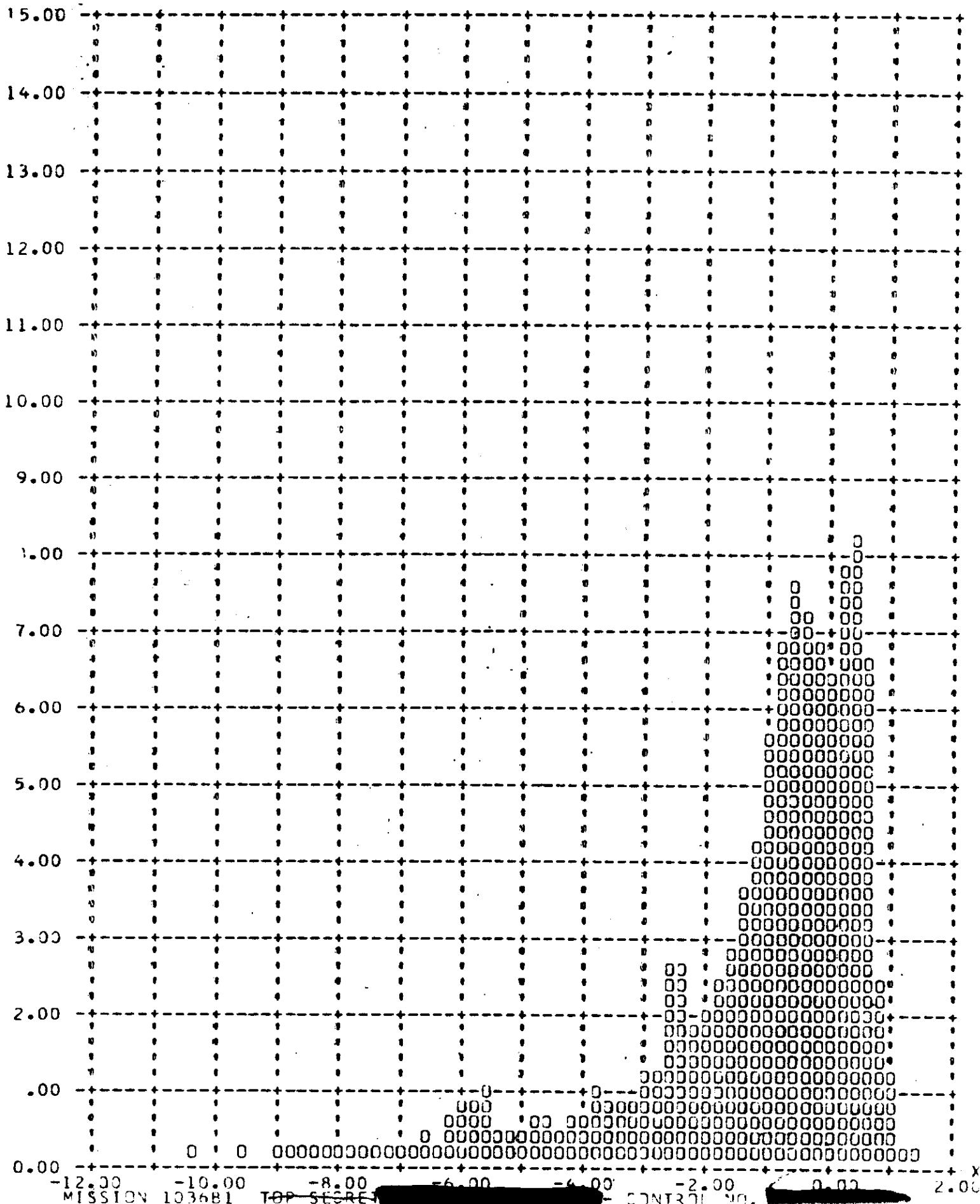


FIGURE 14-6

FRAMES 1-6 OF EACH DP OMITTED 90 PERCENT = 3.33

## Y V/H RATIO ERROR - PERCENT (X) VERSUS FREQUENCY - PERCENT (Y)

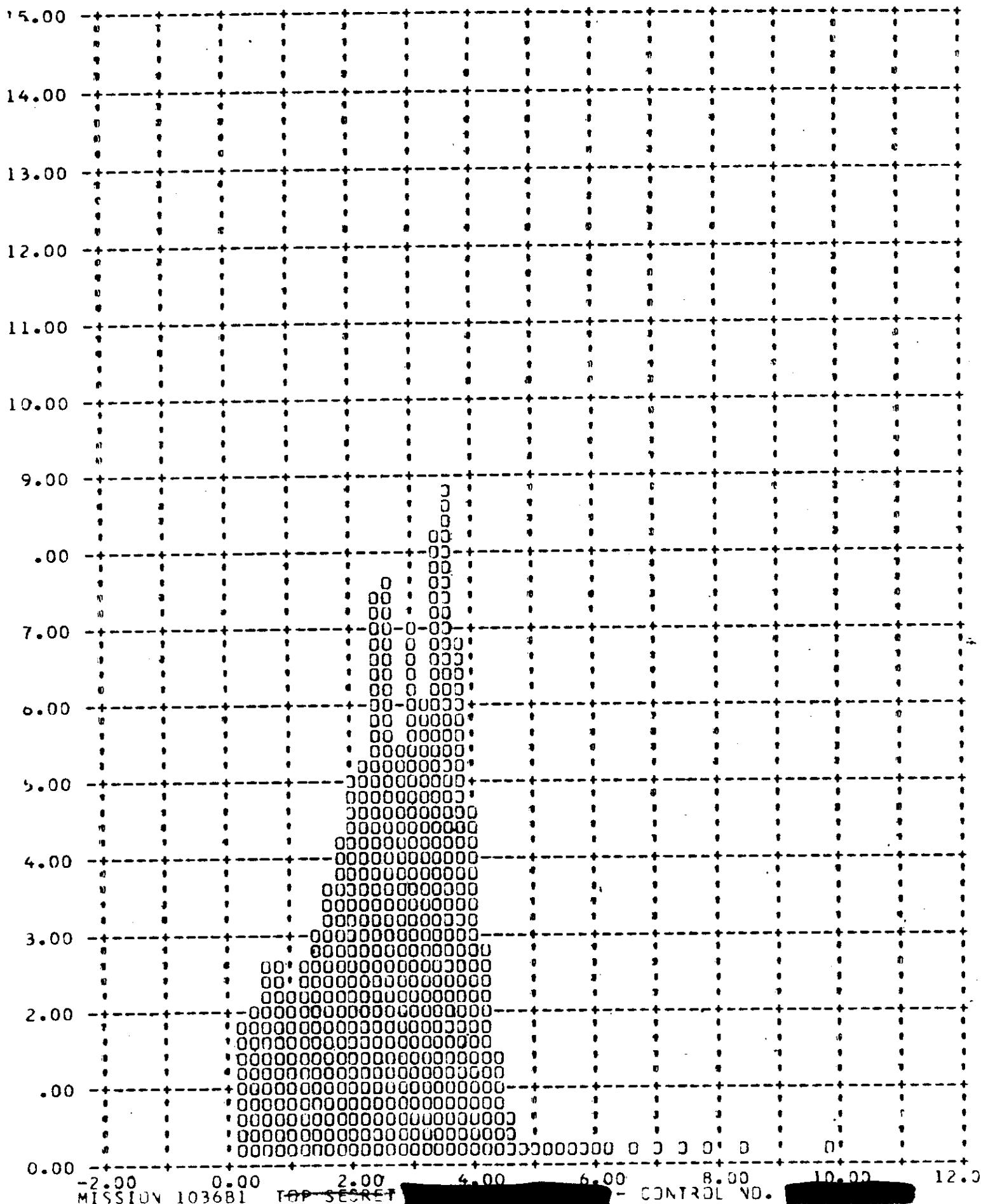


MISSION 1036B1 TOP SECRET

- CONTROL NO.

FRAMES 1-6 OF EACH DP OMITTED 90 PERCENT = 3.79

Y ALONG TRACK RESOLUTION LIMIT - FEET (X) VERSUS FREQUENCY - PERCENT (Y)

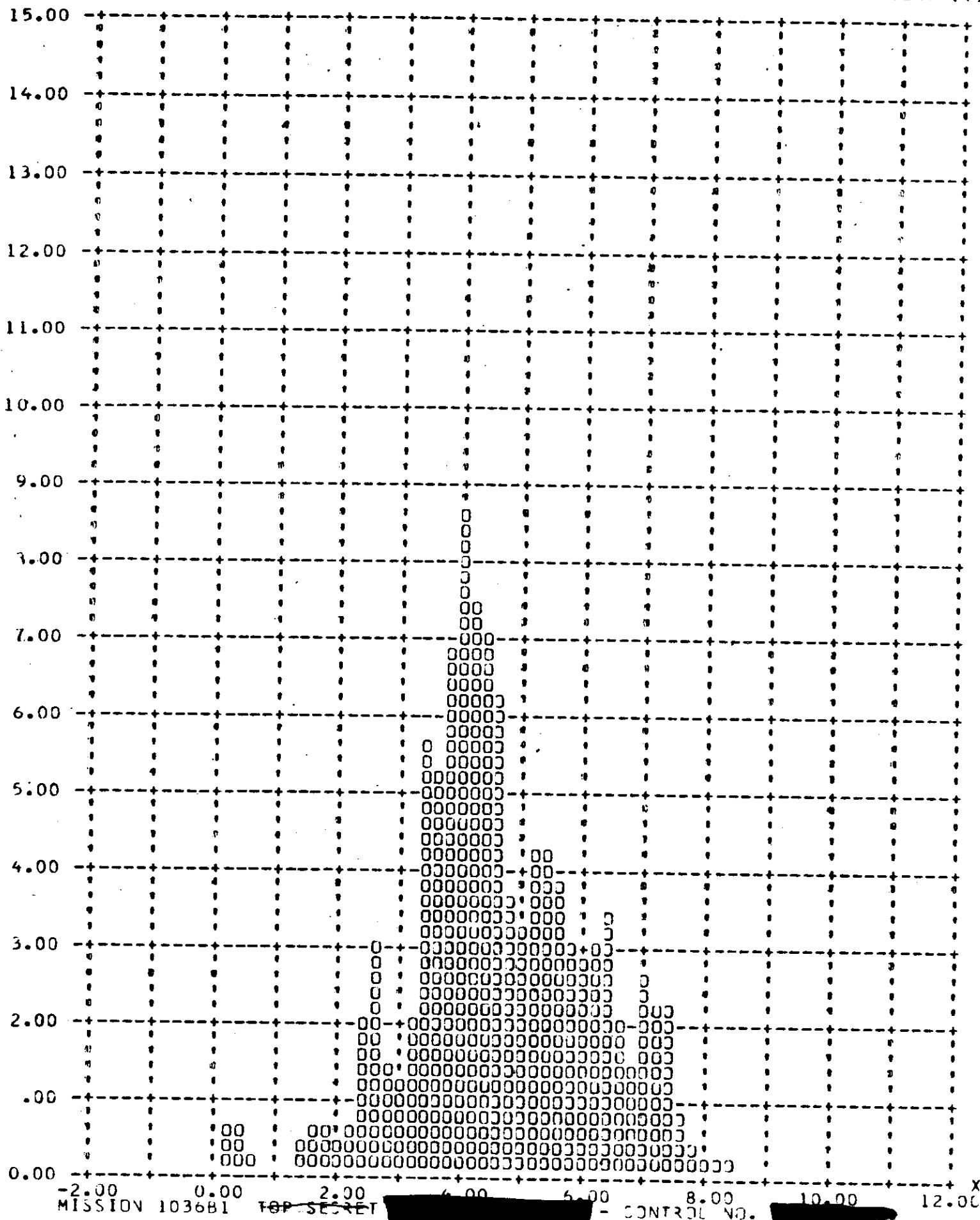


MISSION 1036B1 TOP SECRET

- CONTROL NO.

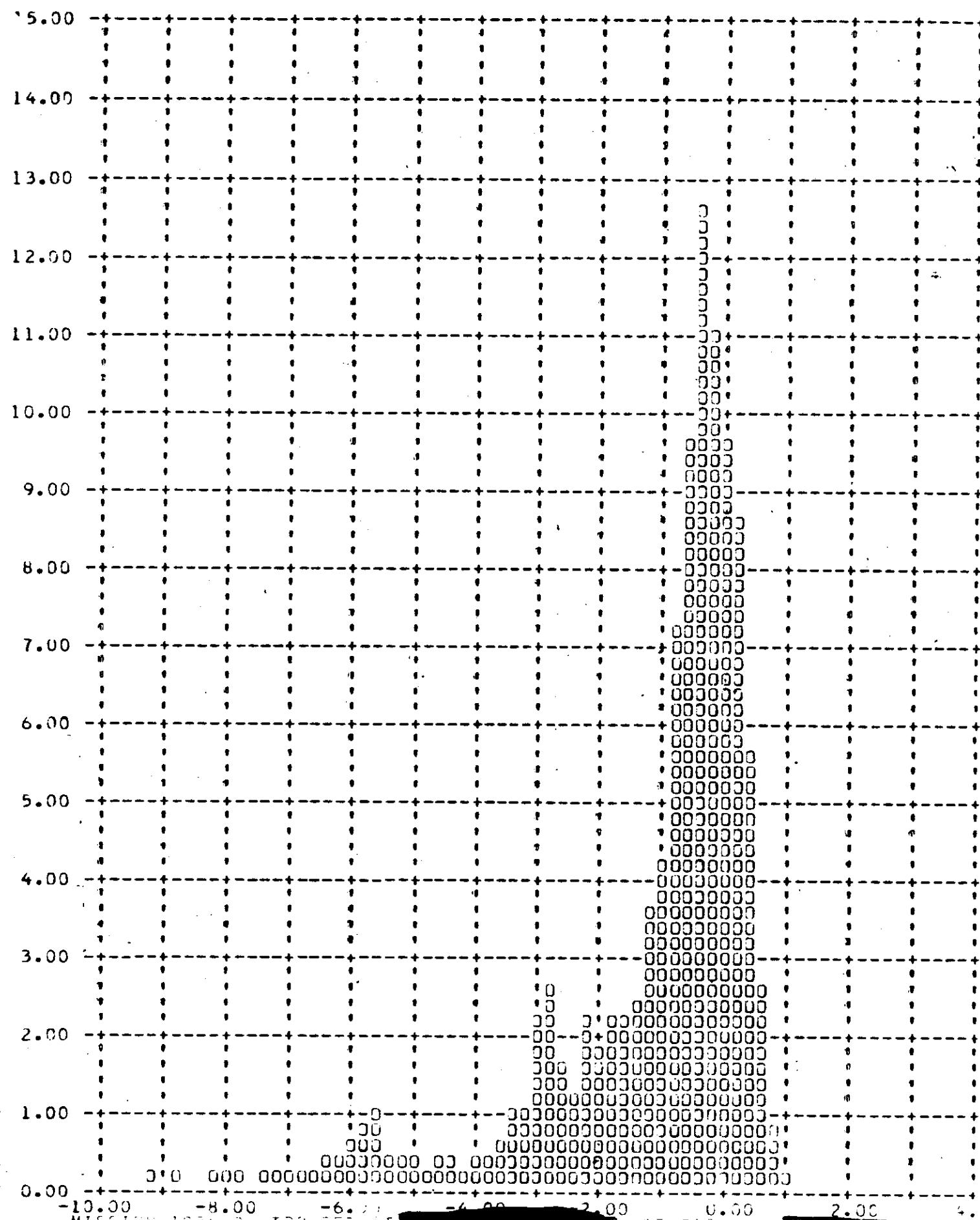
FRAMES 1-6 OF EACH OP OMITTED 90 PERCENT = 6.53

Y CROSS TRACK RESOLUTION LIMIT - FEET (X) VERSUS FREQUENCY - PERCENT (Y)



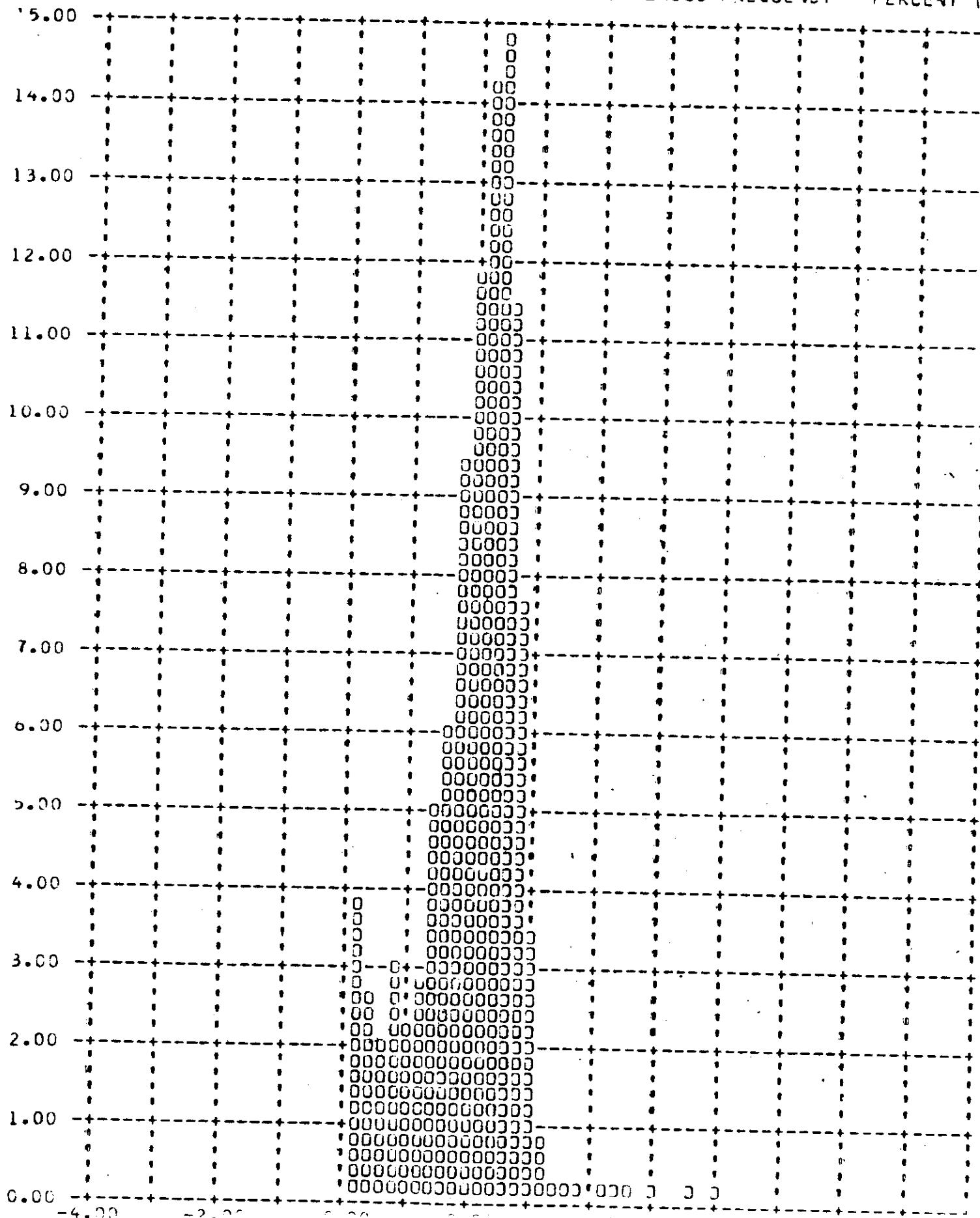
FRAMES 1-6 OF EACH OP OMITTED 90 PERCENT = 3.0

Y V/H RATIO ERROR - PERCENT (X) VERSUS FREQUENCY - PERCENT (Y)



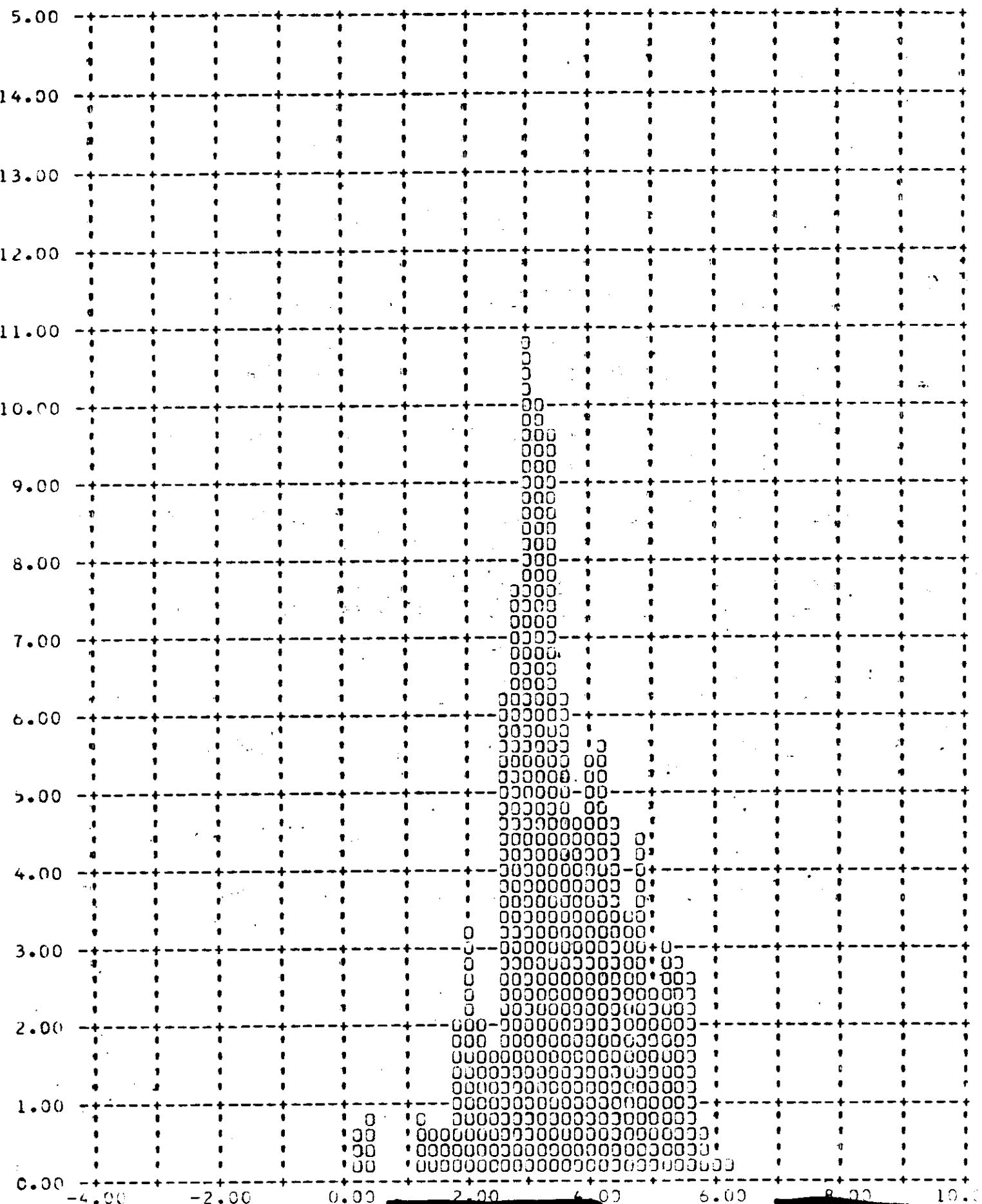
FRAMES 1-6 OF EACH OP OMITTED .90 PERCENT = 2.0

Y ALONG TRACK RESOLUTION LIMIT - FEET (X) VERSUS FREQUENCY - PERCENT (X)



FRAMES 1-6 OF EACH OP OMITTED 90 PERCENT = 4.91

## Y CROSS TRACK RESOLUTION LIMIT - FEET (X) VERSUS FREQUENCY - PERCENT (Y)



# MISSION SUMMARY

92

MISSION NUMBER	PAYOUT NUMBER	VEHICLE NUMBER	LAUNCH DATE	ORBIT INCLINATION (°)	PERIGEE LOCATION (NM)	RECOVERY PASS	MASTER CAMERA NUMBER	SLAVE CAMERA NUMBER	SLIT FILTER TYPE	STELLAR INDEX CAMERA NUMBER
					(°N)		CAMERA SLIT FILTER TYPE	CAMERA SLIT FILTER NUMBER	(-)	
1004	J-05	1174	2/15/64	2138 2	74.9	99.9	29 0	4 9	124	0250 W-21
1006	J-09	1176	6/4/64	2259 2	79.9	84 0	63.2	6 6	148	0200 W-21
1007	J-07	1609	6/19/64	2318 2	85 0	99 2	41.5	6 5	144	0200 W-21
1008	J-10	1177	7/10/64	12314 2	85 0	99 4	40.8	4 9	150	0200 W-21
1009	J-12	1605	8/5/64	2316 2	60 1	99 6	39.5	4 9	154	0200 W-21
1010	J-11	1178	9/14/64	2254 2	84 3	97 4	42.5	6 5	144	0175 W-21
1011	J-3X	1170	10/5/64	2150 2	79 9	99.3	20.9	6 5	160	0175 W-21
1012	J-13	1179	10/17/64	2202 2	75 0	96.2	32 4	4 9	156	0200 W-21
1013	J-15	1173	11/2/64	2130 2	80 0	100 0	25 0	6 5	150	0225 W-21
1014	J-16	1180	11/18/64	2036 2	70 0	103 2	65.6	6 1	162	0250 W-25
1015	J-17	1607	12/19/64	2110 2	74 9	96.7	21.5	6 1	175	0250 W-25
1016	J-18	1608	1/15/65	2101 2	74 9	99.4	30.2	6 1	159	0250 W-25
1017	J-14	1611	2/25/65	2144 2	75 0	97 2	25.9	6 1	145	0250 W-25
1018	J-19	1612	3/13/65	2111 2	98 0	100 2	40.3	6 6	122	0250 W-25
1019	J-04	1614	4/29/65	2144 2	85 0	99 1	27 1	6 0	118	0250 W-25
1020	J-20	1613	6/9/65	2158 2	79 1	97 1	40 6	5 7	136	0250 W-25
1021	J-21	1615	5/18/65	1803 2	75 0	109 2	24 3	6 1	166	0175 W-21
1022	J-22	1617	7/19/65	2201 2	85 0	99 7	30.3	6 3	144	0250 W-25
1023	J-23	1618	8/17/65	2100 2	70 0	97.8	29 0	6 1	170	0225 W-25
1024	J-24	1619	9/22/65	2131 2	80 0	95 9	18 4	6 1	172	0225 W-25
1025	JX-20	1616	10/5/65	1746 2	75 0	112 9	44.3	6 1	142	0175 W-21
1026	J-26	1620	10/28/65	2117 2	75 0	93.0	17.0	6 1	174	0225 W-25
1027	JX-27	1621	12/9/65	2110 2	80 0	97.4	17.3	3 3	164	0250 W-25
1028	J-26	1610	12/24/65	2106 2	80 0	97.6	28 4	6 1	144	0250 W-25

## SECTION 15

**RADIATION DOSAGE**

Each recovery system flown on a Corona mission contains a sealed packet of Eastman Type 3401 and Royal X Pan emulsions to determine the total radiation received at the take-up cassette. Both film types have been irradiated by LMSC at various levels and the base plus fog densities recorded after controlled processing.

Following recovery the film dosimeter packets are removed at A/P and processed with a pre-flight sample of the same film type and sensitometric control film. The resulting base plus fog density measurement of the dosimeter strips is used to ascertain the total radiation level. The table below presents the base plus fog readings for the dosimeter strips and the radiation level equivalents.

<u>Emulsion</u>	Mission 1036-1		Mission 1036-2	
	<u>B + F</u>	<u>Radiation</u>	<u>B + F</u>	<u>Radiation</u>
Type 3401	0.15	0.3 R	0.18	0.6 R
Royal X Pan	0.23	0.3 R	0.28	0.6 R

These levels are below that which will degrade the photography.

**SECTION I****SYSTEM RELIABILITY**

Reliability calculations for the payload are based on a sample beginning with M-7. Hence both the major part of the Mural Program and the "J" Program are covered in the calculation. For certain auxiliaries, i.e., the stellar-index camera and the horizon cameras, the sample size is changed to recognize incorporation of modified equipment or new designs where reliability was one of the principal reasons for the modification. However, for primary mission function, the sample size is consistent with reliability reporting for the vehicle.

The reliability estimates of this section deal exclusively with the payload. Failures to achieve orbit or vehicle induced failures are thereby excluded. Recoveries before a complete mission has been completed are considered as full missions providing that early termination was caused by reasons not connected with payload operation. Film quality is not considered in the reliability estimate calculation. Hence, only electrical and mechanical functioning are considered.

The reliability estimate is also divided into primary and secondary functions. The primary functions are operation of the panoramic cameras, main camera door operation, operation of the payload clock, and recovery operations. The secondary mission functions are horizon camera operation excluding catastrophic open shutter failure mode, auxiliary data recording, and stellar-index camera operation. A summary of estimated reliability is shown in Table 16-I.

**Panoramic Camera Reliability**

Sample Size - 155 opportunities to operate.

One failure - S/I Programmer on System J-19

Assume - 3000 cycles per camera per mission.

Estimated Reliability = 98.9% at 50% confidence level

### Main Camera Door Reliability

Sample Size - 52 vehicles x 2 doors = 104 opportunities to operate  
Estimated Reliability = 99.3% at 50% confidence level.

### Payload Command and Control

Sample Size - 8520 hours operation in sample  
Two failures

Estimated Reliability = 97.0% at 50% confidence level

### Payload Clock Reliability

Sample Size - 8520 hours operation in sample  
No failures

Estimated Reliability = 99.2% at 50% confidence level

Estimated Reliability of Payload Functioning on orbit = 97.3% at  
50% confidence level

### Recovery System Reliability

69 opportunities to recover

1 failure - improper separation due to water seal - cutter failure

Estimated Reliability = 97.6% at 50% confidence level

### Stellar-Index Camera Reliability

Sample begins with J5

Sample size = 20,830 cycles

Four failures

Estimated Reliability = 90.9% at 50% confidence level

### Horizon Camera Reliability

Sample begins with J5 - 85,500 cycles

Estimated Reliability of Single Camera = 98.8% at 50% confidence level

Estimated Reliability of Four Horizon Cameras at a Parallel

Redundant System = 99.9% at 50% confidence level.

# ESTIMATED RELIABILITY SUMMARY (AT 50% CONFIDENCE LEVEL)

MISSION NUMBER	PRIMARY FUNCTIONS						SECONDARY FUNCTIONS					
	PANORAMIC CAMERA DOORS			COMMAND & CONTROL SYSTEM			PAYLOAD CLOCK			ON-ORBIT FUNCTIONS		
	SAMPLE	SAMPLE	SAMPLE	SAMPLE	SAMPLE	SAMPLE	SAMPLE	SAMPLE	SAMPLE	RECOVERY SYSTEM	STELLAR - INDEX CAMERAS	HORIZON CAMERAS
1001	FAILURES	FAILURES	FAILURES	FAILURES	FAILURES	FAILURES	FAILURES	FAILURES	FAILURES	SAMPLE	SAMPLE	SAMPLE
1002	RELIABILITY	RELIABILITY	RELIABILITY	RELIABILITY	RELIABILITY	RELIABILITY	RELIABILITY	RELIABILITY	RELIABILITY	FAILURES	FAILURES	FAILURES
1003	OPERATIONS	52	DOORS	3124	HOURS	3124	HOURS	3124	HOURS	10 CAPTURES	3400 CAPTURES	12,000 CAPTURES
1004	97.3	0	98.6	0	0	98.0	0	98.1	0	80.7	83.1	91.7
1005	64	54	3216	3216	0	98.0	0	98.2	0	20	4250	15,000
1006	97.4	0	98.7	0	0	98.0	0	98.2	0	91.5	89.3	93.4
1007	68	56	3432	3432	0	98.0	0	98.4	0	22	5100	18,000
1008	97.6	0	98.8	0	0	98.1	0	98.4	0	24	98.5	21,000
1009	72	58	3600	3600	0	98.1	0	98.6	0	26	5525	73.7
1010	97.7	0	98.9	0	0	98.1	0	98.6	0	24	93.0	0
1011	78	60	3720	3720	0	98.2	0	98.9	0	28	5325	94.7
1012	97.8	0	98.9	0	0	98.2	0	98.9	0	26	5950	24,000
1013	78	62	3940	3940	0	98.3	0	98.9	0	28	93.6	0
1014	97.9	0	99.0	0	0	98.3	0	98.0	0	30	93.7	25,500
1015	82	64	4056	4056	0	98.3	0	98.0	0	32	7225	0
1016	97.9	0	99.0	0	0	98.4	0	98.1	0	34	94.0	26,500
1017	84	66	4320	4320	0	98.3	0	98.1	0	32	7650	31,500
1018	98.0	0	99.0	0	0	98.3	0	98.4	0	36	8925	34,500
1019	98.1	0	99.0	0	0	98.4	0	98.4	0	34	7650	37,500
1020	98.2	0	99.0	0	0	98.4	0	98.5	0	36	8980	40,500
1021	98.3	0	99.1	0	0	98.5	0	98.6	0	36	8980	40,500
1022	102	74	5136	5136	0	98.6	0	98.7	0	36	807500	43,500
1023	98.4	0	99.1	0	0	98.7	0	98.8	0	36	807500	43,500
1024	98.5	0	99.1	0	0	98.7	0	98.9	0	36	807500	43,500
1025	98.6	0	99.1	0	0	98.7	0	99.0	0	36	807500	43,500
1026	98.7	0	99.1	0	0	98.7	0	99.1	0	36	807500	43,500
1027	98.8	0	99.1	0	0	98.7	0	99.1	0	36	807500	43,500
1028	98.9	0	99.1	0	0	98.7	0	99.1	0	36	807500	43,500
1029	99.0	0	99.1	0	0	98.7	0	99.1	0	36	807500	43,500
1030	99.1	0	99.1	0	0	98.7	0	99.1	0	36	807500	43,500
1031	99.2	0	99.1	0	0	98.7	0	99.1	0	36	807500	43,500
1032	99.3	0	99.1	0	0	98.7	0	99.1	0	36	807500	43,500
1033	99.4	0	99.1	0	0	98.7	0	99.1	0	36	807500	43,500
1034	99.5	0	99.1	0	0	98.7	0	99.1	0	36	807500	43,500
1035	99.6	0	99.1	0	0	98.7	0	99.1	0	36	807500	43,500
1036	99.7	0	99.1	0	0	98.7	0	99.1	0	36	807500	43,500
1037	99.8	0	99.1	0	0	98.7	0	99.1	0	36	807500	43,500
1038	99.9	0	99.1	0	0	98.7	0	99.1	0	36	807500	43,500
1039	100.0	0	99.1	0	0	98.7	0	99.1	0	36	807500	43,500
1040	100.1	0	99.1	0	0	98.7	0	99.1	0	36	807500	43,500
1041	100.2	0	99.1	0	0	98.7	0	99.1	0	36	807500	43,500
1042	100.3	0	99.1	0	0	98.7	0	99.1	0	36	807500	43,500
1043	100.4	0	99.1	0	0	98.7	0	99.1	0	36	807500	43,500
1044	100.5	0	99.1	0	0	98.7	0	99.1	0	36	807500	43,500
1045	100.6	0	99.1	0	0	98.7	0	99.1	0	36	807500	43,500
1046	100.7	0	99.1	0	0	98.7	0	99.1	0	36	807500	43,500
1047	100.8	0	99.1	0	0	98.7	0	99.1	0	36	807500	43,500
1048	100.9	0	99.1	0	0	98.7	0	99.1	0	36	807500	43,500
1049	101.0	0	99.1	0	0	98.7	0	99.1	0	36	807500	43,500
1050	101.1	0	99.1	0	0	98.7	0	99.1	0	36	807500	43,500
1051	101.2	0	99.1	0	0	98.7	0	99.1	0	36	807500	43,500
1052	101.3	0	99.1	0	0	98.7	0	99.1	0	36	807500	43,500
1053	101.4	0	99.1	0	0	98.7	0	99.1	0	36	807500	43,500
1054	101.5	0	99.1	0	0	98.7	0	99.1	0	36	807500	43,500
1055	101.6	0	99.1	0	0	98.7	0	99.1	0	36	807500	43,500
1056	101.7	0	99.1	0	0	98.7	0	99.1	0	36	807500	43,500
1057	101.8	0	99.1	0	0	98.7	0	99.1	0	36	807500	43,500
1058	101.9	0	99.1	0	0	98.7	0	99.1	0	36	807500	43,500
1059	102.0	0	99.1	0	0	98.7	0	99.1	0	36	807500	43,500
1060	102.1	0	99.1	0	0	98.7	0	99.1	0	36	807500	43,500
1061	102.2	0	99.1	0	0	98.7	0	99.1	0	36	807500	43,500
1062	102.3	0	99.1	0	0	98.7	0	99.1	0	36	807500	43,500
1063	102.4	0	99.1	0	0	98.7	0	99.1	0	36	807500	43,500
1064	102.5	0	99.1	0	0	98.7	0	99.1	0	36	807500	43,500
1065	102.6	0	99.1	0	0	98.7	0	99.1	0	36	807500	43,500
1066	102.7	0	99.1	0	0	98.7	0	99.1	0	36	807500	43,500
1067	102.8	0	99.1	0	0	98.7	0	99.1	0	36	807500	43,500
1068	102.9	0	99.1	0	0	98.7	0	99.1	0	36	807500	43,500
1069	103.0	0	99.1	0	0	98.7	0	99.1	0	36	807500	43,500
1070	103.1	0	99.1	0	0	98.7	0	99.1	0	36	807500	43,500
1071	103.2	0	99.1	0	0	98.7	0	99.1	0	36	807500	43,500
1072	103.3	0	99.1	0	0	98.7	0	99.1	0	36	807500	43,500
1073	103.4	0	99.1	0	0	98.7	0	99.1	0	36	807500	43,500
1074	103.5	0	99.1	0	0	98.7	0	99.1	0	36	807500	43,500
1075	103.6	0	99.1	0	0	98.7	0	99.1	0	36	807500	43,500
1076	103.7	0	99.1	0	0	98.7	0	99.1	0	36	807500	43,500
1077	103.8	0	99.1	0	0	98.7	0	99.1	0	36	807500	43,500
1078	103.9	0	99.1	0	0	98.7	0	99.1	0	36	807500	43,500
1079	104.0	0	99.1	0	0	98.7	0	99.1	0	36	807500	43,500
1080	104.1	0	99.1	0	0	98.7	0	99.1	0	36	807500	43,500
1081	104.2	0	99.1	0	0	98.7	0	99.1	0	36	807500	43,500
1082	104.3	0	99.1	0	0	98.7	0	99.1	0	36	807500	43,500
1083	104.4	0	99.1	0	0	98.7	0	99.1	0	36	807500	43,500
1084	104.5	0	99.1	0	0	98.7	0	99.1	0	36	807500	43,500
1085	104.6	0	99.1	0	0	98.7	0	99.1	0	36	807500	43,500
1086	104.7	0	99.1	0	0	98.7	0	99.1	0	36	807500	43,500
1087	104.8	0	99.1	0	0	98.7	0	99.1	0	36	807500	43,500
1088	104.9	0	99.1	0	0	98.7	0	99.1	0	36	807500	43,500
1089	105.0	0	99.1	0	0	98.7	0	99.1	0	36	807500	43,500
1090	105.1	0	99.1	0	0	98.7	0	99.1	0	36	807500	43,500
1091	105.2	0	99.1	0	0	98.7	0	99.1	0	36	807500	43,500
1092	105.3	0	99.1	0	0	98.7	0	99.1	0	36	807500	43,500
1093	105.4	0	99.1	0	0	98.7	0	99.1	0	36	807500	43,500
1094	105.5	0	99.1	0	0	98.7	0	99.1	0	36	807500	43,500
1095	105.6	0	99.1	0	0	98.7	0	99.1	0	36	807500	43,500
1096	105.7	0	99.1	0	0	98.7	0	99.1	0	36	807500	43,500
1097	105.8	0	99.1	0	0	98.7	0	99.1	0	36	807500	43,500
1098	105.9	0	99.1	0	0	98.7	0	99.1	0	36	807500	43,500
1099	106.0	0	99.1	0	0	98.7	0	99.1	0	36	807500	43,500
1100	106.1	0	99.1	0	0	98.7	0	99.1	0	36	807500	43,500
1101	106.2	0	99.1	0	0	98.7	0	99.1	0	36	807500	43,500
1102	106.3	0	99.1	0	0	98.7	0	99.1	0	36	807500	43,500
1103	106.4	0	99.1	0	0	98.7	0	99.1	0	36	807500	43,500
1104	106.5	0	99.1	0	0	98.7	0	99.1	0	36	807500	43,500
1105	106.6	0	99.1	0	0	98.7	0	99.1	0	36	807500	43,500
1106	106.7	0	99.1	0	0	98.7	0	99.1	0	36	807500	43,500
1107	106.8	0	99.1	0	0	98.7	0	99.1	0	36	807500	43,500
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### **SECTION FIX NEGATED PREVIOUS FAILURE CONSIDERATIONS**

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# ESTIMATED RELIABILITY SUMMARY

(AT 50% CONFIDENCE LEVEL)

MISSION NUMBER	PRIMARY FUNCTIONS			SECONDARY FUNCTIONS		
	PANORAMIC CAMERA		PANORAMIC CAMERA COMMAND & CONTROL SYSTEM	ON-ORBIT FUNCTIONS		HORIZON CAMERAS
	SAMPLE	DOORS	SAMPLE	SAMPLE	SAMPLE	
	FAILURES	RELIABILITY	FAILURES	RELIABILITY	FAILURES	FAILURES
	RELIABILITY	RELIABILITY	RELIABILITY	RELIABILITY	RELIABILITY	RELIABILITY
1020	108	78	5544	43	10680	48,000
		0	99.1	96.9	2	0
		0	97.1	98.9	69.9	97.9
		0	97.6	96.9	46,500	
		0	97.0	98.8	2	0
		0	97.4	96.9	11,550	51,000
		0	97.3	98.9	2	0
		0	97.3	96.9	96.3	90.7
		0	97.0	98.2	12,190	54,000
		0	97.4	96.2	96.5	91.1
		0	97.6	98.2	13,040	57,000
		0	97.2	98.9	96.6	91.6
		0	97.0	96.3	13,890	60,000
		0	97.2	96.1	96.7	92.1
		0	97.0	96.0	14,740	63,000
		0	97.4	96.4	96.8	92.6
		0	97.2	96.0	15,165	64,500
		0	97.0	95.9	97.0	90.0
		0	97.2	96.3	53	92.1
		0	97.0	96.0	96.5	91.6
		0	97.4	96.0	55	92.6
		0	97.2	96.0	96.8	92.1
		0	97.0	96.0	16,015	67,500
		0	97.2	96.3	97.1	90.7
		0	97.0	96.0	16,580	70,500
		0	97.2	96.7	97.1	90.7
		0	97.0	96.8	61	17,430
		0	97.2	96.9	97.2	90.7
		0	97.0	96.9	4	89.3
		0	97.2	96.9	4	89.6
		0	97.0	96.7	63	14,280
		0	97.2	96.7	97.2	90.7
		0	97.0	96.9	4	89.3
		0	97.2	96.9	63	14,510
		0	97.0	96.9	4	89.6
		0	97.2	96.9	63	14,710

**ESTIMATE OF RIVER INFILTRATION**  
(AT 50% CONFIDENCE LEVEL)

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FUNCTIONS

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## SECTION I

## SUMMARY DATA

The comparison of the operating parameters and the performance achieved by previous missions has been difficult due to the large volume of data that results from each mission. Some of the pertinent characteristics from prior missions have been summarized in Tables 17-1 through 17-3.

The summary data was started with Mission 1004 as the J-05 camera system was the first to incorporate the major modifications of the titanium drum and scan arm, four roller scan head and Corona J capabilities. Only those missions that culminated in the recovery of some photography have been listed, therefore Missions 1003, 1005 and 1032 are deleted.

# MISSION SUMMARY

MISSION NUMBER	PAYOUT NUMBER	VEHICLE NUMBER	LAUNCH DATE	ORBIT INCLINATION (°)	PERIGEE LOCATION (NM)	RECOVERY PASS	MASTER CAMERA NUMBER	SLAVE CAMERA NUMBER	CAMERA SLIT (1-1)	FILTER TYPE	STELLAR INDEX	CAMERA NUMBER			
1029	J-27	1623	2/2/66	2132 2	75 1	99 5	22 5	81	160	0 275	W-25	0 175	W-21	079/94/91	
1030	J-29	1622	3/9/66	2202 2	75 0	97 5	16 7	81	159	0 275	W-25	0 175	W-21	076/70/94	
1031	J-30	1627	4/7/66	2202 2	75 1	104 5	23 3	113	177	0 225	W-23A	0 150	W-21	094/100/07	
1032	J-28	1625	5/3/66	1925 2	—	—	—	—	—	—	—	—	—	082/85/02	
1033	J-33	1630	5/24/66	0213 2	66 1	102 0	60 7	82	178	194	0 200	W-21	0 150	W-21	081/97/101
1034	J-31	1626	6/21/66	2131 2	80 1	105 4	18 2	81	161	186	0 200	W-23A	0 150	W-21	091/105/09
1035	J-36	1628	9/20/66	2114 2	85 0	99 5	29 1	81	160	188	0 225	W-23A	0 175	W-21	083/109/76
1036	J-32	1631	8/9/66	2046 2	100 0	102 4	22 9	115	212	190	0 200	W-23A	0 150	W-21	087/107/05
														095/112/13	
														096/104/16	
														089/110/11	
														089/108/06	

# PERFORMANCE SUMMARY

MISSION NUMBER	CAMERA SERIAL NUMBER	N I P VALUE	VISUAL RES	AFSPL	NTFF/AIM	SLIT AVERAGE (μ)	SLIT HIGH (μ)	SLIT ALL (μ)	90% ATTITUDE ERROR (%)			90% ATTITUDE RATES (YR/HR)			90% V/H ERROR (R)	90% RESOLUTION LIMIT (FEET) CROSS TRACK	
									PITCH	ROLL	YAW	PITCH	ROLL	YAW			
1004-1	FWD 124	85	78	97	109	115	127	0.45	0.42	0.08	30.0	25.0	21.0	5.1	7.7	6.1	
1004-2	AFT 125	85	86	350	80	43	96	320	117	124	0.82	0.90	0.91	4.9	6.8	6.5	
1006-1	FWD 148	90	78	65	68	113	106	89	0.74	0.50	0.91	44.0	30.0	29.0	4.9	6.5	6.5
1006-2	AFT 149	90	74	350	64	43	90	320	84	97	0.41	0.42	1.14	26.8	27.8	15.4	
1007-1	FWD 144	85	80	60	60	81	72	90	0.84	0.90	0.49	0.40	1.08	31.1	27.9	30.0	
1007-2	AFT 145	85	79	350	63	43	81	320	87	92	0.74	0.47	—	43.0	25.8	1.9	
1008-1	FWD 150	85	80	60	60	81	72	90	0.84	0.90	0.49	0.40	1.08	31.1	27.9	30.0	
1008-2	FWD 151	85	82	350	64	91	83	82	0.84	0.90	0.49	0.40	1.08	31.1	27.9	30.0	
1009-1	FWD 154	85	92	60	65	81	77	92	0.84	0.90	0.49	0.40	1.08	31.1	27.9	30.0	
1009-2	FWD 155	85	94	350	65	—	—	80	0.84	0.90	0.49	0.40	1.08	31.1	27.9	30.0	
1010-1	FWD 152	85	90	90	87	87	87	72	79	79	0.48	0.65	0.59	33.6	23.9	29.6	
1010-2	FWD 153	85	92	350	66	60	88	80	87	96	0.93	0.30	0.87	39.1	24.0	32.5	
1011-1	FWD 160	90	90	62	62	81	85	87	98	93	0.59	0.70	1.21	45.4	22.7	27.6	
1012-1	AFT 156	95	92	350	76	77	80	96	80	78	87	0.65	0.59	0.97	43.1	27.2	32.5
1012-2	FWD 157	85	91	—	—	80	87	89	80	84	98	0.65	0.51	—	47.1	33.2	42.4
1013-1	FWD 158	90	84	350	76	77	80	96	80	78	87	0.65	0.59	0.97	45.2	30.7	30.7
1014-1	FWD 162	80	87	—	—	80	94	80	85	99	99	0.64	0.52	1.34	36.9	29.0	32.3
1014-2	FWD 139	80	83	—	—	80	86	80	78	74	86	0.62	0.41	1.46	35.0	36.1	38.5
1015-1	FWD 138	85	87	—	—	80	86	84	84	70	77	1.06	0.55	1.44	34.8	36.4	38.3
1016-1	FWD 132	85	85	—	—	80	94	86	85	90	90	0.64	0.59	0.53	47.0	29.2	39.2
1016-2	FWD 133	85	91	—	—	80	86	80	78	80	89	0.64	0.59	0.53	46.9	39.1	27.0
1017-1	FWD 140	85	83	72	—	80	73	80	90	97	90	0.64	0.59	0.53	47.0	29.4	39.2
1017-2	AFT 165	85	85	—	—	80	75	80	84	84	84	0.64	0.59	0.53	46.9	39.1	27.0
1018-1	FWD 152	85	79	—	—	80	74	72	72	90	90	0.50	0.61	0.64	39.1	27.0	32.3
1018-2	FWD 123	85	84	88	—	80	74	70	62	92	92	0.91	0.48	0.76	47.9	36.7	34.8
	AFT								81	94	94	0.49	0.76	2.50	35.5	32.2	36.4
									80	80	94	0.49	0.76	2.49	35.3	32.0	36.5
									65	80	86	0.61	0.69	0.63	36.3	33.8	34.7
									70	80	86	0.61	0.69	0.63	34.7	30.7	30.7
									71	77	89	0.61	0.69	0.63	34.8	30.7	30.7
									91	91	91	0.61	0.69	0.63	34.8	30.7	30.7

TABLE 17-2

# PERFORMANCE SUMMARY

MISSION NUMBER	CAMERA SERIAL NUMBER	N.I.P. VALUE	VISUAL RES.	AFSPPF SLIT AVERAGE (μ)	NIF/AIM SLIT AVERAGE (μ)	AVERAGE SLIT (μ)	90% ATTITUDE ERROR (°)			90% ALTITUDE RATES (IN/H)			90% V/H ERROR (%)			90% RESOLUTION LIP EFFECT CROSS TRACK		
							PAN	ROLL	PITCH	PAN	ROLL	PITCH	PAN	ROLL	PITCH	PAN	ROLL	PITCH
1019-1	FWD 118	85	8.1	—	8.0	7.6	80	88	104	0.43	0.36	0.97	31.6	34.7	33.0	3.3	9.3	9.1
1020-1	FWD 136	80	8.8	—	8.0	6.3	69	78	90	0.44	0.37	0.96	31.6	34.9	33.1	3.8	5.0	6.5
1020-2	FWD 137	—	8.9	—	—	8.0	82	80	—	0.46	0.35	0.78	37.4	31.8	26.7	5.4	5.8	6.4
1021-1	FWD 166	85	8.8	—	—	—	—	—	—	0.41	0.35	0.78	37.4	31.8	26.7	5.5	5.9	5.9
1021-2	FWD 167	85	9.0	—	—	8.0	90	80	66	0.55	0.37	0.67	1.06	42.6	23.9	42.5	6.4	7.6
1022-1	FWD 168	85	8.8	—	—	8.0	83	80	84	0.49	0.40	0.51	0.90	29.4	27.3	31.0	5.4	5.5
1022-2	FWD 169	85	9.1	—	—	8.0	68	74	74	0.40	0.31	0.51	0.90	29.4	27.3	31.1	5.4	5.5
1023-1	FWD 170	85	8.8	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
1023-2	FWD 171	85	8.5	—	—	8.0	87	80	83	0.41	0.33	0.50	0.50	33.0	28.7	23.5	3.4	4.0
1024-1	FWD 172	85	8.5	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
1024-2	FWD 173	85	8.5	—	—	8.0	95	80	94	0.42	0.25	0.62	0.25	32.2	24.9	30.5	2.6	6.8
1025-1	FWD 174	85	8.5	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
1025-2	FWD 175	85	8.5	—	—	8.0	97	80	97	0.50	0.41	0.85	0.85	28.1	26.7	25.9	2.0	6.7
1026-1	FWD 176	85	8.5	—	—	8.0	97	80	101	0.44	0.31	0.85	0.85	28.6	29.7	29.0	2.2	6.6
1026-2	FWD 177	85	8.5	—	—	8.0	85	80	96	0.47	0.32	0.82	0.82	28.0	26.1	29.0	1.7	6.7
1027-1	FWD 178	85	8.5	—	—	9.1	91	89	83	0.52	0.44	0.82	0.82	28.1	26.0	29.0	1.8	6.7
1028-1	FWD 179	85	8.5	—	—	8.0	88	80	80	0.49	0.24	0.70	0.70	37.9	33.2	28.5	6.1	6.1
1028-2	FWD 180	85	8.5	—	—	8.0	85	93	90	0.59	0.55	0.56	0.65	41.1	46.5	30.8	6.1	6.1
1029-1	FWD 181	85	8.5	—	—	8.0	88	80	92	0.43	0.31	0.51	0.51	37.9	33.2	28.5	6.1	6.1
1029-2	FWD 182	85	8.5	—	—	8.0	91	83	91	0.44	0.32	0.51	0.51	37.9	33.2	28.5	6.1	6.1
1030-1	FWD 183	85	8.5	—	—	8.0	74	77	79	0.41	0.37	0.51	0.51	47.2	25.5	26.4	4.7	10.5
1030-2	FWD 184	85	8.5	—	—	8.0	57	60	69	0.41	0.37	0.51	0.51	47.3	25.2	26.2	3.8	6.0
1031-1	FWD 185	85	8.5	—	—	9.1	77	71	74	0.42	0.37	0.50	0.50	36.6	28.0	30.5	3.9	4.0
1031-2	FWD 186	85	8.5	—	—	8.0	67	60	67	0.42	0.37	0.50	0.50	36.6	28.0	30.5	3.2	4.2
1032-1	FWD 187	85	8.5	—	—	9.1	91	83	89	0.43	0.37	0.50	0.50	42.7	25.7	25.7	6.1	6.1
1032-2	FWD 188	85	8.5	—	—	8.0	75	77	84	0.42	0.37	0.50	0.50	42.5	25.6	25.6	6.1	6.1
1033-1	FWD 189	85	8.5	—	—	8.0	67	60	67	0.42	0.37	0.50	0.50	42.5	25.6	25.6	6.1	6.1
1033-2	FWD 190	85	8.5	—	—	8.0	75	73	80	0.42	0.37	0.50	0.50	42.5	25.6	25.6	6.1	6.1
	FWD 191	85	8.5	—	—	9.1	91	83	91	0.43	0.37	0.50	0.50	42.5	25.6	25.6	6.1	6.1
	FWD 192	85	8.5	—	—	8.0	74	76	77	0.43	0.37	0.50	0.50	42.5	25.6	25.6	6.1	6.1
	FWD 193	85	8.5	—	—	8.0	77	80	71	0.43	0.37	0.50	0.50	42.5	25.6	25.6	6.1	6.1
	FWD 194	85	8.5	—	—	9.1	91	84	91	0.43	0.37	0.50	0.50	42.5	25.6	25.6	6.1	6.1
	FWD 195	85	8.5	—	—	8.0	67	60	67	0.43	0.37	0.50	0.50	42.5	25.6	25.6	6.1	6.1
	AFT 196	85	8.5	—	—	8.0	91	83	91	0.43	0.37	0.50	0.50	42.5	25.6	25.6	6.1	6.1
	AFT 197	85	8.5	—	—	8.0	75	77	80	0.43	0.37	0.50	0.50	42.5	25.6	25.6	6.1	6.1
	AFT 198	85	8.5	—	—	8.0	71	74	71	0.43	0.37	0.50	0.50	42.5	25.6	25.6	6.1	6.1
	AFT 199	85	8.5	—	—	9.1	91	84	91	0.43	0.37	0.50	0.50	42.5	25.6	25.6	6.1	6.1
	AFT 200	85	8.5	—	—	8.0	75	77	80	0.43	0.37	0.50	0.50	42.5	25.6	25.6	6.1	6.1
	AFT 201	85	8.5	—	—	9.1	91	84	91	0.43	0.37	0.50	0.50	42.5	25.6	25.6	6.1	6.1
	AFT 202	85	8.5	—	—	8.0	75	77	80	0.43	0.37	0.50	0.50	42.5	25.6	25.6	6.1	6.1
	AFT 203	85	8.5	—	—	9.1	91	84	91	0.43	0.37	0.50	0.50	42.5	25.6	25.6	6.1	6.1
	AFT 204	85	8.5	—	—	8.0	75	77	80	0.43	0.37	0.50	0.50	42.5	25.6	25.6	6.1	6.1
	AFT 205	85	8.5	—	—	9.1	91	84	91	0.43	0.37	0.50	0.50	42.5	25.6	25.6	6.1	6.1
	AFT 206	85	8.5	—	—	8.0	75	77	80	0.43	0.37	0.50	0.50	42.5	25.6	25.6	6.1	6.1
	AFT 207	85	8.5	—	—	9.1	91	84	91	0.43	0.37	0.50	0.50	42.5	25.6	25.6	6.1	6.1
	AFT 208	85	8.5	—	—	8.0	75	77	80	0.43	0.37	0.50	0.50	42.5	25.6	25.6	6.1	6.1
	AFT 209	85	8.5	—	—	9.1	91	84	91	0.43	0.37	0.50	0.50	42.5	25.6	25.6	6.1	6.1
	AFT 210	85	8.5	—	—	8.0	75	77	80	0.43	0.37	0.50	0.50	42.5	25.6	25.6	6.1	6.1
	AFT 211	85	8.5	—	—	9.1	91	84	91	0.43	0.37	0.50	0.50	42.5	25.6	25.6	6.1	6.1
	AFT 212	85	8.5	—	—	8.0	75	77	80	0.43	0.37	0.50	0.50	42.5	25.6	25.6	6.1	6.1
	AFT 213	85	8.5	—	—	9.1	91	84	91	0.43	0.37	0.50	0.50	42.5	25.6	25.6	6.1	6.1
	AFT 214	85	8.5	—	—	8.0	75	77	80	0.43	0.37	0.50	0.50	42.5	25.6	25.6	6.1	6.1
	AFT 215	85	8.5	—	—	9.1	91	84	91	0.43	0.37	0.50	0.50	42.5	25.6	25.6	6.1	6.1
	AFT 216	85	8.5	—	—	8.0	75	77	80	0.43	0.37	0.50	0.50	42.5	25.6	25.6	6.1	6.1
	AFT 217	85	8.5	—	—	9.1	91	84	91	0.43	0.37	0.50	0.50	42.5	25.6	25.6	6.1	6.1
	AFT 218	85	8.5	—	—	8.0	75	77	80	0.43	0.37	0.50	0.50	42.5	25.6	25.6	6.1	6.1
	AFT 219	85	8.5	—	—	9.1	91	84	91	0.43	0.37	0.50	0.50	42.5	25.6	25.6	6.1	6.1
	AFT 220	85	8.5	—	—	8.0	75	77	80	0.43	0.37	0.50	0.50	42.5	25.6	25.6	6.1	6.1
	AFT 221	85	8.5	—	—	9.1	91	84	91	0.43	0.37	0.50	0.50	42.5	25.6	25.6	6.1	6.1
	AFT 222	85	8.5	—	—	8.0	75	77	80	0.43	0.37	0.50	0.50	42.5	25.6	25.6	6.1	6.1
	AFT 223	85	8.5	—	—	9.1	91	84	91	0.43	0.37	0.50	0.50	42.5	25.6	25.6	6.1	6.1
	AFT 224	85	8.5	—	—	8.0	75	77	80	0.43	0.37	0.50	0.50	42.5	25.6	25.6	6.1	6.1
	AFT 225	85	8.5	—	—	9.1	91	84	91	0.43	0.37	0.50	0.50	42.5	25.6	25.6	6.1	6.1
	AFT 226	85	8.5	—	—	8.0	75	77	80	0.43	0.37	0.50	0.50	42.5	25.6	25.6	6.1	6.1
	AFT 227	85	8.5	—	—	9.1	91	84	91	0.43	0.37	0.50	0.50	42.5	25.6	25.6	6.1	6.1
	AFT 228	85	8.5	—	—	8.0	75	77	80	0.43	0.37	0.50	0.50	42.5	25.6	25.6	6.1	6.1
	AFT 229	85	8.5	—	—	9.1	91	84	91	0.43	0.37	0.50	0.50	42.5	25.6	25.6	6.1	6.1
	AFT 230	85	8.5	—	—	8.0	75	77	80	0.43	0.37							

# PERFORMANCE SUMMARY

MISSION NUMBER	CAMERA	SERIAL NUMBER	A/P	AFTERFLY MIT/AIR		50% ATTITUDE CORR (%)		ECC & ATTITUDE STATES (deg)		0.05 RH ERROR (%)		50% RESOLUTION LIMIT (deg)		1 MC ERROR		
				AVERAGE	STDEV	AVERAGE	STDEV	ROLL	PITCH	ROLL	PITCH	ALONG TRACK	CROSS TRACK	ALONG TRACK	CROSS TRACK	
034-1	FWD	186	90	75	9	0.20	0.19	0.03	19.1	20.4	24.3	15.0	17.6	5.9		
	AFT			93	90	0.50	0.5	0.91	19.3	20.4	24.5	15.2	17.6	4.8		
	FWD	187	80	74	86	0.34	0.30	0.21	21.1	23.6	26.2	16.7	10.4	7.1		
	AFT			69	86	0.54	0.16	0.51	21.1	22.0	26.2	16.7	8.3	4.5		
1034-1	FWD	188	65	66	—	0.16	0.55	2.39	18.9	27.9	35.9	4.0	4.9	7	4.0	
	AFT			80	80	—	0.17	0.54	24.3	23.4	32.2	4.1	3.7	2.4	4.1	
1034-2	FWD	189	85	81	22	0.16	0.50	5.07	18.4	30.1	37.5	4.0	5.2	4.0	5.2	
	AFT			81	22	0.17	0.51	3.02	14.9	24.7	36.3	2.4	3.3	2.4	3.4	
1036-1	FWD	190	85	89	—	0.76	0.36	0.60	31.2	35.6	49.6	7.6	5.1	6.8	—	
	AFT			54	80	—	0.76	0.96	0.60	31.1	35.5	49.4	7.5	5.1	5.5	—
1036-2	FWD	191	85	73	84	—	0.54	0.70	0.40	33.0	39.7	43.3	3.3	3.9	3.5	—
	AFT			84	85	—	0.94	0.70	0.40	32.9	32.9	32.9	2.1	2.1	2.1	—

TOP SECRET C

# EXPOSURE - PROCESSING SUMMARY

MISSION NUMBER	CAMERA	SOLAR ELEVATION RANGE (°)	SOLAR AZIMUTH RANGE (°)	PREDICTED PROCESSING				COMPUTED PROCESSING				TERRAIN D-MIN				CLOUD D-MAX				TERRAIN D-MAX				CLOUD D-MAX				OVER EXPOSED				CLOUD COVER (%)			
				HIGH	LOW	F	P	H	P	F	P	LOW	HIGH	MEAN	LOW	HIGH	MEAN	LOW	HIGH	MEAN	LOW	HIGH	MEAN	LOW	HIGH	MEAN	LOW	HIGH	MEAN	LOW	HIGH	MEAN			
1004-1	FWD	-3	61	25	124	5	76	19	4	79	17	0	79	21	0.26	1.89	0.83	0.78	0.43	2.43	1.97	2.02	0	2.43	2.08	0	4	60	31	5	35				
1004-2	AFT	-3	61	25	124	5	74	21	4	79	17	0	80	20	0.22	1.56	0.76	0.70	0.93	2.45	1.92	1.94	0	2.43	1.98	2.03	0	4	67	26	5	35			
1004-2	FWD	-4	66	10	131	7	76	17	37	50	13	4	83	13	0.29	1.80	0.83	0.78	0.36	2.30	1.84	1.90	0	2.41	2.37	1.87	0	4	59	27	9	35			
1006-1	FWD	38	56	92	140	-1	99	0	1	51	46	0	51	49	0.23	1.87	0.71	0.68	0.80	2.31	1.58	1.52	0	2.40	2.20	2.24	0	4	67	20	9	35			
1006-2	AFT	38	56	92	140	-1	99	0	0	23	77	0	24	76	0.38	1.66	0.87	0.84	0.96	2.35	1.72	1.72	0	2.40	2.20	2.28	0	4	72	21	1	60			
1007-1	FWD	12	49	50	103	0	95	1	20	79	0	25	75	0.26	1.54	0.62	0.58	0.65	2.19	1.48	1.47	0	2.50	2.12	2.18	0	4	72	4	0	45				
1007-2	AFT	11	49	48	102	0	100	0	0	42	48	6	27	77	0.26	1.76	0.59	0.55	0.70	2.21	1.44	1.40	0	2.40	2.20	2.24	2	4	77	9	3	45			
1008-1	FWD	32	57	43	112	0	100	0	25	75	3	28	65	0.26	1.74	0.51	0.48	0.70	2.52	1.52	1.54	0	2.39	2.17	2.21	0	4	67	5	0	60				
1008-1	AFT	31	57	38	111	0	100	0	19	41	40	3	89	9	0.24	1.56	0.60	0.56	0.64	2.27	1.40	0.90	0	2.37	2.15	2.20	1	4	80	5	0	60			
1008-1	FWD	30	61	50	102	0	100	0	4	32	64	-35	64	0.32	1.48	0.66	0.62	0.78	2.24	1.55	1.54	0	2.35	2.11	2.24	2	4	86	6	0	65				
1008-2	AFT	30	51	50	102	0	100	0	4	27	69	0	34	66	0.32	1.57	0.71	0.69	0.81	2.21	1.57	1.58	0	2.37	2.21	2.24	2	4	84	13	0	65			
1008-2	FWD	29	56	42	105	0	100	0	3	31	66	0	27	73	0.14	1.81	0.76	0.72	0.57	2.10	1.54	1.55	0	2.40	2.20	2.25	2	4	75	23	0	65			
1009-1	FWD	12	49	42	132	0	100	0	1	26	73	0	34	66	0.32	1.40	0.63	0.62	0.85	2.41	1.53	1.52	0	2.51	2.30	2.36	5	4	77	14	0	65			
1009-2	AFT	12	49	42	132	0	100	0	40	60	0	45	55	0.28	1.42	0.70	0.64	0.92	2.28	1.58	1.55	0	2.51	2.30	2.36	5	4	77	20	0	65				
1009-2	FWD	23	58	35	138	2	98	0	3	21	76	0	30	60	0.29	1.55	0.69	0.64	0.75	2.37	1.53	1.56	0	2.45	2.25	2.30	4	4	74	17	0	65			
1010-1	FWD	18	47	45	83	0	21	79	0	13	97	0	91	0	0.24	1.49	0.60	0.56	0.66	2.36	1.48	1.48	0	2.42	2.18	2.22	1	4	77	18	0	65			
1010-1	AFT	18	47	45	83	0	21	79	0	19	81	0	16	84	0.27	1.25	0.57	0.52	0.70	2.42	1.41	1.41	0	2.42	2.16	2.20	1	4	75	4	0	65			
1010-2	FWD	15	52	38	76	0	50	50	0	23	77	0	25	75	0.20	1.48	0.59	0.56	0.50	2.36	1.41	1.41	0	2.44	2.14	2.20	2	4	81	6	0	65			
1010-2	AFT	15	52	38	76	0	50	50	0	23	77	0	25	75	0.20	1.48	0.59	0.56	0.50	2.36	1.41	1.41	0	2.44	2.14	2.20	2	4	87	6	0	65			
1011-1	FWD	2	55	33	66	0	64	36	2	23	75	2	23	75	0.24	1.49	0.59	0.56	0.56	2.36	1.48	1.48	0	2.40	2.18	2.22	1	4	76	8	0	65			
1012-1	FWD	0	45	35	66	0	67	33	3	47	50	0	50	57	0.25	1.49	0.55	0.54	0.54	2.35	1.57	1.55	0	2.37	2.11	2.18	3	4	77	11	0	65			
1012-1	AFT	0	45	35	66	0	67	31	7	56	37	0	65	55	0.25	1.30	0.59	0.53	0.54	2.35	1.58	1.57	0	2.42	2.16	2.20	1	4	75	8	0	65			
1012-2	FWD	0	57	34	106	0	77	34	6	44	50	0	49	51	0.26	1.40	0.61	0.58	0.47	2.27	1.44	1.40	0	2.42	2.20	2.26	9	4	80	10	0	65			
1013-1	FWD	0	56	28	83	0	64	36	0	42	58	0	50	57	0.20	1.27	0.68	0.62	0.48	2.33	1.55	1.58	0	2.36	2.16	2.22	7	4	80	7	0	65			
1014-1	FWD	0	59	15	71	0	21	79	-1	38	61	0	63	57	0	37	17	0	99	0.40	0.36	0.26	2.36	1.40	1.42	4	4	77	10	0	65				
1014-1	AFT	0	59	14	69	0	31	69	0	13	87	0	36	64	0	18	26	0	51	0.48	0.42	0.25	2.38	1.42	1.42	4	4	77	12	0	65				
1014-2	FWD	0	77	-2	71	0	21	79	0	6	91	0	61	39	0	17	0	0	56	0.31	0.23	0.23	2.32	1.30	1.36	4	4	74	12	0	65				
1014-2	AFT	0	77	0	76	0	34	0	29	71	0	55	92	0	69	32	0	18	0	0	44	0.40	0.27	0.28	2.34	1.34	1.36	4	4	74	12	0	65		
1015-1	FWD	5	66	19	68	0	92	2	2	95	0	2	98	0	25	70	0	54	0.47	0.47	0.47	2.28	1.44	1.46	4	4	76	7	0	65					
1015-1	AFT	4	66	18	67	0	30	70	0	5	95	0	4	96	0	29	72	0	50	0.56	0.46	0.26	2.28	1.49	1.49	4	4	76	7	0	65				
1015-2	FWD	-1	50	21	99	0	0	0	15	63	24	0	82	18	0	20	60	0	88	0.55	0.49	0.26	2.32	1.52	1.52	4	4	77	13	0	65				
1015-2	AFT	-1	57	19	98	0	17	63	24	68	18	4	90	6	0	20	62	0	65	0.61	0.46	0.25	2.25	1.53	1.53	4	4	77	13	0	65				
1016-1	FWD	5	69	15	76	0	7	93	-1	41	58	0	59	41	0	13	65	0	44	0.51	0.45	0.26	2.32	1.53	1.53	4	4	77	11	0	65				
1016-1	AFT	4	69	12	76	0	27	73	0	26	74	0	42	58	0	22	65	0	44	0.58	0.52	0.26	2.34	1.54	1.54	4	4	77	11	0	65				
1016-2	FWD	6	77	13	134	0	0	0	0	31	69	0	46	52	0	6	91	0	91	0	0	64	0.62	0.54	0.26	2.34	1.55	1.55	4	4	77	10	0	65	
1016-2	AFT	6	78	10	125	0	0	0	22	78	9	53	58	5	72	23	0	18	61	0	65	0.62	0.58	0.26	2.34	1.56	1.56	4	4	77	9	0	65		
1018-1	FWD	8	77	14	134	0	0	0	16	74	6	17	79	4	16	0	0	50	0	50	0.49	0.49	0.26	2.34	1.57	1.57	4	4	77	9	0	65			
1018-1	AFT	8	77	10	132	0	15	85	1	50	49	0	49	0	0	0	26	50	0	79	0.94	0.26	0.26	2.34	1.58	1.58	4	4	77	9	0	65			

# EXPOSURE - PROCESSING SUMMARY

MISSION NUMBER	CAMERA	SOLAR RANGE (°)		PREDICTED PROCESSING (%)		REPORTED PROCESSING (%)		COMPUTED PROCESSING (%)		TEARIN D-MIN		TERRAIN D-MAX		CLOUD RANGE		D-MAX			
		LOW	HIGH	F	T	F	T	F	T	RANGE LOW	RANGE HIGH	MEAN	MEDIAN	LOW	HIGH	MEAN	MEDIAN		
1019-1	FWD	24	70	152	0	21	79	22	32	46	4	56	40	0.26	192	0.71	0.61		
1019-1	AFT	23	70	152	0	92	8	26	55	19	3	87	10	0.13	170	0.66	0.60		
1020-1	FWD	30	75	156	0	19	87	13	48	39	1	58	41	0.23	30	0.55	0.52		
1020-1	AFT	29	75	156	0	64	36	15	56	29	0	74	26	0.23	120	0.55	0.54		
1020-2	FWD	47	69	158	35	—	—	—	—	—	—	—	—	—	—	—	—		
1020-2	AFT	46	69	177	33	—	—	—	—	—	—	—	—	—	—	—	—		
1021-1	FWD	15	66	148	-23	0	68	32	39	47	1	52	47	0.25	190	0.64	0.56		
1021-1	AFT	14	66	147	-25	0	59	11	15	38	47	0	57	17	0.21	170	0.65	0.57	
1021-2	FWD	13	52	133	-41	0	29	71	13	41	46	0	57	43	0.18	150	0.54	0.50	
1021-2	AFT	13	52	133	-41	0	100	0	53	25	22	0	59	50	0.33	138	0.76	0.76	
1022-1	FWD	28	67	150	0	36	64	16	35	56	0	42	38	0.19	149	0.45	0.40		
1022-1	AFT	27	67	157	26	0	89	11	7	42	51	0	53	47	0.24	148	0.57	0.50	
1022-2	FWD	29	74	152	0	100	0	10	44	46	0	53	47	0.21	100	0.39	0.35		
1022-2	AFT	28	74	152	0	100	0	10	44	46	0	53	47	0.21	100	0.39	0.35		
1023-1	FWD	22	62	164	0	5	95	19	54	27	0	72	28	0.15	126	0.39	0.35		
1023-1	AFT	20	61	163	0	11	89	0	35	61	0	42	58	0.20	140	0.53	0.48		
1023-2	FWD	29	81	177	0	7	93	0	19	81	0	18	82	0.22	138	0.48	0.42		
1023-2	AFT	28	80	153	76	0	3	97	0	34	66	0	28	70	0.22	160	0.52	0.48	
1024-1	FWD	10	61	24	37	0	100	0	57	43	0	72	28	0.17	174	0.35	0.32		
1024-1	AFT	9	61	21	36	0	100	0	28	72	0	82	18	0.20	122	0.40	0.37		
1024-2	FWD	19	79	11	151	0	100	0	12	19	69	0	25	75	0.24	117	0.46	0.42	
1024-2	AFT	18	79	9	151	0	100	0	100	21	79	0	24	76	0.26	130	0.49	0.42	
1025-1	FWD	0	70	123	-18	0	68	32	10	41	49	0	58	44	0.18	142	0.43	0.37	
1025-1	AFT	0	70	121	-19	0	72	28	8	49	43	0	61	39	0.18	169	0.49	0.42	
1025-2	FWD	0	56	124	-31	0	72	29	3	42	55	0	56	44	0.18	122	0.45	0.39	
1025-2	AFT	0	56	122	-33	0	73	27	3	45	52	0	51	49	0.21	132	0.48	0.42	
1026-1	FWD	0	57	23	155	0	4	96	0	4	95	0	4	96	0	35	0.31	0.27	
1026-1	AFT	0	57	21	155	0	4	95	0	4	96	0	4	96	0	35	0.31	0.27	
1026-2	FWD	1	72	9	84	0	0	1	15	94	0	15	95	0	19	32	0.36	0.30	
1026-2	AFT	0	57	15	78	0	0	2	5	93	0	15	85	0	21	35	0.39	0.32	
1027-1	FWD	3	63	26	110	0	0	0	100	0	0	3	97	0	26	54	0.52	0.46	
1027-1	AFT	2	63	26	108	0	0	0	21	79	0	20	80	0	26	53	0.50	0.46	
1028-1	FWD	3	75	155	0	4	96	0	4	96	0	11	89	0	22	0.37	0.32		
1028-1	AFT	1	73	143	0	5	95	0	16	84	0	15	90	0	15	85	0.23	0.23	
1028-2	FWD	2	81	48	0	5	97	0	16	90	0	15	94	0	16	94	0.23	0.23	
1028-2	AFT	1	80	5	43	0	16	90	0	16	90	0	15	94	0	16	94	0.23	0.23
1029-1	FWD	3	63	18	30	0	8	92	0	16	83	0	14	86	0	25	0.57	0.48	
1029-1	AFT	2	62	16	28	0	20	80	0	21	79	0	25	75	0	16	73	0.57	0.48
1029-2	FWD	0	80	4	45	0	10	90	0	24	74	0	25	75	0	20	0.54	0.45	
1029-2	AFT	0	80	4	45	0	10	90	0	24	74	0	25	75	0	20	0.54	0.45	
1030-1	FWD	5	63	27	130	0	58	42	3	32	65	1	52	47	0.30	130	0.56	0.52	
1030-1	AFT	4	63	22	129	0	4	54	0	46	54	0	71	29	0.25	164	0.56	0.52	
1030-2	FWD	3	78	7	157	-1	23	76	0	28	72	0	30	74	0	17	0.57	0.57	
1030-2	AFT	2	78	7	157	-1	23	76	0	28	72	0	30	74	0	17	0.57	0.57	
1031-1	FWD	17	70	20	10	0	99	1	18	34	48	0	31	49	0	25	0.37	0.30	
1031-1	AFT	17	70	18	14	0	98	1	18	34	48	0	31	47	0	25	0.37	0.30	
1031-2	FWD	19	82	6	67	0	99	1	18	34	48	0	31	47	0	25	0.37	0.30	
1031-2	AFT	17	70	18	14	0	98	1	18	34	48	0	31	47	0	25	0.37	0.30	
1033-1	FWD	0	47	46	0	85	11	0	18	34	48	0	31	49	0	25	0.37	0.30	
1033-1	AFT	1	47	45	0	85	11	0	18	34	48	0	31	47	0	25	0.37	0.30	
1033-2	FWD	0	54	54	0	81	0	18	43	42	0	47	53	0	24	0.49	0.42	0.49	
1033-2	AFT	0	54	54	0	81	0	18	43	42	0	47	53	0	24	0.49	0.42	0.49	

# EXPOSURE - PROCESSING SUMMARY

MISSION NUMBER	CAMERA RANGE (°)	ELEVATION RANGE (°)	SOLAR AZIMUTH PROCESSING RANGE (°)	REPORTED PROCESSING (%)						COMPUTED PROCESSING (%)						TERRAIN D-MIN			TERRAIN D-MAX			CLOUD D-MAX			OVER PROCESSED (%)			OVER EXPOSED (%)									
				P	I	F	P	I	F	P	I	F	P	I	F	RANGE LOW	RANGE HIGH	MEAN	RANGE LOW	RANGE HIGH	MEAN	RANGE LOW	RANGE HIGH	MEAN	RANGE LOW	RANGE HIGH	MEAN	RANGE LOW	RANGE HIGH	MEAN	RANGE LOW	RANGE HIGH	MEAN				
1034-1	FWD	2.3	77	16	165	0	96	4	21	76	0	20	80	0	25	80	0	57	0	50	0	55	2	42	1	58	1	61	0	88	2	45	2	22	1.8	35	
1034-1	AFT	2.3	77	10	165	0	55	45	2	67	0	16	84	0	29	53	0	56	0	50	0	51	2	35	1	60	0	97	2	42	1.9	2.25	1.8	35			
1034-2	FWD	2.9	86	0	178	0	89	12	9	26	65	0	27	73	0	19	52	0	57	0	52	0	57	2	40	1	63	1	60	1	21	2	47	2	25	1.2	45
1034-2	AFT	3.0	86	0	178	0	41	59	6	37	57	0	34	66	0	26	60	0	54	0	49	0	50	2	32	1	59	1	62	1	18	2	48	2	22	1.2	45
1035-1	FWD	1.5	68	19	144	0	17	83	0	11	89	0	5	95	0	28	90	0	52	0	45	0	61	2	44	1	40	1	40	1	06	2	43	2	15	2.2	3
1035-1	AFT	1.3	68	18	144	0	5	95	1	14	85	0	9	91	0	24	39	0	50	0	43	0	60	2	42	1	48	1	53	0	90	2	55	2	15	2.2	3
1035-2	FWD	1.4	81	10	158	0	22	78	4	18	82	0	21	50	0	52	0	47	0	43	0	60	2	33	1	32	1	30	1	96	2	50	2	09	2.18	24	
1035-2	AFT	1.5	81	8	158	0	23	77	1	20	79	0	12	88	0	21	39	0	56	0	51	0	50	2	34	1	34	1	30	0	74	2	60	2	09	2.16	35
1036-1	FWD	1.3	82	7	170	0	66	34	8	14	76	-1	14	85	0	20	19	0	49	0	42	0	66	2	40	1	54	1	53	1	0	2	47	2	28	3.3	59
1036-1	AFT	1.5	83	5	171	0	5	95	3	9	58	0	10	90	0	24	1.65	0	55	0	51	0	55	2	25	1	19	1	52	1	20	2	43	2	23	1.2	40
1036-2	FWD	1.0	78	12	167	0	15	85	1	19	80	0	18	82	0	26	43	0	47	0	42	0	50	2	20	1	30	1	36	1	18	2	60	2	12	1.6	35
1036-2	AFT	1.2	78	9	168	0	4	96	3	20	77	0	17	83	0	28	1.14	0	49	0	44	0	48	2	15	1	40	1	37	1	40	1	40	2	15	2.20	4

~~TOP SECRET~~

C/[REDACTED] NO. [REDACTED]

SECTION A

APPENDIX

100

~~TOP SECRET~~ C/[REDACTED]

~~TOP SECRET~~

- CONTROL NO.

MISSION \* 1036-1 \* INSTRUMENT \* FRWD

11/28/65 DENSITY FREQ DISTR.

~~TOP SECRET~~

- CONTROL NO.

TABLE A-1

~~TOP SECRET~~

- CONTROL NO.

MISSION \* 1036-1 \* INSTRUMENT \* FRWD

11/28/66 DENSITY FREQ DISTR

DENSITY VALUE	PRIMARY		INTERMEDIATE		FULL		ALL LEVELS	
	MIN	MAX LIM	MIN	MAX LIM	MIN	MAX LIM	MIN	MAX LIM
0.51	0	0	0	0	3	0	3	0
0.52	0	0	0	0	7	0	7	0
0.53	0	0	0	0	2	0	2	0
0.54	0	0	0	0	6	0	6	0
0.55	0	0	0	0	3	0	3	0
0.56	0	0	0	0	6	0	6	0
0.57	0	0	0	0	2	0	2	0
0.58	0	0	0	0	3	0	3	0
0.59	0	0	0	0	6	0	6	0
0.60	0	0	0	0	2	0	2	0
0.61	0	0	0	0	3	0	3	0
0.62	0	0	0	0	6	0	6	0
0.63	0	0	0	0	2	0	2	0
0.64	0	0	0	0	3	0	3	0
0.65	0	0	0	0	6	0	6	0
0.66	0	0	0	0	2	0	2	0
0.67	0	0	0	0	3	0	3	0
0.68	0	0	0	0	6	0	6	0
0.69	0	0	0	0	2	0	2	0
0.70	0	0	0	0	3	0	3	0
0.71	0	0	0	0	6	0	6	0
0.72	0	0	0	0	2	0	2	0
0.73	0	0	0	0	3	0	3	0
0.74	0	0	0	0	6	0	6	0
0.75	0	0	0	0	2	0	2	0
0.76	0	0	0	0	3	0	3	0
0.77	0	0	0	0	6	0	6	0
0.78	0	0	0	0	2	0	2	0
0.79	0	0	0	0	3	0	3	0
0.80	0	0	0	0	6	0	6	0
0.81	0	0	0	0	2	0	2	0
0.82	0	0	0	0	3	0	3	0
0.83	0	0	0	0	6	0	6	0
0.84	0	0	0	0	2	0	2	0
0.85	0	0	0	0	3	0	3	0
0.86	0	0	0	0	6	0	6	0
0.87	0	0	0	0	2	0	2	0
0.88	0	0	0	0	3	0	3	0
0.89	0	0	0	0	6	0	6	0
0.90	0	0	0	0	2	0	2	0
0.91	0	0	0	0	3	0	3	0
0.92	0	0	0	0	6	0	6	0
0.93	0	0	0	0	2	0	2	0
0.94	0	0	0	0	3	0	3	0
0.95	0	0	0	0	6	0	6	0
0.96	0	0	0	0	2	0	2	0
0.97	0	0	0	0	3	0	3	0
0.98	0	0	0	0	6	0	6	0
0.99	0	0	0	0	2	0	2	0
1.00	0	0	0	0	3	0	3	0
SUBTOTAL	20	0	8	0	61	0	71	12

~~TOP SECRET~~

- CONTROL NO.

TABLE A-1

~~TOP SECRET~~

- CONTROL NO. [REDACTED]

MISSION # 1036-1 \* INSTRUMENT # FRWD 11/28/66 DENSITY FREQ DISTR

DENSITY VALUE	PRIMARY MIN MAX LIM	INTERMEDIATE MIN MAX LIM	FULL MIN MAX LIM	ALL LEVELS MIN MAX LIM
1.01	0	0	0	0
1.02	00	00	00	00
1.03	000	000	000	000
1.04	0000	0000	0000	0000
1.05	00000	00000	00000	00000
1.06	000000	000000	000000	000000
1.07	0000000	0000000	0000000	0000000
1.08	00000000	00000000	00000000	00000000
1.09	000000000	000000000	000000000	000000000
1.10	0000000000	0000000000	0000000000	0000000000
1.11	00000000000	00000000000	00000000000	00000000000
1.12	000000000000	000000000000	000000000000	000000000000
1.13	0000000000000	0000000000000	0000000000000	0000000000000
1.14	00000000000000	00000000000000	00000000000000	00000000000000
1.15	000000000000000	000000000000000	000000000000000	000000000000000
1.16	0000000000000000	0000000000000000	0000000000000000	0000000000000000
1.17	00000000000000000	00000000000000000	00000000000000000	00000000000000000
1.18	000000000000000000	000000000000000000	000000000000000000	000000000000000000
1.19	0000000000000000000	0000000000000000000	0000000000000000000	0000000000000000000
1.20	00000000000000000000	00000000000000000000	00000000000000000000	00000000000000000000
1.21	000000000000000000000	000000000000000000000	000000000000000000000	000000000000000000000
1.22	0000000000000000000000	0000000000000000000000	0000000000000000000000	0000000000000000000000
1.23	00000000000000000000000	00000000000000000000000	00000000000000000000000	00000000000000000000000
1.24	000000000000000000000000	000000000000000000000000	000000000000000000000000	000000000000000000000000
1.25	0000000000000000000000000	0000000000000000000000000	0000000000000000000000000	0000000000000000000000000
1.26	00000000000000000000000000	00000000000000000000000000	00000000000000000000000000	00000000000000000000000000
1.27	000000000000000000000000000	000000000000000000000000000	000000000000000000000000000	000000000000000000000000000
1.28	0000000000000000000000000000	0000000000000000000000000000	0000000000000000000000000000	0000000000000000000000000000
1.29	00000000000000000000000000000	00000000000000000000000000000	00000000000000000000000000000	00000000000000000000000000000
1.30	000000000000000000000000000000	000000000000000000000000000000	000000000000000000000000000000	000000000000000000000000000000
1.31	0000000000000000000000000000000	0000000000000000000000000000000	0000000000000000000000000000000	0000000000000000000000000000000
1.32	00000000000000000000000000000000	00000000000000000000000000000000	00000000000000000000000000000000	00000000000000000000000000000000
1.33	000000000000000000000000000000000	000000000000000000000000000000000	000000000000000000000000000000000	000000000000000000000000000000000
1.34	0000000000000000000000000000000000	0000000000000000000000000000000000	0000000000000000000000000000000000	0000000000000000000000000000000000
1.35	00000000000000000000000000000000000	00000000000000000000000000000000000	00000000000000000000000000000000000	00000000000000000000000000000000000
1.36	000000000000000000000000000000000000	000000000000000000000000000000000000	000000000000000000000000000000000000	000000000000000000000000000000000000
1.37	0000000000000000000000000000000000000	0000000000000000000000000000000000000	0000000000000000000000000000000000000	0000000000000000000000000000000000000
1.38	00000000000000000000000000000000000000	00000000000000000000000000000000000000	00000000000000000000000000000000000000	00000000000000000000000000000000000000
1.39	000000000000000000000000000000000000000	000000000000000000000000000000000000000	000000000000000000000000000000000000000	000000000000000000000000000000000000000
1.40	0000000000000000000000000000000000000000	0000000000000000000000000000000000000000	0000000000000000000000000000000000000000	0000000000000000000000000000000000000000
1.41	00000000000000000000000000000000000000000	00000000000000000000000000000000000000000	00000000000000000000000000000000000000000	00000000000000000000000000000000000000000
1.42	000000000000000000000000000000000000000000	000000000000000000000000000000000000000000	000000000000000000000000000000000000000000	000000000000000000000000000000000000000000
1.43	0000000000000000000000000000000000000000000	0000000000000000000000000000000000000000000	0000000000000000000000000000000000000000000	0000000000000000000000000000000000000000000
1.44	00000000000000000000000000000000000000000000	00000000000000000000000000000000000000000000	00000000000000000000000000000000000000000000	00000000000000000000000000000000000000000000
1.45	000000000000000000000000000000000000000000000	000000000000000000000000000000000000000000000	000000000000000000000000000000000000000000000	000000000000000000000000000000000000000000000
1.46	0000000000000000000000000000000000000000000000	0000000000000000000000000000000000000000000000	0000000000000000000000000000000000000000000000	0000000000000000000000000000000000000000000000
1.47	00000000000000000000000000000000000000000000000	00000000000000000000000000000000000000000000000	00000000000000000000000000000000000000000000000	00000000000000000000000000000000000000000000000
1.48	000000000000000000000000000000000000000000000000	000000000000000000000000000000000000000000000000	000000000000000000000000000000000000000000000000	000000000000000000000000000000000000000000000000
1.49	0000000000000000000000000000000000000000000000000	0000000000000000000000000000000000000000000000000	0000000000000000000000000000000000000000000000000	0000000000000000000000000000000000000000000000000
1.50	00000000000000000000000000000000000000000000000000	00000000000000000000000000000000000000000000000000	00000000000000000000000000000000000000000000000000	00000000000000000000000000000000000000000000000000
SUBTOTAL	0	1	3 11 3	1 102 4 114 4

~~TOP SECRET~~

- CONTROL NO. [REDACTED]

TABLE A-1

~~TOP SECRET~~

- CONTROL NO.

MISSION \* 1036-1 \* INSTRUMENT \* FRWD

11/28/65 DENSITY FREQ DISTR

DENSITY VALUE	PRIMARY		INTERMEDIATE		FULL		ALL LEVELS	
	MIN	MAX LIM	MIN	MAX LIM	MIN	MAX LIM	MIN	MAX LIM
1.51	0	0	0	0	0	0	0	0
1.52	0	0	0	0	0	0	0	1
1.53	0	0	0	0	0	0	0	1
1.54	0	0	0	0	0	0	0	1
1.55	0	0	0	0	0	0	0	1
1.56	0	0	0	0	0	0	0	1
1.57	0	0	0	0	0	0	0	1
1.58	0	0	0	0	0	0	0	1
1.59	0	0	0	0	0	0	0	1
1.60	0	0	0	0	0	0	0	1
1.61	0	0	0	0	0	0	0	1
1.62	0	0	0	0	0	0	0	1
1.63	0	0	0	0	0	0	0	1
1.64	0	0	0	0	0	0	0	1
1.65	0	0	0	0	0	0	0	1
1.66	0	0	0	0	0	0	0	1
1.67	0	0	0	0	0	0	0	1
1.68	0	0	0	0	0	0	0	1
1.69	0	0	0	0	0	0	0	1
1.70	0	0	0	0	0	0	0	1
1.71	0	0	0	0	0	0	0	1
1.72	0	0	0	0	0	0	0	1
1.73	0	0	0	0	0	0	0	1
1.74	0	0	0	0	0	0	0	1
1.75	0	0	0	0	0	0	0	1
1.76	0	0	0	0	0	0	0	1
1.77	0	0	0	0	0	0	0	1
1.78	0	0	0	0	0	0	0	1
1.79	0	0	0	0	0	0	0	1
1.80	0	0	0	0	0	0	0	1
1.81	0	0	0	0	0	0	0	1
1.82	0	0	0	0	0	0	0	1
1.83	0	0	0	0	0	0	0	1
1.84	0	0	0	0	0	0	0	1
1.85	0	0	0	0	0	0	0	1
1.86	0	0	0	0	0	0	0	1
1.87	0	0	0	0	0	0	0	1
1.88	0	0	0	0	0	0	0	1
1.89	0	0	0	0	0	0	0	1
1.90	0	0	0	0	0	0	0	1
1.91	0	0	0	0	0	0	0	1
1.92	0	0	0	0	0	0	0	1
1.93	0	0	0	0	0	0	0	1
1.94	0	0	0	0	0	0	0	1
1.95	0	0	0	0	0	0	0	1
1.96	0	0	0	0	0	0	0	1
1.97	0	0	0	0	0	0	0	1
1.98	0	0	0	0	0	0	0	1
1.99	0	0	0	0	0	0	0	1
2.00	0	0	0	0	0	0	0	1
SUBTOTAL	0	0	0	0	3	25	10	97
								13
								122
								24

~~TOP SECRET~~

- CONTROL NO.

TABLE A-1

~~TOP SECRET~~

- CONTROL NO.

MISSION \* 1036-1 \* INSTRUMENT \* FRWD 11/28/66 DENSITY FREQ DISTR

DENSITY VALUE	PRIMARY			INTERMEDIATE			FULL			ALL LEVELS		
	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM
2.01	0	0	0	0	0	0	0	1	0	0	1	1
2.02	0	0	0	0	0	0	1	0	0	1	0	0
2.03	0	0	0	0	0	0	1	0	0	1	0	0
2.04	0	0	0	0	0	0	1	0	0	1	0	0
2.05	0	0	0	0	0	0	1	0	0	1	0	0
2.06	0	0	0	0	0	0	1	0	0	1	0	0
2.07	0	0	0	0	0	0	1	0	0	1	0	0
2.08	0	0	0	0	0	0	1	0	0	1	0	0
2.09	0	0	0	0	0	0	1	0	0	1	0	0
2.10	0	0	0	0	0	0	1	0	0	1	0	0
2.11	0	0	0	0	0	0	1	0	0	1	0	0
2.12	0	0	0	0	0	0	1	0	0	1	0	0
2.13	0	0	0	0	0	0	1	0	0	1	0	0
2.14	0	0	0	0	0	0	1	0	0	1	0	0
2.15	0	0	0	0	0	0	1	0	0	1	0	0
2.16	0	0	0	0	0	0	1	0	0	1	0	0
2.17	0	0	0	0	0	0	1	0	0	1	0	0
2.18	0	0	0	0	0	0	1	0	0	1	0	0
2.19	0	0	0	0	0	0	1	0	0	1	0	0
2.20	0	0	0	0	0	0	1	0	0	1	0	0
2.21	0	0	0	0	0	0	1	0	0	1	0	0
2.22	0	0	0	0	0	0	1	0	0	1	0	0
2.23	0	0	0	0	0	0	1	0	0	1	0	0
2.24	0	0	0	0	0	0	1	0	0	1	0	0
2.25	0	0	0	0	0	0	1	0	0	1	0	0
2.26	0	0	0	0	0	0	1	0	0	1	0	0
2.27	0	0	0	0	0	0	1	0	0	1	0	0
2.28	0	0	0	0	0	0	1	0	0	1	0	0
2.29	0	0	0	0	0	0	1	0	0	1	0	0
2.30	0	0	0	0	0	0	1	0	0	1	0	0
2.31	0	0	0	0	0	0	1	0	0	1	0	0
2.32	0	0	0	0	0	0	1	0	0	1	0	0
2.33	0	0	0	0	0	0	1	0	0	1	0	0
2.34	0	0	0	0	0	0	1	0	0	1	0	0
2.35	0	0	0	0	0	0	1	0	0	1	0	0
2.36	0	0	0	0	0	0	1	0	0	1	0	0
2.37	0	0	0	0	0	0	1	0	0	1	0	0
2.38	0	0	0	0	0	0	1	0	0	1	0	0
2.39	0	0	0	0	0	0	1	0	0	1	0	0
2.40	0	0	0	0	0	0	1	0	0	1	0	0
2.41	0	0	0	0	0	0	1	0	0	1	0	0
2.42	0	0	0	0	0	0	1	0	0	1	0	0
2.43	0	0	0	0	0	0	1	0	0	1	0	0
2.44	0	0	0	0	0	0	1	0	0	1	0	0
2.45	0	0	0	0	0	0	1	0	0	1	0	0
2.46	0	0	0	0	0	0	1	0	0	1	0	0
2.47	0	0	0	0	0	0	1	0	0	1	0	0
2.48	0	0	0	0	0	0	1	0	0	1	0	0
2.49	0	0	0	0	0	0	1	0	0	1	0	0
2.50	0	0	0	0	0	0	1	0	0	1	0	0
SUBTOTAL	0	0	4	0	1	21	14	188	0	15	213	

~~TOP SECRET~~

- CONTROL NO.

TABLE A-1

~~TOP SECRET~~

- CONTROL NO.

MISSION # 1036-1 \* INSTRUMENT # FRWD

11/28/66

DENSITY FREQ DISTR

DENSITY VALUE	PRIMARY			INTERMEDIATE			FULL			ALL LEVELS		
	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM
2.51	0	0	0	0	0	0	0	0	0	0	0	0
2.52	0	0	0	0	0	0	0	0	0	0	0	0
2.53	0	0	0	0	0	0	0	0	0	0	0	0
2.54	0	0	0	0	0	0	0	0	0	0	0	0
2.55	0	0	0	0	0	0	0	0	0	0	0	0
2.56	0	0	0	0	0	0	0	0	0	0	0	0
2.57	0	0	0	0	0	0	0	0	0	0	0	0
2.58	0	0	0	0	0	0	0	0	0	0	0	0
2.59	0	0	0	0	0	0	0	0	0	0	0	0
2.60	0	0	0	0	0	0	0	0	0	0	0	0
2.61	0	0	0	0	0	0	0	0	0	0	0	0
2.62	0	0	0	0	0	0	0	0	0	0	0	0
2.63	0	0	0	0	0	0	0	0	0	0	0	0
2.64	0	0	0	0	0	0	0	0	0	0	0	0
2.65	0	0	0	0	0	0	0	0	0	0	0	0
2.66	0	0	0	0	0	0	0	0	0	0	0	0
2.67	0	0	0	0	0	0	0	0	0	0	0	0
2.68	0	0	0	0	0	0	0	0	0	0	0	0
2.69	0	0	0	0	0	0	0	0	0	0	0	0
2.70	0	0	0	0	0	0	0	0	0	0	0	0
SUBTOTAL	0	0	0	0	0	0	0	0	0	0	0	0
TOTAL	3	3	5	38	38	34	222	222	202	263	263	241

MISSION 1036-1 INSTR - FRWD 11/28/66 PROCESSING AND EXPOSURE ANALYSIS

PROCESS LEVEL	SAMPLE SIZE	UNDER EXPOSED	UNDER PROCESSED	CORRECT EXP+PRDS	OVER PROCESSED	OVER EXPOSED
PRIMARY	3	0 PC	0 PC	100 PC	0 PC	0 PC
INTERMEDIATE	38	5 PC	34 PC	39 PC	13 PC	8 PC
FULL	222	38 PC	0 PC	61 PC	0 PC	0 PC
ALL LEVELS	263	33 PC	5 PC	59 PC	2 PC	1 PC
PROCESS LEVEL	BASE + FOG	UNDER EXPOSED	UNDER PROCESSED	CORRECT EXP+PRDS	OVER PROCESSED	OVER EXPOSED
PRIMARY	0.01-0.09	0.01-0.13	0.14-0.39	0.40-0.90	-----	0.91 AND JF
INTERMED	0.10-0.17	0.01-0.20	0.21-0.39	0.40-0.90	0.91-1.34	1.35 AND JF
FULL	0.18 AND UP	0.01-0.39	-----	0.40-0.90	0.91-1.69	1.70 AND UP

~~TOP SECRET~~

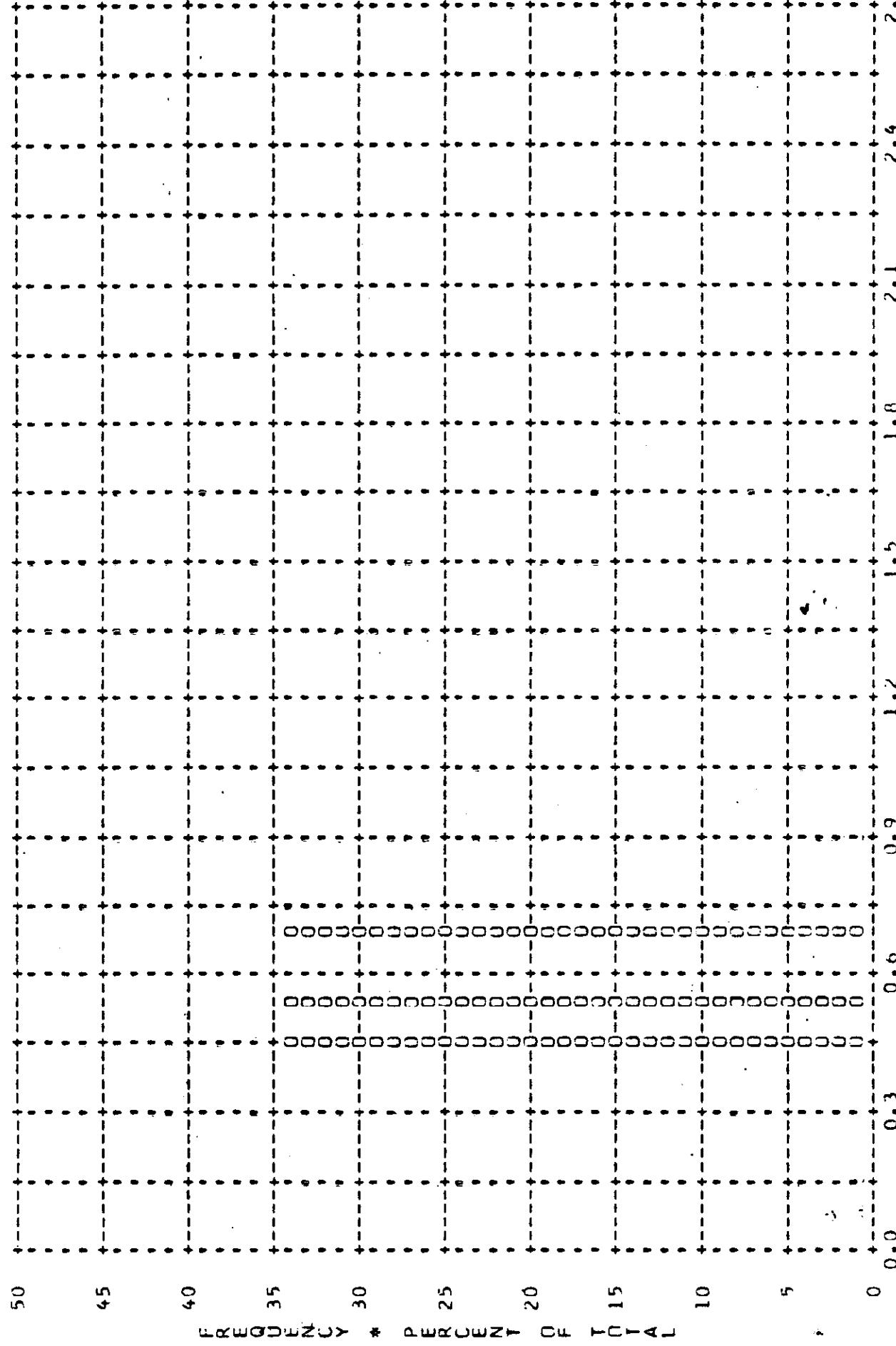
- CONTROL NO.

TABLE A-1

~~TOP SECRET~~

CONTRL NO.

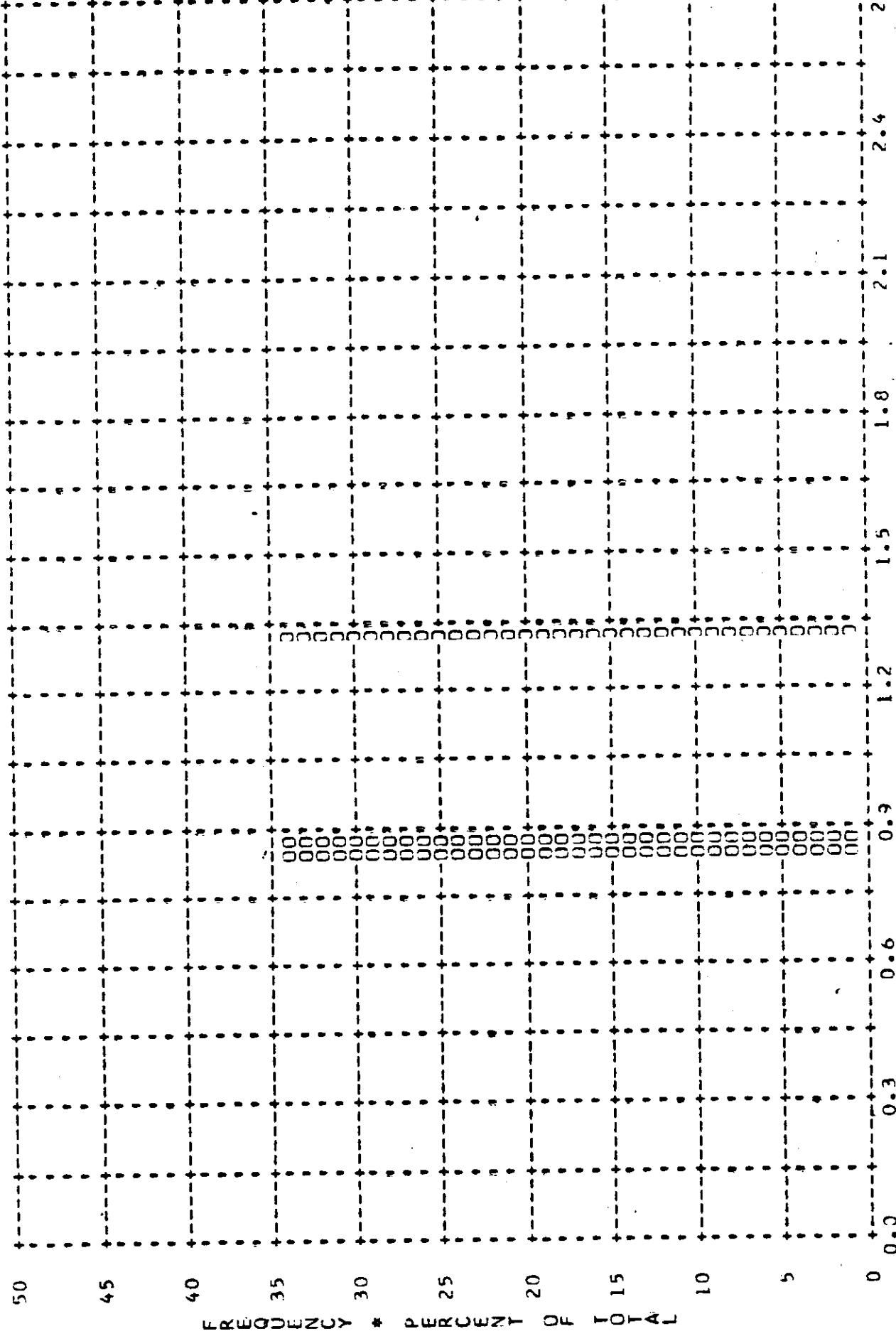
MISSION \* 1036-1 \* INSTR \* FRWD \* 11/28/66 PLOT OF MIN \* TERRAIN \* PROCESSING \* PRIMARY  
ARITH MEAN \* 0.55 \* MEDIAN \* 0.54 \* STD DEV \* 0.12 \* RANGE \* 0.44 TO 0.67 WITH 3 SAMPLES



- CONTROL NO. [REDACTED]

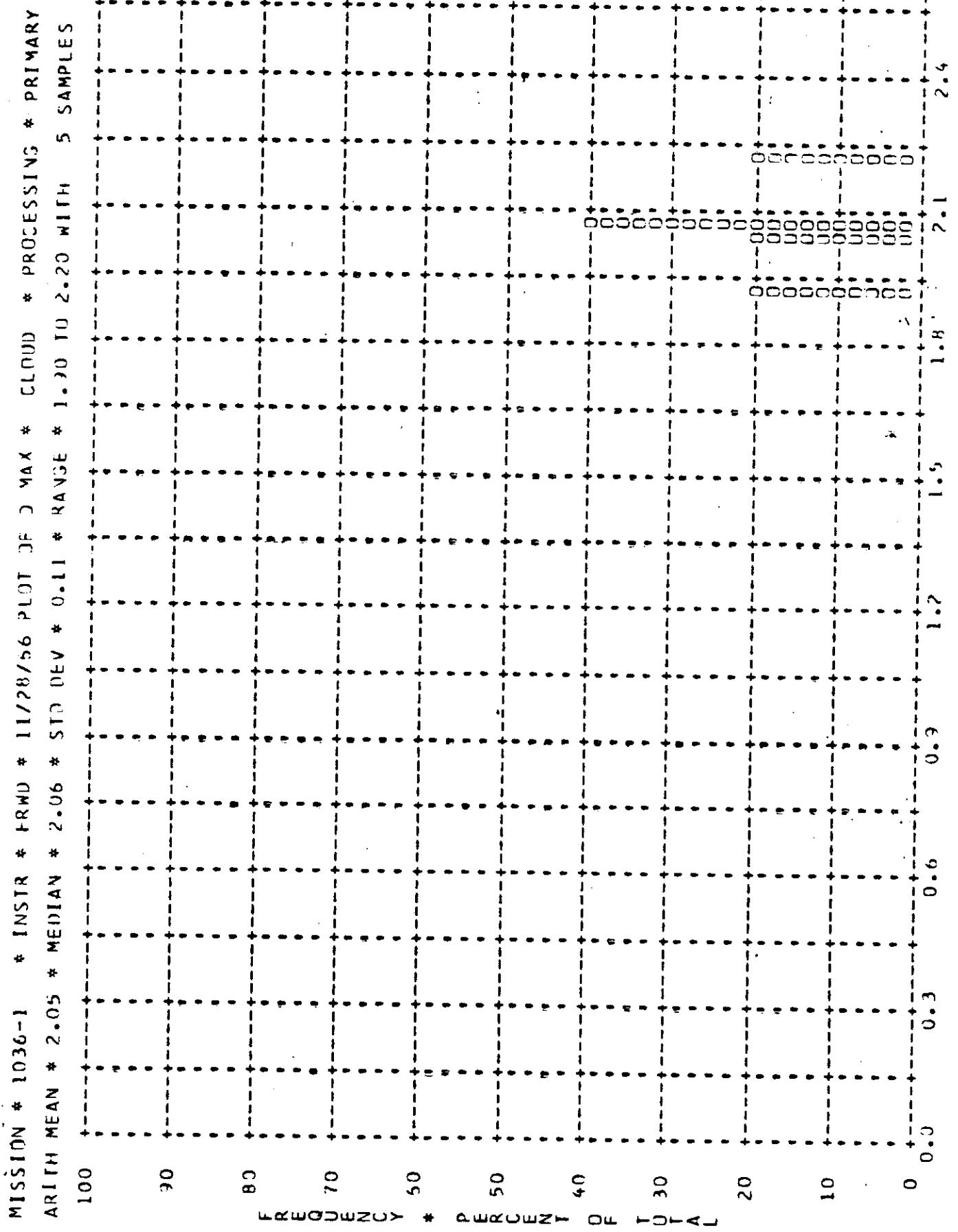
- TEST SET

MISSION \* 1036-1 \* INSTR \* FRWD \* 11/28/66 2107Z MAX \* TERRAIN \* PROCESSING \* PRIMARY  
ARITH MEAN \* 1.01 \* MEDIAN \* 0.87 \* STD DEV \* 0.27 \* RANGE \* 0.84 TO 1.32 WITH 3 SAMPLES



~~TOP SECRET~~

- CONTROL NO. [REDACTED]



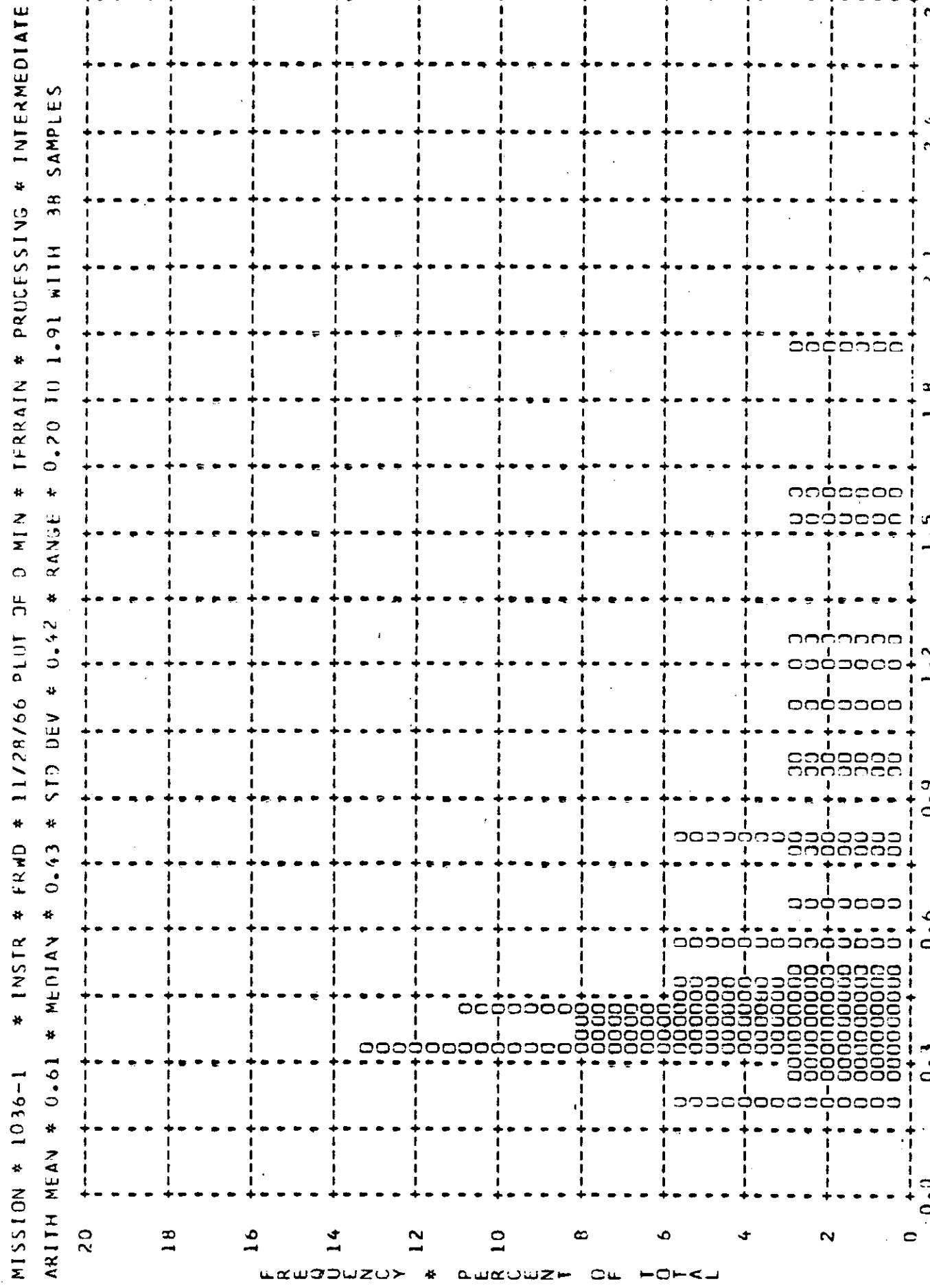
A-9

LAWRENCE

FIGURE A-3

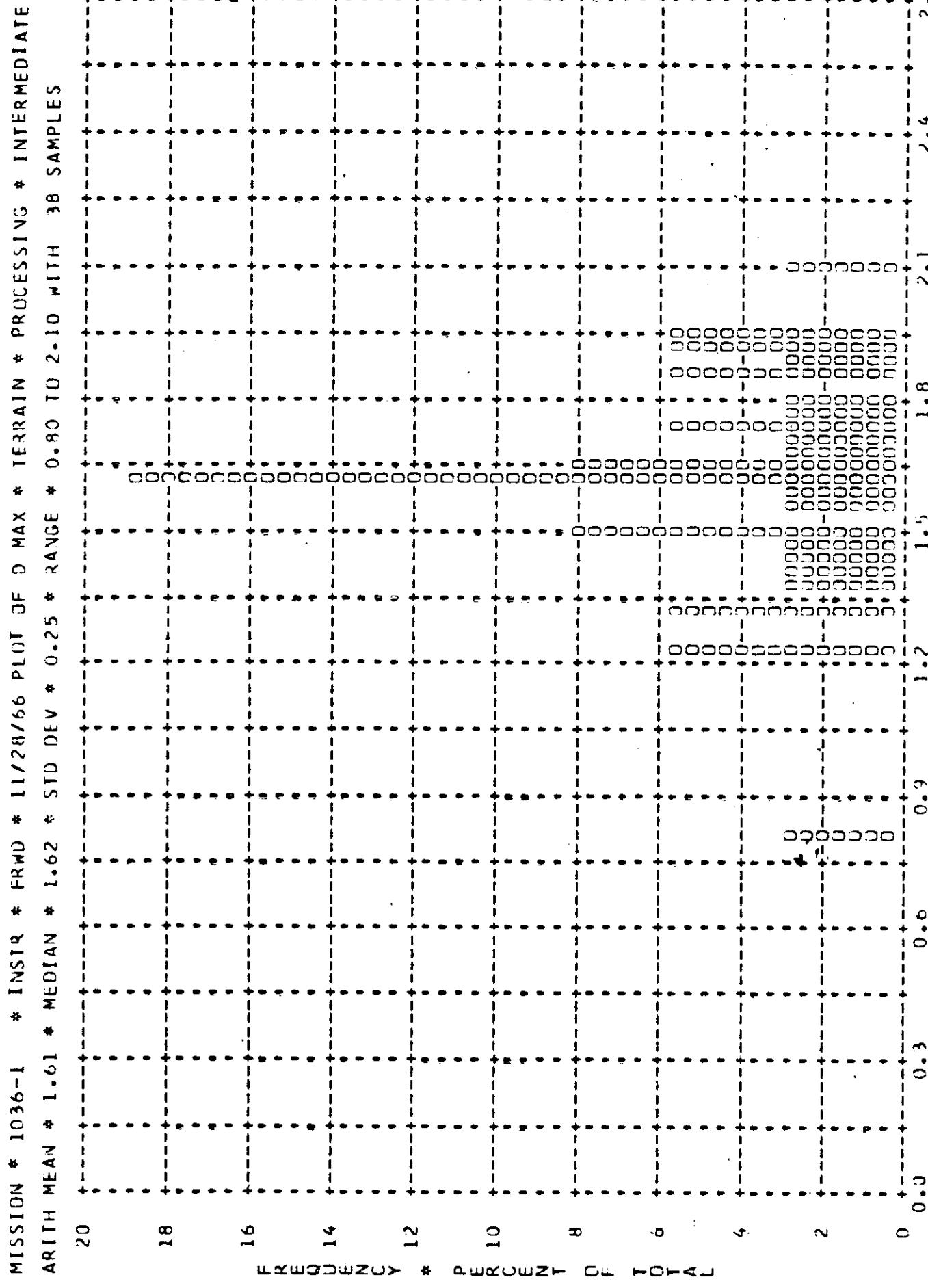
TOP SECRET

- CONTROL NO.



~~TOP SECRET~~

- CONTROL NO.



~~TOP SECRET~~

- CONTROL NO. [REDACTED]

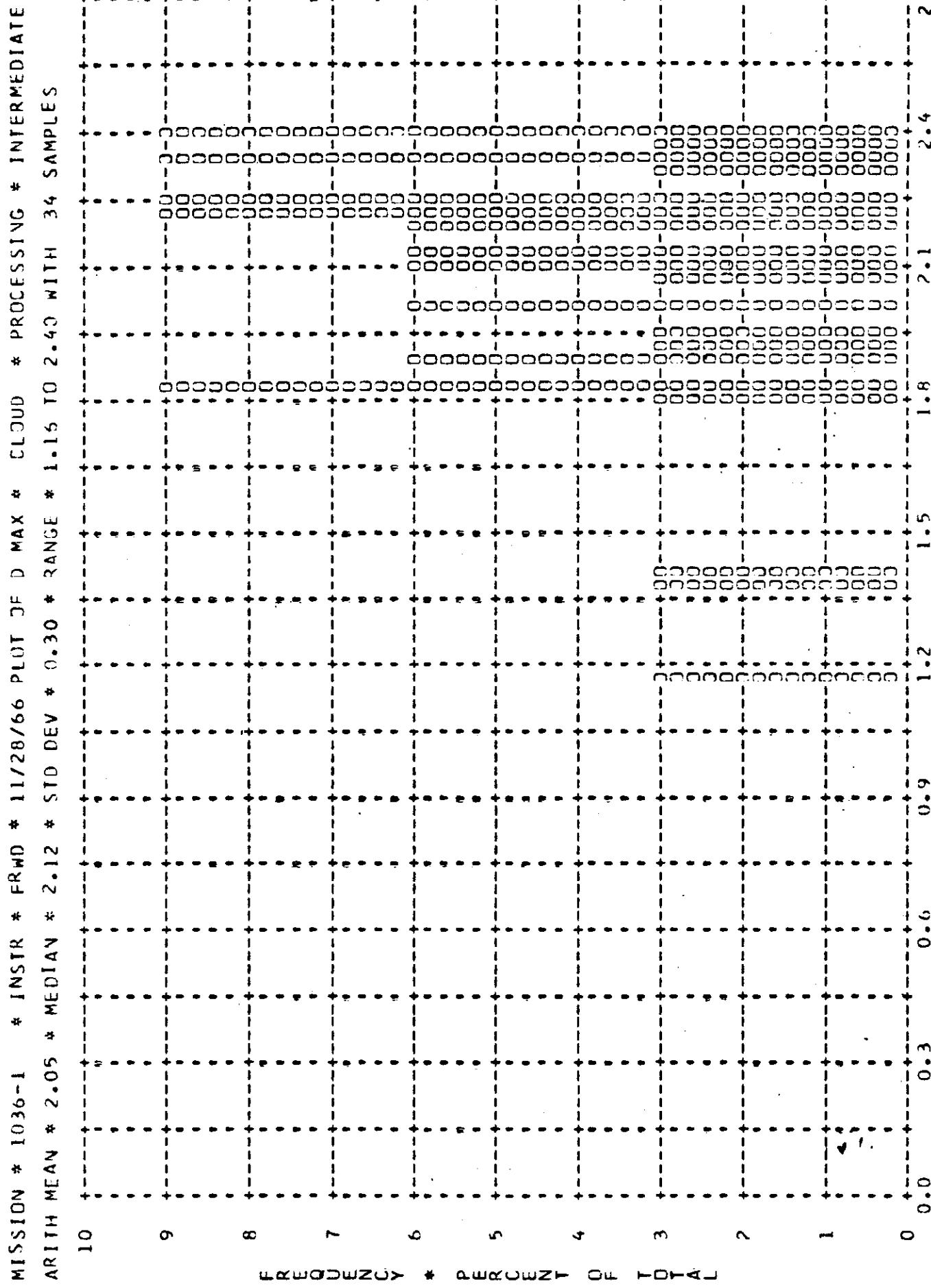
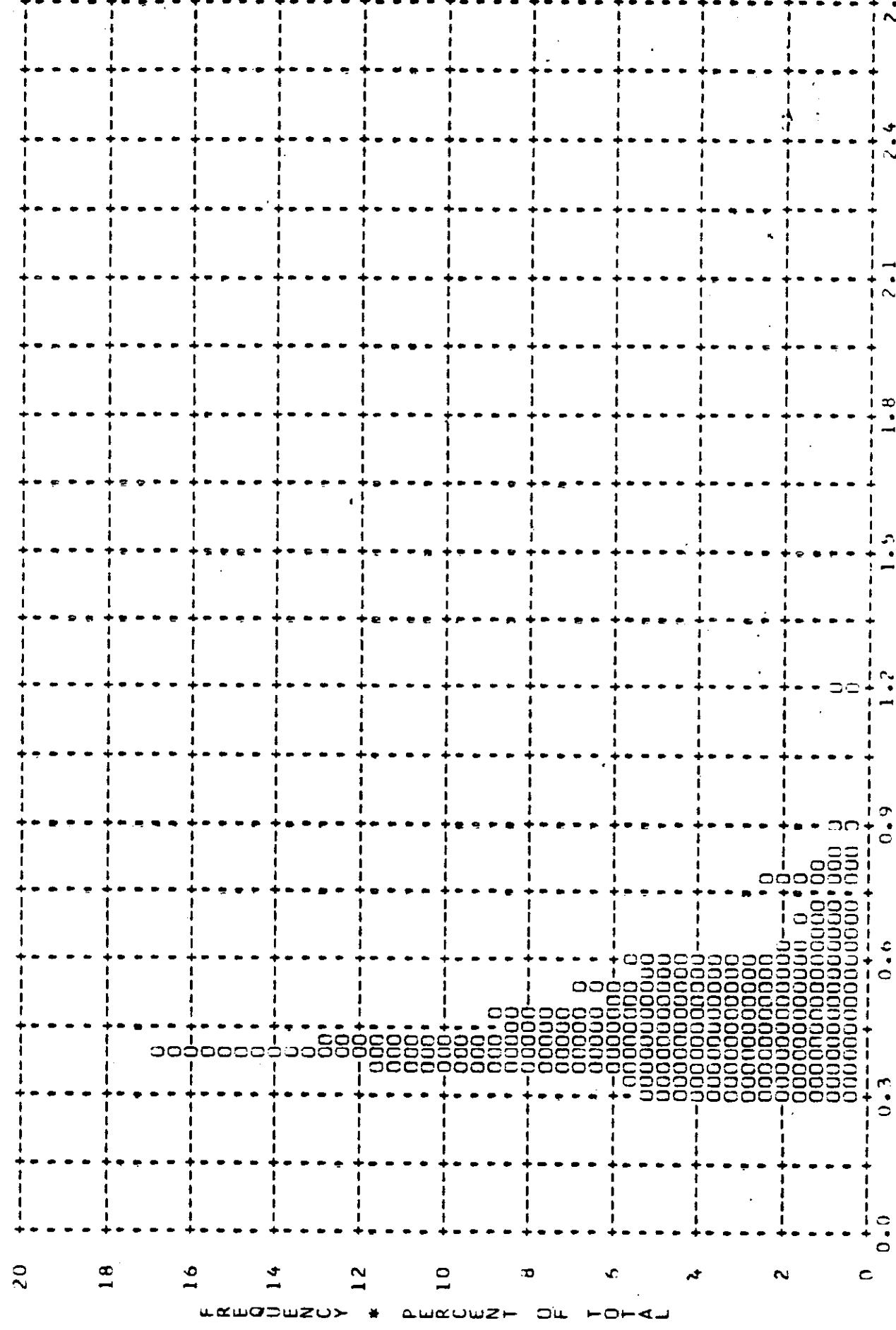


FIGURE A-6

~~TOP SECRET~~

CONTROL NO.

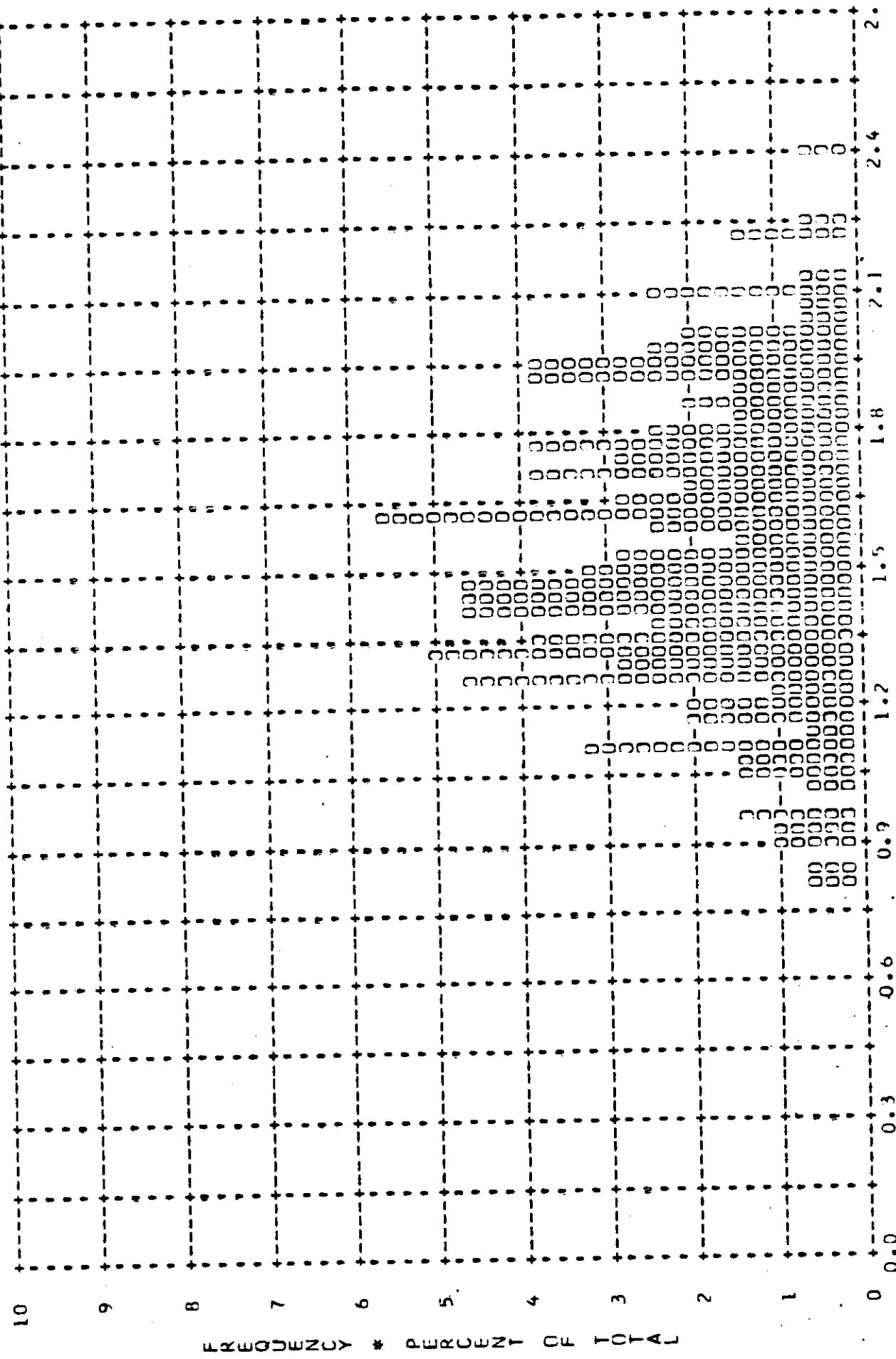
MISSION \* 1036-1 \* INSTR \* FRWD \* 11/28/66 PLOT JFD MIN \* TERRAIN \* PROCESSING \* FULL  
ARITH MEAN \* 0.46 \* MEDIAN \* 0.42 \* STD DEV \* 0.13 \* RANGE \* 0.28 TO 1.18 WITH 222 SAMPLES



TOP SECRET

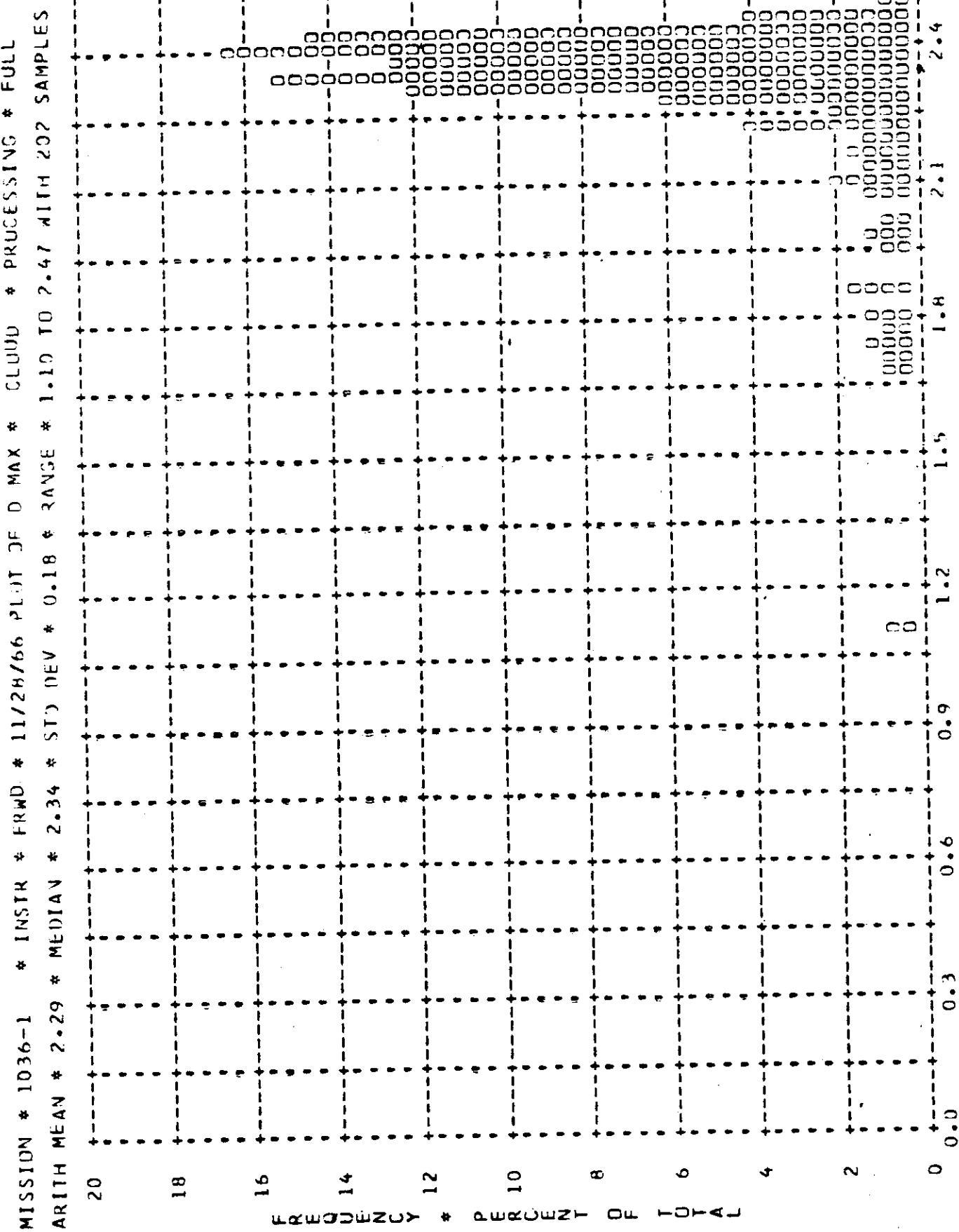
- CONTROL N7.

MISSION \* 1036-1 \* INSTR \* FWD \* 11/28/66 PLNT OF MAX \* TERRAIN \* PROCESSING \* FULL  
ARITH MEAN \* 1.54 \* MEDIAN \* 1.51 \* STD DEV \*.32 \* RANGE \* 0.81 TO 2.40 WITH 222 SAMPLES



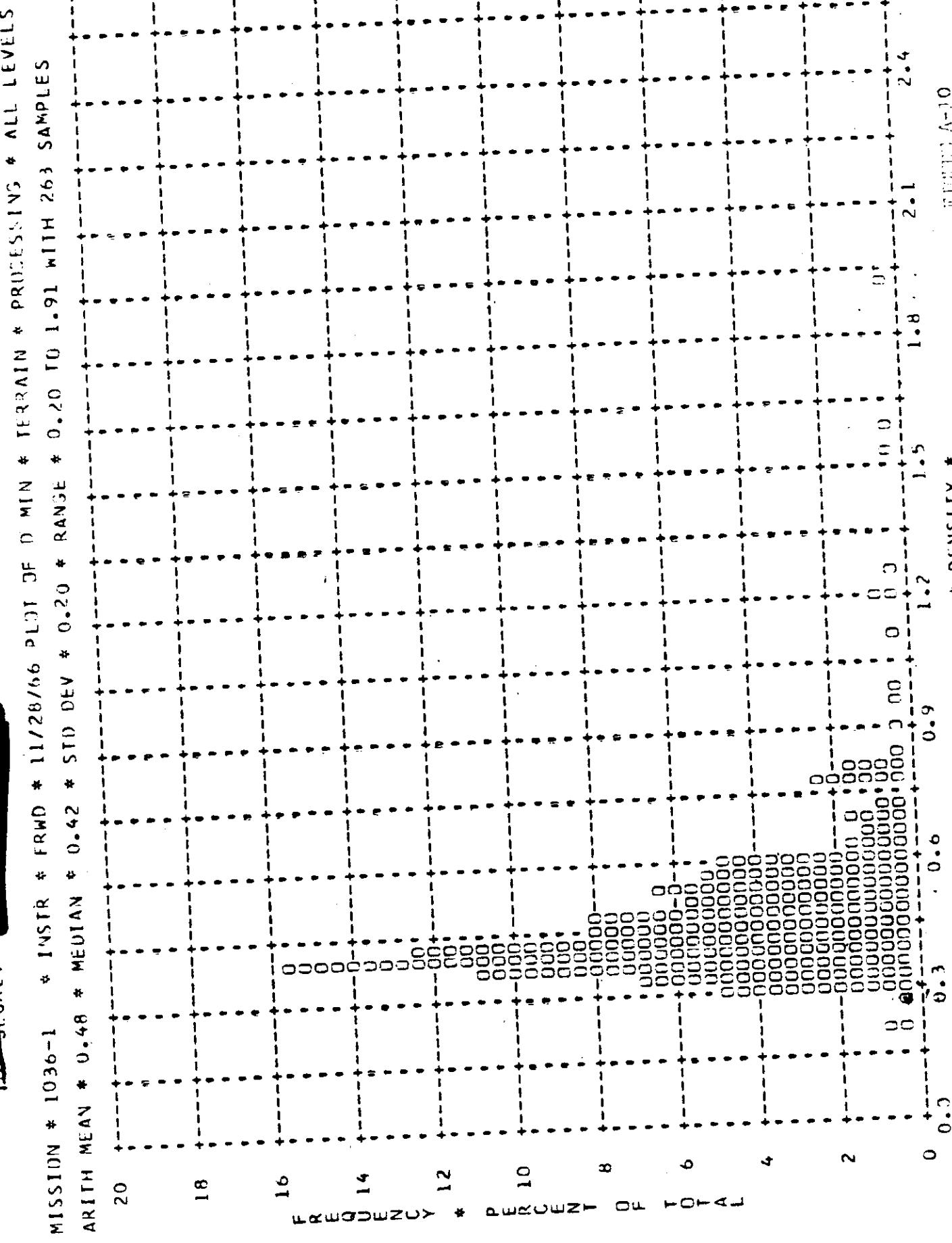
~~CONFIDENTIAL~~

- CONTROL NO. [REDACTED]



TOP SECRET

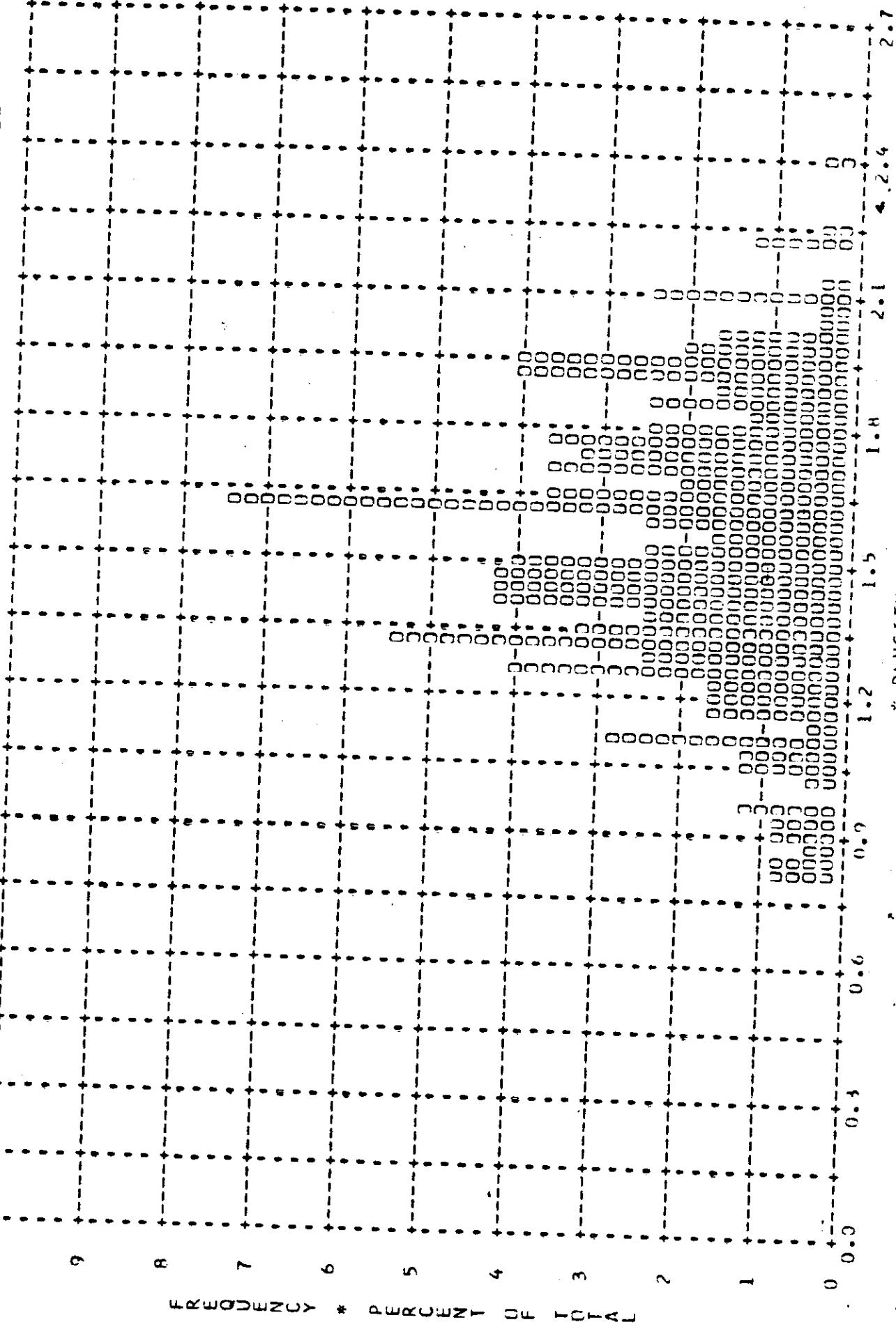
- CONTR. NO.



ପ୍ରକାଶକ

- CONTROL V.O.

MISSION # 1036-1 \* INSTR # FRWD \* 11/28/06 PILOT JF D MAX \* TERRAIN \* PROCESSING \* ALL LEVELS  
ARITH MEAN # 1.54 \* MEDIAN # 1.53 \* STD DEV # 0.31 \* RANGE # 0.80 TO 2.40 WITH 263 SAMPLES



DATA CENTER

- CONTROL NO.

MISSION \* 1036-1 \* INSTR \* FRWD \* 11/28/66 PLOT OF ID MAX \* CLOUN \* PROCESSING \* ALL LEVELS  
ARITH MEAN \* 2.26 \* MEDIAN \* 2.33 \* STD DEV \* 0.22 \* RANGE \* 1.10 TO 2.47 WITH 241 SAMPLES

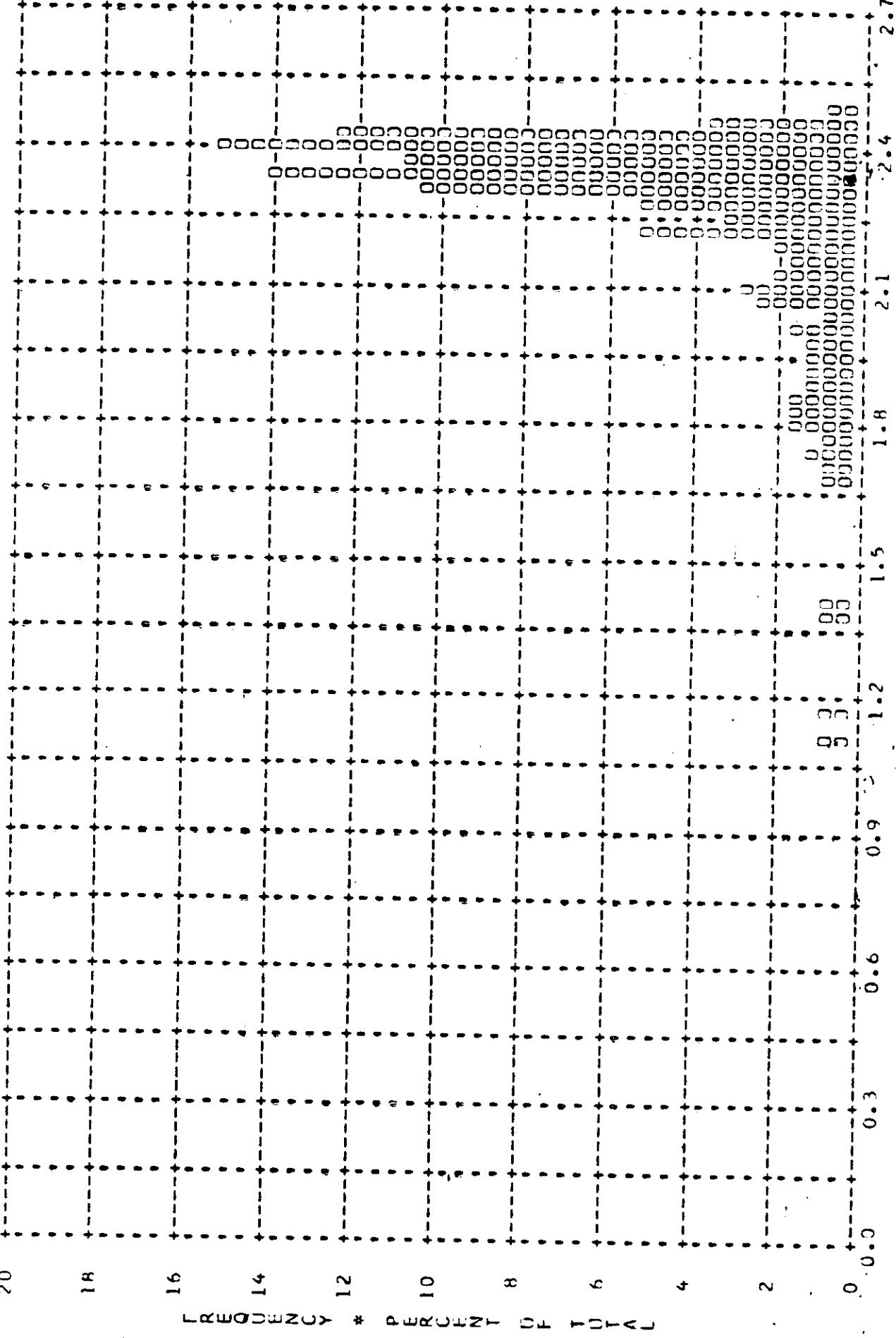


FIGURE A-12

~~TOP SECRET~~

- CONTROL NO.

MISSION \* 1036-1 \* INSTRUMENT \* AFT 11/28/66 DENSITY FREQ DISTR

DENSITY VALUE	PRIMARY			INTERMEDIATE			FULL			ALL LEVELS		
	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM
0.01	0	0	0	0	0	0	0	0	0	0	0	0
0.02	0	0	0	0	0	0	0	0	0	0	0	0
0.03	0	0	0	0	0	0	0	0	0	0	0	0
0.04	0	0	0	0	0	0	0	0	0	0	0	0
0.05	0	0	0	0	0	0	0	0	0	0	0	0
0.06	0	0	0	0	0	0	0	0	0	0	0	0
0.07	0	0	0	0	0	0	0	0	0	0	0	0
0.08	0	0	0	0	0	0	0	0	0	0	0	0
0.09	0	0	0	0	0	0	0	0	0	0	0	0
0.10	0	0	0	0	0	0	0	0	0	0	0	0
0.11	0	0	0	0	0	0	0	0	0	0	0	0
0.12	0	0	0	0	0	0	0	0	0	0	0	0
0.13	0	0	0	0	0	0	0	0	0	0	0	0
0.14	0	0	0	0	0	0	0	0	0	0	0	0
0.15	0	0	0	0	0	0	0	0	0	0	0	0
0.16	0	0	0	0	0	0	0	0	0	0	0	0
0.17	0	0	0	0	0	0	0	0	0	0	0	0
0.18	0	0	0	0	0	0	0	0	0	0	0	0
0.19	0	0	0	0	0	0	0	0	0	0	0	0
0.20	0	0	0	0	0	0	0	0	0	0	0	0
0.21	0	0	0	0	0	0	0	0	0	0	0	0
0.22	0	0	0	0	0	0	0	0	0	0	0	0
0.23	0	0	0	0	0	0	0	0	0	0	0	0
0.24	0	0	0	0	0	0	0	0	0	0	0	0
0.25	0	0	0	0	0	0	0	0	0	0	0	0
0.26	0	0	0	0	0	0	0	0	0	0	0	0
0.27	0	0	0	0	0	0	0	0	0	0	0	0
0.28	0	0	0	0	0	0	0	0	0	0	0	0
0.29	0	0	0	0	0	0	0	0	0	0	0	0
0.30	0	0	0	0	0	0	0	0	0	0	0	0
0.31	0	0	0	0	0	0	0	0	0	0	0	0
0.32	0	0	0	0	0	0	0	0	0	0	0	0
0.33	0	0	0	0	0	0	0	0	0	0	0	0
0.34	0	0	0	0	0	0	0	0	0	0	0	0
0.35	0	0	0	0	0	0	0	0	0	0	0	0
0.36	0	0	0	0	0	0	0	0	0	0	0	0
0.37	0	0	0	0	0	0	0	0	0	0	0	0
0.38	0	0	0	0	0	0	0	0	0	0	0	0
0.39	0	0	0	0	0	0	0	0	0	0	0	0
0.40	0	0	0	0	0	0	0	0	0	0	0	0
0.41	0	0	0	0	0	0	0	0	0	0	0	0
0.42	0	0	0	0	0	0	0	0	0	0	0	0
0.43	0	0	0	0	0	0	0	0	0	0	0	0
0.44	0	0	0	0	0	0	0	0	0	0	0	0
0.45	0	0	0	0	0	0	0	0	0	0	0	0
0.46	0	0	0	0	0	0	0	0	0	0	0	0
0.47	0	0	0	0	0	0	0	0	0	0	0	0
0.48	0	0	0	0	0	0	0	0	0	0	0	0
0.49	0	0	0	0	0	0	0	0	0	0	0	0
0.50	0	0	0	0	0	0	0	0	0	0	0	0
SUBTOTAL	0	0	0	0	10	0	112	0	0	122	0	0

~~TOP SECRET~~

- CONTROL NO.

TABLE A-2

~~TOP SECRET~~

- CONTROL NO.

MISSION \* 1036-1 \* INSTRUMENT \* AFT 11/28/66 DENSITY FREQ DISTR

DENSITY VALUE	PRIMARY			INTERMEDIATE			FULL			ALL LEVELS		
	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM
0.51	0	0	0	1	0	0	11	0	0	12	0	0
0.52	0	0	0	4	0	0	4	0	0	6	0	0
0.53	0	0	0	6	0	0	6	0	0	8	0	0
0.54	0	0	0	8	0	0	8	0	0	8	0	0
0.55	0	0	0	8	0	0	8	0	0	8	0	0
0.56	0	0	0	4	0	0	4	0	0	4	0	0
0.57	0	0	0	7	0	0	7	0	0	7	0	0
0.58	0	0	0	2	0	0	2	0	0	2	0	0
0.59	0	0	0	0	0	0	0	0	0	0	0	0
0.60	0	0	0	0	0	0	0	0	0	0	0	0
0.61	0	0	0	0	0	0	0	0	0	0	0	0
0.62	0	0	0	0	0	0	0	0	0	0	0	0
0.63	0	0	0	0	0	0	0	0	0	0	0	0
0.64	0	0	0	0	0	0	0	0	0	0	0	0
0.65	0	0	0	0	0	0	0	0	0	0	0	0
0.66	0	0	0	0	0	0	0	0	0	0	0	0
0.67	0	0	0	0	0	0	0	0	0	0	0	0
0.68	0	0	0	0	0	0	0	0	0	0	0	0
0.69	0	0	0	0	0	0	0	0	0	0	0	0
0.70	0	0	0	0	0	0	0	0	0	0	0	0
0.71	0	0	0	0	0	0	0	0	0	0	0	0
0.72	0	0	0	0	0	0	0	0	0	0	0	0
0.73	0	0	0	0	0	0	0	0	0	0	0	0
0.74	0	0	0	0	0	0	0	0	0	0	0	0
0.75	0	0	0	0	0	0	0	0	0	0	0	0
0.76	0	0	0	0	0	0	0	0	0	0	0	0
0.77	0	0	0	0	0	0	0	0	0	0	0	0
0.78	0	0	0	0	0	0	0	0	0	0	0	0
0.79	0	0	0	0	0	0	0	0	0	0	0	0
0.80	0	0	0	0	0	0	0	0	0	0	0	0
0.81	0	0	0	0	0	0	0	0	0	0	0	0
0.82	0	0	0	0	0	0	0	0	0	0	0	0
0.83	0	0	0	0	0	0	0	0	0	0	0	0
0.84	0	0	0	0	0	0	0	0	0	0	0	0
0.85	0	0	0	0	0	0	0	0	0	0	0	0
0.86	0	0	0	0	0	0	0	0	0	0	0	0
0.87	0	0	0	0	0	0	0	0	0	0	0	0
0.88	0	0	0	0	0	0	0	0	0	0	0	0
0.89	0	0	0	0	0	0	0	0	0	0	0	0
0.90	0	0	0	0	0	0	0	0	0	0	0	0
0.91	0	0	0	0	0	0	0	0	0	0	0	0
0.92	0	0	0	0	0	0	0	0	0	0	0	0
0.93	0	0	0	0	0	0	0	0	0	0	0	0
0.94	0	0	0	0	0	0	0	0	0	0	0	0
0.95	0	0	0	0	0	0	0	0	0	0	0	0
0.96	0	0	0	0	0	0	0	0	0	0	0	0
0.97	0	0	0	0	0	0	0	0	0	0	0	0
0.98	0	0	0	0	0	0	0	0	0	0	0	0
0.99	0	0	0	0	0	0	0	0	0	0	0	0
1.00	0	0	0	0	0	0	0	0	0	0	0	0
SUBTOTAL	0	0	0	10	3	0	117	23	0	127	26	0

~~TOP SECRET~~

- CONTROL NO.

TABLE A-2

TOP SECRET

- CONTROL NO.

MISSION # 1036-1 \* INSTRUMENT # AFT 11/28/66 DENSITY FREQ DISTR

TOP SECRET

- CONTROL NO.

TABLE A-2

~~TOP SECRET~~

- CONTROL NO.

MISSION \* 1036-1 \* INSTRUMENT \* AFT 11/28/66 DENSITY FREQ DISTR

DENSITY VALUE	PRIMARY			INTERMEDIATE			FULL			ALL LEVELS		
	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM
1.51	0	0	0	0	0	0	0	3	3	0	3	0
1.52	0	0	0	0	0	0	0	3	3	0	3	1
1.53	0	0	0	0	0	0	0	1	0	0	0	0
1.54	0	0	0	0	0	0	0	0	6	1	0	6
1.55	0	0	0	0	0	0	0	1	2	3	2	1
1.56	0	0	0	0	0	0	0	1	2	3	5	2
1.57	0	0	0	0	0	0	0	1	2	3	4	1
1.58	0	0	0	0	0	0	0	1	2	3	5	3
1.59	0	0	0	0	0	0	0	1	2	3	4	1
1.60	0	0	0	0	0	0	0	1	2	3	5	2
1.61	0	0	0	0	0	0	0	1	2	3	8	3
1.62	0	0	0	0	0	0	0	1	2	3	3	3
1.63	0	0	0	0	0	0	0	1	2	3	3	3
1.64	0	0	0	0	0	0	0	1	1	1	1	1
1.65	0	0	0	0	0	0	0	1	1	1	1	1
1.66	0	0	0	0	0	0	0	1	1	1	1	1
1.67	0	0	0	0	0	0	0	1	1	1	1	1
1.68	0	0	0	0	0	0	0	1	1	1	1	1
1.69	0	0	0	0	0	0	0	1	1	1	1	1
1.70	0	0	0	0	0	0	0	1	1	1	1	1
1.71	0	0	0	0	0	0	0	1	1	1	1	1
1.72	0	0	0	0	0	0	0	1	1	1	1	1
1.73	0	0	0	0	0	0	0	1	1	1	1	1
1.74	0	0	0	0	0	0	0	1	1	1	1	1
1.75	0	0	0	0	0	0	0	1	1	1	1	1
1.76	0	0	0	0	0	0	0	1	1	1	1	1
1.77	0	0	0	0	0	0	0	1	1	1	1	1
1.78	0	0	0	0	0	0	0	1	1	1	1	1
1.79	0	0	0	0	0	0	0	1	1	1	1	1
1.80	0	0	0	0	0	0	0	1	1	1	1	1
1.81	0	0	0	0	0	0	0	1	1	1	1	1
1.82	0	0	0	0	0	0	0	1	1	1	1	1
1.83	0	0	0	0	0	0	0	1	1	1	1	1
1.84	0	0	0	0	0	0	0	1	1	1	1	1
1.85	0	0	0	0	0	0	0	1	1	1	1	1
1.86	0	0	0	0	0	0	0	1	1	1	1	1
1.87	0	0	0	0	0	0	0	1	1	1	1	1
1.88	0	0	0	0	0	0	0	1	1	1	1	1
1.89	0	0	0	0	0	0	0	1	1	1	1	1
1.90	0	0	0	0	0	0	0	1	1	1	1	1
1.91	0	0	0	0	0	0	0	1	1	1	1	1
1.92	0	0	0	0	0	0	0	1	1	1	1	1
1.93	0	0	0	0	0	0	0	1	1	1	1	1
1.94	0	0	0	0	0	0	0	1	1	1	1	1
1.95	0	0	0	0	0	0	0	1	1	1	1	1
1.96	0	0	0	0	0	0	0	1	1	1	1	1
1.97	0	0	0	0	0	0	0	1	1	1	1	1
1.98	0	0	0	0	0	0	0	1	1	1	1	1
1.99	0	0	0	0	0	0	0	1	1	1	1	1
2.00	0	0	0	0	0	0	0	1	1	1	1	1
SUBTOTAL	0	0	0	1	13	9	0	112	13	1	125	22

~~TOP SECRET~~

- CONTROL NO.

TABLE A-2

~~TOP SECRET~~

- CONTROL NO.

MISSION \* 1036-1 \* INSTRUMENT \* AFT 11/28/66 DENSITY FREQ DISTR

DENSITY VALUE	PRIMARY		INTERMEDIATE		FULL		ALL LEVELS	
	MIN	MAX LIM	MIN	MAX LIM	MIN	MAX LIM	MIN	MAX LIM
2.01	0	0	0	0	0	0	0	0
2.02	0	0	0	0	0	0	0	0
2.03	0	0	0	0	0	0	0	0
2.04	0	0	0	0	0	0	0	0
2.05	0	0	0	0	0	0	0	0
2.06	0	0	0	0	0	0	0	0
2.07	0	0	0	0	0	0	0	0
2.08	0	0	0	0	0	0	0	0
2.09	0	0	0	0	0	0	0	0
2.10	0	0	0	0	0	0	0	0
2.11	0	0	0	0	0	0	0	0
2.12	0	0	0	0	0	0	0	0
2.13	0	0	0	0	0	0	0	0
2.14	0	0	0	0	0	0	0	0
2.15	0	0	0	0	0	0	0	0
2.16	0	0	0	0	0	0	0	0
2.17	0	0	0	0	0	0	0	0
2.18	0	0	0	0	0	0	0	0
2.19	0	0	0	0	0	0	0	0
2.20	0	0	0	0	0	0	0	0
2.21	0	0	0	0	0	0	0	0
2.22	0	0	0	0	0	0	0	0
2.23	0	0	0	0	0	0	0	0
2.24	0	0	0	0	0	0	0	0
2.25	0	0	0	0	0	0	0	0
2.26	0	0	0	0	0	0	0	0
2.27	0	0	0	0	0	0	0	0
2.28	0	0	0	0	0	0	0	0
2.29	0	0	0	0	0	0	0	0
2.30	0	0	0	0	0	0	0	0
2.31	0	0	0	0	0	0	0	0
2.32	0	0	0	0	0	0	0	0
2.33	0	0	0	0	0	0	0	0
2.34	0	0	0	0	0	0	0	0
2.35	0	0	0	0	0	0	0	0
2.36	0	0	0	0	0	0	0	0
2.37	0	0	0	0	0	0	0	0
2.38	0	0	0	0	0	0	0	0
2.39	0	0	0	0	0	0	0	0
2.40	0	0	0	0	0	0	0	0
2.41	0	0	0	0	0	0	0	0
2.42	0	0	0	0	0	0	0	0
2.43	0	0	0	0	0	0	0	0
2.44	0	0	0	0	0	0	0	0
2.45	0	0	0	0	0	0	0	0
2.46	0	0	0	0	0	0	0	0
2.47	0	0	0	0	0	0	0	0
2.48	0	0	0	0	0	0	0	0
2.49	0	0	0	0	0	0	0	0
2.50	0	0	0	0	0	0	0	0
SUBTOTAL	0	0	0	0	16	0	203	8 219

~~TOP SECRET~~

- CONTROL NO.

TABLE A-2

~~TOP SECRET~~

- CONTROL NO.

MISSION # 1036-1 \* INSTRUMENT \* AFT 11/28/66 DENSITY FREQ DISTR

DENSITY VALUE	PRIMARY			INTERMEDIATE			FULL			ALL LEVELS		
	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM
2.51	0	0	0	0	0	0	0	0	0	0	0	0
2.52	0	0	0	0	0	0	0	0	0	0	0	0
2.53	0	0	0	0	0	0	0	0	0	0	0	0
2.54	0	0	0	0	0	0	0	0	0	0	0	0
2.55	0	0	0	0	0	0	0	0	0	0	0	0
2.56	0	0	0	0	0	0	0	0	0	0	0	0
2.57	0	0	0	0	0	0	0	0	0	0	0	0
2.58	0	0	0	0	0	0	0	0	0	0	0	0
2.59	0	0	0	0	0	0	0	0	0	0	0	0
2.60	0	0	0	0	0	0	0	0	0	0	0	0
2.61	0	0	0	0	0	0	0	0	0	0	0	0
2.62	0	0	0	0	0	0	0	0	0	0	0	0
2.63	0	0	0	0	0	0	0	0	0	0	0	0
2.64	0	0	0	0	0	0	0	0	0	0	0	0
2.65	0	0	0	0	0	0	0	0	0	0	0	0
2.66	0	0	0	0	0	0	0	0	0	0	0	0
2.67	0	0	0	0	0	0	0	0	0	0	0	0
2.68	0	0	0	0	0	0	0	0	0	0	0	0
2.69	0	0	0	0	0	0	0	0	0	0	0	0
2.70	0	0	0	0	0	0	0	0	0	0	0	0
SUBTOTAL	0	0	0	0	0	0	0	0	0	0	0	0
TOTAL	0	0	0	27	27	26	233	233	218	260	260	244

MISSION 1036-1 INSTR - AFT 11/28/66 PROCESSING AND EXPOSURE ANALYST

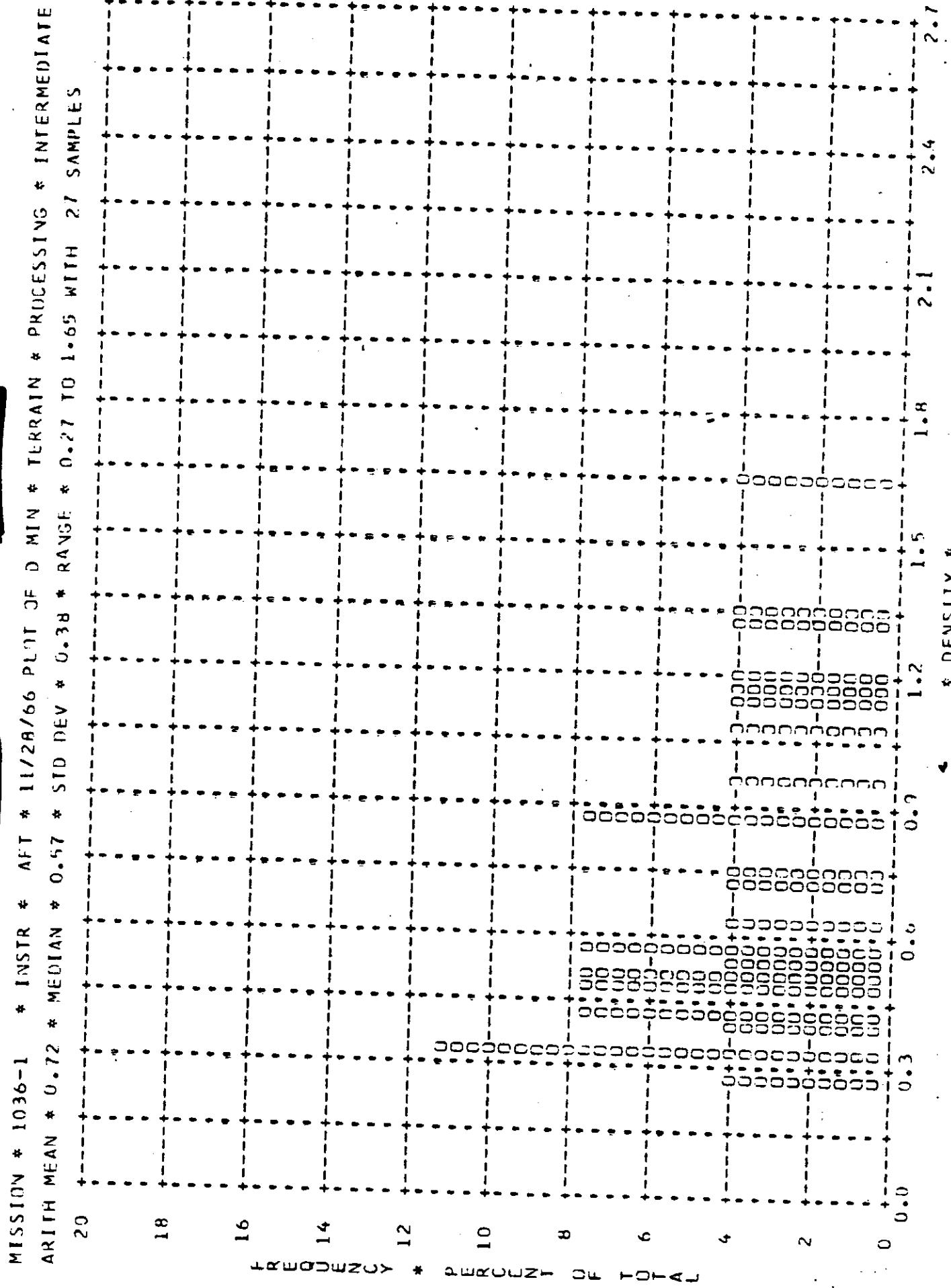
PROCESS LEVEL	SAMPLE SIZE	UNDER EXPOSED		UNDER PROCESSED		CORRECT EXP+PRDC		OVER PROCESSED		OVER EXPOSED	
		PC	PC	PC	PC	PC	PC	PC	PC	PC	PC
PRIMARY	0	0	0	0	0	0	0	0	0	0	0
INTERMEDIATE	27	0	0	19	52	0	26	0	4	0	0
FULL	233	14	14	0	83	3	3	0	0	0	0
ALL LEVELS	260	12	12	2	80	5	5	0	0	0	0
PROCESS LEVEL	BASE + FOG	UNDER EXPOSED	UNDER PROCESSED	CORRECT EXP+PRDC	OVER PROCESSED	OVER EXPOSED					
PRIMARY	0.01-0.09	0.01-0.13	0.14-0.39	0.40-0.90	-----	-----	0.91	AND UP			
INTERMED	0.10-0.17	0.01-0.20	0.21-0.39	0.40-0.90	0.91-1.34	1.35	AND UP				
FULL	0.18 AND UP	0.01-0.39	-----	0.40-0.90	0.91-1.69	1.70	AND UP				

~~TOP SECRET~~

- CONTROL NO.

TABLE A-2

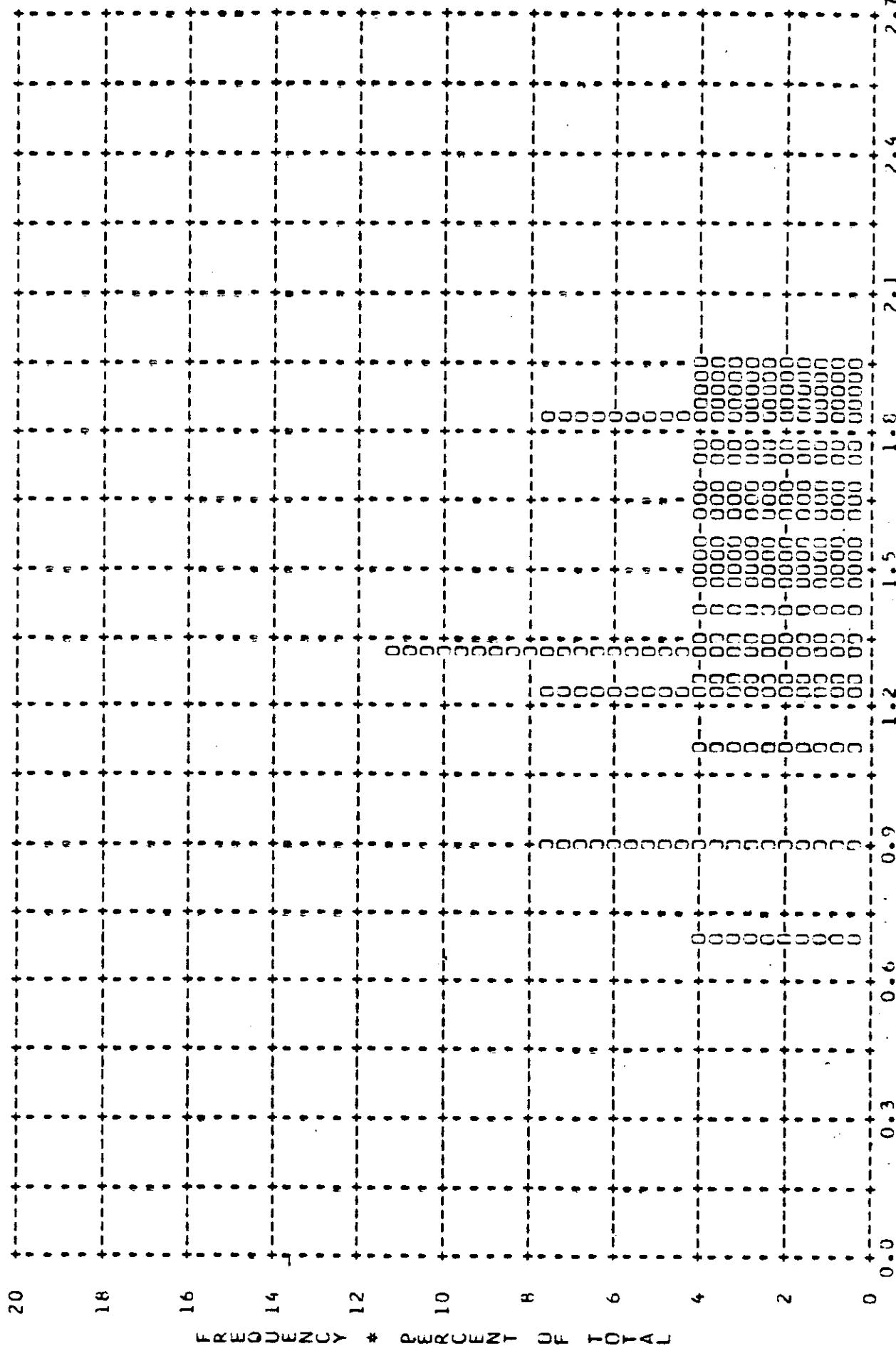
~~TOP SECRET~~



~~TOP SECRET~~

- CONTROL NO.

MISSION \* 1036-1 \* INSTR \* AFT \* 11/28/66 PLUT DF D MAX \* TERRAIN \* PROCESSING \* INTERMEDIATE  
ARITH MEAN \* 1.47 \* MEDIAN \* 1.50 \* STD DEV \* 0.33 \* RANGE \* 0.69 TO 1.94 WITH 27 SAMPLES



~~TOP SECRET~~

NO.

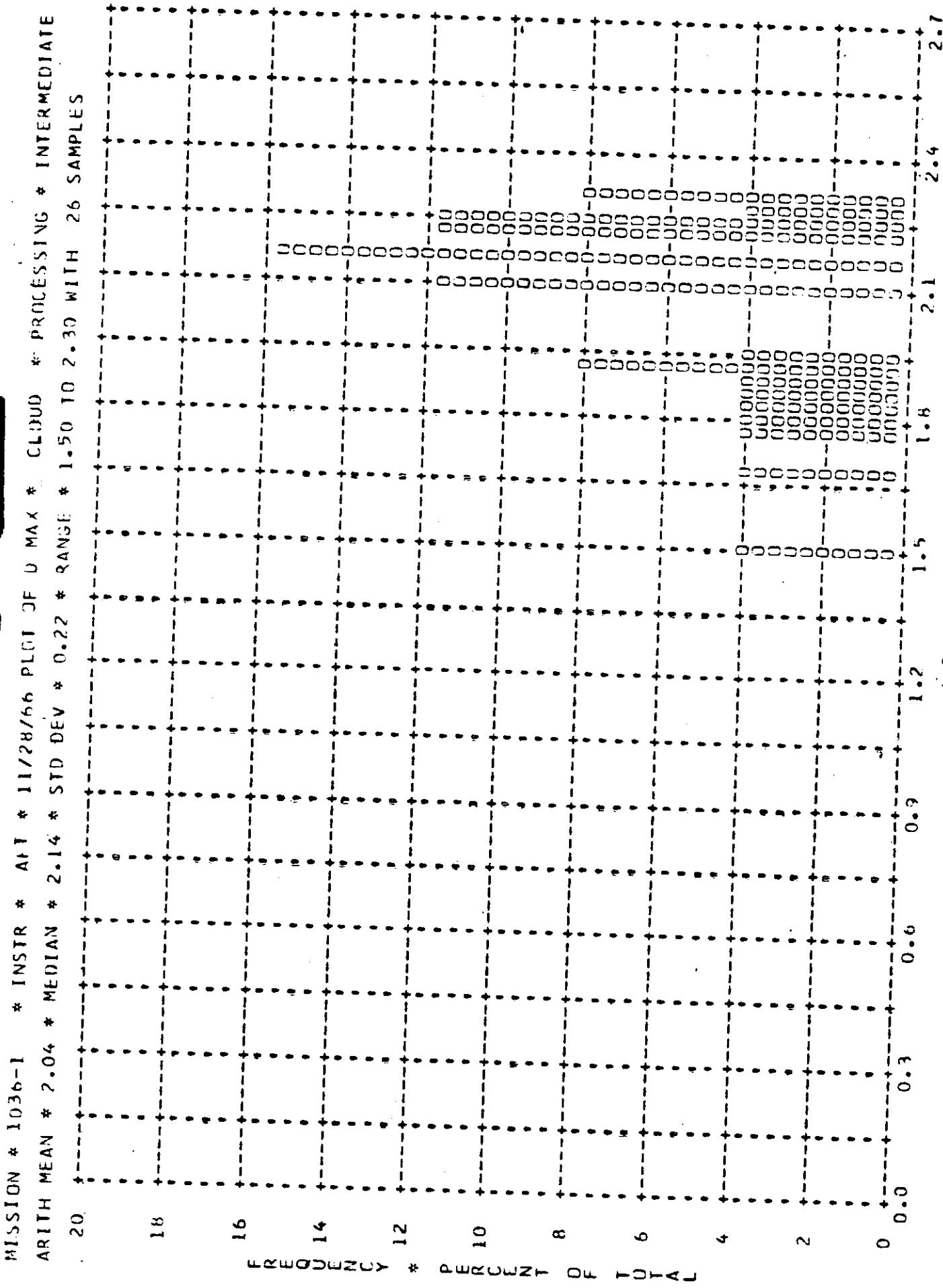
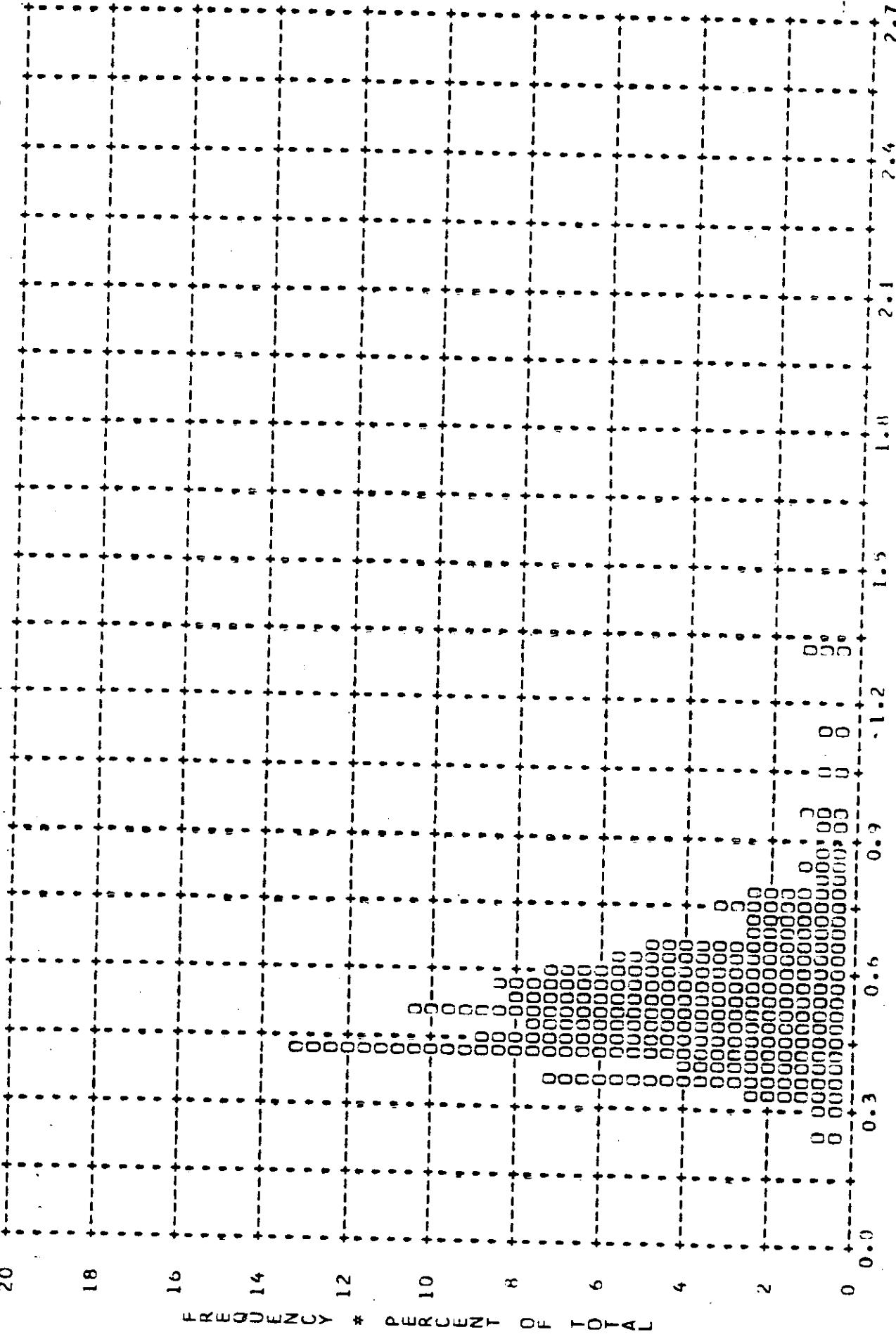


FIGURE A-15

HOP SECURE

- CONTROL NO. [REDACTED]

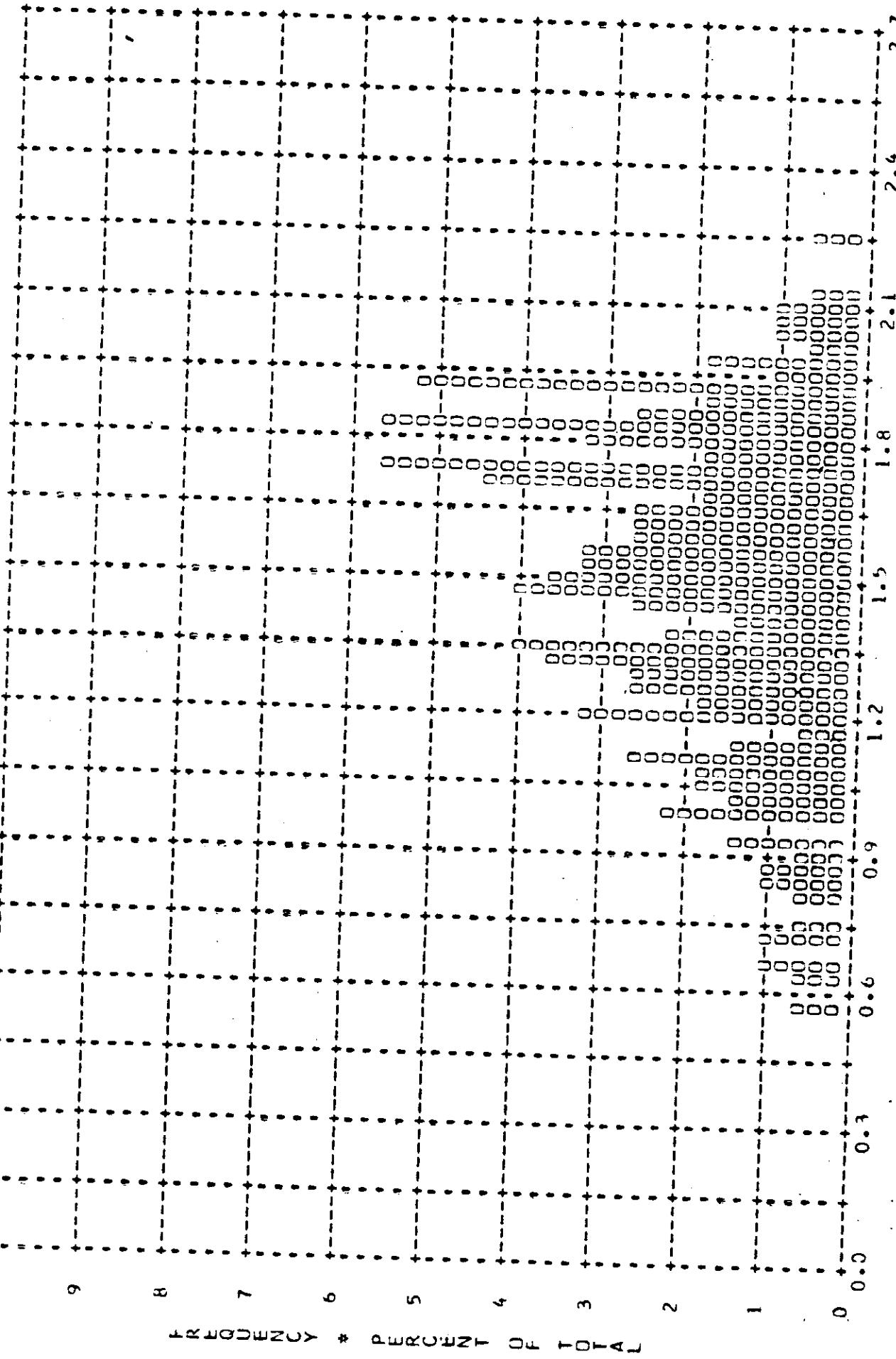
MISSION \* 1036-1 \* INSTR \* AFT \* 11/28/66 PLOT OF MIN \* TERRAIN \* PROCESSING \* FULL  
ARITH MEAN \* 0.53 \* MEDIAN \* 0.51 \* STD DEV \* 0.16 \* RANGE \* 0.24 TO 1.30 WITH 233 SAMPLES



~~TOP SECRET~~

- CONTROL VO.

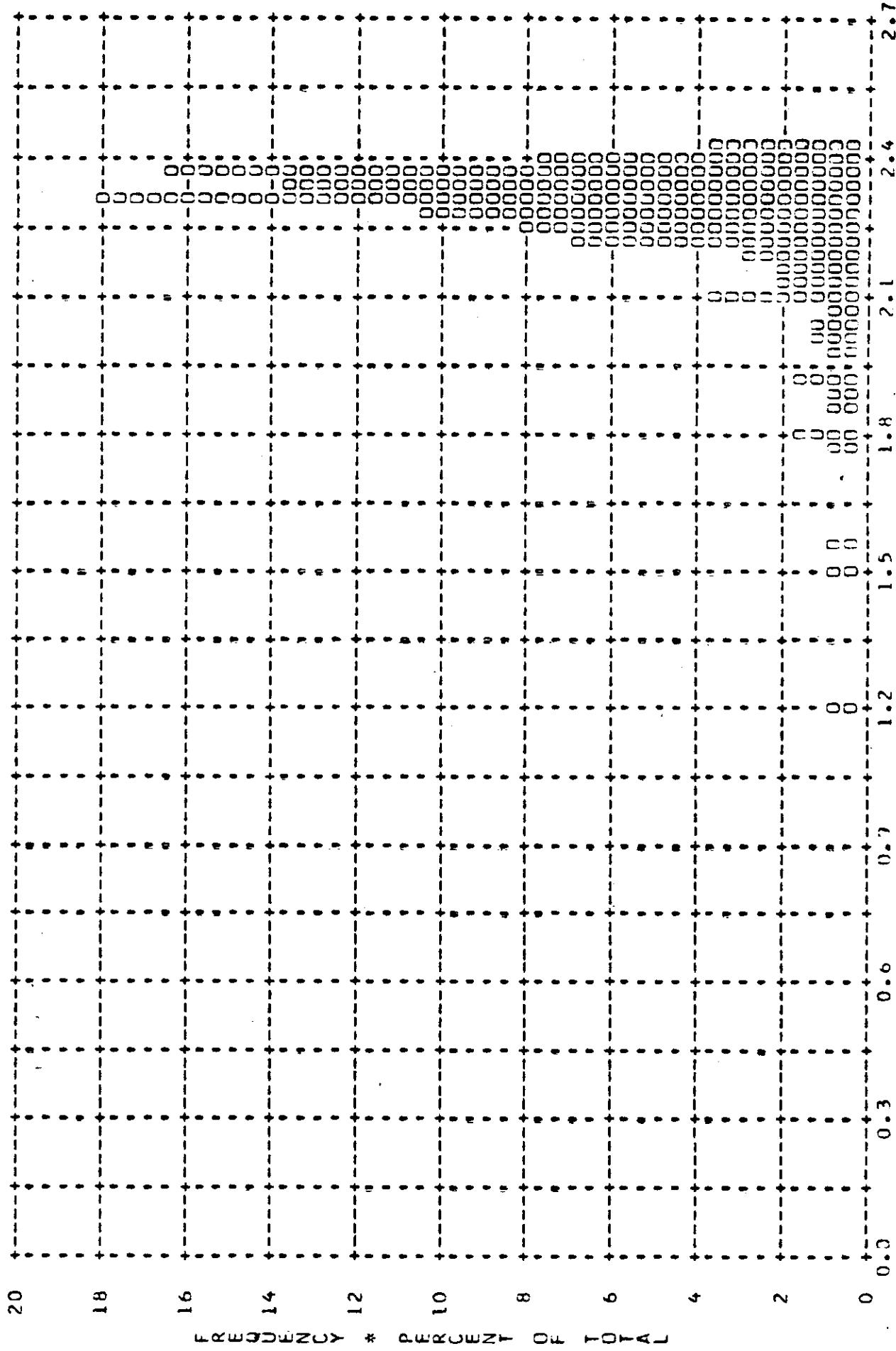
MISSION \* 1036-1 \* INSTR \* AFT \* 11/28/66 PLUT DF D MAX \* TERRAIN \* PROCESSING \* FULL  
ARITH MEAN \* 1.49 \* MEDIAN \* 1.52 \* STD DEV \* 0.34 \* RANGE \* 0.55 TO 2.25 WITH 233 SAMPLES



TOP SECRET

- CONTROL NO.

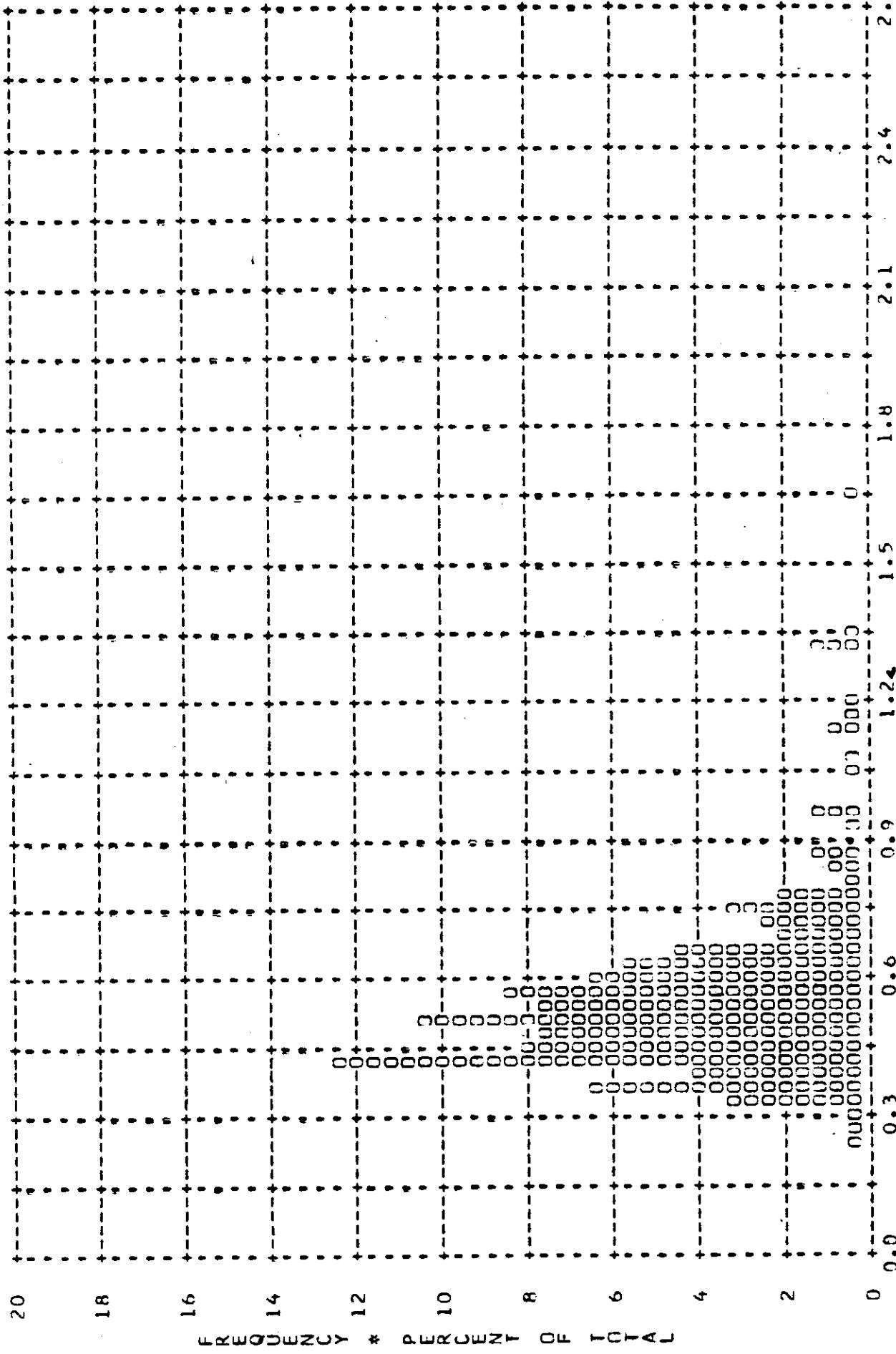
MISSION \* 1036-1 \* INSTR \* AFT \* 11/28/66 PLUT CF D MAX \* CLOUD \* PROCESSING \* FULL  
ARITH MEAN \* 2.26 \* MEDIAN \* 2.30 \* STD DEV \* 0.16 \* RANGE \* 1.20 TO 2.43 WITH 218 SAMPLES



~~TOP SECRET~~

- CONTROL NO.

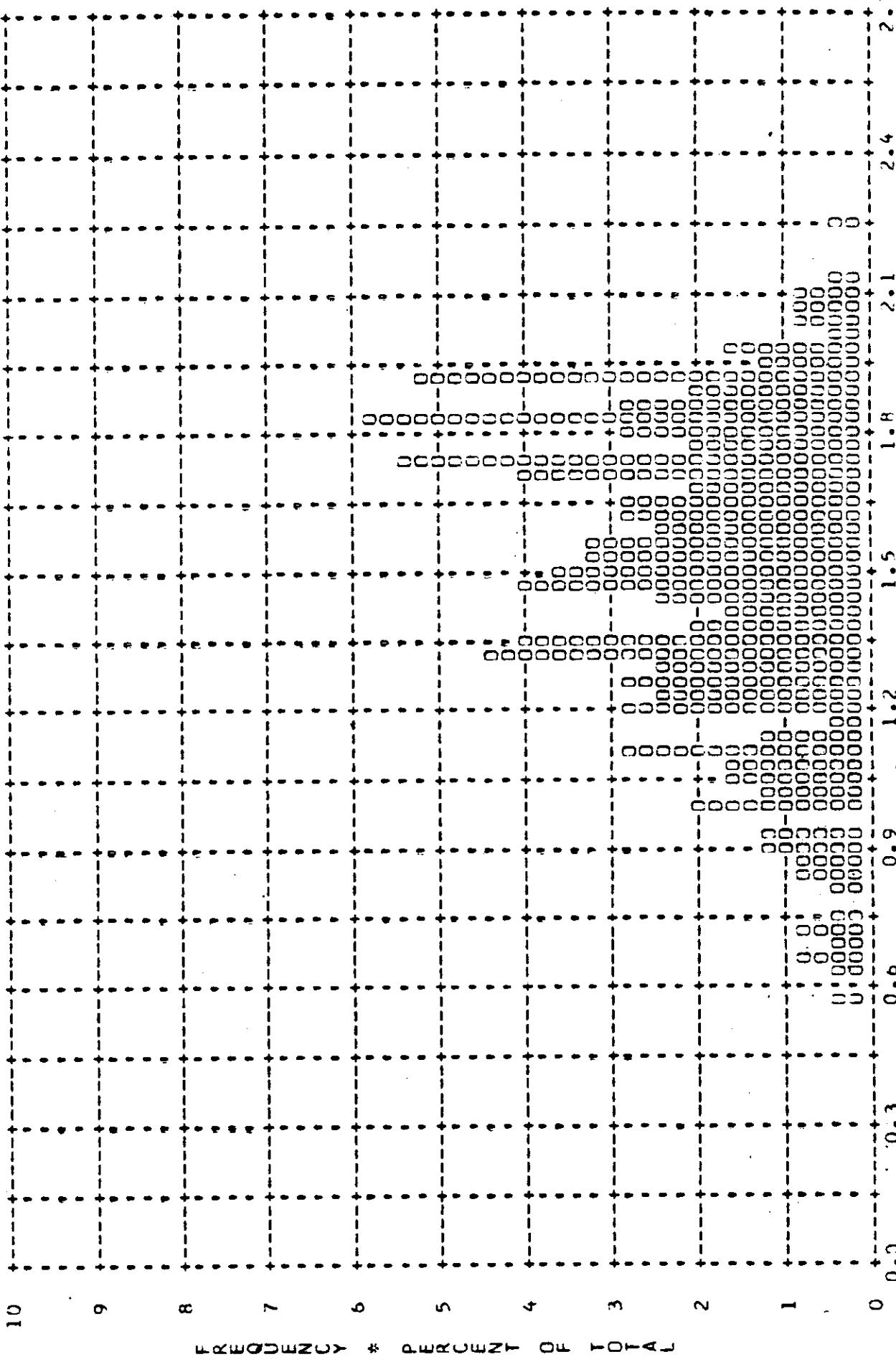
MISSION \* 1036-1 \* INSTR \* AFT \* 11/28/66 PLOT OF D MIN \* TERRAIN \* PROCESSING \* ALL LEVELS  
ARITH MEAN \* 0.55 \* MEDIAN \* 0.51 \* STD DEV \* 0.20 \* RANGE \* 0.24 TO 1.65 WITH 260 SAMPLES



~~TOP SECRET~~

- CONTROL NO.

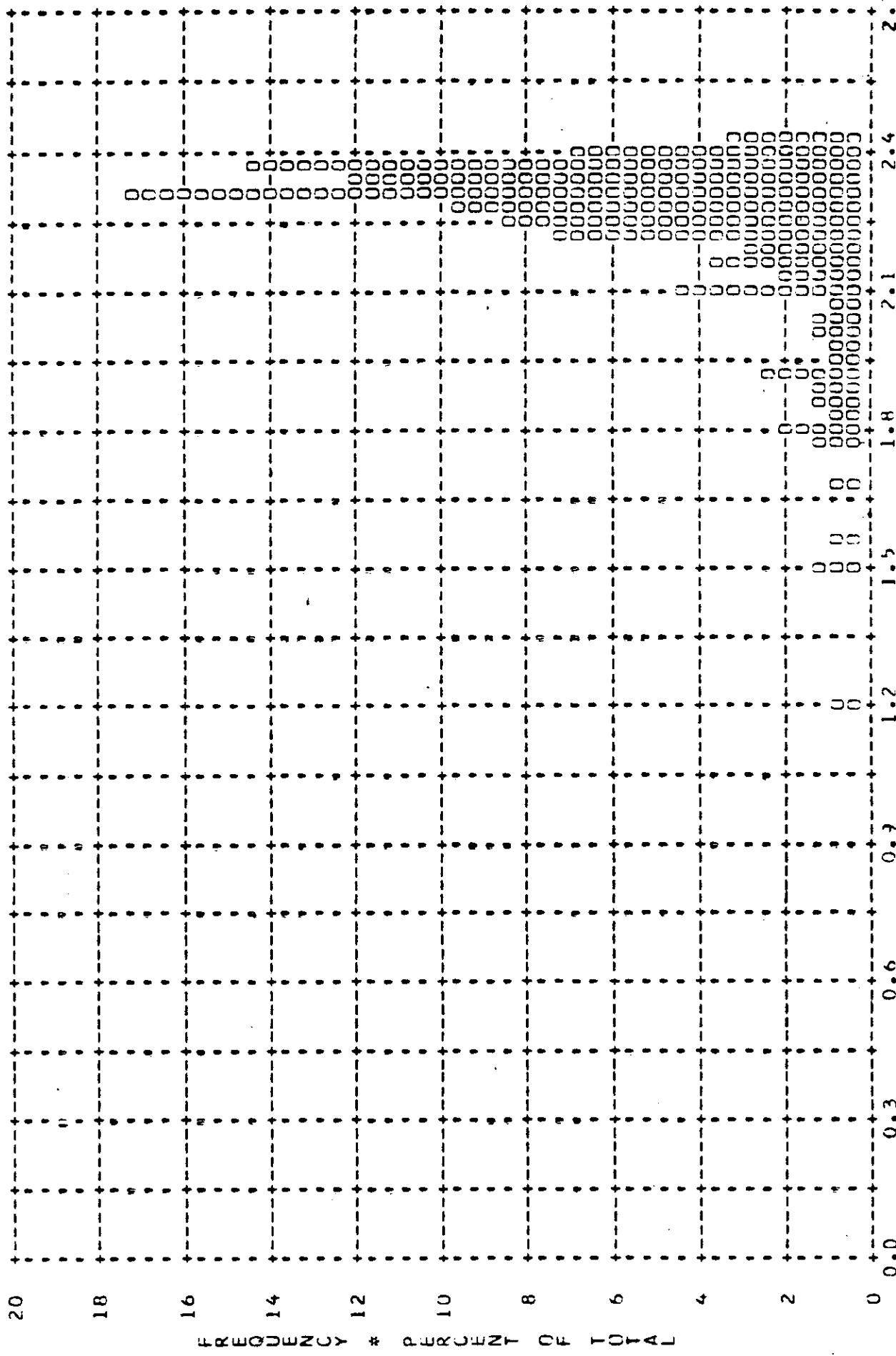
MISSION \* 1036-1 \* INSTR \* AFT \* 11/28/66 PLT1 DF D MAX \* TERRAIN \* PROCESSING \* ALL LEVELS  
ARITH MEAN \* 1.49 \* MEDIAN \* 1.52 \* STD DEV \* 0.34 \* RANGE \* 0.55 TO 2.25 WITH 260 SAMPLES



~~TOP SECRET~~

CONTROL NO.

MISSION \* 1036-1 \* INSTR \* AFT \* 11/28/66 PLOT DF D MAX \* CLOUD \* PROCESSING \* ALL LEVELS  
ARITH MEAN \* 2.23 \* MEDIAN \* 2.29 \* STD DEV \* 0.18 \* RANGE \* 1.20 TO 2.43 WITH 244 SAMPLES



~~TOP SECRET~~

- CONTROL NO.

MISSION \* 1036-2 \* INSTRUMENT \* FRWD 11/28/66 DENSITY FREQ DISTR

DENSITY VALUE	PRIMARY		INTERMEDIATE		FULL		ALL LEVELS	
	MIN	MAX LIM	MIN	MAX LIM	MIN	MAX LIM	MIN	MAX LIM
0.01	0	0	0	0	0	0	0	0
0.02	0	0	0	0	0	0	0	0
0.03	0	0	0	0	0	0	0	0
0.04	0	0	0	0	0	0	0	0
0.05	0	0	0	0	0	0	0	0
0.06	0	0	0	0	0	0	0	0
0.07	0	0	0	0	0	0	0	0
0.08	0	0	0	0	0	0	0	0
0.09	0	0	0	0	0	0	0	0
0.10	0	0	0	0	0	0	0	0
0.11	0	0	0	0	0	0	0	0
0.12	0	0	0	0	0	0	0	0
0.13	0	0	0	0	0	0	0	0
0.14	0	0	0	0	0	0	0	0
0.15	0	0	0	0	0	0	0	0
0.16	0	0	0	0	0	0	0	0
0.17	0	0	0	0	0	0	0	0
0.18	0	0	0	0	0	0	0	0
0.19	0	0	0	0	0	0	0	0
0.20	0	0	0	0	0	0	0	0
0.21	0	0	0	0	0	0	0	0
0.22	0	0	0	0	0	0	0	0
0.23	0	0	0	0	0	0	0	0
0.24	0	0	0	0	0	0	0	0
0.25	0	0	0	0	0	0	0	0
0.26	0	0	0	0	0	0	0	0
0.27	0	0	0	0	0	0	0	0
0.28	0	0	0	0	0	0	0	0
0.29	0	0	0	0	0	0	0	0
0.30	0	0	0	0	0	0	0	0
0.31	0	0	0	0	0	0	0	0
0.32	0	0	0	0	0	0	0	0
0.33	0	0	0	0	0	0	0	0
0.34	0	0	0	0	0	0	0	0
0.35	0	0	0	0	0	0	0	0
0.36	0	0	0	0	0	0	0	0
0.37	0	0	0	0	0	0	0	0
0.38	0	0	0	0	0	0	0	0
0.39	0	0	0	0	0	0	0	0
0.40	0	0	0	0	0	0	0	0
0.41	0	0	0	0	0	0	0	0
0.42	0	0	0	0	0	0	0	0
0.43	0	0	0	0	0	0	0	0
0.44	0	0	0	0	0	0	0	0
0.45	0	0	0	0	0	0	0	0
0.46	0	0	0	0	0	0	0	0
0.47	0	0	0	0	0	0	0	0
0.48	0	0	0	0	0	0	0	0
0.49	0	0	0	0	0	0	0	0
0.50	0	0	0	0	0	0	0	0
SUBTOTAL	0	0	0	25	0	159	184	2

~~TOP SECRET~~

CONTROL NO.

TABLE A-3

~~TOP SECRET~~

- CONTROL NO.

MISSION # 1036-2 \* INSTRUMENT # FRWD

11/28/66 DENSITY FREQ DISTR

DENSITY VALUE	PRIMARY		INTERMEDIATE		FULL		ALL LEVELS	
	MIN	MAX LIM	MIN	MAX LIM	MIN	MAX LIM	MIN	MAX LIM
0.51	0	0	0	0	1	0	0	0
0.52	0	0	0	0	1	0	0	0
0.53	0	0	0	0	1	0	0	0
0.54	0	0	0	0	1	0	0	0
0.55	0	0	0	0	1	0	0	0
0.56	0	0	0	0	1	0	0	0
0.57	0	0	0	0	1	0	0	0
0.58	0	0	0	0	1	0	0	0
0.59	0	0	0	0	1	0	0	0
0.60	0	0	0	0	1	0	0	0
0.61	0	0	0	0	1	0	0	0
0.62	0	0	0	0	1	0	0	0
0.63	0	0	0	0	1	0	0	0
0.64	0	0	0	0	1	0	0	0
0.65	0	0	0	0	1	0	0	0
0.66	0	0	0	0	1	0	0	0
0.67	0	0	0	0	1	0	0	0
0.68	0	0	0	0	1	0	0	0
0.69	0	0	0	0	1	0	0	0
0.70	0	0	0	0	1	0	0	0
0.71	0	0	0	0	1	0	0	0
0.72	0	0	0	0	1	0	0	0
0.73	0	0	0	0	1	0	0	0
0.74	0	0	0	0	1	0	0	0
0.75	0	0	0	0	1	0	0	0
0.76	0	0	0	0	1	0	0	0
0.77	0	0	0	0	1	0	0	0
0.78	0	0	0	0	1	0	0	0
0.79	0	0	0	0	1	0	0	0
0.80	0	0	0	0	1	0	0	0
0.81	0	0	0	0	1	0	0	0
0.82	0	0	0	0	1	0	0	0
0.83	0	0	0	0	1	0	0	0
0.84	0	0	0	0	1	0	0	0
0.85	0	0	0	0	1	0	0	0
0.86	0	0	0	0	1	0	0	0
0.87	0	0	0	0	1	0	0	0
0.88	0	0	0	0	1	0	0	0
0.89	0	0	0	0	1	0	0	0
0.90	0	0	0	0	1	0	0	0
0.91	0	0	0	0	1	0	0	0
0.92	0	0	0	0	1	0	0	0
0.93	0	0	0	0	1	0	0	0
0.94	0	0	0	0	1	0	0	0
0.95	0	0	0	0	1	0	0	0
0.96	0	0	0	0	1	0	0	0
0.97	0	0	0	0	1	0	0	0
0.98	0	0	0	0	1	0	0	0
0.99	0	0	0	0	1	0	0	0
1.00	0	0	0	0	1	0	0	0
SUBTOTAL :	0	0	0	0	25	1	0	0

~~TOP SECRET~~

- CONTROL NO.

TABLE A-3

~~TOP SECRET~~

- CONTROL NO. [REDACTED]

MISSION \* 1036-2 \* INSTRUMENT \* FRWD

11/28/66 DENSITY FREQ DISTR

DENSITY VALUE	PRIMARY			INTERMEDIATE			FULL			ALL LEVELS		
	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM
1.01	0	0	0	0	0	0	0	1	3	0	0	0
1.02	0	0	0	0	0	0	0	1	3	1	2	2
1.03	0	0	0	0	0	0	0	1	2	2	3	2
1.04	0	0	0	0	0	0	0	1	2	1	8	1
1.05	0	0	0	0	0	0	0	1	0	0	0	0
1.06	0	0	0	0	0	0	0	0	0	0	0	0
1.07	0	0	0	0	0	0	0	0	0	0	0	0
1.08	0	0	0	0	0	0	0	0	0	0	0	0
1.09	0	0	0	0	0	0	0	0	0	0	0	0
1.10	0	0	0	0	0	0	0	0	0	0	0	0
1.11	0	0	0	0	0	0	0	0	0	0	0	0
1.12	0	0	0	0	0	0	0	0	0	0	0	0
1.13	0	0	0	0	0	0	0	0	0	0	0	0
1.14	0	0	0	0	0	0	0	0	0	0	0	0
1.15	0	0	0	0	0	0	0	0	0	0	0	0
1.16	0	0	0	0	0	0	0	0	0	0	0	0
1.17	0	0	0	0	0	0	0	0	0	0	0	0
1.18	0	0	0	0	0	0	0	0	0	0	0	0
1.19	0	0	0	0	0	0	0	0	0	0	0	0
1.20	0	0	0	0	0	0	0	0	0	0	0	0
1.21	0	0	0	0	0	0	0	0	0	0	0	0
1.22	0	0	0	0	0	0	0	0	0	0	0	0
1.23	0	0	0	0	0	0	0	0	0	0	0	0
1.24	0	0	0	0	0	0	0	0	0	0	0	0
1.25	0	0	0	0	0	0	0	0	0	0	0	0
1.26	0	0	0	0	0	0	0	0	0	0	0	0
1.27	0	0	0	0	0	0	0	0	0	0	0	0
1.28	0	0	0	0	0	0	0	0	0	0	0	0
1.29	0	0	0	0	0	0	0	0	0	0	0	0
1.30	0	0	0	0	0	0	0	0	0	0	0	0
1.31	0	0	0	0	0	0	0	0	0	0	0	0
1.32	0	0	0	0	0	0	0	0	0	0	0	0
1.33	0	0	0	0	0	0	0	0	0	0	0	0
1.34	0	0	0	0	0	0	0	0	0	0	0	0
1.35	0	0	0	0	0	0	0	0	0	0	0	0
1.36	0	0	0	0	0	0	0	0	0	0	0	0
1.37	0	0	0	0	0	0	0	0	0	0	0	0
1.38	0	0	0	0	0	0	0	0	0	0	0	0
1.39	0	0	0	0	0	0	0	0	0	0	0	0
1.40	0	0	0	0	0	0	0	0	0	0	0	0
1.41	0	0	0	0	0	0	0	0	0	0	0	0
1.42	0	0	0	0	0	0	0	0	0	0	0	0
1.43	0	0	0	0	0	0	0	0	0	0	0	0
1.44	0	0	0	0	0	0	0	0	0	0	0	0
1.45	0	0	0	0	0	0	0	0	0	0	0	0
1.46	0	0	0	0	0	0	0	0	0	0	0	0
1.47	0	0	0	0	0	0	0	0	0	0	0	0
1.48	0	0	0	0	0	0	0	0	0	0	0	0
1.49	0	0	0	0	0	0	0	0	0	0	0	0
1.50	0	0	0	0	0	0	0	0	0	0	0	0
SUBTOTAL	0	0	0	1	27	4	92	15	5	119	7	

~~TOP SECRET~~

- CONTROL NO. [REDACTED]

TABLE A-3

~~TOP SECRET~~

- CONTROL NO.

MISSION # 1036-2 \* INSTRUMENT \* FRWD 11/28/66 DENSITY FREQ DISTR

~~TOP SECRET~~

- CONTROL NO.

TABLE A-3

~~TOP SECRET~~

- CONTROL NO.

MISSION \* 1036-2 \* INSTRUMENT \* FRWD

11/26/66 DENSITY FREQ DISTR

DENSITY VALUE	PRIMARY MIN MAX LIM	INTERMEDIATE MIN MAX LIM	FULL MIN MAX LIM	ALL LEVELS MIN MAX LIM
2.01	00	00	00	24
2.02	00	00	00	12
2.03	00	00	00	23
2.04	00	00	00	11
2.05	00	00	00	34
2.06	00	00	00	74
2.07	00	00	00	14
2.08	00	00	00	22
2.09	00	00	00	5
2.10	00	00	00	35
2.11	00	00	00	31
2.12	00	00	00	13
2.13	00	00	00	5
2.14	00	00	00	3
2.15	00	00	00	2
2.16	00	00	00	2
2.17	00	00	00	9
2.18	00	00	00	2
2.19	00	00	00	2
2.20	00	00	00	2
2.21	00	00	00	2
2.22	00	00	00	2
2.23	00	00	00	2
2.24	00	00	00	2
2.25	00	00	00	2
2.26	00	00	00	2
2.27	00	00	00	2
2.28	00	00	00	2
2.29	00	00	00	2
2.30	00	00	00	2
2.31	00	00	00	2
2.32	00	00	00	2
2.33	00	00	00	2
2.34	00	00	00	2
2.35	00	00	00	2
2.36	00	00	00	2
2.37	00	00	00	2
2.38	00	00	00	2
2.39	00	00	00	2
2.40	00	00	00	2
2.41	00	00	00	2
2.42	00	00	00	2
2.43	00	00	00	2
2.44	00	00	00	2
2.45	00	00	00	2
2.46	00	00	00	2
2.47	00	00	00	2
2.48	00	00	00	2
2.49	00	00	00	2
2.50	00	00	00	2
SUBTOTAL	00	00	24	161
			2	185
			3	

~~TOP SECRET~~

- CONTROL NO.

TABLE A-3

~~TOP SECRET~~

- CONTROL NO.

MISSION # 1036-2 \* INSTRUMENT \* FRWD 11/28/66 DENSITY FREQ DISTR

DENSITY VALUE	PRIMARY			INTERMEDIATE			FULL			ALL LEVELS		
	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM
2.51	0	0	0	0	0	0	0	0	0	0	0	0
2.52	0	0	0	0	0	0	0	0	0	0	0	0
2.53	0	0	0	0	0	0	0	0	0	0	0	0
2.54	0	0	0	0	0	0	0	0	0	0	0	0
2.55	0	0	0	0	0	0	0	0	0	0	0	0
2.56	0	0	0	0	0	0	0	0	0	0	0	0
2.57	0	0	0	0	0	0	0	0	0	0	0	0
2.58	0	0	0	0	0	0	0	0	0	0	0	0
2.59	0	0	0	0	0	0	0	0	0	0	0	0
2.60	0	0	0	0	0	1	0	0	0	0	0	0
2.61	0	0	0	0	0	0	0	0	0	0	0	0
2.62	0	0	0	0	0	0	0	0	0	0	0	0
2.63	0	0	0	0	0	0	0	0	0	0	0	0
2.64	0	0	0	0	0	0	0	0	0	0	0	0
2.65	0	0	0	0	0	0	0	0	0	0	0	0
2.66	0	0	0	0	0	0	0	0	0	0	0	0
2.67	0	0	0	0	0	0	0	0	0	0	0	0
2.68	0	0	0	0	0	0	0	0	0	0	0	0
2.69	0	0	0	0	0	0	0	0	0	0	0	0
2.70	0	0	0	0	0	0	0	0	0	0	0	0
SUBTOTAL	0	0	0	0	0	1	0	0	0	0	0	1
TOTAL	0	0	0	51	51	41	224	224	201	275	275	242

MISSION 1036-2 INSTR - FRWD 11/28/66 PROCESSING AND EXPOSURE ANALYSIS

PROCESS LEVEL	SAMPLE SIZE	UNDER EXPOSED		UNDER PROCESSED		CORRECT EXP+PROC		OVER PROCESSED		OVER EXPOSED																	
		PRIMARY	INTERMEDIATE	FULL	ALL LEVELS	0	51	224	275	0 PC	0 PC	33 PC	0 PC	0 PC	61 PC	51 PC	53 PC	0 PC	6 PC	3 PC	3 PC	0 PC	0 PC	0 PC			
PRIMARY	0	0	0	0	0	0	0	0 PC	0 PC	33 PC	0 PC	0 PC	0 PC	0 PC	0 PC	0 PC	0 PC	0 PC	0 PC	0 PC	0 PC	0 PC	0 PC	0 PC	0 PC	0 PC	0 PC
INTERMEDIATE	51	0	0	0	0	0	0	0 PC	0 PC	33 PC	0 PC	0 PC	0 PC	0 PC	0 PC	0 PC	0 PC	0 PC	0 PC	0 PC	0 PC	0 PC	0 PC	0 PC	0 PC	0 PC	0 PC
FULL	224	0	0	0	0	0	0	46 PC	46 PC	0 PC	0 PC	0 PC	0 PC	0 PC	0 PC	0 PC	0 PC	0 PC	0 PC	0 PC	0 PC	0 PC	0 PC	0 PC	0 PC	0 PC	0 PC
ALL LEVELS	275	0	0	0	0	0	0	38 PC	38 PC	6 PC	6 PC	6 PC	6 PC	6 PC	6 PC	6 PC	53 PC	53 PC	53 PC	53 PC	53 PC	53 PC	53 PC	53 PC	53 PC	53 PC	53 PC
PROCESS LEVEL	BASE + FOG	UNDER EXPOSED		UNDER PROCESSED		CORRECT EXP+PROC		OVER PROCESSED		OVER EXPOSED																	
PRIMARY	0.01-0.09	0.01-0.13	0.14-0.39	0.40-0.90	-----	-----	-----	-----	-----	-----	0.91 AND UP																
INTERMED	0.10-0.17	0.01-0.20	0.21-0.39	0.40-0.90	0.91-1.34	1.35 AND UP	1.70 AND UP	1.70 AND UP	1.70 AND UP	1.70 AND UP	0.91-1.34	0.91-1.34	0.91-1.34	0.91-1.34	0.91-1.34	0.91-1.34	0.91-1.34	0.91-1.34	0.91-1.34	0.91-1.34	0.91-1.34	0.91-1.34	0.91-1.34	0.91-1.34	0.91-1.34	0.91-1.34	0.91-1.34
FULL	0.18 AND UP	0.01-0.39	-----	0.40-0.90	0.91-1.69	1.70 AND UP	1.70 AND UP	1.70 AND UP	1.70 AND UP	1.70 AND UP	0.91-1.69	0.91-1.69	0.91-1.69	0.91-1.69	0.91-1.69	0.91-1.69	0.91-1.69	0.91-1.69	0.91-1.69	0.91-1.69	0.91-1.69	0.91-1.69	0.91-1.69	0.91-1.69	0.91-1.69	0.91-1.69	0.91-1.69

~~TOP SECRET~~

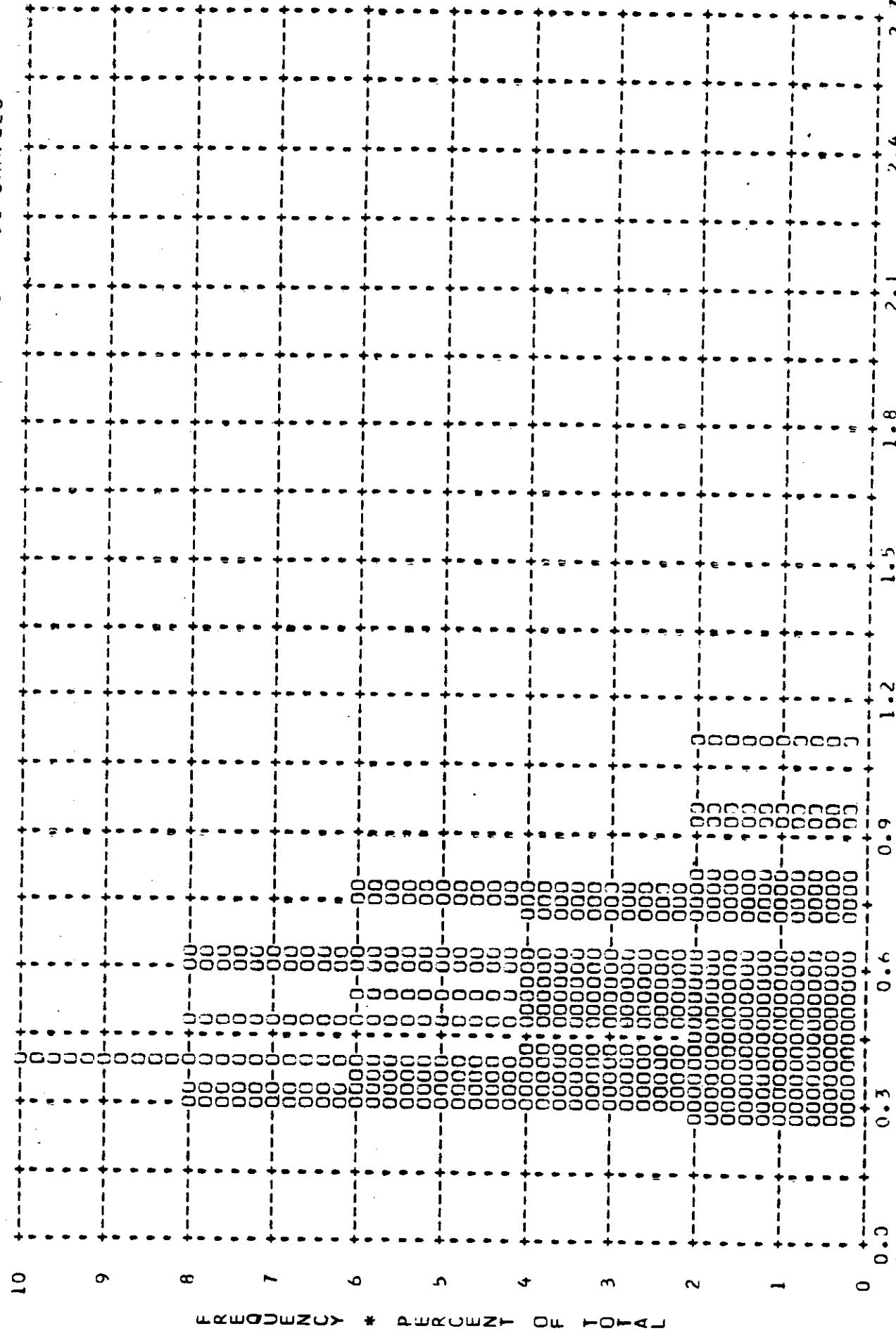
- CONTROL NO.

TABLE A-3

~~TOP SECRET~~

- CONTROL NO. [REDACTED]

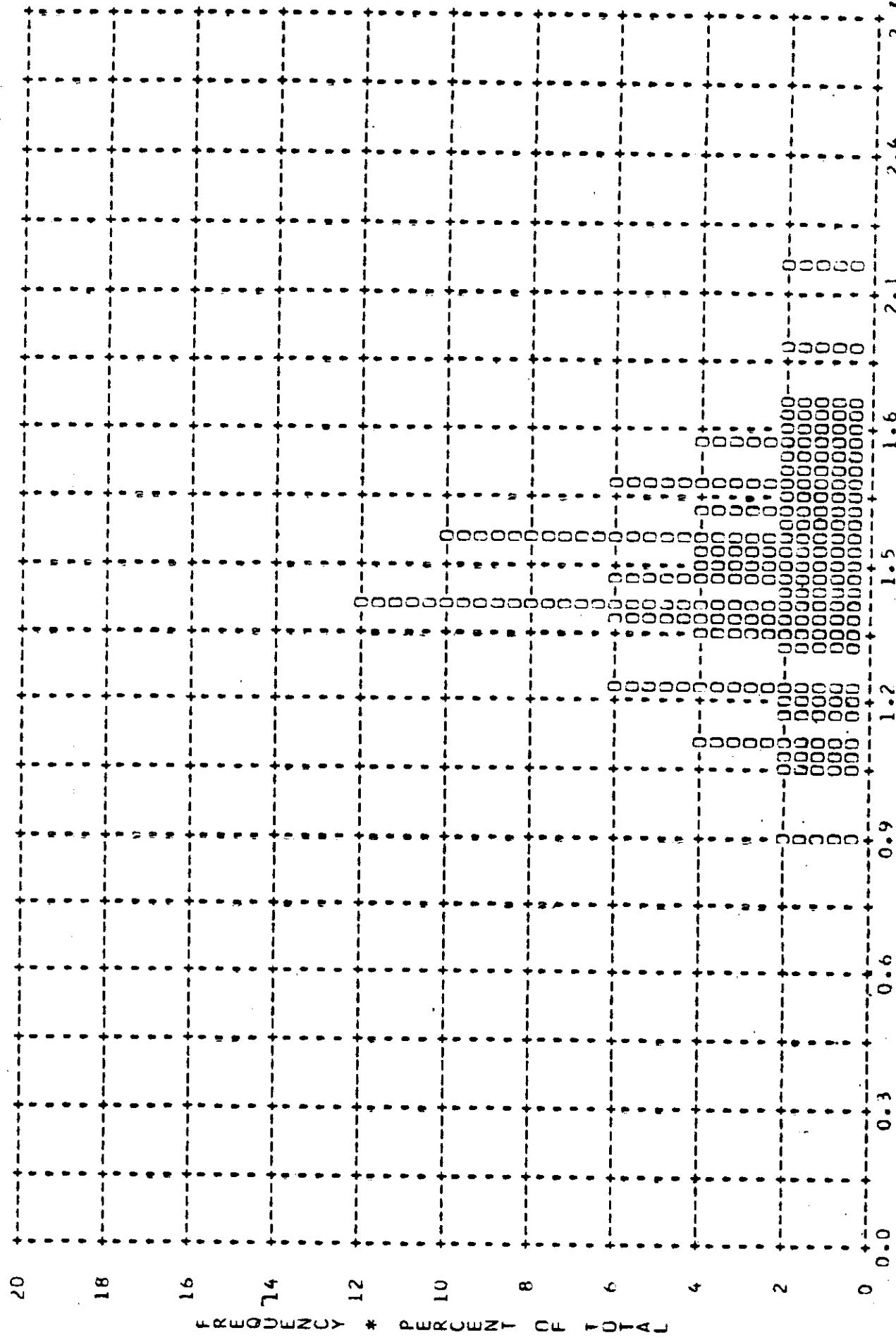
MISSION \* 1036-2 \* INSTR \* FRWD \* 11/28/66 PLOT OF D MIN \* TERRAIN \* PROCESSING \* INTERMEDIATE  
ARITH MFAN \* 0.53 \* MEDIAN \* 0.51 \* STD DIV \* 0.20 \* RANGE \* 0.27 TO 1.10 WITH 51 SAMPLES



REFUGEE

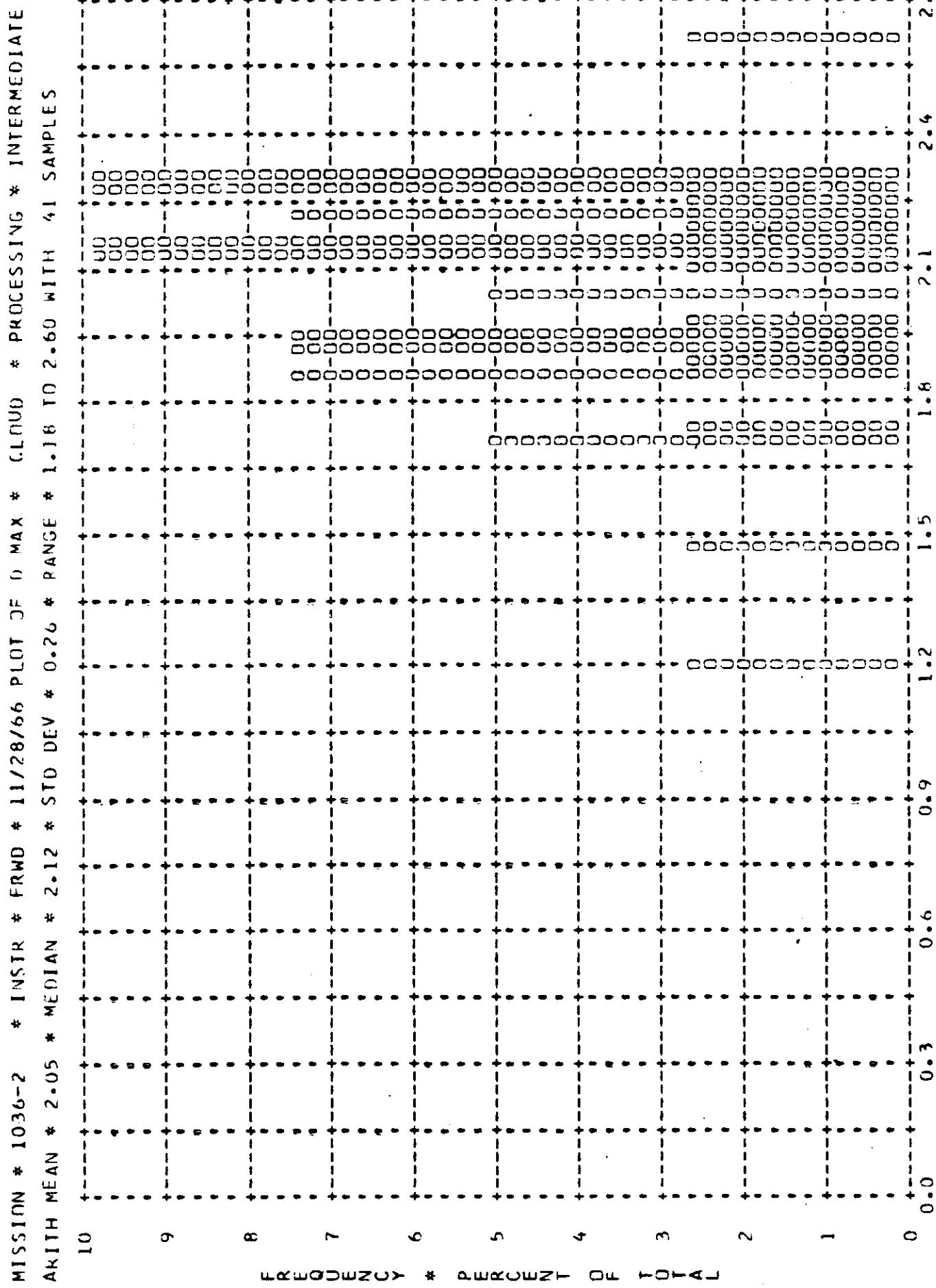
CONTROL NO.

MISSION \* 1036-2 \* INSTR \* FRWD \* 11/28/66 PLOT JF U MAX \* TERRAIN \* PROCESSING \* INTERMEDIATE  
ARITH MEAN \* 1.48 \* MEDIAN \* 1.47 \* STD DEV \* 0.25 \* RANGE \* 0.30 TO 2.16 WITH 51 SAMPLES



~~TOP SECRET~~

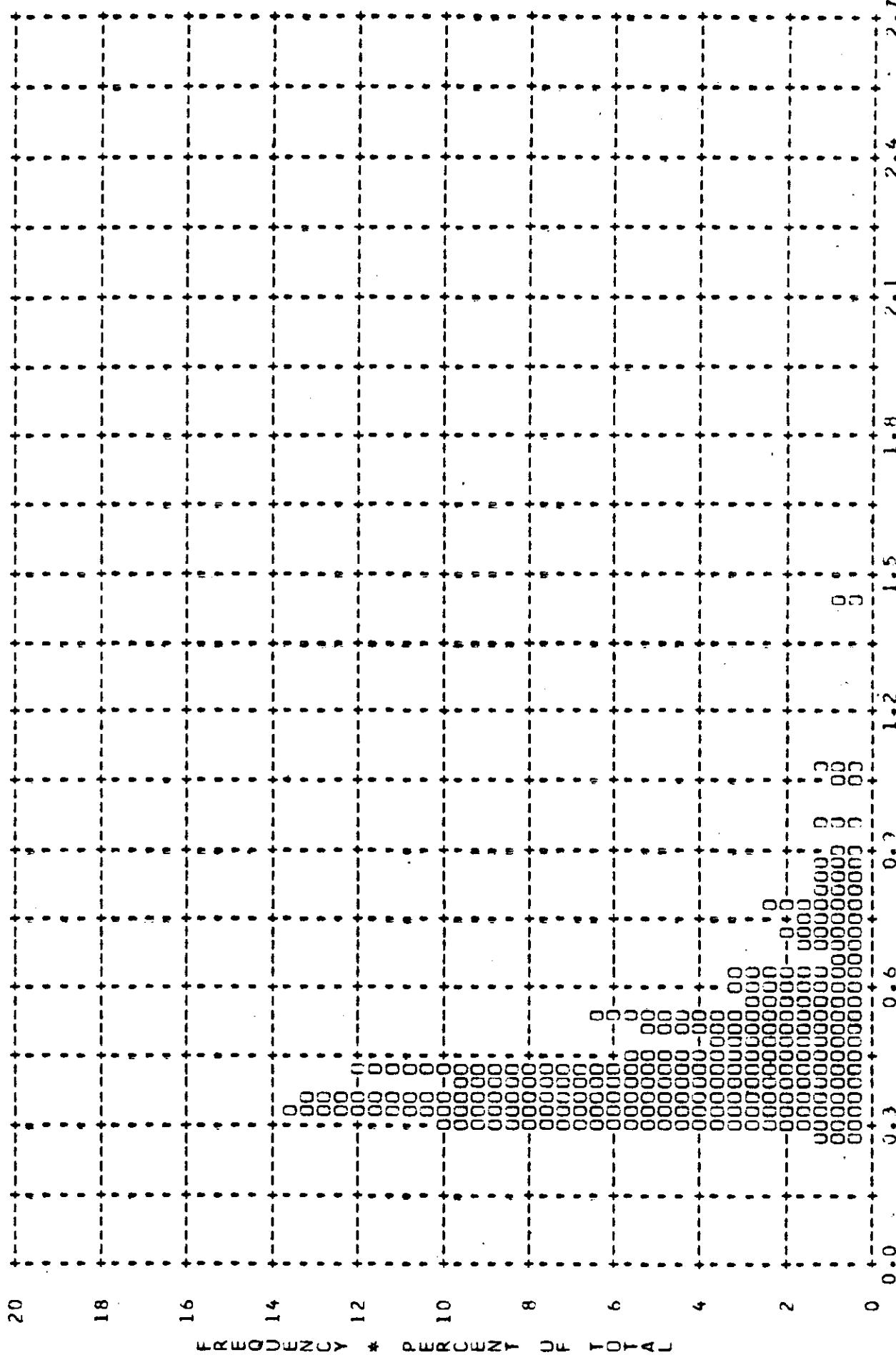
- CONTROL NO. [REDACTED]



~~TOP SECRET~~

- CONTROL NO.

MISSION \* 1036-2 \* INSTR \* FRWD \* 11/28/66 PLUT OF D MIN \* TERRAIN \* PROCESSING \* FULL  
ARITH MEAN \* 0.46 \* MEDIAN \* 0.40 \* STD DEV \* 0.18 \* RANGE \* 0.26 TO 1.43 WITH 224 SAMPLES



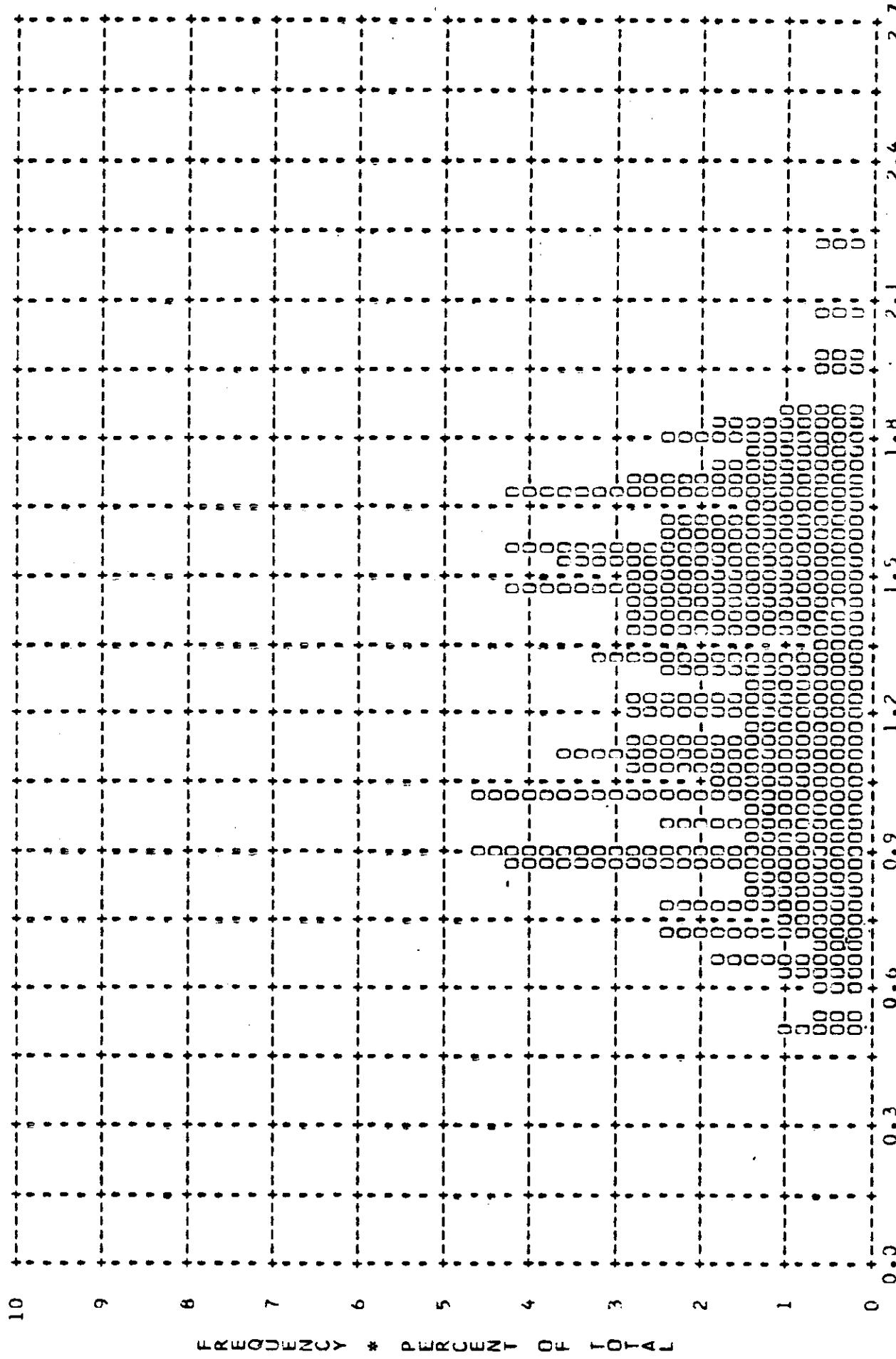
1142

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~~TOP SECRET~~

- CONTROL V.

MISSION \* 1036-2 \* INSTR \* FRWD \* 11/28/66 PLUT OF U MAX \* TERRAIN & PROCESSING \* FULL  
ARITH MEAN \* 1.26 \* MEDIAN \* 1.28 \* STD DEV \* 0.36 \* RANGE \* 0.50 TO 2.20 WITH 224 SAMPLES

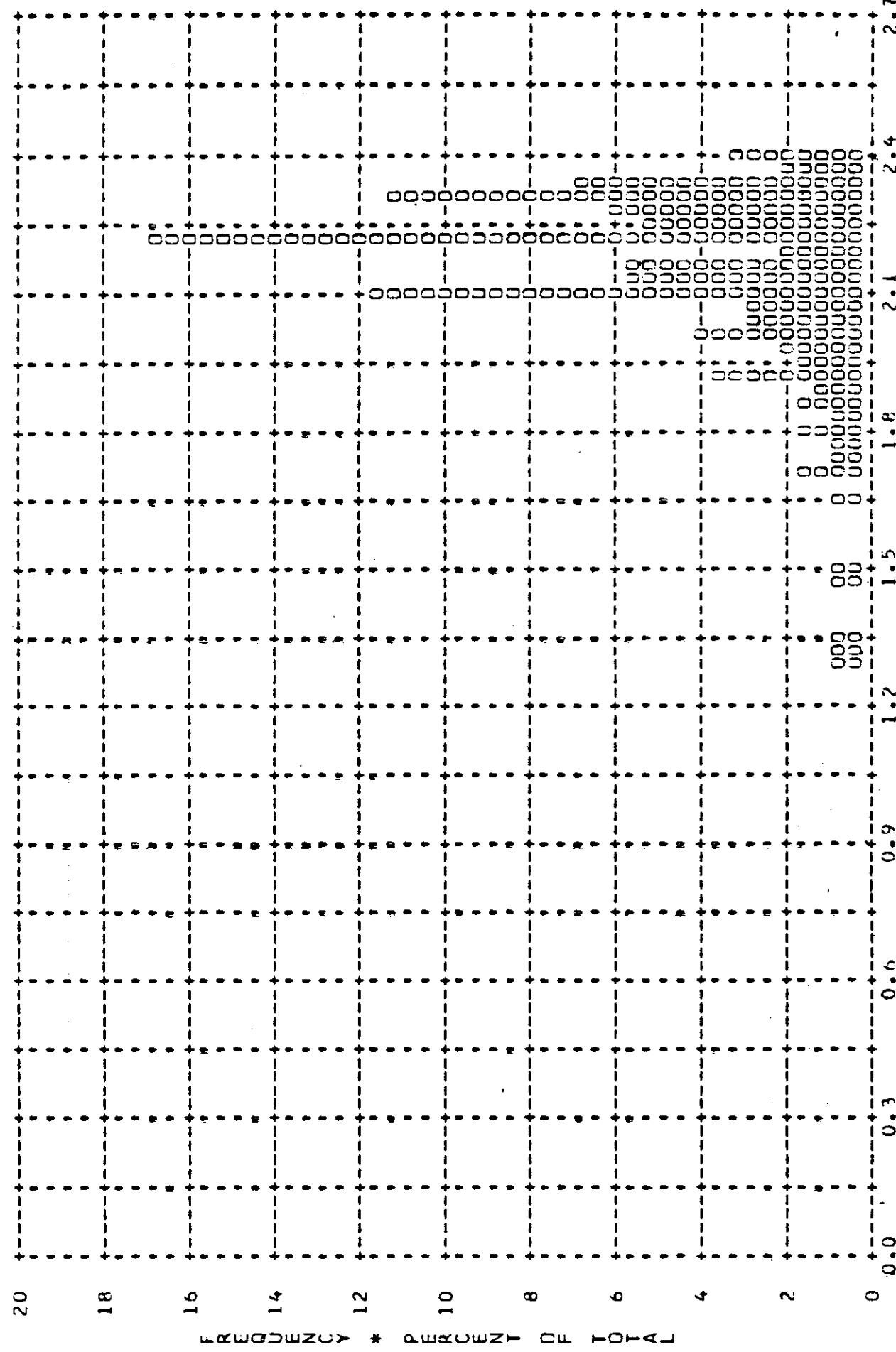


A-21

~~TOP SECRET~~

- CONTROL NO.

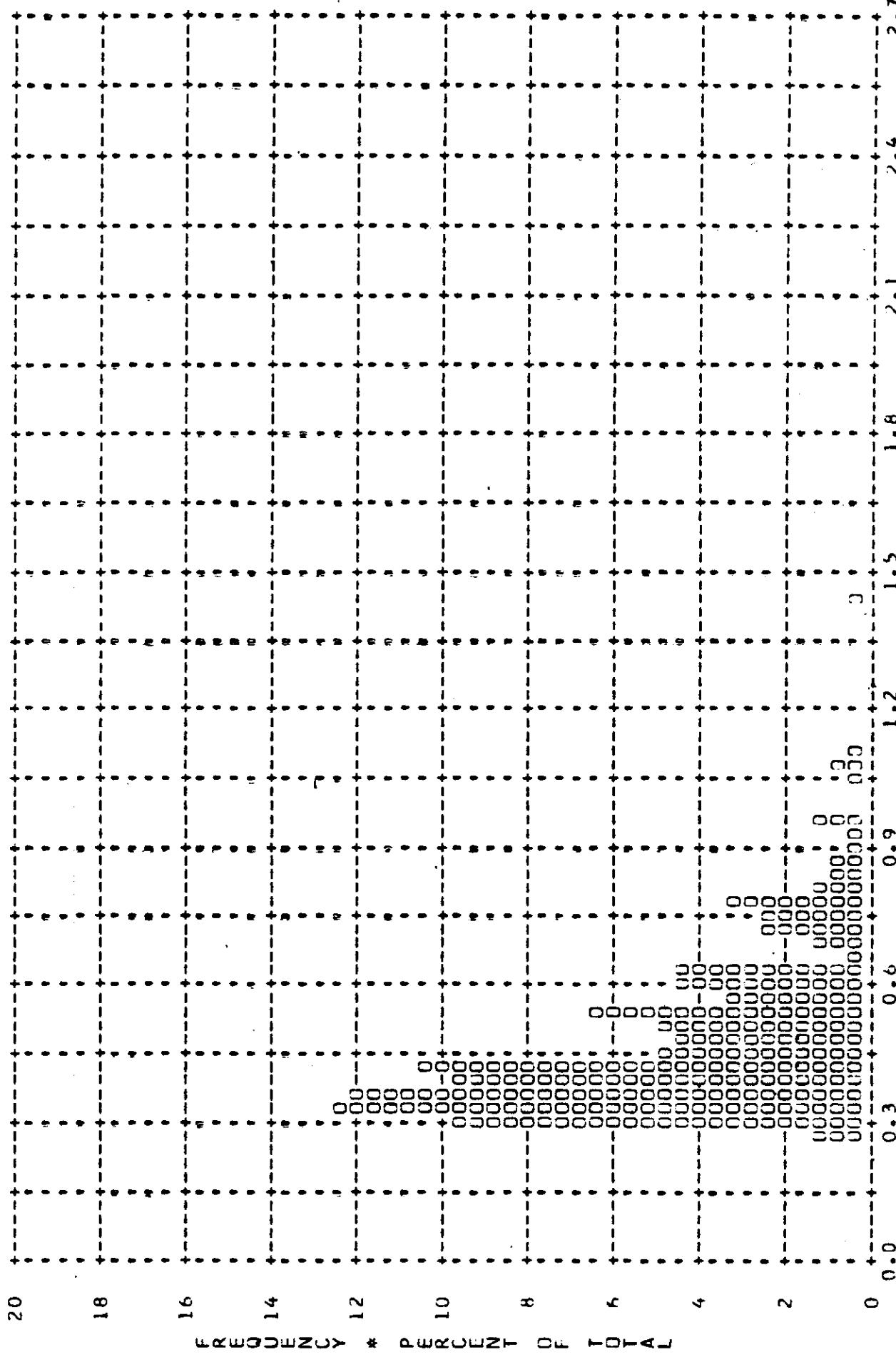
MISSION \* 1036-2 \* INSTR \* FWD \* 11/28/66 PLOT JFD MAX \* CLOUD \* PROCESSING & FULL.  
ARITH MEAN \* 2.13 \* MEDIAN \* 2.18 \* STD DEV \* 0.20 \* RANGE \* 1.29 TO 2.40 WITH 201 SAMPLES



~~TOP SECRET~~

- CONTROL NO.

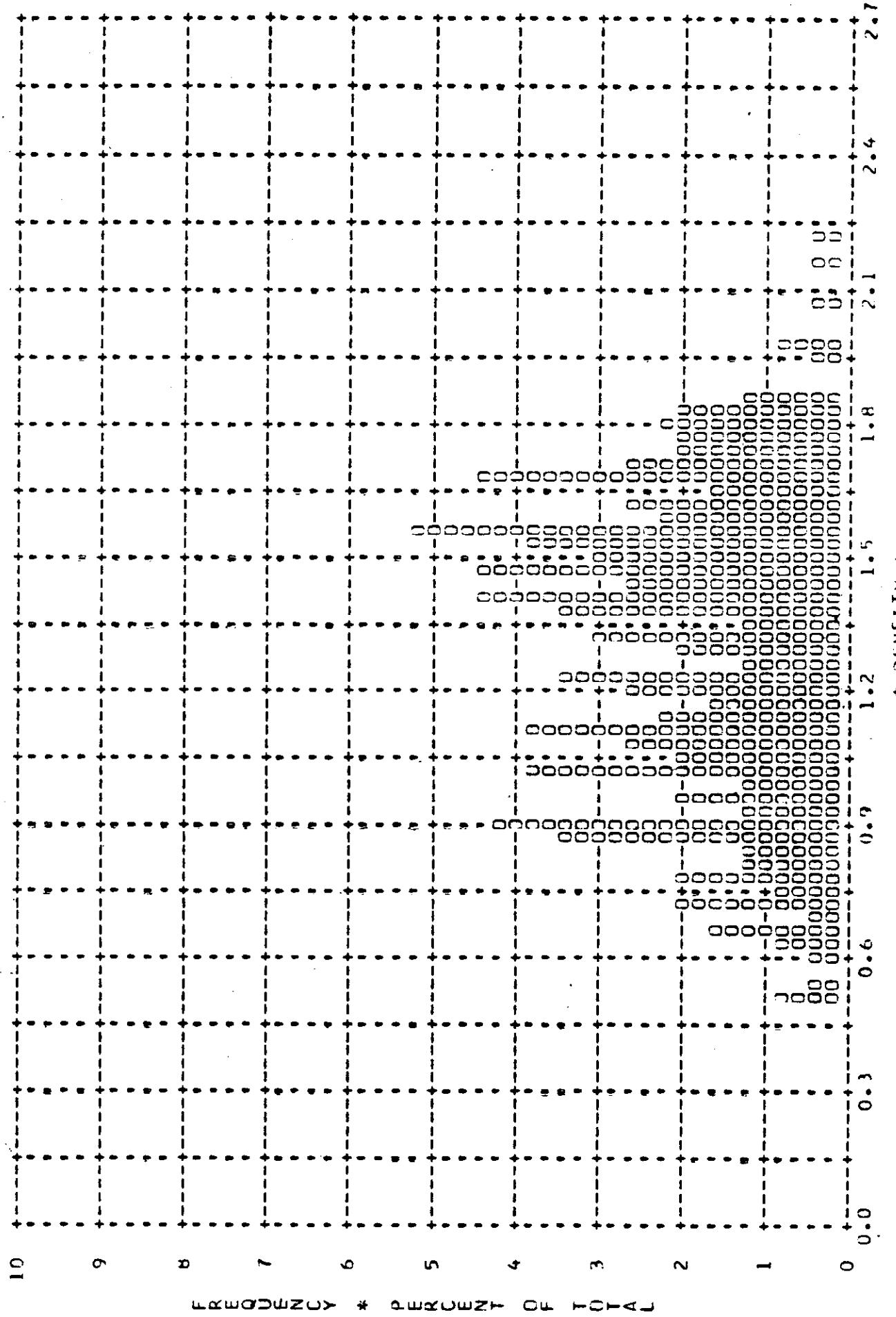
MISSION \* 1036-2 \* INSTR \* FRWD \* 11/28/66 PLOT OF D MIN \* TERRAIN \* PROCESSING \* ALL LEVELS  
ARITH MEAN \* 0.47 \* MEDIAN \* 0.42 \* STD DEV \* 0.18 \* RANGE \* 0.26 TO 1.43 WITH 275 SAMPLES



~~TOP SECRET~~

- CONTROL NO.

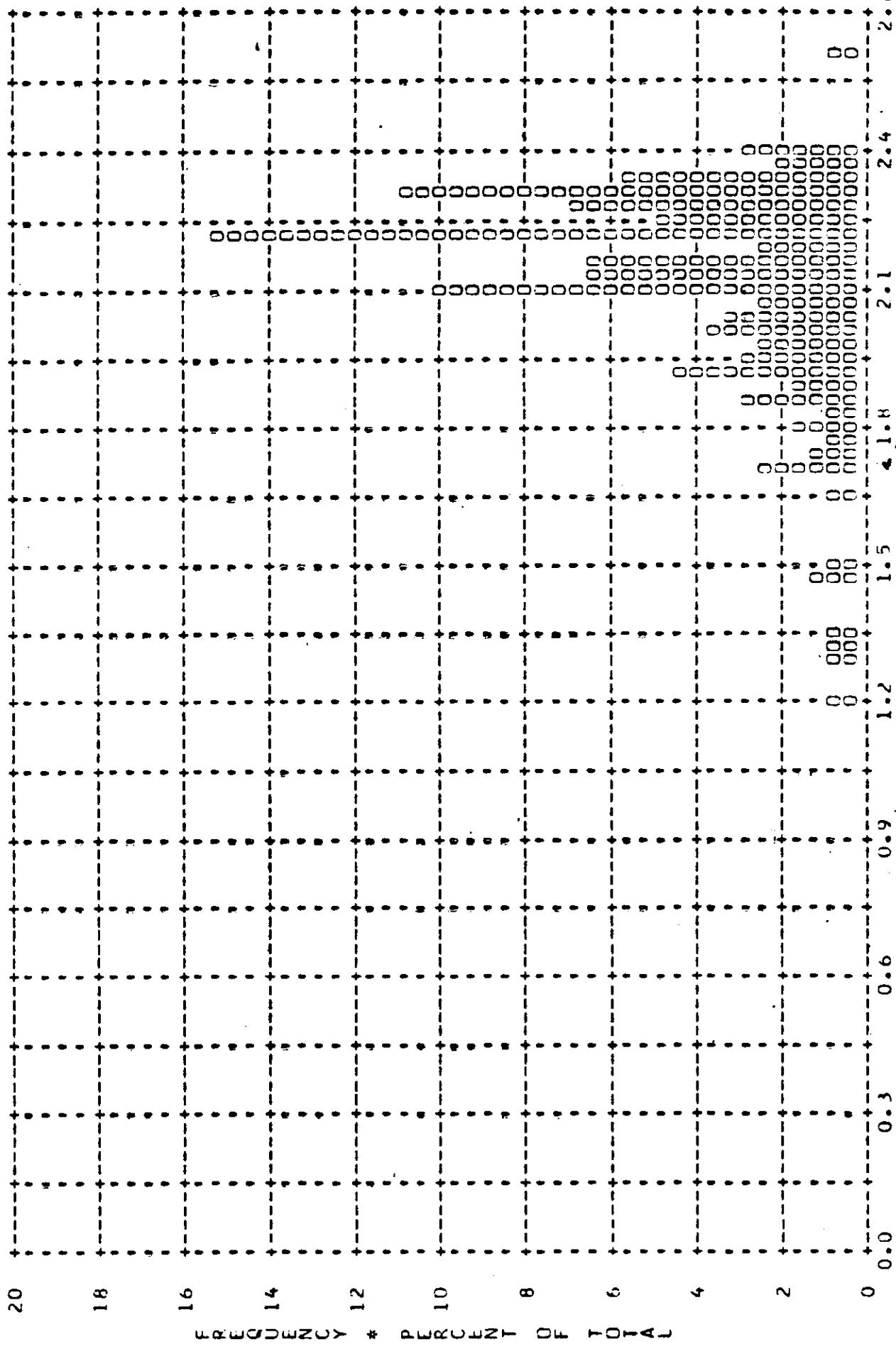
MISSION \* 1036-2 \* INSTR \* FRWD \* 11/28/66 PLOT OF D MAX \* TERRAIN \* PROCESSING \* ALL LEVELS  
ARITH MEAN \* 1.30 \* MEDIAN \* 1.36 \* STD DEV \* 0.35 \* RANGE \* 0.50 IN 2.20 WITH 275 SAMPLES



~~TOP SECRET~~

CONTROL NO.

MISSION \* 1036-2 \* INSTR \* FRWD \* 11/28/66 PLOT OF 10 MAX \* CLOUD \* PROCESSING \* ALL LEVELS  
ARITH MEAN \* 2.12 \* MEDIAN \* 2.16 \* STD DEV \* 0.21 \* RANGE \* 1.18 TO 2.60 WITH 242 SAMPLES



~~TOP SECRET~~

- CONTROL NO.

MISSION # 1036-2 \* INSTRUMENT # AFT 11/28/66 DENSITY FREQ DISTR

DENSITY VALUE	PRIMARY MIN	PRIMARY MAX	PRIMARY LIM	INTERMEDIATE MIN	INTERMEDIATE MAX	INTERMEDIATE LIM	FULL MIN	FULL MAX	FULL LIM	ALL LEVELS MIN	ALL LEVELS MAX	ALL LEVELS LIM
0.01	0	0	0	0	0	0	0	0	0	0	0	0
0.02	0	0	0	0	0	0	0	0	0	0	0	0
0.03	0	0	0	0	0	0	0	0	0	0	0	0
0.04	0	0	0	0	0	0	0	0	0	0	0	0
0.05	0	0	0	0	0	0	0	0	0	0	0	0
0.06	0	0	0	0	0	0	0	0	0	0	0	0
0.07	0	0	0	0	0	0	0	0	0	0	0	0
0.08	0	0	0	0	0	0	0	0	0	0	0	0
0.09	0	0	0	0	0	0	0	0	0	0	0	0
0.10	0	0	0	0	0	0	0	0	0	0	0	0
0.11	0	0	0	0	0	0	0	0	0	0	0	0
0.12	0	0	0	0	0	0	0	0	0	0	0	0
0.13	0	0	0	0	0	0	0	0	0	0	0	0
0.14	0	0	0	0	0	0	0	0	0	0	0	0
0.15	0	0	0	0	0	0	0	0	0	0	0	0
0.16	0	0	0	0	0	0	0	0	0	0	0	0
0.17	0	0	0	0	0	0	0	0	0	0	0	0
0.18	0	0	0	0	0	0	0	0	0	0	0	0
0.19	0	0	0	0	0	0	0	0	0	0	0	0
0.20	0	0	0	0	0	0	0	0	0	0	0	0
0.21	0	0	0	0	0	0	0	0	0	0	0	0
0.22	0	0	0	0	0	0	0	0	0	0	0	0
0.23	0	0	0	0	0	0	0	0	0	0	0	0
0.24	0	0	0	0	0	0	0	0	0	0	0	0
0.25	0	0	0	0	0	0	0	0	0	0	0	0
0.26	0	0	0	0	0	0	0	0	0	0	0	0
0.27	0	0	0	0	0	0	0	0	0	0	0	0
0.28	0	0	0	0	0	0	0	0	0	0	0	0
0.29	0	0	0	0	0	0	0	0	0	0	0	0
0.30	0	0	0	0	0	0	0	0	0	0	0	0
0.31	0	0	0	0	0	0	0	0	0	0	0	0
0.32	0	0	0	0	0	0	0	0	0	0	0	0
0.33	0	0	0	0	0	0	0	0	0	0	0	0
0.34	0	0	0	0	0	0	0	0	0	0	0	0
0.35	0	0	0	0	0	0	0	0	0	0	0	0
0.36	0	0	0	0	0	0	0	0	0	0	0	0
0.37	0	0	0	0	0	0	0	0	0	0	0	0
0.38	0	0	0	0	0	0	0	0	0	0	0	0
0.39	0	0	0	0	0	0	0	0	0	0	0	0
0.40	0	0	0	0	0	0	0	0	0	0	0	0
0.41	0	0	0	0	0	0	0	0	0	0	0	0
0.42	0	0	0	0	0	0	0	0	0	0	0	0
0.43	0	0	0	0	0	0	0	0	0	0	0	0
0.44	0	0	0	0	0	0	0	0	0	0	0	0
0.45	0	0	0	0	0	0	0	0	0	0	0	0
0.46	0	0	0	0	0	0	0	0	0	0	0	0
0.47	0	0	0	0	0	0	0	0	0	0	0	0
0.48	0	0	0	0	0	0	0	0	0	0	0	0
0.49	0	0	0	0	0	0	0	0	0	0	0	0
0.50	0	0	0	0	0	0	0	0	0	0	0	0
SUBTOTAL	0	0	0	27	1	0	14	1	1	16	2	2
							171	1	1	198		

~~TOP SECRET~~

- CONTROL NO.

TABLE A-4

~~TOP SECRET~~

- CONTROL NO.

MISSION \* 1036-2 \* INSTRUMENT \* AFT 11/28/66 DENSITY FREQ DISTB

DENSITY VALUE	PRIMARY MIN	PRIMARY MAX	PRIMARY LIM	INTERMEDIATE MIN	INTERMEDIATE MAX	INTERMEDIATE LIM	FULL MIN	FULL MAX	FULL LIM	ALL LEVELS MIN	ALL LEVELS MAX	ALL LEVELS LIM
0.51	0	0	0	0	0	0	0	0	0	0	0	0
0.52										0	5	4
0.53										4	2	4
0.54										3	3	5
0.55										2	2	2
0.56										1	1	7
0.57										1	3	3
0.58										1	0	0
0.59										0	4	0
0.60										0	0	0
0.61										0	0	0
0.62										0	0	0
0.63										0	0	0
0.64										0	0	0
0.65										0	0	0
0.66										0	0	0
0.67										0	0	0
0.68										0	0	0
0.69										0	0	0
0.70										0	0	0
0.71										0	0	0
0.72										0	0	0
0.73										0	0	0
0.74										0	0	0
0.75										0	0	0
0.76										0	0	0
0.77										0	0	0
0.78										0	0	0
0.79										0	0	0
0.80										0	0	0
0.81										0	0	0
0.82										0	0	0
0.83										0	0	0
0.84										0	0	0
0.85										0	0	0
0.86										0	0	0
0.87										0	0	0
0.88										0	0	0
0.89										0	0	0
0.90										0	0	0
0.91										0	0	0
0.92										0	0	0
0.93										0	0	0
0.94										0	0	0
0.95										0	0	0
0.96										0	0	0
0.97										0	0	0
0.98										0	0	0
0.99										0	0	0
1.00										0	0	0
UBTOTAL										5	36	45

~~TOP SECRET~~

CONTROL NO.

TABLE A-4

~~TOP SECRET~~

- CONTROL NO.

MISSION \* 1036-2 \* INSTRUMENT \* AFT 11/28/66 DENSITY FREQ DISTR

DENSITY VALUE	PRIMARY			INTERMEDIATE			FULL			ALL LEVELS		
	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM
1.01	0	0	0	1	0	0	0	0	0	0	0	0
1.02	0	0	0	1	0	0	0	0	0	0	0	0
1.03	0	0	0	1	0	0	0	0	0	0	0	0
1.04	0	0	0	1	0	0	0	0	0	0	0	0
1.05	0	0	0	1	0	0	0	0	0	0	0	0
1.06	0	0	0	1	0	0	0	0	0	0	0	0
1.07	0	0	0	1	0	0	0	0	0	0	0	0
1.08	0	0	0	1	0	0	0	0	0	0	0	0
1.09	0	0	0	1	0	0	0	0	0	0	0	0
1.10	0	0	0	1	0	0	0	0	0	0	0	0
1.11	0	0	0	1	0	0	0	0	0	0	0	0
1.12	0	0	0	1	0	0	0	0	0	0	0	0
1.13	0	0	0	1	0	0	0	0	0	0	0	0
1.14	0	0	0	1	0	0	0	0	0	0	0	0
1.15	0	0	0	1	0	0	0	0	0	0	0	0
1.16	0	0	0	1	0	0	0	0	0	0	0	0
1.17	0	0	0	1	0	0	0	0	0	0	0	0
1.18	0	0	0	1	0	0	0	0	0	0	0	0
1.19	0	0	0	1	0	0	0	0	0	0	0	0
1.20	0	0	0	1	0	0	0	0	0	0	0	0
1.21	0	0	0	1	0	0	0	0	0	0	0	0
1.22	0	0	0	1	0	0	0	0	0	0	0	0
1.23	0	0	0	1	0	0	0	0	0	0	0	0
1.24	0	0	0	1	0	0	0	0	0	0	0	0
1.25	0	0	0	1	0	0	0	0	0	0	0	0
1.26	0	0	0	1	0	0	0	0	0	0	0	0
1.27	0	0	0	1	0	0	0	0	0	0	0	0
1.28	0	0	0	1	0	0	0	0	0	0	0	0
1.29	0	0	0	1	0	0	0	0	0	0	0	0
1.30	0	0	0	1	0	0	0	0	0	0	0	0
1.31	0	0	0	1	0	0	0	0	0	0	0	0
1.32	0	0	0	1	0	0	0	0	0	0	0	0
1.33	0	0	0	1	0	0	0	0	0	0	0	0
1.34	0	0	0	1	0	0	0	0	0	0	0	0
1.35	0	0	0	1	0	0	0	0	0	0	0	0
1.36	0	0	0	1	0	0	0	0	0	0	0	0
1.37	0	0	0	1	0	0	0	0	0	0	0	0
1.38	0	0	0	1	0	0	0	0	0	0	0	0
1.39	0	0	0	1	0	0	0	0	0	0	0	0
1.40	0	0	0	1	0	0	0	0	0	0	0	0
1.41	0	0	0	1	0	0	0	0	0	0	0	0
1.42	0	0	0	1	0	0	0	0	0	0	0	0
1.43	0	0	0	1	0	0	0	0	0	0	0	0
1.44	0	0	0	1	0	0	0	0	0	0	0	0
1.45	0	0	0	1	0	0	0	0	0	0	0	0
1.46	0	0	0	1	0	0	0	0	0	0	0	0
1.47	0	0	0	1	0	0	0	0	0	0	0	0
1.48	0	0	0	1	0	0	0	0	0	0	0	0
1.49	0	0	0	1	0	0	0	0	0	0	0	0
1.50	0	0	0	1	0	0	0	0	0	0	0	0
SUBTOTAL	0	0	0	3	0	0	27	0	1	99	4	126

~~TOP SECRET~~

CONTROL NO.

TABLE A-4

~~TOP SECRET~~

- CONTROL NO.

MISSION \* 1036-2 \* INSTRUMENT \* AFT 11/28/66 DENSITY FREQ DISTR

DENSITY VALUE	PRIMARY MIN	PRIMARY MAX	PRIMARY LIM	INTERMEDIATE MIN	INTERMEDIATE MAX	INTERMEDIATE LIM	FULL MIN	FULL MAX	FULL LIM	ALL LEVELS MIN	ALL LEVELS MAX	ALL LEVELS LIM
1.51	0	0	0	0	0	0	0	0	0	0	0	0
1.52	0	0	0	0	0	0	0	0	0	0	0	0
1.53	0	0	0	0	0	0	0	0	0	0	0	0
1.54	0	0	0	0	0	0	0	0	0	0	0	0
1.55	0	0	0	0	0	0	0	0	0	0	0	0
1.56	0	0	0	0	0	0	0	0	0	0	0	0
1.57	0	0	0	0	0	0	0	0	0	0	0	0
1.58	0	0	0	0	0	0	0	0	0	0	0	0
1.59	0	0	0	0	0	0	0	0	0	0	0	0
1.60	0	0	0	0	0	0	0	0	0	0	0	0
1.61	0	0	0	0	0	0	0	0	0	0	0	0
1.62	0	0	0	0	0	0	0	0	0	0	0	0
1.63	0	0	0	0	0	0	0	0	0	0	0	0
1.64	0	0	0	0	0	0	0	0	0	0	0	0
1.65	0	0	0	0	0	0	0	0	0	0	0	0
1.66	0	0	0	0	0	0	0	0	0	0	0	0
1.67	0	0	0	0	0	0	0	0	0	0	0	0
1.68	0	0	0	0	0	0	0	0	0	0	0	0
1.69	0	0	0	0	0	0	0	0	0	0	0	0
1.70	0	0	0	0	0	0	0	0	0	0	0	0
1.71	0	0	0	0	0	0	0	0	0	0	0	0
1.72	0	0	0	0	0	0	0	0	0	0	0	0
1.73	0	0	0	0	0	0	0	0	0	0	0	0
1.74	0	0	0	0	0	0	0	0	0	0	0	0
1.75	0	0	0	0	0	0	0	0	0	0	0	0
1.76	0	0	0	0	0	0	0	0	0	0	0	0
1.77	0	0	0	0	0	0	0	0	0	0	0	0
1.78	0	0	0	0	0	0	0	0	0	0	0	0
1.79	0	0	0	0	0	0	0	0	0	0	0	0
1.80	0	0	0	0	0	0	0	0	0	0	0	0
1.81	0	0	0	0	0	0	0	0	0	0	0	0
1.82	0	0	0	0	0	0	0	0	0	0	0	0
1.83	0	0	0	0	0	0	0	0	0	0	0	0
1.84	0	0	0	0	0	0	0	0	0	0	0	0
1.85	0	0	0	0	0	0	0	0	0	0	0	0
1.86	0	0	0	0	0	0	0	0	0	0	0	0
1.87	0	0	0	0	0	0	0	0	0	0	0	0
1.88	0	0	0	0	0	0	0	0	0	0	0	0
1.89	0	0	0	0	0	0	0	0	0	0	0	0
1.90	0	0	0	0	0	0	0	0	0	0	0	0
1.91	0	0	0	0	0	0	0	0	0	0	0	0
1.92	0	0	0	0	0	0	0	0	0	0	0	0
1.93	0	0	0	0	0	0	0	0	0	0	0	0
1.94	0	0	0	0	0	0	0	0	0	0	0	0
1.95	0	0	0	0	0	0	0	0	0	0	0	0
1.96	0	0	0	0	0	0	0	0	0	0	0	0
1.97	0	0	0	0	0	0	0	0	0	0	0	0
1.98	0	0	0	0	0	0	0	0	0	0	0	0
1.99	0	0	0	0	0	0	0	0	0	0	0	0
2.00	0	0	0	0	0	0	0	0	0	0	0	0
SUBTOTAL	0	0	0	0	0	0	0	0	0	0	0	0
							17	18	19	31	86	142

~~TOP SECRET~~

CONTROL NO.

TABLE A-4

~~TOP SECRET~~

- CONTROL NO.

MISSION \* 1036-2 \* INSTRUMENT \* APT 11/28/66 DENSITY FREQ DISTR

DENSITY VALUE	PRIMARY MIN MAX LIM	INTERMEDIATE MIN MAX LIM	FULL MIN MAX LIM	ALL LEVELS MIN MAX LIM
2.01	0 0	0 0	0 0	0 0
2.02	0 0	0 0	0 0	0 0
2.03	0 0	0 0	0 0	0 0
2.04	0 0	0 0	0 0	0 0
2.05	0 0	0 0	0 0	0 0
2.06	0 0	0 0	0 0	0 0
2.07	0 0	0 0	0 0	0 0
2.08	0 0	0 0	0 0	0 0
2.09	0 0	0 0	0 0	0 0
2.10	0 0	0 0	0 0	0 0
2.11	0 0	0 0	0 0	0 0
2.12	0 0	0 0	0 0	0 0
2.13	0 0	0 0	0 0	0 0
2.14	0 0	0 0	0 0	0 0
2.15	0 0	0 0	0 0	0 0
2.16	0 0	0 0	0 0	0 0
2.17	0 0	0 0	0 0	0 0
2.18	0 0	0 0	0 0	0 0
2.19	0 0	0 0	0 0	0 0
2.20	0 0	0 0	0 0	0 0
2.21	0 0	0 0	0 0	0 0
2.22	0 0	0 0	0 0	0 0
2.23	0 0	0 0	0 0	0 0
2.24	0 0	0 0	0 0	0 0
2.25	0 0	0 0	0 0	0 0
2.26	0 0	0 0	0 0	0 0
2.27	0 0	0 0	0 0	0 0
2.28	0 0	0 0	0 0	0 0
2.29	0 0	0 0	0 0	0 0
2.30	0 0	0 0	0 0	0 0
2.31	0 0	0 0	0 0	0 0
2.32	0 0	0 0	0 0	0 0
2.33	0 0	0 0	0 0	0 0
2.34	0 0	0 0	0 0	0 0
2.35	0 0	0 0	0 0	0 0
2.36	0 0	0 0	0 0	0 0
2.37	0 0	0 0	0 0	0 0
2.38	0 0	0 0	0 0	0 0
2.39	0 0	0 0	0 0	0 0
2.40	0 0	0 0	0 0	0 0
2.41	0 0	0 0	0 0	0 0
2.42	0 0	0 0	0 0	0 0
2.43	0 0	0 0	0 0	0 0
2.44	0 0	0 0	0 0	0 0
2.45	0 0	0 0	0 0	0 0
2.46	0 0	0 0	0 0	0 0
2.47	0 0	0 0	0 0	0 0
2.48	0 0	0 0	0 0	0 0
2.49	0 0	0 0	0 0	0 0
2.50	0 0	0 0	0 0	0 0
SUBTOTAL	0 0	0 0	0 0	2 163
			25	2 188

~~TOP SECRET~~

- CONTROL NO.

TABLE A-4

~~TOP SECRET~~

- CONTROL NO.

MISSION # 1036-2 \* INSTRUMENT \* AFT 11/28/66 DENSITY FREQ DISTR

DENSITY VALUE	PRIMARY			INTERMEDIATE			FULL			ALL LEVELS		
	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM
2.51	0	0	0	0	0	0	0	0	0	0	0	0
2.52	0	0	0	0	0	0	0	0	0	0	0	0
2.53	0	0	0	0	0	0	0	0	0	0	0	0
2.54	0	0	0	0	0	0	0	0	0	0	0	0
2.55	0	0	0	0	0	0	0	0	0	0	0	0
2.56	0	0	0	0	0	0	0	0	0	0	0	0
2.57	0	0	0	0	0	0	0	0	0	0	0	0
2.58	0	0	0	0	0	0	0	0	0	0	0	0
2.59	0	0	0	0	0	0	0	0	0	0	0	0
2.60	0	0	0	0	0	0	0	0	0	0	0	0
2.61	0	0	0	0	0	0	0	0	0	0	0	0
2.62	0	0	0	0	0	0	0	0	0	0	0	0
2.63	0	0	0	0	0	0	0	0	0	0	0	0
2.64	0	0	0	0	0	0	0	0	0	0	0	0
2.65	0	0	0	0	0	0	0	0	0	0	0	0
2.66	0	0	0	0	0	0	0	0	0	0	0	0
2.67	0	0	0	0	0	0	0	0	0	0	0	0
2.68	0	0	0	0	0	0	0	0	0	0	0	0
2.69	0	0	0	0	0	0	0	0	0	0	0	0
2.70	0	0	0	0	0	0	0	0	0	0	0	0
SUBTOTAL	0	0	0	0	0	0	0	0	0	0	0	0
TOTAL	0	0	0	48	48	43	224	224	194	272	272	237

MISSION 1036-2 INSTR - AFT 11/28/66 PROCESSING AND EXPOSURE ANALY.

PROCESS LEVEL	SAMPLE SIZE	UNDER EXPOSED		UNDER PROCESSED		CORRECT EXP+PROC		OVER PROCESSED		OVER EXPOSED	
		0	PC	0	PC	0	PC	10	PC	0	PC
PRIMARY	0	0	PC	0	PC	0	PC	0	PC	0	PC
INTERMEDIATE	48	0	PC	25	PC	65	PC	10	PC	0	PC
FULL	224	34	PC	0	PC	63	PC	2	PC	0	PC
ALL LEVELS	272	28	PC	4	PC	64	PC	4	PC	0	PC
PROCESS LEVEL	BASE + FOG	UNDER EXPOSED		UNDER PROCESSED		CORRECT EXP+PROC		OVER PROCESSED		OVER EXPOSED	
PRIMARY	0.01-0.09	0.01-0.13		0.14-0.39		0.40-0.90		-----		0.91	AND
INTERMED	0.10-0.17	0.01-0.20		0.21-0.39		0.40-0.90		0.91-1.34		1.35	AND
FULL	0.18 AND UP	0.01-0.39		-----		0.40-0.90		0.91-1.69		1.70	AND

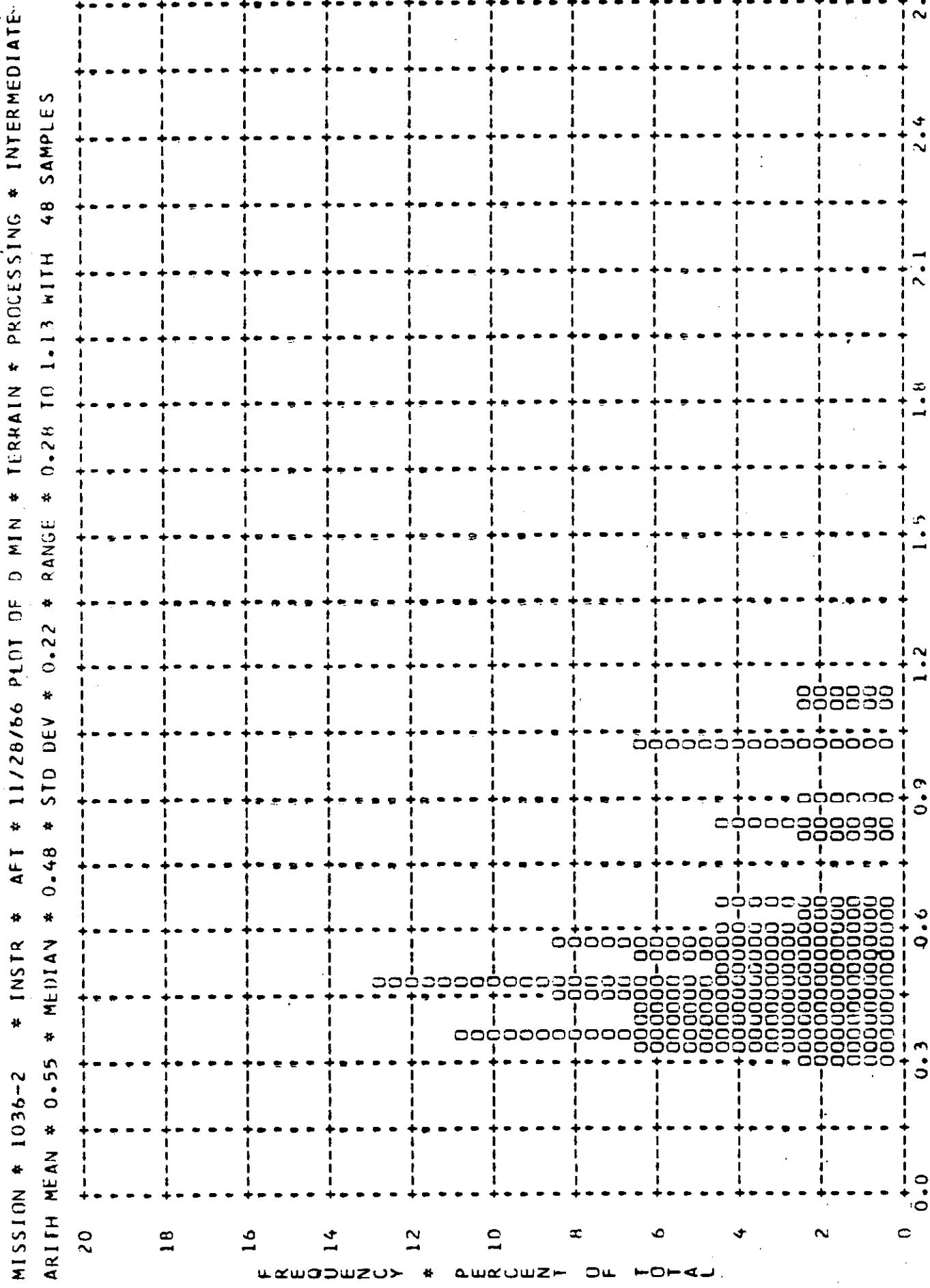
~~TOP SECRET~~

- CONTROL NO.

TABLE A-4

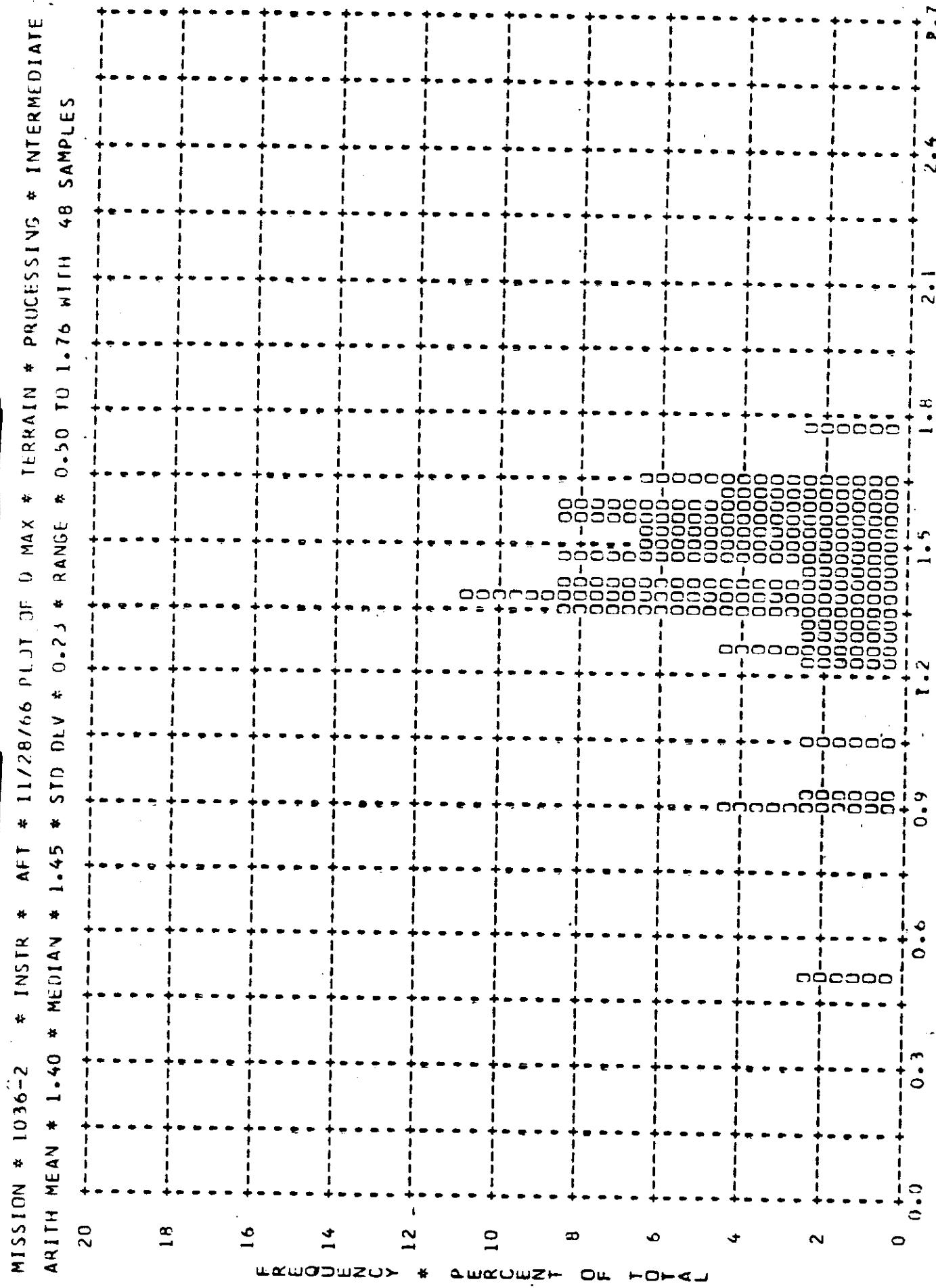
TOP SECRET

- CONJUL NO.



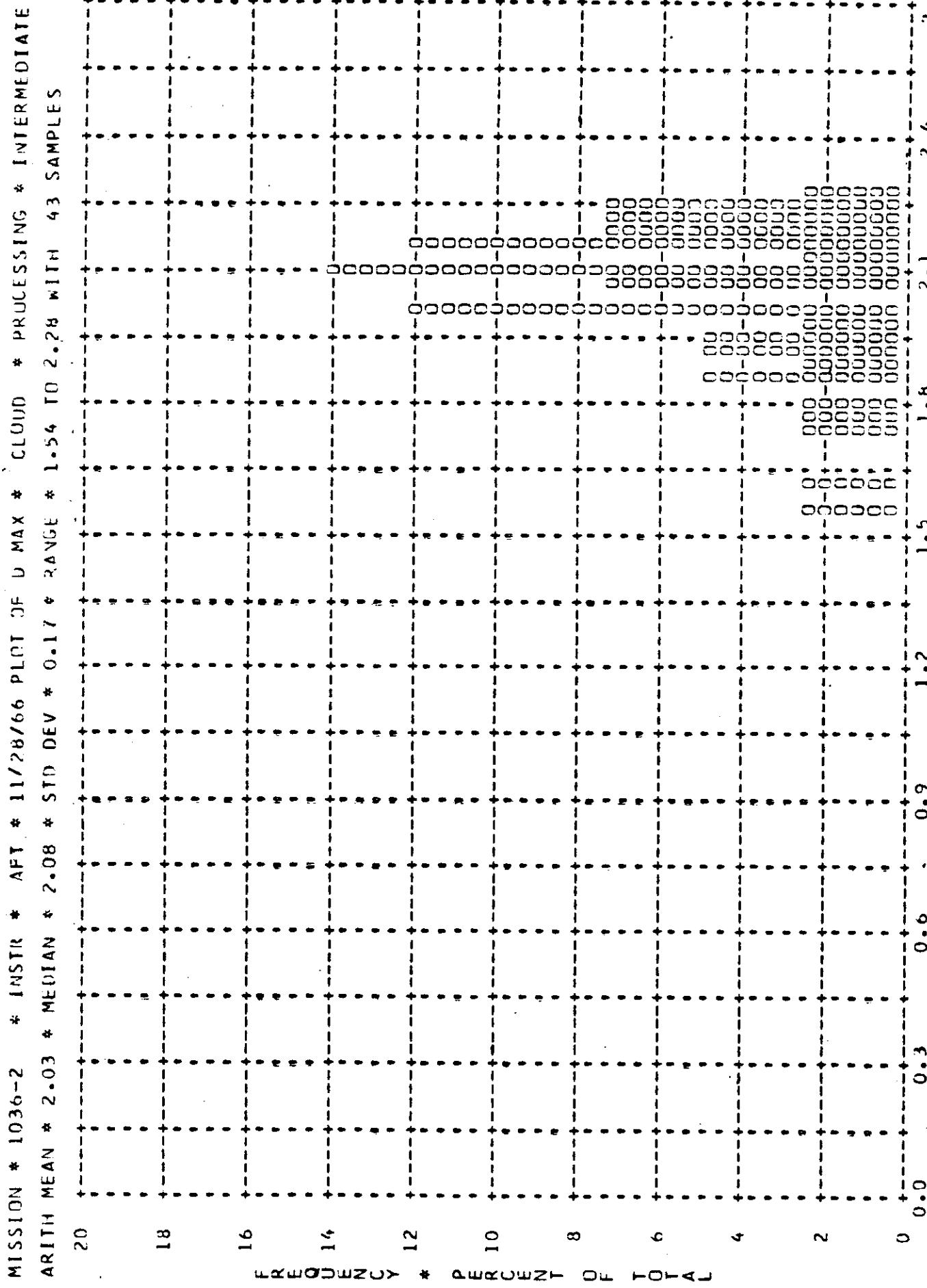
TOP SECRET

- CONTROL NO.



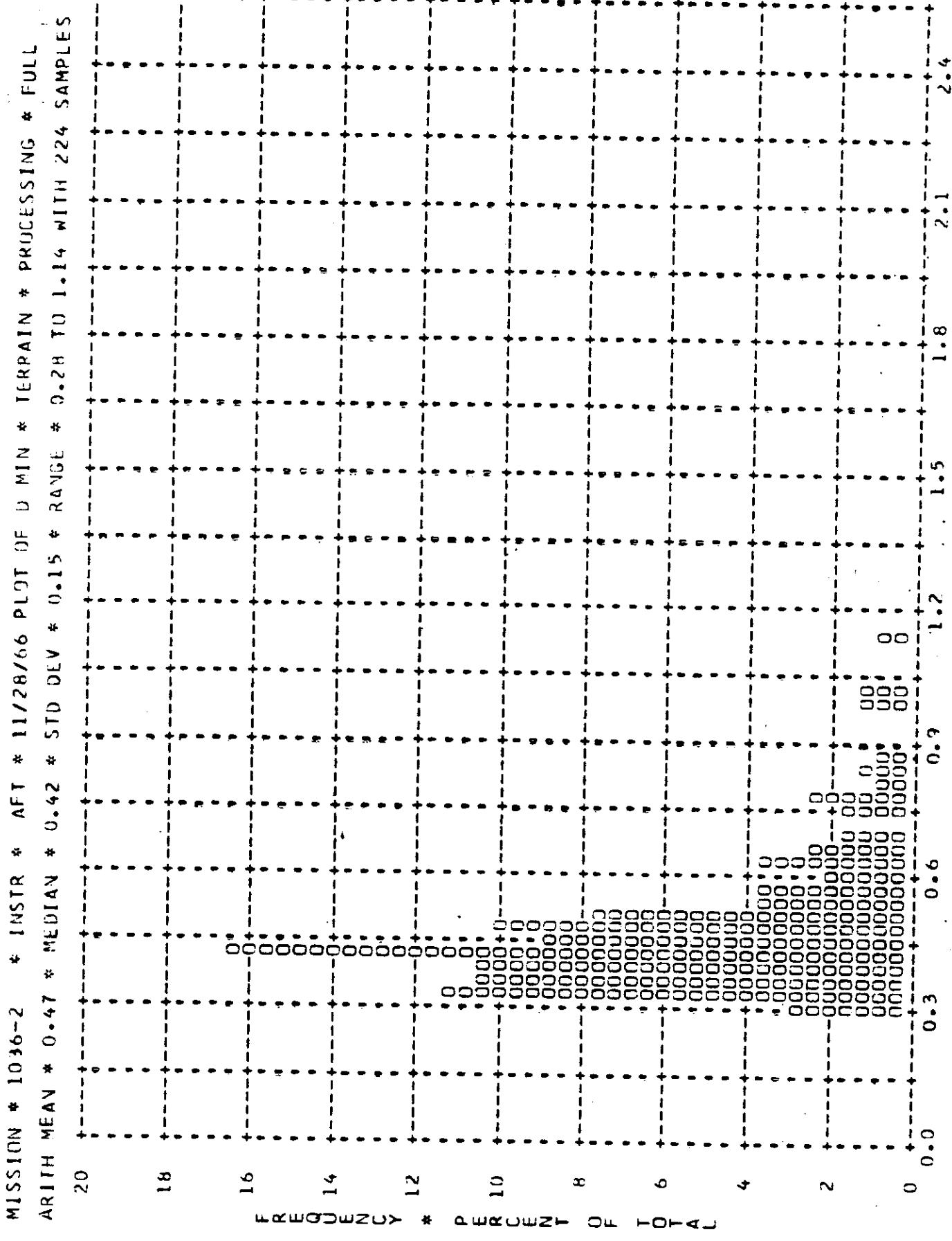
100 SECRET

CONT'D N.



~~TOP SECRET~~

- CONTROL VO.



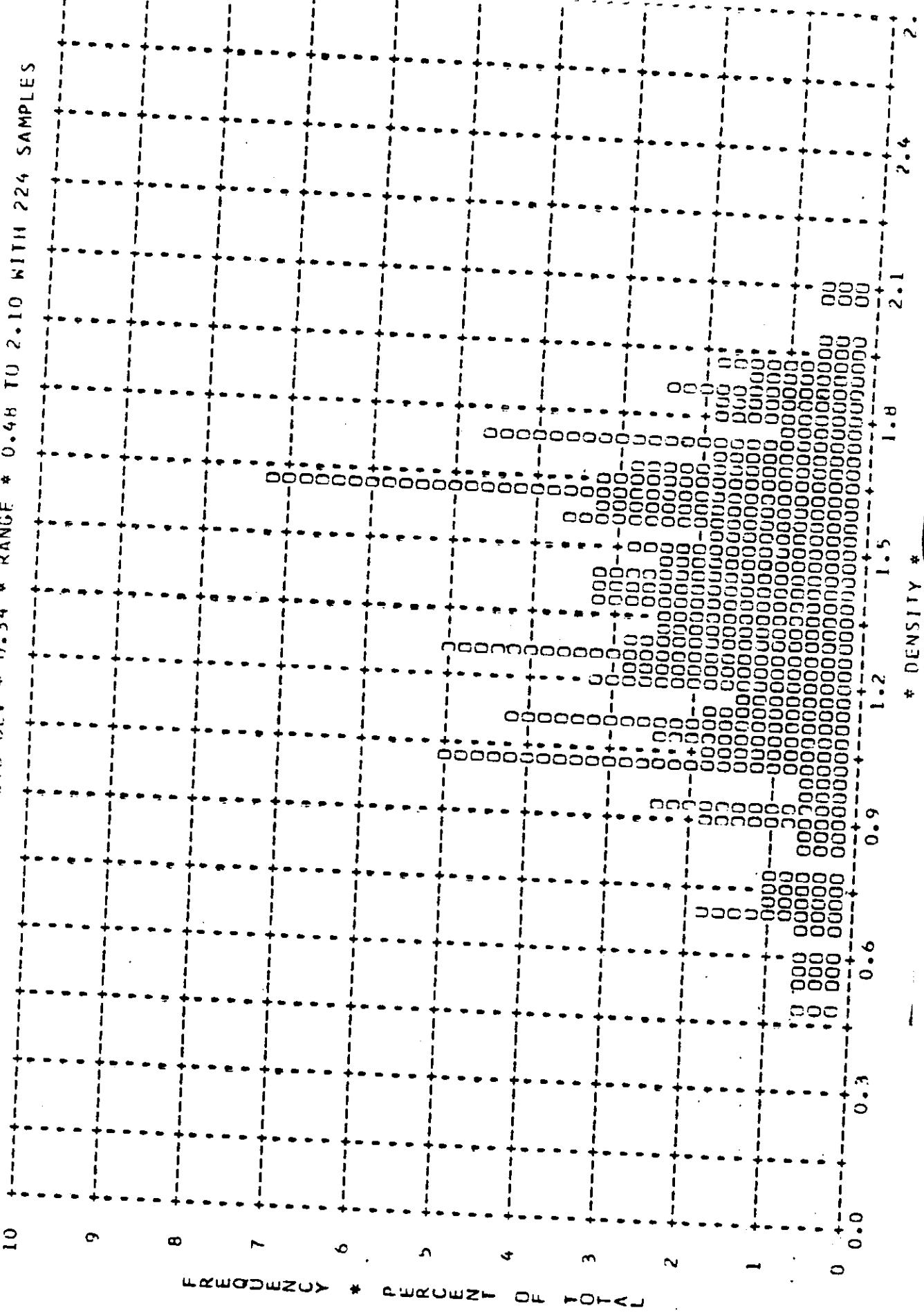
~~TOP SECRET~~

FIGURE A-34

~~Line~~ ~~STERE~~

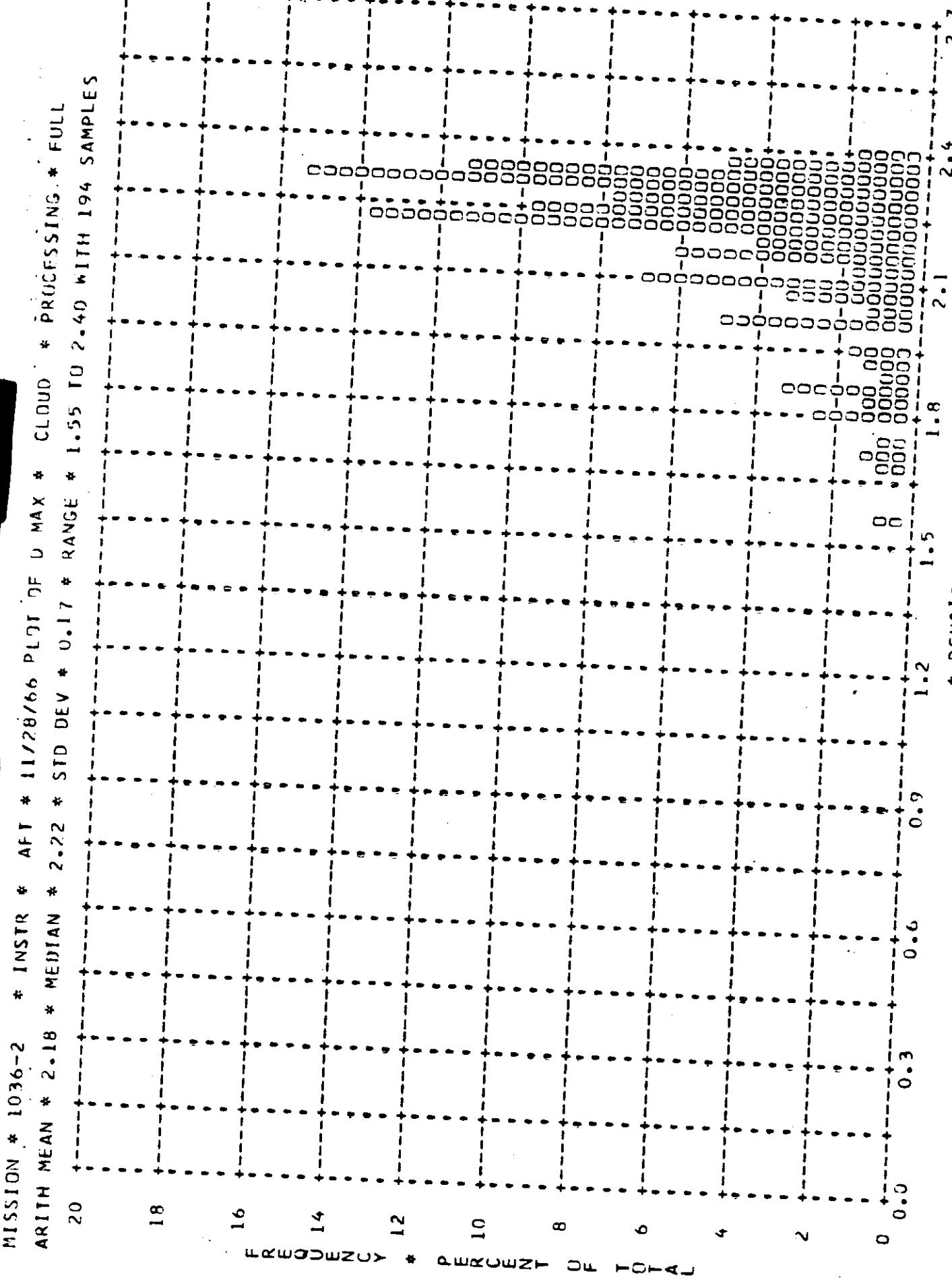
- CONTROL NO.

MISSION \* 1036-2 \* INSTR \* AFT \* 11/28/66 PLOT OF D MAX \* TERRAIN \* PROCESSING \* FULL  
ARITH MEAN \* 1.36 \* MEDIAN \* 1.40 \* STD DEV \* 0.34 \* RANGE \* 0.48 TO 2.10 WITH 224 SAMPLES



~~TOP SECRET~~

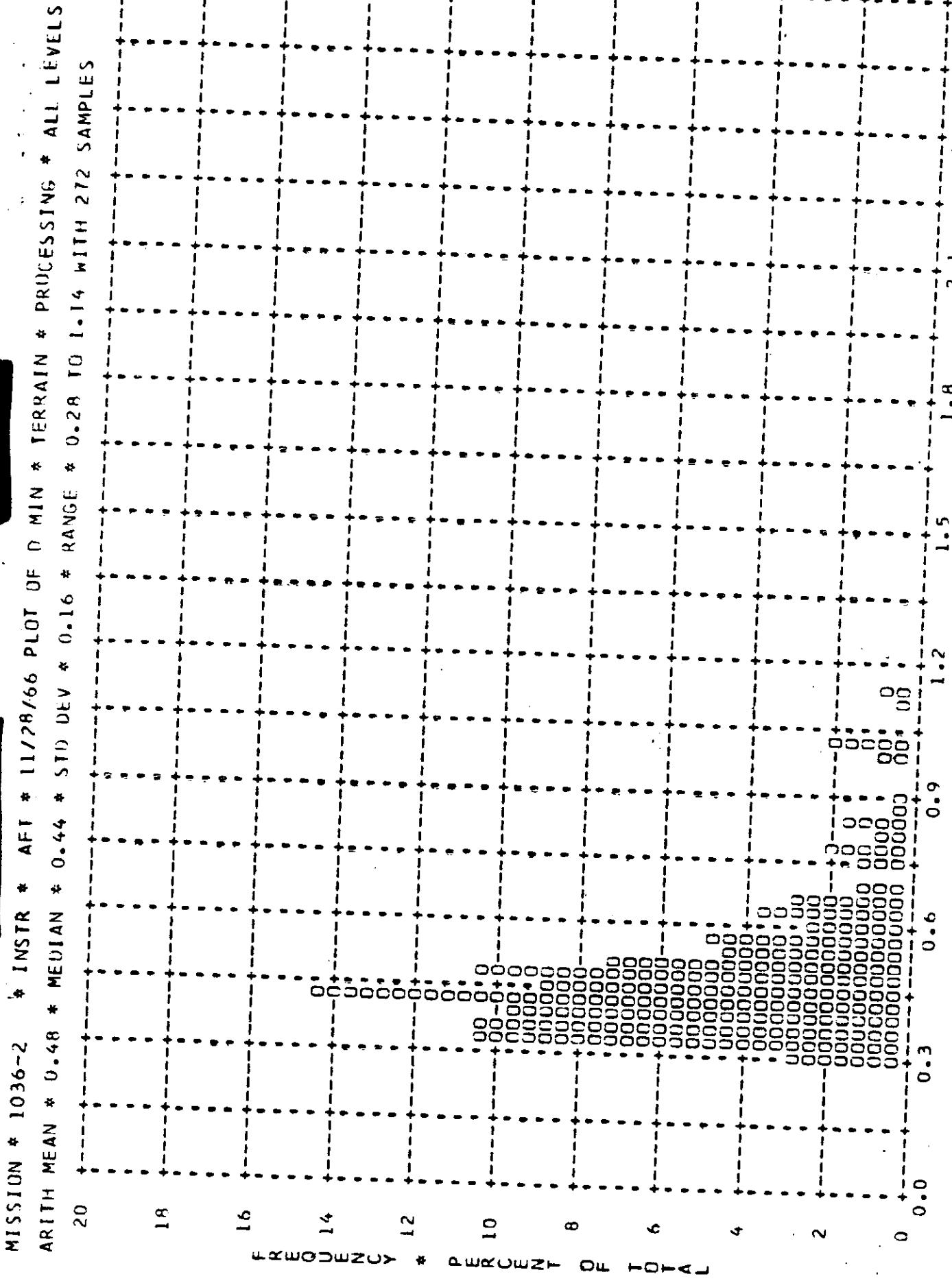
- CURRENT NO.



~~TOP SECRET~~

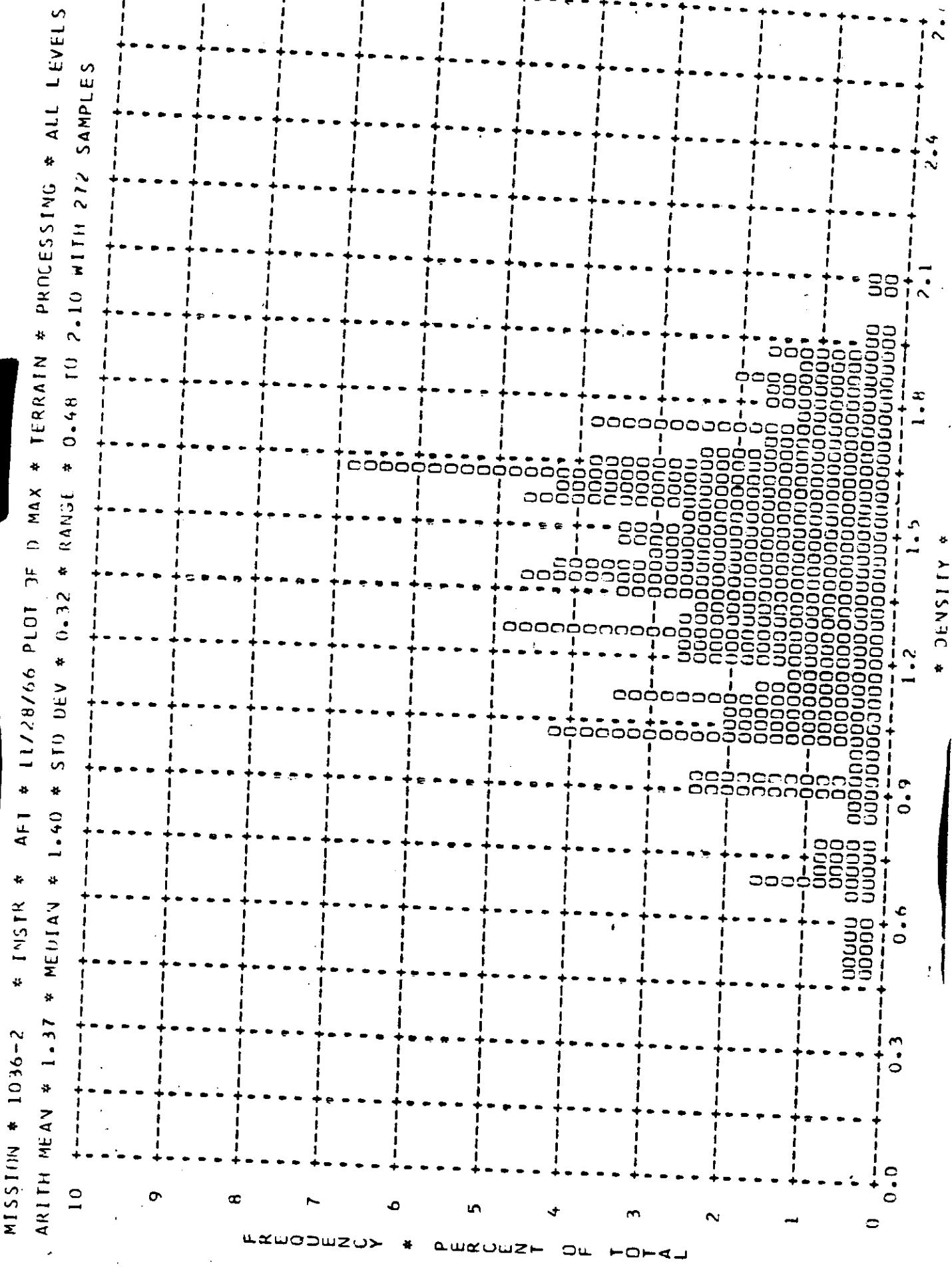
~~TOP SECRET~~

- CONTROL NO.



TOP SECRET

- CONTROL NO.



~~TOP SECRET~~

- CONTROL NO.

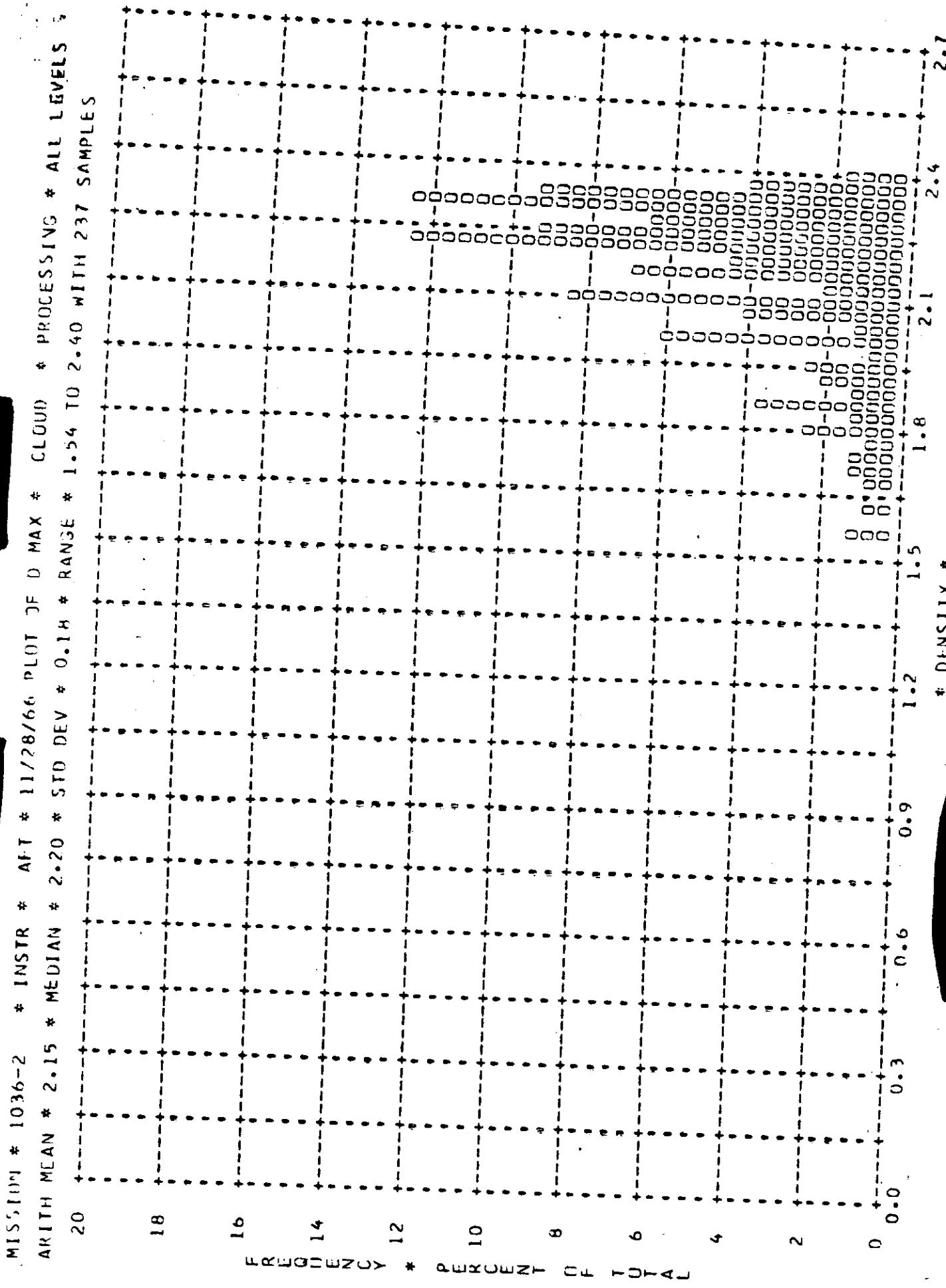


FIGURE A-39

~~TOP SECRET C~~

Distribution:

Copy No.

To

[REDACTED]  
[REDACTED]  
[REDACTED]  
[REDACTED]  
[REDACTED]  
[REDACTED]  
[REDACTED]

~~TOP SECRET C~~